

Tensor de Maxwell



$$\text{Carga puntual} \longrightarrow \vec{F} = q\vec{E} + q\frac{\vec{v}}{\epsilon} \times \vec{B}$$

$$\text{Distribución en volumen} \longrightarrow \vec{F} = \rho\vec{E} + \frac{\vec{j}}{\epsilon} \times \vec{B}$$

$$\frac{d\vec{P}_{\text{rec}}}{dt} = \vec{F}_0 + \vec{F}_{\text{EM}} = \vec{F}_0 + \int dv \left(\rho\vec{E} + \frac{\vec{j}}{\epsilon} \times \vec{B} \right)$$

Origen no es EM

→ de las ecuaciones de Maxwell (vacío)

$$\left\{ \begin{array}{l} \rho = \frac{1}{4\pi} \vec{\nabla} \cdot \vec{E} \\ \frac{\vec{j}}{\epsilon} = \frac{1}{4\pi} (\vec{\nabla} \times \vec{B} - \frac{1}{c} \frac{\partial \vec{E}}{\partial t}) \end{array} \right.$$

$$\Rightarrow \frac{d\vec{P}_{\text{rec}}}{dt} + \frac{d\vec{P}_{\text{EM}}}{dt} = \vec{F}_0 + \frac{1}{4\pi} \int_v dv \vec{\nabla} \cdot \vec{T} = \vec{F}_0 + \frac{1}{4\pi} \int_{S(v)} \vec{T} \cdot d\vec{s}$$

$$\frac{d\vec{P}_{\text{rec},i}}{dt} + \frac{d\vec{P}_{\text{EM},i}}{dt} = F_{0,i} + \frac{1}{4\pi} \int_{S(v)} T_{ij} n_j ds$$

el campo EM puede transportar Energía e Impulso

$$\text{Impulso lineal EM: } \vec{P}_{\text{EM}} = \frac{1}{4\pi c} \int_v dv \vec{E} \times \vec{B}$$

$$\text{Tensor de Maxwell: } T_{ij} = E_i E_j + B_i B_j - \frac{1}{2} \delta_{ij} (E^2 + B^2) \rightarrow \text{rango 2}$$

$$\rightarrow \text{Si } \frac{d\vec{P}}{dt} = 0 \implies \vec{F}_0 = -\frac{1}{4\pi} \int_{S(v)} \vec{T} \cdot d\vec{s}$$

Fuerza electro-magnética estática:

$$\vec{F} = \frac{1}{4\pi} \int_{S(v)} \vec{T} \cdot d\vec{s}$$

S: cualquier sup. que encierre la distribución

En electrostática ($B_i = 0$)

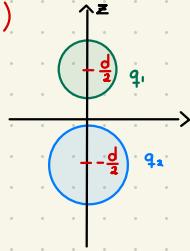
→ Campo ortogonal a la superficie $\vec{E} \cdot \hat{n} = E \hat{n}$

$$\vec{T} \cdot \hat{n} = (\vec{E} \cdot \hat{n}) \vec{E} - \frac{1}{2} E^2 \hat{n} = \frac{1}{2} E^2 \hat{n}$$

→ Campo paralelo a la superficie $\vec{E} \cdot \hat{n} = 0$

$$\vec{T} \cdot \hat{n} = (\vec{E} \cdot \hat{n}) \vec{E} - \frac{1}{2} E^2 \hat{n} = -\frac{1}{2} E^2 \hat{n}$$

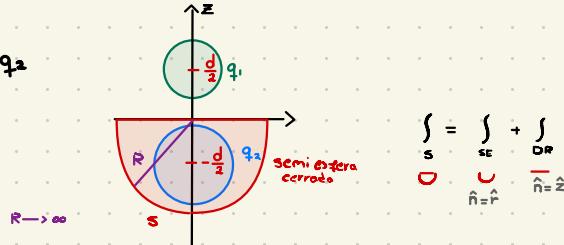
1)



1. Usar el tensor de Maxwell para encontrar:

(a) La fuerza entre dos esferas de radios a y b , con cargas q_1 y q_2 y separadas una distancia $d > a + b$

Fuerza sobre q_2



$$\vec{\overline{F}}_a = \frac{1}{4\pi} \int_{DR} ds \vec{T} \cdot \hat{n} + \frac{1}{4\pi} \int_{SE} ds \vec{T} \cdot \hat{n}$$

$$\left| \int_{SE} ds \vec{E} \cdot \hat{n} \right| \leq \int_{SE} ds |\vec{E} \cdot \hat{n}| \leq \int_{SE} ds \frac{3}{2} E^2 \quad \text{Campo total !!}$$

$$|\vec{\tau} \cdot \hat{n}| = |(\vec{E} \cdot \hat{n})\vec{E} - \frac{1}{2}\vec{E}^2\hat{n}| = |\vec{E} \cdot \hat{n}| |\vec{E}| + \frac{1}{2}\vec{E}^2 |\hat{n}| \leq \frac{3}{2} \vec{E}^2$$

Desarrollo multipolar:

$$|\vec{E}| \leq \frac{q_1 + q_2}{R_p} + |\vec{p} \cdot \hat{r} - \vec{p}'| \frac{1}{R^3} + \dots$$

$$\left| \int_{SE} ds \hat{T} \cdot \hat{n} \right| \leq \int_{SE} ds \frac{3}{2} E^2 \leq \frac{3}{2} \left(\frac{|Q|}{R^4} + |3\vec{P} \cdot \hat{R} - \vec{P}^2| \frac{1}{R^3} + \dots \right)^2 \cdot \underbrace{\frac{1}{2} 4\pi R^2}_{R \rightarrow \infty} \rightarrow 0$$

$$\therefore \overline{F}_2 = \frac{1}{4\pi} \int ds \overline{F} \cdot \hat{n}$$

$$\vec{F}_2 = \frac{1}{4\pi} \int_{D_R} d\vec{s} \vec{\tau} \cdot \hat{n} = \frac{1}{4\pi} \int_{D_R} d\vec{s} \left((\vec{E}_D \cdot \hat{n}) \vec{E}_D - \frac{1}{2} E_D^2 \hat{n} \right) \quad \vec{E}_D = \vec{E}(z=0)$$

campo sobre el plano

En cilíndricas:

$$\vec{E}_D = \frac{q_1}{(d^2/4 + \rho^2)^{3/2}} (\rho \hat{r} + \frac{d}{2} \hat{z}) + \frac{q_2}{(d^2/4 + \rho^2)^{3/2}} (\rho \hat{r} - \frac{d}{2} \hat{z}) = \frac{Q \rho \hat{r} + q \frac{d}{2} \hat{z}}{(d^2/4 + \rho^2)^{3/2}} \quad Q = q_1 + q_2, \quad q = q_1 - q_2$$

$$\Rightarrow \vec{E}_D = \frac{Q \rho^2 + q^2 d^2/4}{(d^2/4 + \rho^2)^3}$$

$$\Rightarrow \frac{1}{8\pi} \int_{D_R} d\vec{s} \vec{E}_D \cdot \hat{n} = \frac{1}{8\pi} \int_0^{2\pi} \int_0^\infty \rho d\rho d\phi \vec{E}_D \cdot \hat{z} = \frac{1}{8\pi} \int_0^{2\pi} \hat{z} \left(Q^2 \int_0^\infty \frac{\rho^2 d\rho}{(d^2/4 + \rho^2)^3} + q^2 d^2/4 \int_0^\infty \frac{\rho d\rho}{(d^2/4 + \rho^2)^3} \right) = \frac{1}{4d^4} (Q^2 + q^2) \hat{z}$$

$$\Rightarrow \vec{E}_D \cdot \hat{n} = \vec{E}_D \cdot \hat{z} = \frac{q \frac{d}{2}}{(d^2/4 + \rho^2)^{3/2}}$$

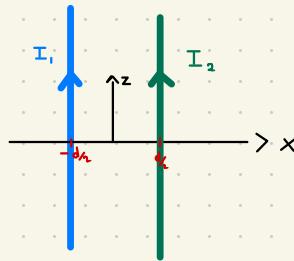
$$\Rightarrow \frac{1}{4\pi} \int_{D_R} d\vec{s} (\vec{E}_D \cdot \hat{n}) \vec{E}_D = \frac{1}{4\pi} \int_0^{2\pi} \int_0^\infty \rho d\rho d\phi \frac{q \frac{d}{2}}{(d^2/4 + \rho^2)^{3/2}} \frac{Q \rho \hat{r} + q \frac{d}{2} \hat{z}}{(d^2/4 + \rho^2)^{3/2}} = \frac{q d}{8\pi} \int_0^{2\pi} \int_0^\infty \rho d\rho d\phi \frac{Q \rho \hat{r} + q \frac{d}{2} \hat{z}}{(d^2/4 + \rho^2)^3}$$

$$\int_0^{2\pi} \hat{r} d\phi = 0 \quad \Rightarrow \quad = \frac{q d}{8\pi} \int_0^{2\pi} q \frac{d}{2} \hat{z} \int_0^\infty \frac{\rho d\rho}{(d^2/4 + \rho^2)^3} = \frac{q^2}{2d^2} \hat{z}$$

$$\Rightarrow \vec{F}_2 = \frac{1}{4\pi} \int_{D_R} d\vec{s} \left((\vec{E}_D \cdot \hat{n}) \vec{E}_D - \frac{1}{2} E_D^2 \hat{n} \right) = \frac{q^2}{2d^2} \hat{z} - \frac{1}{4d^4} (Q^2 + q^2) \hat{z} = \boxed{\frac{-1}{2d^2} q_1 q_2 \hat{z}} \quad \text{notar: indep.} \rightarrow \text{radios}$$

solo usamos los campos sobre el plano!

b)

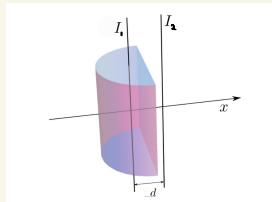


$$\mathbf{E} = \mathbf{0}$$

$$\vec{\tau} \cdot \hat{n} = (\vec{B} \cdot \hat{n}) \vec{B} - \frac{1}{2} \vec{B}^2 \hat{n} =$$

$$\vec{\tau}_2 = \frac{1}{4\pi} \int_{\text{plane}} ds \vec{\tau} \cdot \hat{n} + \frac{1}{4\pi} \int_{\text{3D}} ds \vec{\tau} \cdot \hat{n}$$

~~$\int_0^L dz \int_0^{2\pi} R d\phi \vec{\tau} \cdot \hat{n} \sim LR \frac{\pi^2}{R^2} \xrightarrow[R \rightarrow \infty]{} 0$~~



$$\vec{\tau}_2 = \frac{1}{4\pi} \int_{\text{plane}} ds \vec{\tau} \cdot \hat{n}$$

E) campo de un hilo conductor

$$\vec{B} = \frac{I}{c\rho} \hat{e} = \frac{I}{c\rho} \hat{z} \times \hat{r}$$

en el plano $x=0$:

$$\vec{B}_P = \vec{B}(x=0) = \frac{2I_-}{c(d^2_4+y^2)} \hat{z} \times \left(-\frac{d\hat{x}}{2} + y\hat{y} \right) + \frac{2I_+}{c(d^2_4+y^2)} \hat{z} \times \left(\frac{d\hat{x}}{2} + y\hat{y} \right) = \frac{2}{c(d^2_4+y^2)} \hat{z} \times \left(-\frac{dI_-}{2}\hat{x} + I_+ y\hat{y} \right)$$

$$I_\pm = I, \pm I_+$$

$$\rightarrow \vec{B}_P^t = \frac{q}{c(d^2_4+y^2)} \left(\frac{dI_-}{4}\hat{x} + I_+ y\hat{y} \right)$$

$$\Rightarrow \frac{1}{4\pi} \int_{\text{plane}} ds \left(-\frac{1}{2} \vec{B}_P^t \right) \hat{x} = -\frac{1}{8\pi} \int_0^L dz \int_{-\infty}^{\infty} dy \vec{B}_P^t \hat{x} = -\frac{1}{8\pi} \frac{q}{c} \left(I_- \frac{d}{4} \int_{-\infty}^{\infty} \frac{1}{(d^2_4+y^2)^2} dy + I_+ \int_{-\infty}^{\infty} \frac{y^2}{(d^2_4+y^2)^2} dy \right) = -\frac{L}{2cd} \left(I_- \frac{4\pi}{d^3} + I_+ \frac{\pi}{d} \right) \hat{x}$$

$$\rightarrow \vec{B}_P \cdot \hat{n} = \vec{B}_P \cdot \hat{x} = \frac{-a I_+ \gamma}{c(d\gamma_q + \gamma)}$$

$$\Rightarrow \frac{1}{4\pi} \int_{\text{plane}} ds (\vec{B}_P \cdot \hat{n}) \vec{B}_P = \frac{L}{4\pi} \int_{-\infty}^{\infty} dy \left(\frac{-a I_+ \gamma}{c(d\gamma_q + \gamma)} \right) \frac{(a)}{c(d\gamma_q + \gamma)} \frac{(dI_- \hat{y} + I_+ \gamma \hat{x})}{2}$$

$$= \frac{L}{c\pi} I_+ \left(\int_{-\infty}^{\frac{dI_-}{2}} dy \cancel{\frac{\gamma}{(d\gamma_q + \gamma)^2}} + I_+ \hat{x} \int_{-\infty}^{\infty} dy \frac{\gamma^2}{(d\gamma_q + \gamma)} \right) = \frac{L}{c d} I_+^2 \hat{x}$$

○ ~~impar~~

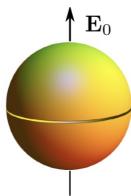
π/d

$$\Rightarrow \vec{F}_2 = \frac{1}{4\pi} \int_{\text{plane}} ds \vec{I} \cdot \hat{n} = -\frac{L}{2cd} (I_-^2 + I_+^2) \hat{x} + \frac{L}{c d} I_+^2 \hat{x}$$

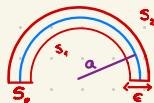
$$\boxed{\frac{\vec{F}_2}{L} = \frac{2}{c d} I_- I_+ \hat{x}}$$

3. Una esfera conductora descargada tiene radio a y está en un campo eléctrico externo uniforme \mathbf{E}_0 .

- (a) Calcular la fuerza que tiende a separar o a unir los hemisferios según la dirección de \mathbf{E}_0 .
- (b) Calcular la fuerza si ahora la esfera tiene carga neta Q . ¿Puede obtenerse este resultado sumando a la fuerza obtenida en el ítem anterior la fuerza calculada en la segunda parte del problema 2?



Fuerza sobre el hemisferio superior



$$\vec{F} = \frac{1}{4\pi} \int_S ds \bar{\tau} \cdot \hat{n} + \frac{1}{4\pi} \int_{S_1} ds \bar{\tau} \cdot \hat{n} + \frac{1}{4\pi} \int_{S_2} ds \bar{\tau} \cdot \hat{n} + \frac{1}{4\pi} \int_{S_2} ds \bar{\tau} \cdot \hat{n}$$

en el límite la contribución es la misma con $\hat{n}_1 = -\hat{n}_2$

$$\vec{F} = \frac{1}{4\pi} \int_S ds (\bar{\tau}_2 - \bar{\tau}_1) \cdot \hat{n}_2$$

pero dentro del conductor $\vec{E}_i = 0 \Rightarrow \bar{\tau}_1 \cdot \hat{n} = (\vec{E}_i \cdot \hat{n}) \vec{E}_i - \frac{1}{2} E_i^2 \hat{n} = 0$

$$\vec{F} = \frac{1}{4\pi} \int_S ds \bar{\tau}_2 \cdot \hat{n}_2$$

a) Esfera conductora \Rightarrow potencial sobre la superficie es constante $\therefore V$

Campo externo $\vec{E}_0 = E_0 \hat{z}$

\Rightarrow potencial total: suma de 1 que da origen a \vec{E}_0 y otro dado por la distribución de cargas sobre la esfera

$$\varphi = -E_0 r \cos\theta + \sum_{k=0}^{\infty} A_k \frac{r^k}{k+1} P_k(\cos\theta)$$

\curvearrowright sim. azimutal.

$$\varphi(r=a) = V \Rightarrow A_1 = E_0 a^2 ; A_0 = Va$$

$$\left. \begin{array}{l} \varphi = -E_0 r \cos\theta + \frac{Va}{r} + \frac{E_0 a^3}{r^3} \cos\theta \\ \vec{E} = \vec{E}_0 + \frac{Va}{r^2} \hat{r} + \left(\frac{a}{r}\right)^3 \left(3 E_0 \cos\theta \hat{r} - \vec{E}_0\right) \end{array} \right\} \begin{array}{l} r > a: \\ r < a: \end{array} \quad \left. \begin{array}{l} \varphi = V \\ E = 0 \end{array} \right\}$$

Término monopolar: $\frac{Va}{r} \Rightarrow$ esfera descargada $V=0$

$$\Rightarrow \vec{E} = \vec{E}_0 + \left(\frac{a}{r}\right)^3 \left(3 E_0 \cos\theta \hat{r} - \vec{E}_0\right) \quad r > a$$

y en el límite $\epsilon \rightarrow 0$: $\vec{E} = 3 E_0 \cos\theta \hat{r}$

$$\vec{T} \cdot \hat{n} = \vec{T} \cdot \hat{r} = (\vec{E} \cdot \hat{r}) \vec{E} - \frac{1}{2} \vec{E}^2 \hat{r} = \frac{1}{2} \vec{E}^2 \hat{r} = \frac{q}{2} E_0^2 \cos^2\theta \hat{r}$$

$$\Rightarrow \vec{F} = \frac{1}{4\pi} \int_S dS \vec{T}_a \cdot \hat{n}_a = \frac{q}{8\pi} \int_0^{2\pi} \int_0^{\pi/2} \sin\theta d\theta d\phi E_0^2 \cos^3\theta \hat{r} = \frac{q}{8\pi} \cancel{\frac{1}{4}} \int_0^{\pi/2} \int_0^{2\pi} \sin\theta d\theta E_0^2 \cos^3\theta \hat{z}$$

$$\int_0^{2\pi} d\phi \hat{r} = 2\pi \cos\hat{z}$$

$$= \frac{q}{4} E_0 a^3 \int_0^1 d(\cos\theta) \cos^3\theta \hat{z} = \boxed{\frac{q}{16} E_0 a^3 \hat{z} = \vec{F}}$$

b) $Q \neq 0$

$$\vec{E} = \vec{E}_0 + \frac{\sqrt{Q}}{r^2} \hat{r} + \left(\frac{Q}{r}\right)^3 \left(3 E_0 \cos\theta \hat{r} - \vec{E}_0\right) \quad r > a$$

en el límite $\epsilon \rightarrow 0$: $\vec{E} = \left(\frac{Q}{a^3} + 3 E_0 \cos\theta\right) \hat{r}$

$$\vec{T} \cdot \hat{n} = \vec{T} \cdot \hat{r} = \frac{1}{2} E^* \hat{r}$$

$$\Rightarrow \vec{F} = \frac{1}{4\pi} \frac{a^5}{0} \int_0^{2\pi} d\phi \frac{1}{2} \left(\frac{Q}{a^3} + 3 E_0 \cos\theta \right)^2 \hat{r} = \frac{a^5}{4} \int_0^{2\pi} d\phi \cos\theta \left(\frac{Q^2}{a^6} + 6 \frac{Q}{a^3} E_0 \cos\theta + 9 E_0^2 \cos^2\theta \right) \cos\theta \hat{z}$$

$$\boxed{\vec{F} = \left(\frac{Q^2}{a^6} + \frac{Q E_0}{2} + \frac{9}{16} E_0^2 \hat{z} \right) \hat{z}}$$