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Sat Jun 23 22:33:43 EDT 2018

#### Simulation input data:

B = 10.0 mmW = 70.0 mm $a_0 = 1.5 \text{ mm}$  $c_0 = 4.0 \text{ mm}$ 

L=10. mm

#MATERIAL= merged\_a36\_fitted.html (initiation)

Kt = 2.0

#TYPE= plate\_surface\_flaw

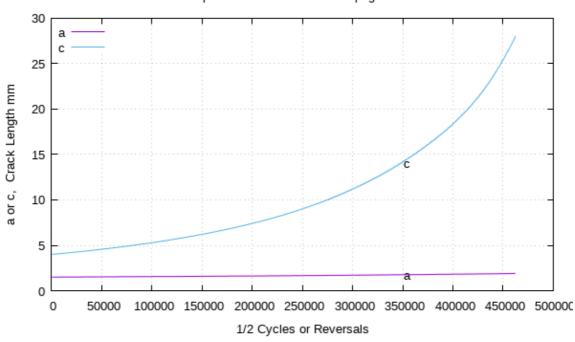
#ACTIVATE\_MmMb= 1 \_\_\_\_\_#ACTIVATE\_MkmMkb= 1 \_\_\_\_\_#ACTIVATE\_fw= 1

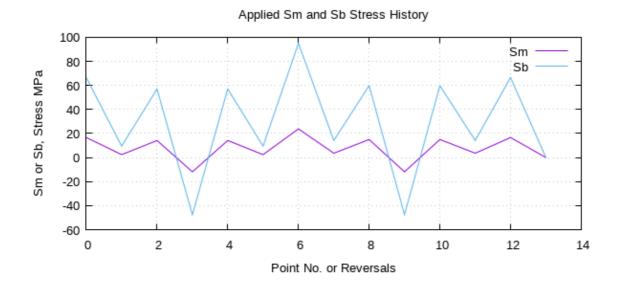
#### **Crack Propagation Results:**

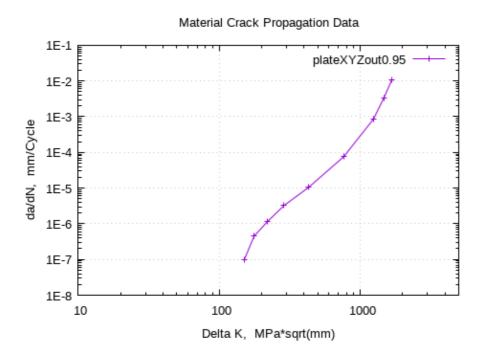
(#plateWeldflaw.f vers. 4.0 # makereport1 vers. 2.4 # plateWeldFAD.f vers. 0.6 starts...)

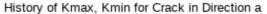
- No. of Reversals= 462217 revs. or 231108 cycles
- Final \_\_\_\_  $\mathbf{a} = 0.190E + 01 \text{ mm}$
- Final \_\_\_\_ c = 0.280E+02 mm
- No. of History Reps.= 33016 reps. + 7 revs.
- No. records = 462218 in random access data file

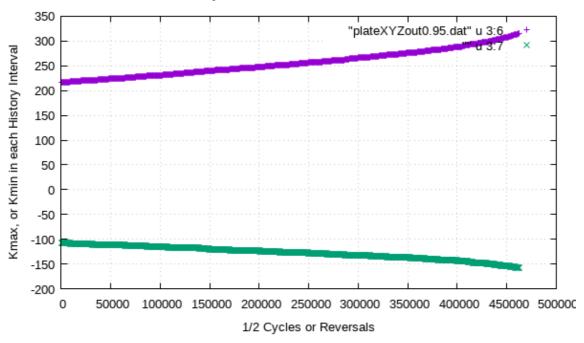




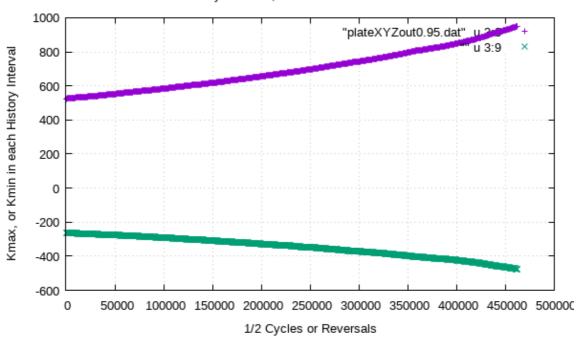


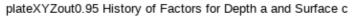


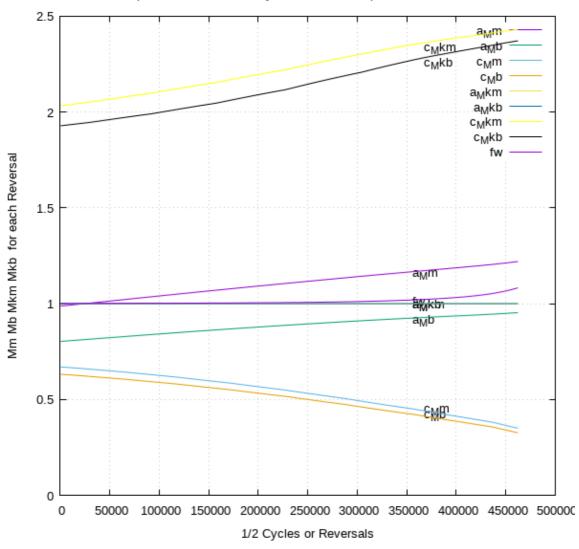




#### History of Kmax, Kmin for Crack in Direction c

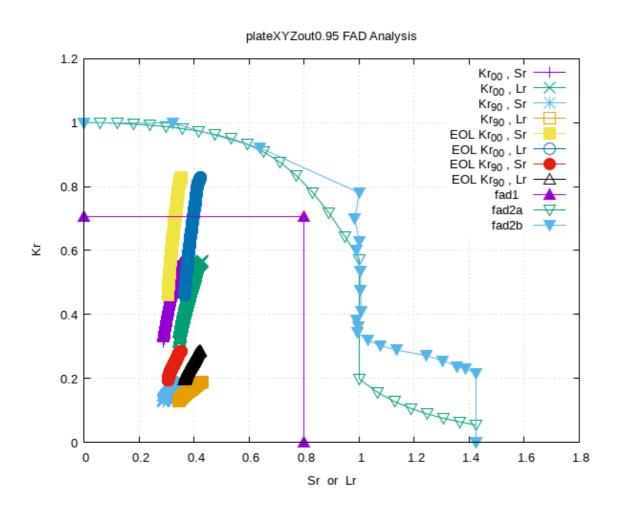






# FAD Results for plateXYZout0.95 #TensileFile= a36\_Mattos\_mono\_engrSS\_FLAT.txt

#PmEOL= 70. #PbEOL= 100. #Kmat= 1675. #PinJoint= 0



# **Crack Initiation Life Results for plateXYZout0.95** (Using Kt= 2.0)

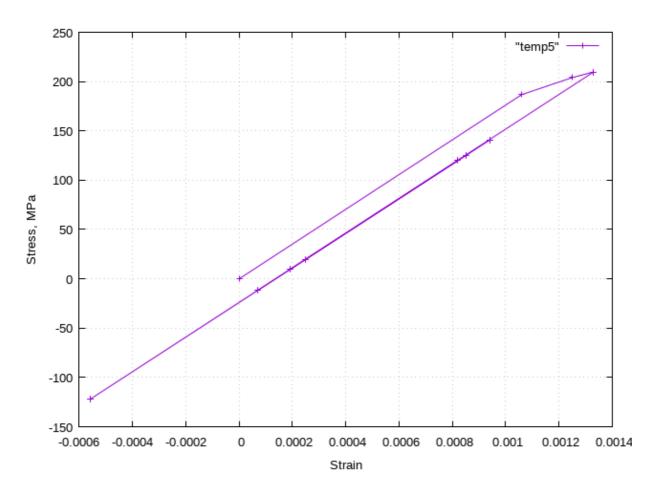
Files Used:

- Stress History (Sb+Sm)
- Rainflow File
- Material File

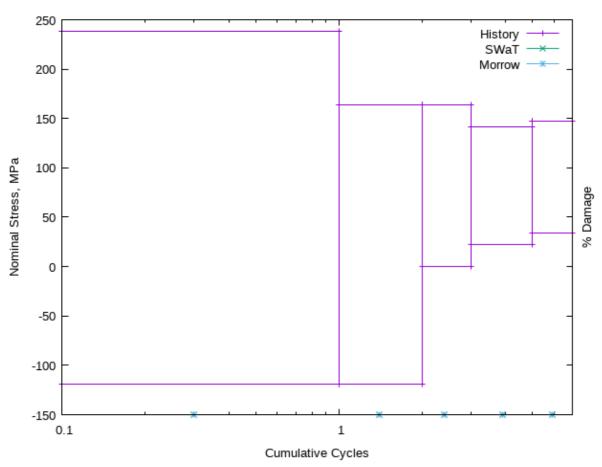
Predicted History Repetitions to Initiation:

StrainLife\_Reps SWT\_Life\_Reps StressLife\_Reps Morrow\_Reps Goodman\_Reps (Reps= Repetion Infinity Infinity Infinity Infinity

## **Local Stress and Strain Response:**



## **Cumulative Cycle Plot of History and Damage:**



(Rectangles are Rainflow Cycle Sets: Sorted by Range: largest on Left)

## **Detailed Damage for each Rainflow Cycle Set:**

```
Smax
              Smin
                          N Sigmax Sigmin Delta Epsmax Epsmin DeltaEps %Eps %SWT
Loop
                             210. -122. 332. 0.00133 -.00056 0.00188
   238.0 -118.8
                       1.0
                                                                     0.0
                                                                             0.0
                                                                                  0.0
                             141. -122. 263. 0.00094 -.00056 0.00149
   164.0 -118.8
                       1.0
                                                                       0.0
                                                                             0.0
                                                                                  0.0
                                   -12. 153. 0.00094 0.00007 0.00087
                                                                            0.0
   164.0
            0.0
                       1.0
                             141.
                                                                       0.0
                                                                                  0.0
                                     9. 111. 0.00082 0.00019 0.00063
   141.4
            22.6
                       2.0
                             120.
                                                                       0.0
                                                                            0.0
                                                                                  0.0
                                    20. 105. 0.00085 0.00025 0.00060
   147.0
            34.0
                       2.0
                             125.
                                                                       0.0
                                                                            0.0
                                                                                  0.0
```

## Appendix 1: Print of "pdprop.env" Simulation Control file

```
# plate_tru_flaw
#
                                # plate_embedded_flaw
                                # plate_edge_flaw
                                # pipe_inside_flaw
                                # pipe_full_inside_flaw
                                # pipe_full_outside_flaw
                                # rod surface flaw
                                # rod_full_outside_flaw
                                # These problem types are used to pull in the
                                # appropriate Fw, Mm, Mb, files etc.
# The factors described in this section may be ignored if not applicable to
# the particular problem type described above.
# (All dimensions in mm)
#B= 10.0 # plate (or pipe wall) thickness
\#W= 70.0 \# plate width
\#\text{ri}=200. \# Internal diameter if pipe problem. Ignored if not pipe \#\text{azero}=1.5 \# initial crack depth
#czero= 4.0 # initial 1/2 crack width at surface
#L= 10.  # Weld Feature width. Ignored if ACTIVATE_MkmMkb= 0 (above)
#HISTORYFILE= load1.txt  # historyFileName
           # Adjustments to load file variables:
            # Note that the MEANADD (below) is added AFTER the MAGFACTOR is applied.
\#MAGFACTOR\_m= 1.0 \# Multiply factor on membrane load. Result should be MPa
#MAGFACTOR_b= 1.0
                    # Multiply factor on bending load term. Result should be MPa
\#MEANADD_m = 0.0 \# Mean shift in MPa added to membrane stress.
#MEANADD_b= 0.0
                    # Mean shift in MPa added to bending stress.
#MAXREPS= 1000000 # Max no. history repeats in simulation.
                      # One repetition or application of the load history is
                      # also called a "block" of cycles.
#MATERIAL= merged_a36_fitted.html  #File name of material fitted data
                                 This file is used to define the cyclic
                                  stress-strain curve, and the Neuber Product curve.
#Kt= 2.0
                      #Stress Conc. Factor, presently only for crack initiation calcs.
                                      # Can be "table" or "Paris"
#DADN= table
                                    # Kth a m Kc units (ignored if #DADN= table )
#DADN_PARIS= 0.0 0.0 0.0 0.0 none
#DADN_TABLE= a36+1015.dadn # da/dN digitized da/dN curve for material,
                                  including the threshold, and KIc.
                                  If a threshold exists, put in a vertical line
                                  (with two identical X-axis points).
                                  If the threshold needs to be "turned off" then
                                  do NOT put in a vertical line at low da/dN.
                                  (Ignored when #DADN= PARIS )
#TensileFile= a36_Mattos_mono_engrSS_FLAT.txt #enter "none" if no FAD
\#PmEOL = 70.
                        #Set these so that Pm+Pb= 0.82*Syield for default.
#PbEOL= 100.
#Kmat= 1675.
#PinJoint= 0
                            #Set = 1 if struture is pinJointed (for bending)
                                # At the end of each block check if the previous
#BLOCKSKIP= 1.0 percent
                                  two blocks of cycles had similar damage (crack
                                  extension) within this percentage. If TRUE then
```

```
# simply skip the simulation of the next block,
but just add the expected damage. Continue by
simulating the block after the skip.

A value of 0.0 will disallow skipping blocks.

#SAVELEVEL= 0  #Amount of output saved to disk:
# 3=lots 2=medium 1=minimal
# 0= save #crk= data into binary direct access file only
# No #crk= data will be written into the text logfile.
# Use for large output files with lots of cycles.
```

## Appendix 2: Print of da/dn vs DeltaK Table in file plateXYZout0.95

## Appendix 3: Print of Stress-Strain-Init.Life file: "matfile"

#SAE Standard Fatigue Data File format

##

Pick one: #FDE\_plot #FDE\_fit # #

```
#Copyright (C) 2012 F.D.E. Committee
#This data file is free software - you can redistribute it and/or
#modify it under the terms of the GNU General Public License as
#published by the Free Software Foundation; either version 2 of the
#license, or (at your option) any later version.
#This data file is distributed in the hope that it will be useful,
#but WITHOUT ANY WARRANTY - without even the implied warranty of
#MERCHANTABILITY or FITNESS FOR A PARTICULAR PURPOSE. See the
#GNU General PUblic License for more details.
#You should have received a copy of the GNU General PUblic License
#along with this program - if not, write to the Free Software
#Foundation, Inc., 59 Temple Place - Suite 330, Boston, MA 02111-1307, USA
#Try also their web site: http://www.gnu.org/copyleft/gpl.html
# NOTE: Fitted Data !!
# A36 Steel Merged Data Sets from Refs. 1 and 2:
# Ref.1: P.Dindinger report to Fat.Des.+Eval. Comm. Apr.2012
# Ref.2: G.A.Miller and H.S.Reemsnyder, "Strain-Cycle Fatigue of Sheet and
# Plate Steels I: Test Method Development and Data Presentation,"
# SAE Paper 830175, Detroit MI, Feb28-Mar.4, 1983
\# NOTE that original test data ends at 2Nf = 1.3million.
#FileType= strain_life
```

```
#DataType= fitted
#TIMEcol= 0
#NAME= ASTM-A36
#NAME= Structural
#NAME= Steel
#Stress_units= ksi
#Strain_units= strain
#Sy= 38.4 0.2pc offset, 265 mpa
#Su= 69. ksi from Miller/Reemsnyder = 475 mpa
#eu= 0 #strain at Su not reported
\#E=29528. \text{ ksi} = 203600 \text{ mpa}
#FractureStrain= 0 not reported
#FractureStress= 0. not reported
#monotonic_K= 0 not reported
#monotonic_n= 0 not reported
#BHN= 138.
#%RA= 0. % not reported
#saedigcurve_v2.2.f starts.
# NOTE!! The Following Points are FITTED DATA: #NOTE!! Fitted Stress computed using F
# Total Strain 2Nf Stress Mean Plastic Strain Initial
 #Original test data ends at 2Nf = 1.3million.
#Points below are extrapolation:
0.00125 2000000 29.6 0. 0.00025 29528. #Fitted_point
0.00106 5000000 27.1 0. 0.00014 29528. #Fitted_point
#
#
```