



hpfem-mpt - A tutorial.

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Outline

- Introduction to the MPT
- Installing
- Tutorial 1: Conducting sphere
- Tutorial 2: Analogue Detonator
- Tutorial 3: Setting up your own geometries

Eddy current model



Eddy current approximation:

 $\sqrt{\epsilon_*\mu_*}\alpha\omega\ll 1, \epsilon_*\omega/\sigma_*\ll 1$ (rigorous justification involves the topology of the object).

In absence of a conducting object the fields from a coil E_0 , H_0 satisfy

$$abla imes E_0 = \mathrm{i}\omega \mu_0 H_0, \qquad
abla imes H_0 = J_0 \qquad \qquad \mathrm{in} \, \mathbb{R}^2$$

In the presence of a conductor body B_{α} with

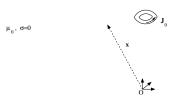
$$\mu_{\alpha} = \left\{ \begin{array}{ll} \mu_{0} & \text{in } \mathbb{R}^{3} \backslash B_{\alpha} \\ \mu_{*} & \text{in } B_{\alpha} \end{array} \right. \qquad \sigma_{\alpha} = \left\{ \begin{array}{ll} 0 & \text{in } \mathbb{R}^{3} \backslash B_{\alpha} \\ \sigma_{*} & \text{in } B_{\alpha} \end{array} \right.$$

the interaction fields E_{α} , H_{α} satisfy

$$\nabla \times E_{\alpha} = i\omega \mu_{\alpha} H_{\alpha}, \qquad \nabla \times H_{\alpha} = \sigma_{\alpha} E_{\alpha} + J_{0} \qquad \text{in } \mathbb{R}^{3}$$

$$\nabla \cdot E_{\alpha} = 0, \qquad \nabla \cdot \mu_{\alpha} H_{\alpha} = 0 \qquad \text{in } \mathbb{R}^{3}$$

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 $\sqrt{\epsilon_*\mu_*}\alpha\omega\ll 1, \epsilon_*\omega/\sigma_*\ll 1 \text{(rigorous justification involves the topology of the object)}.$

In absence of a conducting object the fields from a coil E_0 , H_0 satisfy

$$\nabla \times \boldsymbol{E}_0 = i\omega \mu_0 \boldsymbol{H}_0, \qquad \nabla \times \boldsymbol{H}_0 = \boldsymbol{J}_0 \qquad \qquad \text{in } \mathbb{R}^3$$

$$\nabla \cdot \boldsymbol{E}_0 = 0, \qquad \nabla \cdot \boldsymbol{H}_0 = 0 \qquad \qquad \text{in } \mathbb{R}^3$$

In the presence of a conductor body B_{α} with

$$\mu_{\alpha} = \left\{ \begin{array}{ll} \mu_0 & \text{in } \mathbb{R}^3 \backslash B_{\alpha} \\ \mu_* & \text{in } B_{\alpha} \end{array} \right. \qquad \sigma_{\alpha} = \left\{ \begin{array}{ll} 0 & \text{in } \mathbb{R}^3 \backslash B_{\alpha} \\ \sigma_* & \text{in } B_{\alpha} \end{array} \right.$$

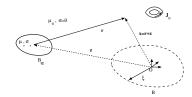
the interaction fields E_{α} , H_{α} satisfy

$$\nabla \times \boldsymbol{E}_{\alpha} = i\omega \mu_{\alpha} \boldsymbol{H}_{\alpha}, \qquad \nabla \times \boldsymbol{H}_{\alpha} = \sigma_{\alpha} \boldsymbol{E}_{\alpha} + \boldsymbol{J}_{0} \qquad \text{in } \mathbb{R}^{3}$$

$$\nabla \cdot \boldsymbol{E}_{\alpha} = 0, \qquad \nabla \cdot \mu_{\alpha} \boldsymbol{H}_{\alpha} = 0 \qquad \text{in } \mathbb{R}^{3}$$

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Eddy current model



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In absence of a conducting object the fields from a coil E_0 , H_0 satisfy

$$abla imes E_0 = i\omega \mu_0 H_0, \qquad \nabla imes H_0 = J_0 \qquad \qquad \text{in } \mathbb{R}^3$$

$$abla imes E_0 = 0, \qquad \nabla imes H_0 = 0 \qquad \qquad \text{in } \mathbb{R}^3$$

In the presence of a conductor body B_{α} with

$$\mu_{\alpha} = \left\{ \begin{array}{ll} \mu_0 & \text{in } \mathbb{R}^3 \backslash B_{\alpha} \\ \mu_* & \text{in } B_{\alpha} \end{array} \right. \qquad \sigma_{\alpha} = \left\{ \begin{array}{ll} 0 & \text{in } \mathbb{R}^3 \backslash B_{\alpha} \\ \sigma_* & \text{in } B_{\alpha} \end{array} \right.$$

the interaction fields E_{α} , H_{α} satisfy

$$\nabla \times \boldsymbol{E}_{\alpha} = i\omega \mu_{\alpha} \boldsymbol{H}_{\alpha}, \qquad \nabla \times \boldsymbol{H}_{\alpha} = \sigma_{\alpha} \boldsymbol{E}_{\alpha} + \boldsymbol{J}_{0} \qquad \text{in } \mathbb{R}^{3}$$

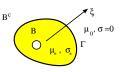
$$\nabla \cdot \boldsymbol{E}_{\alpha} = 0, \qquad \nabla \cdot \mu_{\alpha} \boldsymbol{H}_{\alpha} = 0 \qquad \text{in } \mathbb{R}^{3}$$

PDL (Swansea University)

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By setting $B_{\alpha} = \alpha B + z$ we have derived that

$$(\boldsymbol{H}_{\alpha}-\boldsymbol{H}_{0})(\boldsymbol{x})_{j}=\boldsymbol{D}_{x}^{2}G(\boldsymbol{x},\boldsymbol{z})_{jm}\widetilde{\widetilde{\mathcal{M}}}_{mi}\boldsymbol{H}_{0}(\boldsymbol{z})_{i}+O(\alpha^{4}),$$



as $\alpha \to 0$ (PDL, WRBL (2015b)) where $G(x,z) = 1/(4\pi |x-z|)$.

$$\check{C}_{mi} := \frac{\beta}{2} \hat{e}_m \cdot \int_B \boldsymbol{\xi} \times (\boldsymbol{\theta}_i + \hat{e}_i \times \boldsymbol{\xi}) d\boldsymbol{\xi} \qquad \mathcal{N}_{mi} := \alpha^3 \left(1 - \frac{\mu_0}{\mu_*} \right) \int_B \left(\hat{e}_m \cdot \hat{e}_i + \frac{1}{2} \hat{e}_m \cdot \nabla_{\boldsymbol{\xi}} \times \boldsymbol{\theta}_i \right) d\boldsymbol{\xi}$$

$$\vdots \dots^3$$

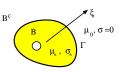
$$\begin{split} \nabla_{\xi} \times \mu_{*}^{-1} \nabla_{\xi} \times \theta_{i} - \mathrm{i} \omega \sigma_{*} \alpha^{2} \theta_{i} &= \mathrm{i} \omega \sigma_{*} \alpha^{2} \hat{e}_{i} \times \xi & \text{in } B \\ \nabla_{\xi} \cdot \theta_{i} &= 0, \quad \nabla_{\xi} \times \mu_{0}^{-1} \nabla_{\xi} \times \theta_{i} &= \mathbf{0} & \text{in } B^{c} \\ [\hat{n} \times \theta_{i}]_{\Gamma} &= \mathbf{0}, \quad [\hat{n} \times \mu^{-1} \nabla_{\xi} \times \theta_{i}]_{\Gamma} &= -2[\mu^{-1}]_{\Gamma} \hat{n} \times \hat{e}_{i} & \text{on } \Gamma \\ \theta_{i} &= O(|\xi|^{-1}) & \text{as } |\xi| \end{split}$$

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Summary of key results

By setting $B_{\alpha} = \alpha B + z$ we have derived that

$$(\boldsymbol{H}_{\alpha}-\boldsymbol{H}_{0})(\boldsymbol{x})_{j}=\boldsymbol{D}_{x}^{2}G(\boldsymbol{x},\boldsymbol{z})_{jm}\widetilde{\mathcal{M}}_{mi}\boldsymbol{H}_{0}(\boldsymbol{z})_{i}+O(\alpha^{4}),$$



as $\alpha \to 0$ (PDL, WRBL (2015b)) where $G(x,z) = 1/(4\pi |x-z|)$.

The rank 2 MPT has coefficients $\widetilde{\mathcal{M}}_{mi} := -\check{\mathcal{C}}_{mi} + \mathcal{N}_{mi}$ it is **symmetric** and so only 6 are needed where

$$\begin{split} \check{C}_{\textit{mi}} &:= \frac{\beta}{2} \hat{\pmb{e}}_{\textit{m}} \cdot \int_{B} \pmb{\xi} \times (\pmb{\theta}_{\textit{i}} + \hat{\pmb{e}}_{\textit{i}} \times \pmb{\xi}) \mathrm{d} \pmb{\xi} \\ &\text{and } \beta = -\frac{\mathrm{i}\nu\alpha^{3}}{2} \;. \end{split}$$

To compute the tensors we solve

$$\begin{split} \nabla_{\xi} \times \mu_{*}^{-1} \nabla_{\xi} \times \boldsymbol{\theta}_{i} - \mathrm{i} \omega \sigma_{*} \alpha^{2} \boldsymbol{\theta}_{i} &= \mathrm{i} \omega \sigma_{*} \alpha^{2} \hat{\boldsymbol{e}}_{i} \times \boldsymbol{\xi} & \text{in } \boldsymbol{B} \\ \nabla_{\xi} \cdot \boldsymbol{\theta}_{i} &= 0, & \nabla_{\xi} \times \mu_{0}^{-1} \nabla_{\xi} \times \boldsymbol{\theta}_{i} &= \mathbf{0} & \text{in } \boldsymbol{B}^{c} \\ [\hat{\boldsymbol{n}} \times \boldsymbol{\theta}_{i}]_{\Gamma} &= \mathbf{0}, & [\hat{\boldsymbol{n}} \times \mu^{-1} \nabla_{\xi} \times \boldsymbol{\theta}_{i}]_{\Gamma} &= -2[\mu^{-1}]_{\Gamma} \hat{\boldsymbol{n}} \times \hat{\boldsymbol{e}}_{i} & \text{on } \Gamma \\ \boldsymbol{\theta}_{i} &= O(|\boldsymbol{\xi}|^{-1}) & \text{as } |\boldsymbol{\xi}| \to \infty \end{split}$$

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Further details

For further details on MPTs and their properties please see the following:

- PDL, WRBL, "Characterizing the shape and material properties of hidden targets from magnetic induction data", <u>IMA Journal of Applied Mathematics</u>, vol 80, pp 1776-1798, 2015.
- PDL, WRBL "Understanding the magnetic polarizability tensor", IEEE Trans.
 Magn. doi: 10.1109/TMAG.2015.2507169 (2016).
- PDL E-Presentation "Characterising the shape and material properties of hidden conducting targets in metal detection", <u>Video</u>, LMS-EPSRC Symposium on Maxwell's equations, 2016.
- PDL Presentation "A justification for the rank 2 magnetic polarizability tensor description of conducting objects in metal detection", <u>Slides</u>, CIRCLE, The University of Manchester, 2016.

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Dependencies

hpfem-mpt is designed to be an educational and research tool and is fairly self contained.

This version is implemented in MATLAB, which is not as fast as my FORTRAN version (not available at present), but does offer greater portability as it does not require compilers and the installation of various libraries.

Furthermore, no knowledge of Makefiles is required and comes setup with several examples for you to try out.

hpfem-mpt does however require the following to be installed

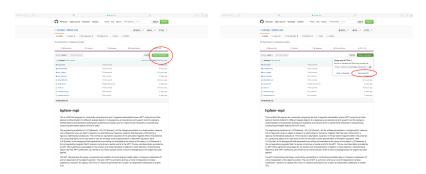
- MATLAB (tested on version 2015b)
- NETGEN Unstructured mesh generator, available here.
- Paraview Visualisation software, available here.



Obtaining the current version

To obtain the current version go to

https://github.com/pdledger/hpfem-mpt/tree/master link



Click on Download or Clone followed by Download ZIP to save the repository to your computer and unzip it.



Getting the mesh files ready

A series of example mesh files are included. To prepare them start ${\tt MATLAB}$ and change the working directory to where the unzipped file is stored.

In the MATLAB command window type

meshextract

This will untar and unzip the mesh files and create a folder called meshes containing the example meshes.

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Tutorial 1 overview

In this tutorial we will

- Understand how to generate meshes of different mesh densities from a .geo file in NETGEN';
- Understand how different problems can be selected in hpfem-mpt;
- Understand how to change the frequency, size and material parameters of an object;
- Understand how the field and the geometry are discretised differently;
- Understand how to perform run hpfem-mpt and perform p-refinement;
- Compare the accuracy of h and p-refinement and the influence on the accuracy of the MPT

Mesh generation-1

A mesh with a coarse discretisation of 2425 elements is saved in sphere11.vol in the meshes folder. This mesh is generated in NETGEN using the sphere11. geo file. It is important to choose the object (here sphin) to be of unit size and to note the order of the tlo

```
algebraic3d #
# Example with two sub-domains: was 10
#
solid sphout = sphere (0, 0, 0; 100) -bco=1;
solid sphin = sphere (0, 0, 0; 1) -bco=2;
solid rest = sphout and not sphin;
tlo rest -transparent -col=[0,0,1];
tlo sphin -col=[1,0,0];
```

as this controls the materials IDs (in this case, 1 is the region outside the sphere and 2 the conducting sphere).

Introduction to the MPT Installing Tutorial 1: Conducting sphere Tutorial 2: Analogue Detonator Tutorial 3: Setting up your own geometries

Mesh generation-2

Opening the geometry file using File > Load Geometry using the default settings in NETGEN and activating create mesh will lead to a mesh with more elements and only a linear geometry approximation.





The mesh of 2425 the meshes folder can be reproduced by using the mesh settings of coarse and second order elements in the Meshing Options palette (Mesh> Meshing Options) in NETGEN.

Using second order elements should always be selected if the geometry is curved as this improves the accuracy of the geometry.

Coarse meshes are generally sufficient since <code>hpfem-mpt</code> includes the possibility to use high order elements built on this coarse tetrahedral mesh.

4 D > 4 A > 4 B > 4 B > B > 9 C + 10 H >

Mesh generation-3

Boundaries are automatically detected (provided the object and far field are not connected) and the default settings do not need to changed.

To save a mesh select File > Save Mesh and save it as a (different) .vol file in the meshes directory.

Should you wish to generate finer meshes, this can easily controlled via the Mesh granularity drop down menu in the Meshing Options palette in NETGEN

NEGEN does offer surface and volume mesh checking (see

Mesh> Check Surface Mesh and Mesh> Check Volume Mesh), but these only work provided that Second order elements are not selected (in Version 4.9.13). So if generating a mesh for a new geometry, first do it with linear geometry, check the mesh, and then repeat the mesh generation for Second order elements, but do not rerun the checks

Selecting the problem

hpfem-mpt offers a set of 10 different examples

In main.m they are listed as

```
% problem 1 = conducting magnetic sphere
% problem 3 = nested sphere conducting and magnetic
% problem 4 = conducting magnetic Remington shell casing
% problem 5 = simple steel gun L shape
% problem 6 = 72 anologue detonator
% problem 7 = belt buckle
% problem 8 = coin
% problem 9 = conducting magnetic torus
% problem 10 = Ansvs Mesh (Sohere)
```

and the problem is selected using the flag problem =1 (default), which controls the problem file to be used. In this case problem1.m in the problemfiles directory.

Controlling the polynomial order of the discretisation

The other important flag in main.m is pm, which controls the polynomial order of the elements

The default is pm=0 which means the lowest order Nédélec elements with constant tangential component approximation on the edges of the elements will be used.

Changing this to pm=1, means Nédélec elements with a linear tangential component approximation will be used, pm=2, means Nédélec elements with a quadratic tangential component approximation will be used, ...

In principal the code allows pm to be repeatability increased. But for practical reasons, going beyond p=5 is not recommended as it will lead to excessive long run times.

It is important to note the field approximation, controlled by pm is different to the geometry approximation. This is because in many cases the geometry is flat sided, but yet we still want to use a high approximation to the transmission problem.



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The problem file-1

The problem file problem1.m contained in the problemfiles directory has already been set up with default output options, material parameters, boundary conditions and source terms and other flags.

Boundary conditions and source terms and other standard flags are handled in

```
% include standard options (include BC, src definition etc)
probdata=[];
probdata=standoptions(probdata);
...
```

and shouldn't ever need to be changed.

The part of problem1.m that has

```
...
job data-----
job = 'spherell' % Job Name
meshtype = 3; % Mesh type 1= FLITE , 2=NG (old style), 3=NG (new style)
```

controls with job which mesh will be used (minus the .vol extension). You can select the sphere you've just generated if you wish.



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The problem file-2

specifies μ_0 (in H/m) and ω (in rad/s). Changes to the frequency are possible here.

For each subdomain we need to specify the relative permeability μ_r and conductivity σ . For non-conducting regions a conductivity of O(0.1) is specified since the regularisation term is computed in the form $\varepsilon = \sigma \mu_0 \omega$ for this subdomain and hence the regularisation parameter $\varepsilon \sim O(10^{-5})$.

For the subdomain(s) corresponding to the conducting object we can change μ_r and σ (in S/m)

The problem file-3

```
For each subdomain specify parameters 
% Mu_r, Ep_r, Sigma, J
% Mat 1
mu(1) = 1;
epl(1) = 0;
sigma(1) = 0.1;
jsrc(1,1:3) = [0 0 0];
% Mat 2
mu(2) = 1.5
epl(2) = 0;
sigma(2) = 5.96e7;
jsrc(2,1:3) = [0 0 0];
% specify the material to be used a conductor conductors
% ie specify regions where gradients basis functions to be included matcond=[2];
```

specifies the materials for each subdomain (according to the order of the TLOs in the geometry file). The array matcond specifies which subdomain numbers are to be treated as conductors (sometimes an object may be made up of several TLOs).

Problem file-4

Recall that our spherical conducting object was assumed to have unit radius in the mesh file.

```
... \$ In this case the mesh is for a unit sized object, it must be scaled (and \$ repositioned) delta = 0.01; \$ Object size shift=[0 0 0]; \$ Object shift
```

control's the object's size. delta=0.01 means that each coordinate direction will be scaled by this factor.

In other words we can compute the MPT for a sphere of radius 0.01m, but computations will be done on the mesh for the unit radius sphere.

This setup means we only need to generate the mesh once to compute MPTs for spheres with a range of radii.

Problem file-5

The default geometry approximation (which will use quadratic geometry if available in the mesh file, linear otherwise) is set up in standoptions call we saw earlier.

In the case of a sphere we want to use a high order geometry approximation, due to its simplicity (and in order confirm exponential convergence of the MPT using *p*-refinement).

The above tells the program to use a 5th order polynomial approximation for the geometry spherical object (Recall the field approximation is separate).

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Running hpfem-mpt

Let us assume we have left the options as their default values, pm=0, problem=1 etc.

To run the program, select the working directory to be the root of the program and type

main

in the command window. The program will read then

- Read the mesh, identify boundaries edges and faces and number the unknowns;
- Compute the geometry approximation;
- Compute boundary condition values, assemble the matrices;
- Solve the linear system;
- Compute the MPT;
- Write output files.



Interpreting the output -1

```
... The number of edge based unknowns is 2767
The total number of edge and face unknowns is2767
The total number of PEC edge and face knowns is180
The total number of edge face and interior unknowns is2767
...
```

Tell us about the size of the computation.

```
... The relative error in the surface of the sphere is3.7288e-06 The relative error in the volume of the sphere is5.6503e-06 ...
```

Tell us about the accuracy of the geometry approximation.

```
... solving linear system completed LU decomposition System solved successfully Number of iterations3
```

Tell us about the linear equation solve.



Interpreting the output -2

```
ptensor = 1.6751e-06 + 6.4681e-07i 1.7022e-09 + 1.2589e-09i -7.4196e-10 - 8.3201e-10i 1.7022e-09 + 1.2589e-09i 1.6787e-06 + 6.4952e-07i -2.3863e-11 - 9.6766e-11i -7.4196e-10 - 8.3201e-10i -2.3863e-11 - 9.6766e-11i 1.6782e-06 + 6.4879e-07i The exact polarisation tensor is diagonal with coefficient 1.7078e-06+6.8041e-07i The relative error in the computed tensor=0.026095
```

Tell us about the computed tensor and, in this case, the expected analytical result.

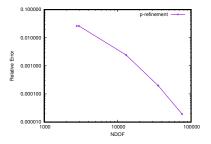
Let us suppose we were not happy with this approximation and wanted to improve it. We can do so by increasing pm

Recording the total number of unknowns the accuracy of the computed tensor we can plot a graph.

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Performing *p*-refinement

Performing calculations with pm=0, pm=1, pm=2, pm=3, pm=4 with a fixed mesh in sequence leads to p-refinement and displaying the results as a graph:



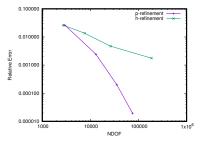
We see that performing p-refinement leads to a downward sloping curve and exponential convergence of the tensor coefficients.

Note that going from pm=0, pm=1 often does not change the accuracy, this is because only the approximation of the field rather its curl is improved for this polynomial increment.



Performing *h*-refinement

As a comparison, we can return to NETGEN and generate and saves meshes with granularities of Coarse (current), Moderate, Fine and Very Fine (provided your machine has enough RAM) and rerun hpfem-mpt with pm=0 in each case. Plotting out the results on the same graph gives: h-refinement"



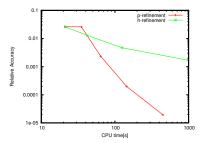
We see that performing h-refinement leads to algebraic convergence and that the previous p-refinement outperforms this.



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Comparing CPU time

By recording the CPU time for both p- and h-refinements it is also possible to compare CPU time:



Again p- outperforms h-refinement. Further savings may also be possible.

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Tutorial 2 overview

In this tutorial we will

- Understand how to work with objects made up of multiple subdomains;
- Understand how to check convergence for problems without analytical solution;
- Visualisation of solutions to the transmission problem using paraview;



We will do this in the context of an idealised landmine component.

Mesh generation

A mesh of 15 856 elements is saved in 72analogue2.vol in the meshes folder. This mesh is generated in <code>NETGEN</code> using the 72analogue.geo file. It is important to note the ordering of the <code>tlo</code>

In this case there are 3 subdomains, the first and second are free space regions. The third region is the object, which is of unit (O(1)) size.

The mesh can be reproduced in NETGEN with the options of moderate mesh granularity and Second order elements.



Problem file

In problem11 andmine.m we highlight how the materials are described

```
% Mu_r, Ep_r, Sigma, J
% Free space
mu(1) = 1;
epl(1) = 0;
sicma(1) = 0.1;
isrc(1.1:3) = [0 \ 0 \ 0];
mu(2) = 1:
epl(2) = 0:
sigma(2) = 0.1;
isrc(2.1:3) = [0 \ 0 \ 0];
% Object
mu(3) = 1.000022;
ep1(3) = 0;
sigma(3) = 3.5e7;
jsrc(3,1:3) = [0 \ 0 \ 0];
% specify the material to be used a conductor conductors
% ie specify regions where gradients basis functions to be included
matcond=[3];
```

For the first two subdomains material parameters are assigned based on them being free space (as per the geometry description). The third subdomain is the object and the parameters are set accordingly. The object size is set to be

```
... delta = 0.01; % Object size
```

Obtaining a converged solution-1

As in the previous tutorial we use p refinement to reach a converged solution. Selecting problem=6 in main.m and running with pm=0 we get

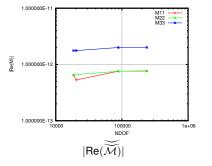
```
ptensor =
 -6.4540e-13 + 9.4842e-10i
                             2.0467e-15 - 5.1568e-13i -1.3046e-15 - 7.6587e-16i
  2.0467e-15 - 5.1568e-13i -6.5501e-13 + 9.5183e-10i -2.6143e-15 + 4.3374e-16i
 -1.3046e-15 - 7.6587e-16i -2.6143e-15 + 4.3374e-16i -1.7662e-12 + 1.0728e-09i
With pm=1
ptensor =
 -5.3017e-13 + 9.2072e-10i
                            -1.9624e-15 + 3.5270e-15i -2.9812e-15 - 1.0256e-15i
 -1.9626e-15 + 3.5270e-15i -5.2463e-13 + 9.2070e-10i 2.6514e-15 + 2.4742e-16i
 -2.9812e-15 - 1.0256e-15i
                             2.6514e-15 + 2.4742e-16i -1.7662e-12 + 1.0728e-09i
With pm=2
ptensor =
 -7.5839e-13 + 9.2023e-10i -1.2124e-16 + 2.4722e-16i -1.2212e-17 - 1.0327e-15i
 -1.2111e-16 + 2.4722e-16i -7.5796e-13 + 9.2023e-10i -1.5706e-16 + 2.0011e-16i
 -1.2287e-17 - 1.0327e-15i -1.5677e-16 + 1.9998e-16i -2.0075e-12 + 1.0728e-09i
```

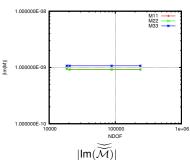
Obtaining a converged solution-2

With pm=3

```
ptensor =
    -7.6488e-13 + 9.2021e-10i    -1.6239e-17 + 4.2696e-16i     1.0980e-17 - 1.0319e-15i
    -1.6228e-17 + 4.2694e-16i    -7.6478e-13 + 9.2021e-10i    -1.6600e-17 + 2.0691e-16i
    1.0995e-17 - 1.0319e-15i    -1.6620e-17 + 2.0691e-16i    -2.0118e-12 + 1.0728e-09i
```

In this case there is no analytical solution with which to make comparisons against. Instead we look for convergence of the MPT coefficients,.





Although we could go higher with p (at greater computational expense) we see that there are only small changes in $|Re(\widetilde{\mathcal{M}})|$ coefficients between p=2 and p=3 (for $|\operatorname{Im}(\widetilde{\mathcal{M}})|$ are already converged at p=1). We deduce the solution has converged at p = 2.

As in the case of the sphere, the tensor is approximately diagonal with the off-diagonal elements several orders of magnitude smaller than the diagonal ones. Rotational and reflectional symmetries tell us that the MPT for this object is described by two independent complex coefficients and this is what we see in this example.

The two independent coefficients are

$$\widetilde{\mathcal{M}}_{11} = \widetilde{\mathcal{M}}_{22} = -7.64 \times 10^{-13} + 9.20 \times 10^{-10}i$$
 $\widetilde{\mathcal{M}}_{33} = -2.01 \times 10^{-12} + 1.07 \times 10^{-9}i$

Provided that the flag is appropriately set in the problem file

```
... % output the VTK file % vtkoption = 0 - do not output % vtkoption = 1 - output vtkoption =1:
```

Provided this flag is set the program will output a <code>[job].vtm</code> and multiple <code>[job]_#.vtu</code> files with <code>job</code> being specified in the problem file. A separate .vtu file is created for each subdomain in the mesh and all are referenced by the <code>[job].vtu</code> file.

These files contain the solution evaluated on a subdivided mesh for the purpose of visualisation.

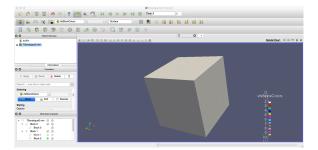
It is necessary to first subdivide the mesh as the visualisation provided by Paraview assumes a low order discretisation and to visualise the high-order solutions produced by hpfem-mpt correctly they must first be evaluated on a subdivided mesh.

The level of sub-division is controlled by pm (upto some prescribed maximum) and uses the curved geometry information received from the mesh.



In Paraview select File->Open and navigate to the root directory of hpfem-mpt where you should see the [job].vtu file listed.

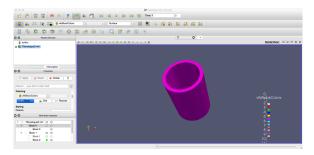
It is important to make sure Information, Multi-block inspector, Pipeline Browser and Properties are all available. To do this go to View and select the appropriate options. Then click Apply.



We are probably most interested in viewing the fields on/in the object so we need to select and deselect appropriate blocks. In Paraview the block numbers are numbered one less than the subdomain numbers in Netgen and hpfem-mpt

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Deselecting the blocks 0 and 1 and zooming on the object we see



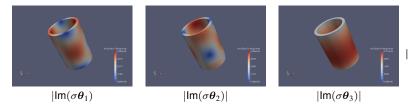
By choosing different options under coloring it is possible to visualise a selection of fields from each of the 3 different transmission problems.

Real and Imaginary parts of the magnetic type field $\nabla \times \theta_i$ (and eddy type current $\sigma \theta_i$) for each of the three problems i = 1, 2, 3 are available.



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As an example we show $|\text{Im}(\sigma\theta_i)|$ for i=1,2,3 on the surface of the object, below



Many more visualisation options are available (including vector quiver plots, cutting planes etc). Please see the Paraview documentation to find out more.

Other examples

Recall that in main.m 10 examples are available

```
% problem 1 = conducting magnetic sphere
% problem 3 = nested sphere conducting and magnetic
% problem 4 = conducting magnetic Remington shell casing
% problem 5 = simple steel gun L shape
% problem 6 = 72 anologue detonator
% problem 7 = belt buckle
% problem 8 = coin
% problem 9 = conducting magnetic torus
% problem 10 = Ansvs Mesh (Sohere)
```

and the results can compared with the values stored in the examples folder (note there may be small differences in values due to recent changes in hpfem-mpt).

The files p.0.dat, p.1.dat etc in the folders for the different objects refer to the MPT coefficients for different order elements p=0, p=1 etc.

Outline

- Introduction to the MPT
- Installing
- Tutorial 1: Conducting sphere
- Tutorial 2: Analogue Detonator
- Tutorial 3: Setting up your own geometries

Tutorial 3 Overview

In this tutorial we will

- Reiterate the key steps to create meshes with NETGEN for new geometries.
- Using problemfile_template.m to create problem files for new geometries



Mesh generation recap-1

 ${\tt NETGEN}$ includes a range of topological primitives that can be combined to create a range of interesting shaped objects.

- Blocks;
- Spheres;
- Cones;
- Ellipsoids;
- Torii;
- Planes

As we have already seen these can be multiply connected and made up of several different subdomains.

When creating the geometry for the object, it should have outer dimensions that are of O(1) and be placed in a region which is truncated by an outer boundary which is a sphere/box/or other convex shape. Typically this should be chosen to have dimensions O(100) to minimise the effect of approximate far field boundary conditions.

The geometry description is first saved in a .geo file that can is then read by NETGEN. For details see the NETGEN documentation.



Mesh generation recap-2

Once loaded in NETGEN it is best to first mesh the geometry using the default first order elements and the run the surface and volume mesh checking (see Mesh> Check Surface Mesh and Mesh> Check Volume Mesh) as discussed in tutorial 1.

Provided these checks are successful, the mesh can be regenerated using Second order elements and the desired level of refinement using Mesh> Meshing Options.



The mesh should then be saved as a .vol file in the meshes directory.

Problem file template - filling in the gaps -1

A problem file template problemfile_template.m is available in the problemfiles directory for you to edit to include the options for your own geometry.

The default options will use quadratic geometry (if available in the mesh file, linear otherwise) and apply the block-Jacobi preconditioner for solving the linear equation system.

The parts requiring input are highlighted in the file. The first is

```
%job data------
§ Input needed here
job = '%insert job name here%' % Job Name
% eg job='spherell' if the mesh file is spherell.vol
meshtype = 3; % Mesh type l= FLITE , 2=NG (old style), 3=NG (new style)
% no change to mesh type required if using NETGEN.
```

where the job name (determined by the .vol file) should be specified. The next is

```
%Input needed here,
omega = %insert frequency in rad/s;
% eg if omega is 133.5 rad/s enter
% omega =133.5;
```

where ω in (rad/s) should be specified.



Problem file template - filling in the gaps-2

Next, the material parameters for each subdomain (according to the TLO list in your . geo file) should be specified

```
% Input needed here
% For each subdomain specify parameters
% Mu_r, Ep_r, Sigma, J
% Mat 1
%eg if the first subdomain is non-conducting enter
%mu(1) = 1;
epl(1) = 0:
sigma(1) = 0.1;
sisrc(1.1:3) = [0 0 0]:
% and the second subdomain is the conducting object with mu r =1.5 and
% sigma =5.96e7 S/m enter
m_{11}(2) = 1.5
ep1(2) = 0;
sigma(2) = 5.96e7;
\frac{1}{3} isrc(2,1:3) = [0 0 0];
% Input needed here
% specify the material to be used a conductor conductors
% ie specify regions where gradients basis functions to be included
matcond= % insert an array contain the list of conductings subdomains.
% eg if the only conducting subdomain is the second one enter
% matcond=[2];
```

and the subdomains which make up the object listed in matcond,



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Problem file template - filling in the gaps-3

Finally, the object size scaling parameter should be entered

```
% Input needed here
% In this case the mesh is for a unit sized object, it must be scaled (and
% repositioned)
delta = % enter the object scaling
% specify what scaling to apply to go from the O(1) object specified in the
% mesh to the actual object. Eg if a conducting object of O(1) is specified
% in the mesh but the true object has dimension of O(0.01) enter
% delta = O.01: % Object size
```

The final stage is to save your modified yourproblemfile.m and include this as an option in main.m and to perform a *p*—convergence study.

Happy computing!



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