

# The Heavy Photon Search Test Detector

M. Battaglieri<sup>a</sup>, S. Boyarinov<sup>b</sup>, S. Bueltmann<sup>c</sup>, V. Burkert<sup>b</sup>, W. Cooper<sup>d</sup>, N. Dashyan<sup>e</sup>, R. De Vita<sup>a</sup>, A. Deur<sup>b</sup>, H. Egiyan<sup>b</sup>, L. Elouadrhiri<sup>b</sup>, R. Essig<sup>f</sup>, V. Fadeyev<sup>g</sup>, C. Field<sup>h</sup>, A. Fradi<sup>i</sup>, A. Freyberger<sup>b</sup>, N. Gevorgyan<sup>e</sup>, F.-X. Girod<sup>b</sup>, N. Graf<sup>h</sup>, M. Graham<sup>h</sup>, K. Griffioen<sup>j</sup>, A. Grillo<sup>g</sup>, B. Guegan<sup>i</sup>, M. Guidal<sup>l</sup>, G. Haller<sup>h</sup>, P. Hansson Adrian<sup>h,\*</sup>, R. Herbst<sup>h</sup>, M. Holtrop<sup>k</sup>, J. Jaros<sup>h</sup>, S. K. Phillips<sup>k</sup>, M. Khandaker<sup>l</sup>, A. Kubarovský<sup>m</sup>, T. Maruyama<sup>h</sup>, J. McCormick<sup>h</sup>, K. Moffeit<sup>h</sup>, O. Moreno<sup>g</sup>, H. Neal<sup>h</sup>, T. Nelson<sup>h</sup>, S. Niccolai<sup>i</sup>, A. Odian<sup>h</sup>, M. Oriunno<sup>h</sup>, R. Paremuzyan<sup>e</sup>, S. Pisano<sup>i</sup>, E. Rauly<sup>i</sup>, P. Rosier<sup>i</sup>, C. Salgado<sup>l</sup>, P. Schuster<sup>n</sup>, Y. Sharabian<sup>b</sup>, K. Slifer<sup>k</sup>, D. Sokhan<sup>i</sup>, S. Stepanyan<sup>b</sup>, P. Stoler<sup>m</sup>, N. Toro<sup>n</sup>, S. Uemura<sup>h</sup>, M. Ungaro<sup>b</sup>, H. Voskanyan<sup>e</sup>, D. Walz<sup>h</sup>, L. Weinstein<sup>c</sup>, B. Wojtsekowski<sup>b</sup>

<sup>a</sup>Istituto Nazionale di Fisica Nucleare, Sezione di Genova e Dipartimento di Fisica dell'Università, 16146 Genova, Italy

<sup>b</sup>Thomas Jefferson National Accelerator Facility, Newport News, Virginia 23606

<sup>c</sup>Old Dominion University, Norfolk, Virginia 23529

<sup>d</sup>Fermi National Accelerator Laboratory, Batavia, IL 60510-5011

<sup>e</sup>Yerevan Physics Institute, 375036 Yerevan, Armenia

<sup>f</sup>Stony Brook University, Stony Brook, NY 11794-3800

<sup>g</sup>University of California, Santa Cruz, CA 95064

<sup>h</sup>SLAC National Accelerator Laboratory, Menlo Park, CA 94025

<sup>i</sup>Institut de Physique Nucléaire d'Orsay, IN2P3, BP 1, 91406 Orsay, France

<sup>j</sup>The College of William and Mary, Department of Physics, Williamsburg, VA 23185

<sup>k</sup>University of New Hampshire, Department of Physics, Durham, NH 03824

<sup>l</sup>Norfolk State University, Norfolk, Virginia 23504

<sup>m</sup>Rensselaer Polytechnic Institute, Department of Physics, Troy, NY 12181

<sup>n</sup>Perimeter Institute, Ontario, Canada N2L 2Y5

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## Abstract

The Heavy Photon Search (HPS), an experiment to search for a hidden sector photon in fixed target electroproduction, is preparing for installation at the Thomas Jefferson National Accelerator Facility (JLab) in the Fall of 2014. As the first stage of this project, the HPS Test Run apparatus was constructed and operated in 2012 to demonstrate the experiment's technical feasibility and to confirm that the trigger rates and occupancies are as expected. This paper describes the HPS Test Run apparatus and readout electronics and its performance. In this setting, a heavy photon can be identified as a narrow  $e^+e^-$  mass peak above the trident background or as a decay vertex displaced from the production target, so charged particle tracking and vertexing are needed for its detection. In the HPS Test Run, charged particles are measured with a compact forward silicon microstrip vertex/tracker inside a dipole magnet. Electromagnetic showers are detected in a PbW<sub>0</sub><sub>4</sub> crystal calorimeter situated behind the magnet used to trigger the experiment and identify electrons and positrons. Both detectors are placed close to the beam line and split top-bottom. This arrangement provides sensitivity to low-mass heavy photons, allows clear passage of the unscattered beam, and avoids the spray of degraded electrons coming from the target. The discrimination between prompt and displaced  $e^+e^-$  pairs requires the first layer of silicon sensors be placed only 10 cm downstream of the target. The expected signal is small, and the trident background huge, so the experiment requires very large statistics. Accordingly, the HPS Test Run utilizes high-rate readout and data acquisition electronics and a fast trigger to perfectly exploit the essentially 100% duty cycle of the CEBAF accelerator.

**Keywords:** silicon microstrip, tracking, vertexing, heavy photon, dark photon, hidden sector, electromagnetic calorimeter

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\*Corresponding author.

Email address: phansson@slac.stanford.edu (B.

Wojtsekowski)

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29    **1. Introduction**

30    The heavy photon ( $A'$ ), aka a "hidden sector" or  
31    "dark" photon, is a particle with mass  $10 - 1000$  MeV  
32    which couples weakly to electric charge by mixing with  
33    the Standard Model photon [1]. Consequently, it can  
34    be radiated by electrons and subsequently decay into  
35     $e^+e^-$  pairs, albeit at rates far below those of QED tri-  
36    dent processes. Heavy photons have been suggested by  
37    numerous beyond Standard Model theories [2], to ex-  
38    plain the discrepancy between theory and experiment of  
39    the muon's  $g - 2$  [3], and as a possible explanation of  
40    recent astrophysical anomalies. Heavy photons couple  
41    directly to hidden sector particles with "dark" or "hid-  
42    den sector" charge; these particles could constitute all  
43    or some of the dark matter [4]. Current phenomenology  
44    highlights the  $20 - 1000$  MeV/c $^2$  mass range, and sug-  
45    gests that the coupling to electric charge,  $\epsilon e$ , has  $\epsilon$  in the  
46    range of  $10^{-3} - 10^{-5}$ . This range of parameters makes  
47     $A'$  searches viable in medium energy fixed target elec-  
48    troproduction [5], but requires large data sets and good  
49    mass resolution to identify a small mass peak above the  
50    copious QED background. At small couplings,  $A'$  be-  
51    come long-lived, so detection of a displaced decay ver-  
52    tex can reject the prompt QED background and boost  
53    experimental sensitivity.

54    The HPS experiment [6] uses both invariant mass and  
55    secondary vertex signatures to search for  $A'$ . It uses a  
56     $\approx 1$  m long silicon tracking and vertexing detector in-  
57    side a dipole magnet to measure charged particle trajec-  
58    tories and a fast electromagnetic calorimeter just down-  
59    stream of the magnet to provide a trigger and identify  
60    electrons. The experiment utilizes very high rate front  
61    end electronics and runs at high trigger rates (up to  
62    50kHz), exploiting the 100% duty cycle of the Thomas  
63    Jefferson National Accelerator Facility (JLab) CEBAF  
64    accelerator to accumulate the needed statistics.

65    The HPS Test Run apparatus, a simplified version  
66    of the HPS experiment, was proposed and approved at  
67    JLab as the first stage of HPS. Its purposes included  
68    demonstrating that the apparatus and data acquisition  
69    systems are technically feasible and the trigger rates and  
70    occupancies to be encountered in electron-beam run-  
71    ning are as simulated. Given dedicated running time  
72    with electron beams, the HPS Test Run apparatus is ca-  
73    pable of searching for heavy photons in unexplored re-  
74    gions of parameter space. The key design criteria for  
75    HPS and the HPS Test Run are the same:

- 76    • large and uniform acceptance in the forward region  
77    close to the beam in order to catch boosted  $A'$  de-  
78    cay products,

- 79    • beam passage through the apparatus in vacuum, to  
80    eliminate direct interactions with the detector and  
81    minimize beam gas interactions,
- 82    • a flexible, redundant and efficient trigger selecting  
83    electron and positron pairs at rates up to 50 kHz,
- 84    • excellent track reconstruction efficiency for elec-  
85    trons and positrons,
- 86    • good angular and momentum resolution to recon-  
87    struct invariant mass precisely,
- 88    • excellent vertex resolution to discriminate dis-  
89    placed  $A'$  decays from prompt QED backgrounds,
- 90    • high rate electronics with excellent timing resolu-  
91    tion to minimize out of time backgrounds,
- 92    • data handling rates of 100 MB/s to permanent stor-  
93    age,
- 94    • detector components that can survive and effi-  
95    ciently operate in a high radiation environment  
96    with local doses exceeding 100 Mrad.

97    The HPS Test Run apparatus was installed on April  
98    19, 2012, and ran parasitically in the photon beam of  
99    the HDice experiment [7] until May 18. The JLab run  
100   schedule precluded any dedicated electron beam run-  
101   ning, but the HPS Test Run was allowed a short and  
102   valuable dedicated run at the end of scheduled CE-  
103   BAF running. This final running provided enough data  
104   to demonstrate the functionality of the apparatus, doc-  
105   ument its performance, and explore trigger rates, as  
106   shown below. This paper reviews the HPS Test Run ap-  
107   paratus; documents the performance of the trigger, data  
108   acquisition, silicon tracking detector, and the electro-  
109   magnetic calorimeter at the level assumed in calculating  
110   the physics reach of the HPS experiment.

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113   sition, silicon tracking detector, and the electro-  
114   magnetic calorimeter at the level assumed in calculating the  
115   physics reach of the HPS experiment.

116   **2. Detector Overview**

117   The HPS Test Run apparatus was designed to run  
118   in Hall B at JLab using the CEBAF electron beam, a  
119   499 MHz beam, at energies of 2.2 and 6.6 GeV and cur-  
120   rents between 200 and 600 nA. The overall design of  
121   the experiment follows from the kinematics of  $A'$  pro-  
122   duction which typically results in a final state particle

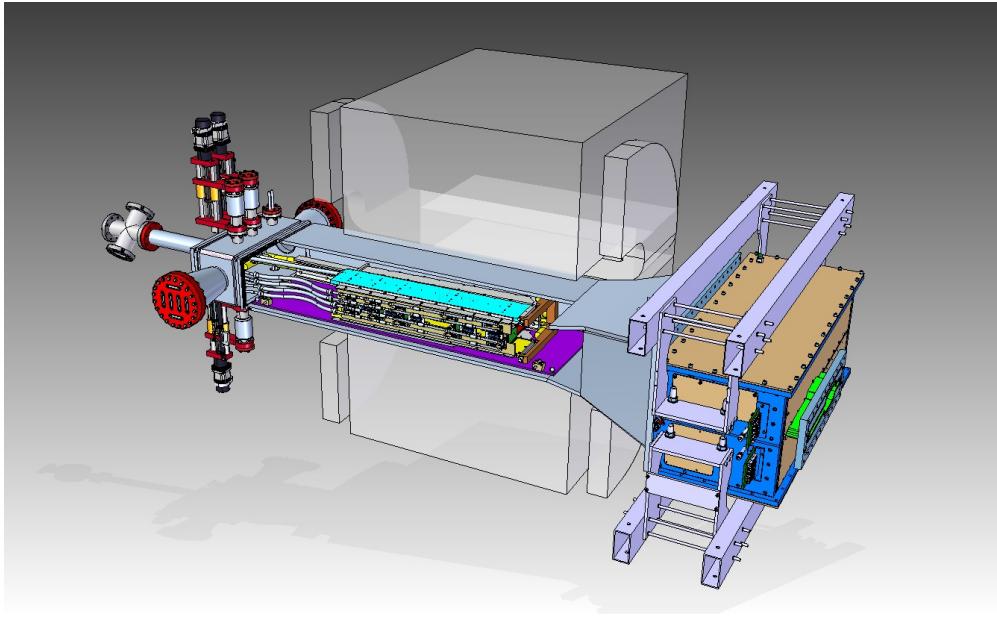


Figure 1: Rendering of the HPS Test Run apparatus installed on the beam line.

123 within a few degrees of the incoming beam, especially 150  
 124 at low  $m_{A'}$ . Detectors must therefore be placed close 151  
 125 to the beam. The intense electron beam enlarges down- 152  
 126 stream after multiple scattering in the target and elec- 153  
 127 trons which have radiated in the target disperse horizon- 154  
 128 tally in the field of the analyzing magnet. Together they 155  
 129 constitute a "wall of flame" which must be completely 156  
 130 avoided. Accordingly, the apparatus is split vertically 157  
 131 to avoid a "dead zone", the region within  $\pm 15$  mrad of 158  
 132 the beam plane. In addition, the beam is transported in 159  
 133 vacuum through the tracker to minimize beam-gas inter- 160  
 134 action backgrounds. Even with these precautions, the 161  
 135 occupancies of sensors near the beam plane are high, 162  
 136 dominated by the multiple Coulomb scattering of the 163  
 137 primary beam, so high rate detectors, a fast trigger, and 164  
 138 excellent time tagging are required to minimize their 165  
 139 impact. The trigger comes from a highly-segmented 166  
 140 lead-tungstate ( $\text{PbWO}_4$ ) crystal calorimeter located just 167  
 141 downstream of the dipole magnet.

142  
 143 A rendering of the apparatus installed on the beam line 171  
 144 is shown in Fig. 1 and an overview of the coverage, seg- 172  
 145 mentation and performance is given in Tab. 1.

146 The silicon tracking and vertexing detector for HPS 173  
 147 Test Run, or SVT, resides in a vacuum chamber in- 174  
 148 side the Pair Spectrometer (PS) dipole magnet in Hall 175  
 149 B at JLab. The SVT has five measurement stations,

150 or "layers," beginning 10 cm downstream of the target. 151 Each layer comprises a pair of closely-spaced silicon 152 microstrip sensors responsible for measuring a single 153 coordinate, or "view". Introduction of a small (50 or 154 100 mrad) stereo angle between the two sensors of each 155 layer provides three-dimensional tracking and vertexing 156 throughout the acceptance of the detector. In order to 157 accommodate the dead zone, the SVT is built in two 158 halves that are approximately mirror reflections of one 159 another about the plane of the nominal electron beam. 160 Each layer in one half is supported on a common sup- 161 port plate with independent cooling and readout.

162 The electromagnetic calorimeter (ECal) is also split 163 into two halves. Each half of the ECal consists of 164 221  $\text{PbWO}_4$  crystals arranged in rectangular formation. 165 There are five rows with 46 modules in each row except 166 the row closest to the beam plane which has 37. The 167 light from each crystal is read out by an Avalanche 168 Photodiode (APD) glued on the back surface of the 169 crystal. Signals from the APDs are amplified using custom- 170 made amplifier boards before being sent to the data ac- 171 quisition electronics.

172 The Data Acquisition system combines two architec- 173 tures, the Advanced Telecom Communications Archi- 174 tecture (ATCA) based SVT readout system and VME- 175 bus Switched Serial (VXS) based digitization and trig- 176 gering system for the ECal. The system was designed 177 to run at up to 20 kHz trigger rate.

Table 1: Overview of the coverage, segmentation and performance of the HPS Test Run detector.

System	Coverage (mrad)	# channels	ADC (bit)	Time resolution (ns)	# layers	Segmentation	Performance
SVT	$15 < \theta_y < XXXX$	12800	14	$\approx 2$ ns	5 (stereo layers)	$\approx 120 \mu\text{m} r - \phi$ $\approx 6 \mu\text{m} z$	$\sigma_{d0,y} \approx 100 \mu\text{m}$ $\sigma_{d0,x} \approx 300 \mu\text{m}$ $\sigma_{d0,z} \approx 1 \text{ mm}$
Ecal	$15 < \theta_y < XXXX$	442	12	4 ns	1	$1.3 \times 1.3 \text{ cm}^2$ $1.6 \times 1.6 \text{ cm}^2$	$\sigma(E)/E \approx 4.5\%$

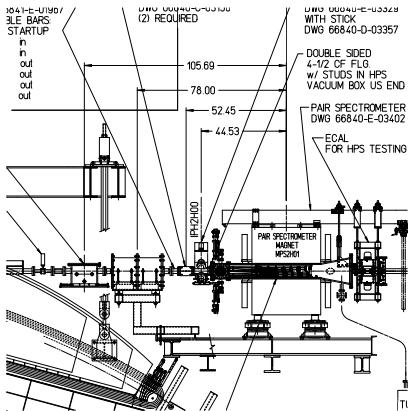


Figure 2: Layout of the HPS parasitic run.

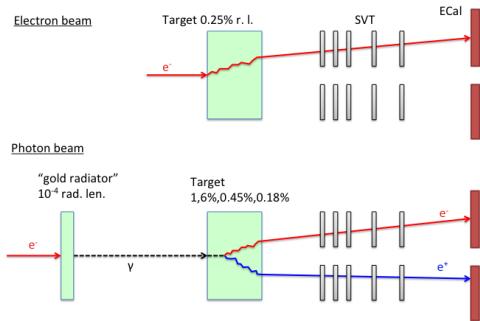


Figure 3: Illustrative comparison of HPS Test Run photon beam compared to the HPS electron beam.

### 178 3. The HPS Test Run Beamline

179 The HPS Test Run studied multiple Coulomb scattering of electrons and positrons from bremsstrahlung photons produced in the Hall B tagged photon facility. 180 Figure 2 shows the layout of the setup on the beam line. 181 The SVT was installed inside the Hall B pair spectrometer magnet vacuum chamber with the ECal mounted downstream of it. Both the SVT and the ECal were retracted off the beam plane compared to nominal electron beam running to allow clean passage of the photon beam through the system.

182 The photon beam was generated in the interaction of 183 5.5 GeV electrons with a  $10^{-4} X_0$  gold radiator located 184  $\approx 9$  m upstream of the PS. The primary beam and scattered 185 electrons are deflected away from detectors by the 186 dipole magnet of the photon tagging system. During the 187 dedicated HPS Test Run period, the collimated (6.4 mm 188 diameter), photon beam passes through the PS pair converter 189 gold foil and later the HPS system as illustrated in Fig. 3. The PS pair converter was located  $\approx 77$  cm 190 upstream of the first layer of the SVT.

191 Data was taken on three different converter thicknesses 192 with photon fluxes between  $0.4\text{--}1.3 \times 10^8/\text{s}$  193 ( $0.55 < E_\gamma < 5.5$  GeV) at beam currents varying 194 between 30–90 nA and repeated with the reverse field set- 195 196 197 198 199 200 201 202

Converter thickn. (% $X_0$ )	Duration (s)	$e^-$ on radiator ( $\mu\text{C}$ )
1.6	911	24.4
0.18	2640	193.5
0.45	2149	140.7
0	1279	88.1

Table 2: Measured integrated currents for the dedicated photon runs.

203 ting of the PS dipole magnet. The photon beam line 204 during the HPS Test Run produced a relatively large 205 fraction of pairs originating upstream of the converter 206 position. This contribution was measured during data 207 taking with “empty” converter runs i.e. removing the 208 converter but with all other conditions the same. The 209 runs taken during the time dedicated to HPS Test Run is 210 summarized in Tab. 2.

### 211 4. Silicon Vertex Tracker

The Silicon Vertex Tracker (SVT) enables efficient reconstruction of charged particles and precision determination of their trajectories. These measurements allow  $A'$  decays to be distinguished from background via simultaneous estimation of the invariant mass of  $e^+e^-$

217 decay products and the position of decay vertexes downstream of the target.  
218

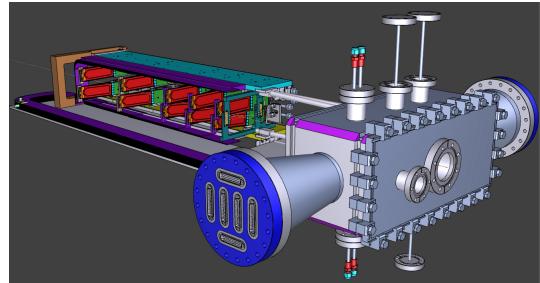
219 The design of the SVT is primarily driven by direct  
220 physics requirements and constraints from the environment  
221 at the interaction region. The A' decay products  
222 have momenta in the range of 1 GeV, so multiple scattering  
223 dominates mass and vertexing uncertainties for  
224 any possible material budget, so the SVT must minimize  
225 the amount of material in the tracking volume.  
226 The signal yield for long-lived A' is very small, so the  
227 rejection of prompt vertexes must be exceedingly pure,  
228 on the order of  $10^{-7}$ , in order to eliminate all prompt  
229 backgrounds. To achieve the required vertexing performance  
230 the first layer of the SVT must be placed no more than about 10 cm downstream of the target.  
231 At that distance, it is found that the active region of  
232 a sensor can be placed as close to 1.5 mm from the center of the beam, defining the 15 mrad “dead zone”  
233 mentioned previously, to maximize low-mass A' acceptance  
234 with decay products nearly collinear with the beam axis. At the edge of this “dead zone,” the radiation  
235 dose approaches  $10^{15}$  electrons/cm<sup>2</sup>/month, or roughly  
236  $3 \times 10^{14}$  1 MeV neutron equivalent/cm<sup>2</sup>/month [8], requiring the sensors to be actively cooled. Meanwhile,  
237 very low-energy delta rays from beam-gas interactions  
238 multiply the density of background hits, so the SVT  
239 must operate inside the beam vacuum. Finally, in order  
240 to protect the sensors, the detector must be movable  
241 so that it can be retracted during periods of uncertain  
242 beam conditions.

#### 247 4.1. Layout

248 The layout of the SVT is summarized in Tab. 4.1 and  
249 rendered in Fig. 4. Each of the layers is comprised  
250 of a pair of closely-spaced silicon microstrip sensors  
251 mounted back-to-back to form a module. A 100 mrad  
252 stereo angle is used in the first three layers to provide  
253 higher-resolution 3D space points for vertexing. Using  
254 50 mrad in the last two layers breaks the tracking  
255 degeneracy of having five identical layers and minimizes  
256 fakes from ghost hits to improve pattern recognition.  
257 Altogether, the SVT has 20 sensors for a total of 12780  
258 readout channels.

Layer	1	2	3	4	5
<i>z</i> from target (cm)	10	20	30	50	70
Stereo angle (mrad)	100	100	100	50	50
Bend res. ( $\mu\text{m}$ )	$\approx 60$	$\approx 60$	$\approx 60$	$\approx 120$	$\approx 120$
Non-bend res. ( $\mu\text{m}$ )	$\approx 6$	$\approx 6$	$\approx 6$	$\approx 6$	$\approx 6$
# of sensors	4	4	4	4	4
Dead zone (mm)	$\pm 1.5$	$\pm 3.0$	$\pm 4.5$	$\pm 7.5$	$\pm 10.5$
Power cons. (W)	6.9	6.9	6.9	6.9	6.9

259 Table 3: Layout of the SVT.



260 Figure 4: A rendering of the SVT showing the modules on their support plates held by the hinged C-support on the left and the motion levers on the right. The sensors are shown in red and the hybrid readout boards in green. The beam enters from the right through a vacuum box with flanges for services.

261 The SVT is built in two separate halves that are mirror  
262 reflections of one another about the plane of the nominal  
263 electron beam. Each half consists of five modules  
264 mounted on a support plate that provides services to the  
265 modules and allows them to be moved as a group relative  
266 to the dead zone. The two halves of the tracker are connected  
267 to hinges mounted on a C-shaped support just beyond the last layer that defines the nominal spacing  
268 between the upper and lower halves of the tracker. A shaft attached to each support plate in front of layer  
269 1 extends upstream and connects to a linear shift that  
270 transfers motion into the vacuum box through bellows  
271 to open and close the two halves around the dead zone.  
272 The C-support is mounted to an aluminum baseplate  
273 that defines the position of the SVT with respect to the  
274 vacuum chamber. Figure 5 shows a photograph of both  
275 completed detector halves prior to final assembly.



276 Figure 5: Both halves of the HPS Test Run SVT after final assembly at SLAC. The cooling manifolds and integrated cable runs are clearly seen.

278    **4.2. Components**

279    The sensors for the SVT are *p*-on-*n*, single sided,  
 280    AC coupled, polysilicon-biased microstrip sensors fab-  
 281    ricated on < 100 > silicon and have 30 (60)  $\mu\text{m}$  sense  
 282    (readout) pitch over their  $4 \times 10 \text{ cm}^2$  surface. This sen-  
 283    sor technology was selected to match the requirement  
 284    of a  $< 1\% X_0$  per layer, single-hit resolution better than  
 285     $50 \mu\text{m}$  and tolerant of a radiation dose of approximately  
 286     $1.5 \times 10^{14} 1 \text{ MeV}$  neutron equivalent/ $\text{cm}^2$  for a six month  
 287    run. The sensors were purchased from the Hamamatsu  
 288    Photonics Corporation for the cancelled Run 2b upgrade  
 289    of the DØ experiment [9] which satisfied the require-  
 290    ment that the technology must be mature and available  
 291    within the time and budget constraints.

292    Despite having only small spots with very high occu-  
 293    pancy (up to  $4 \text{ MHz/mm}^2$ ) closest to the primary beam,  
 294    the rates are still high and lowering the peak occupancy  
 295    to approximately 1% for tracking requires a trigger win-  
 296    dows and hit time tagging of roughly 8 ns. The ECal  
 297    readout and trigger described in Sec. 5.3 can achieve  
 298    such resolution. To reach this performance the sen-  
 299    sors for the SVT are readout by the APV25 ASIC de-  
 300    veloped for the CMS experiment at CERN [10]. The  
 301    APV25 can capture successive samples of the shaper  
 302    output in groups of three at a sampling rate of approx-  
 303    imately 40 MHz. By fitting the known *CR-RC* shaping  
 304    curve to these samples, the initial time of the hit can  
 305    be determined to a precision of 2 ns for  $S/N \approx 25$  [11].  
 306    For electron beam running, six-sample readout and the  
 307    shortest possible shaping time (35 ns) is used to best  
 308    distinguish hits that overlap in time. The APV25 ASICs  
 309    are hosted on simple FR4 hybrid readout boards, out-  
 310    side the tracking volume, with a short twisted-pair pig-  
 311    tail cable to provide power and configuration and signal  
 312    readout. Along with a single sensor, these are glued  
 313    to a polyamide-laminated carbon fiber composite back-  
 314    ing making up a half-module. A window is machined  
 315    in the carbon fiber leaving only a frame around the pe-  
 316    riphery of the silicon to minimize material. A  $50 \mu\text{m}$   
 317    sheet of polyamide is laminated to the surface of the  
 318    carbon fiber with 1 mm overhang at all openings to en-  
 319    sure good isolation between the backside of the sensor,  
 320    carrying high-voltage bias, and the carbon fiber which  
 321    is held near ground.

322    The sensor modules for the SVT consist of a pair  
 323    of identical half-modules, sandwiched back-to-back  
 324    around an aluminum cooling block at one end and a sim-  
 325    ilar PEEK spacer block at the other. Figure 6 shows a  
 326    single module after assembly. The cooling block pro-  
 327    vides the primary mechanical support for the module as  
 328    well as cooling via copper tubes pressed into grooves

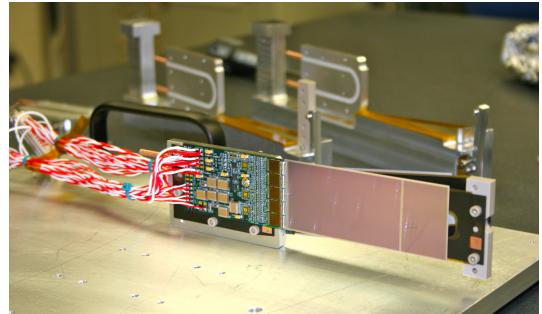


Figure 6: A prototype module assembly (foreground) with the 50 mrad (left) and 100 mrad (right) module assembly fixtures in the background. A pair of cooling blocks and a spacer block can be seen on the fixtures.

in the plates. The spacer block defines the spacing between the sensors at the far end of the module, stiffens the module structure, and improves the stability of the sensor alignment. The average support material in the tracking volume is approximately  $0.06\% X_0$  per double-sided module for a total material budget of 0.7% per layer.

The total SVT power consumption budget of about 50 W is removed by a water/glycol mixture circulated through a flexible manifold attached to the copper tubes in the cooling blocks. During the Test run the sensors where operated at around  $23^\circ\text{C}$ . The power consumption is dominated by five APV25 ASICs on each hybrid board consuming approximately 2 W, radiant heat load is less than 0.5 W per sensor and leakage current is only significant in a small spot after irradiation.

345    **4.3. Production, Assembly and Shipping**

346    Hybrids with APV25 ASICs underwent quick qualifi-  
 347    cation testing and each half-module was run at low tem-  
 348    perature ( $\approx 5^\circ\text{C}$ ) and fully characterized for pedestals,  
 349    gains, noise and time response after assembly. Of 29  
 350    half-modules built, 28 passed qualification testing, leav-  
 351    ing 8 spare modules after completion of the SVT, all ca-  
 352    pable of 1000 V bias voltage without breakdown. Full-  
 353    module assembly and mechanical surveys were per-  
 354    formed at SLAC before final assembly, testing and ship-  
 355    ping of the SVT to JLab. A custom shipping container  
 356    with nested crates and redundant isolation for shock and  
 357    vibration was built in order to safely send the partly as-  
 358    sembled SVT to JLab. At JLab, the entire SVT was  
 359    integrated with the full DAQ and the power supplies be-  
 360    fore moving the module-loaded support plates to Hall B  
 361    for final mechanical assembly and installation inside of  
 362    the vacuum chamber.

363 **4.4. Alignment**

364 The SVT was aligned using a combination of optical,  
 365 laser and touch probe surveys at SLAC and JLab. The  
 366 optical survey of individual modules with precision of  
 367 a few  $\mu\text{m}$  are combined with a touch-probe survey of  
 368 the overall SVT support structure, with 25-100  $\mu\text{m}$  pre-  
 369 cision, to locate the silicon sensor layers with respect  
 370 to the support plates and the mechanical survey balls  
 371 on the base plate. After full assembly and installation  
 372 of the SVT at JLab, a mechanical survey of the SVT  
 373 base plate position inside the pair spectrometer vacuum  
 374 chamber is used to determine the global position of the  
 375 SVT with respect to CEBAF beam line. The resulting  
 376 survey-based alignment has the position of the silicon  
 377 sensors correct to within a few hundred microns mea-  
 378 sured from tracks in the HPS Test Run data. A more  
 379 sophisticated global track-based alignment technique to  
 380 reach final alignment precision well below 50  $\mu\text{m}$  is be-  
 381 ing developed.

382 **5. Electromagnetic Calorimeter**

383 The electromagnetic calorimeter (ECal), installed  
 384 downstream of the PS dipole magnet, performs two es-  
 385 sential functions for the experiment: it provides a trigger  
 386 signal to select what events to read out from the detector  
 387 sub-systems and is used in the analysis to identify elec-  
 388 trons and positrons. The technology and design choices  
 389 are largely driven by the need for a compact forward de-  
 390 sign covering the SVT A' acceptance and able to fully  
 391 absorb electrons and positrons with energy between 0.5-  
 392 6.5 GeV, fine granularity and signal readout speed to  
 393 handle 1 MHz/cm<sup>2</sup> of electromagnetic background and  
 394 be radiation hard. The PbWO<sub>4</sub> crystal inner calorime-  
 395 ter of the CLAS detector [12], in operation since 2005  
 396 in Hall B, meets all the requirements set by HPS. The  
 397 modules from this calorimeter have been subsequently  
 398 repurposed for HPS.

399 **5.1. Components**

400 The ECal module shown in Fig. 7 is based on a  
 401 tapered 160 mm long PbWO<sub>4</sub> crystal with a 13.3  $\times$   
 402 13.3 mm<sup>2</sup> (16  $\times$  16 mm<sup>2</sup>) front (rear) face wrapped in  
 403 VM2000 multilayer polymer mirror film. The scintilla-  
 404 tion light, approximately 3 photoelectrons/MeV, is read-  
 405 out by a 5 $\times$ 5 mm<sup>2</sup> Hamamatsu S8664-55 Avalanche  
 406 Photodiode (APD) with 75% quantum efficiency glued  
 407 to the rear face surface using MeltMount 1.7 thermal  
 408 plastic adhesive. The low gain of APDs ( $\sim 200$ ) was  
 409 compensated with custom made preamplifier boards,  
 410 which provide a factor of 2333 amplification of the APD  
 411 signal.

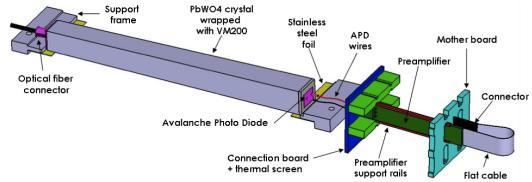


Figure 7: Schematic view of an ECal module.

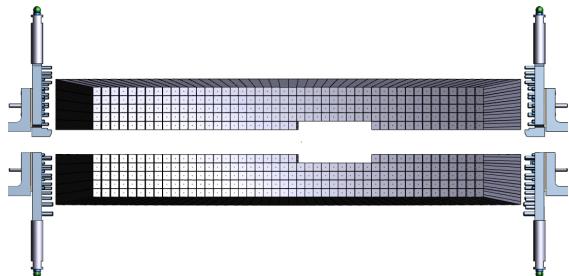


Figure 8: Rendered layout view of the ECal looking downstream.

412 **5.2. Layout**

413 Similar to the SVT, the ECal is built in two separate  
 414 halves that are mirror reflections of one another about  
 415 the plane of the nominal electron beam to avoid inter-  
 416 fering with the 15 mrad "dead zone". As shown in Fig. 8,  
 417 the 221 modules in each half, supported by aluminum  
 418 support frames, are arranged in rectangular formation  
 419 with 5 layers and 46 crystals/layer except for the layer  
 420 closest to the beam where 9 modules were removed to  
 421 allow a larger opening for the outgoing electron and  
 422 photon beams. Each half was enclosed in a tempera-  
 423 ture controlled box (< 1° F stability and < 4° F unifor-  
 424 mity) to stabilize the crystal light yield and the opera-  
 425 tion of the APDs and its preamplifiers. Four printed circuit  
 426 boards mounted on the backplane penetrated the enclo-  
 427 sure and was used to supply the  $\pm 5$  V operating voltage  
 428 for the preamplifiers, 400 V bias voltage to the APDs,  
 429 and to read out signals from the APDs. Each half of  
 430 the ECal was divided into 12 bias voltage groups with a  
 431 gain uniformity of about 20%.

432 During the HPS Test Run, both halves were held in  
 433 place by four vertical bars attached to an above rail,  
 434 placing the front face of the crystals 147 cm from the  
 435 upstream edge of the magnet and with a 8.7 cm gap  
 436 between the innermost edge of the crystals in the two  
 437 halves.

438    5.3. Signal readout

439    After a 2:1 signal splitter, 1/3 of an amplified APD  
 440    signal was fed to a single channel of a JLab flash ADC  
 441    (FADC) board [13]. 2/3 of the signal was sent to a  
 442    discriminator module and then to a TDC for a timing  
 443    measurement. The FADC boards are high speed VXS  
 444    modules digitizing up to 16 APD signals at 250 MHz  
 445    and storing samples in 8  $\mu$ s deep pipelines with 12-bit  
 446    resolution. When a trigger is received, the part of the  
 447    pipeline from 5 samples before and 30 after the sig-  
 448    nals crossed a programmable threshold (for the HPS Test  
 449    Run this was set to  $\approx 70$  MeV) are summed and stored  
 450    in a 17-bit register for readout. In addition a 4 ns res-  
 451    olution timestamp of the threshold crossing is reported  
 452    in the readout for each pulse. This scheme significantly  
 453    compresses the data output of the FADC. During offline  
 454    data analysis, a calibrated pedestal value is subtracted  
 455    to obtain the actual summed energy. Two 20-slot VXS  
 456    crates with 14 (13) FADC boards were employed in the  
 457    HPS Test Run to read out the top (bottom) half of the  
 458    ECal. In the HPS Test Run 385 out of 442 modules  
 459    (87%) were used in offline reconstruction, 39 modules  
 460    were disabled or not read out (no FADC channel avail-  
 461    able, no APD bias voltage or masked out due to exces-  
 462    sive noise) and 18 were masked offline due to noise.

463    6. Trigger and Data Acquisition

464    The DAQ system handles acquisition of data from the  
 465    ECal and SVT sub-detectors with two DAQ architec-  
 466    tures. The SVT DAQ is based on Advanced Telecom  
 467    Communications Architecture (ATCA) hardware while  
 468    the ECal uses VMEbus Switched Serial (VXS) based  
 469    hardware. Data from the sub-detectors are only readout  
 470    when a trigger signal from the trigger system is received  
 471    formed on input from the ECal.

472    6.1. Trigger system

473    The trigger system is designed to select time coinci-  
 474    dences of electromagnetic clusters in the top and bot-  
 475    tom halves of the ECal. Figure 9 shows a schematic  
 476    overview of each stage of the system. Each channel on  
 477    the FADC board has an independent data path to send 5-  
 478    bit pulse energy and 3-bit pulse arrival time information  
 479    every 32 ns to a trigger processing board (CTP), which  
 480    is in the same crate. The 3-bit pulse arrival time allows  
 481    the trigger to know the pulse timing at 4 ns resolution.  
 482    Contrary to the readout path described in Sec. 5.3, this  
 483    energy is a pedestal subtracted time-over-threshold sum  
 484    with programmable offsets and minimum threshold dis-  
 485    criminator for each channel. With input from all FADC

486    channels, i.e. one half of the ECal, the CTP performs  
 487    cluster finding and calculates cluster energy and tim-  
 488    ing information. The 3x3 fixed-window, highly parallel,  
 489    FPGA-based cluster algorithm simultaneously searches  
 490    for up to 125 clusters with energy sum larger than the  
 491    programmable energy threshold ( $\approx 270$  MeV). Crystals  
 492    in the fixed-window are included in the sum if the lead-  
 493    ing edge of the pulse occurred within a 32 ns time win-  
 494    dow to take into account clock skew and jitter through-  
 495    out the system. The CTP only accepts clusters with the  
 496    highest energy 3x3 window locally to deal with over-  
 497    lapping and very large clusters. The sub-system board  
 498    (SSP) receives the clusters from the top and bottom half  
 499    CTP at a maximum of 250MHz and searches for pairs  
 500    of clusters in a 8 ns wide coincidence window. The SSP  
 501    sends triggers to the trigger supervisor (TS), which gen-  
 502    erates all the necessary signals and controls the entire  
 503    DAQ system readout through the trigger interface units  
 504    installed in every crate that participate in the readout  
 505    process.

506    The trigger system is free-running and driven by the  
 507    250 MHz global clock and has essentially zero dead  
 508    time at the occupancies expected for HPS. The trigger  
 509    supervisor can apply dead time if necessary, for exam-  
 510    ple on a ‘busy’ or ‘full’ condition from the front-end  
 511    electronics. The system is designed to handle trigger  
 512    rates above 50 kHz and has a latency set to  $\approx 3$   $\mu$ s to  
 513    match that required by the SVT APV25 ASIC. During  
 514    the HPS Test Run, for the most part the trigger system  
 515    required only a single cluster in either the top or bot-  
 516    tom Ecal halves and was tested to trigger rates above  
 517    100 kHz by lowering thresholds.

518    6.2. SVT Data Acquisition

519    The SVT DAQ is based on the Reconfigurable Clus-  
 520    ter Element (RCE) and cluster interconnect concept de-  
 521    veloped at SLAC as generic building blocks for DAQ  
 522    systems. The RCE is a generic computational build-  
 523    ing block, housed on a separate daughter card called



Figure 9: Block diagram of the ECAL trigger system consisting of the FADC that samples and digitizes signals for each detector channel and sends them for cluster finding in the CTP. The CTP clusters are sent to the SSP where the final trigger decision is taken based on pairs of clusters in both halves of the ECal. The decision is sent to the Trigger Supervisor (TS) that generates the necessary signals to readout the sub-detectors.



Figure 10: The SVT DAQ COB board with four data processing daughter cards (DPMs) visible on the left side.

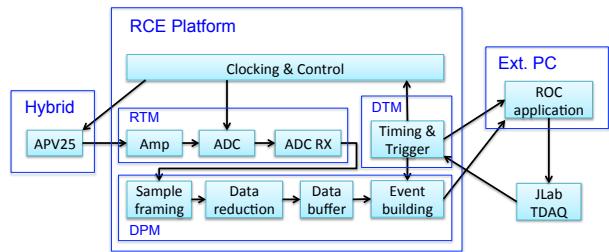


Figure 11: Block diagram overview of the SVT DAQ.

Data Processing Module (DPM), that are realized on an ATCA front board called the Cluster On Board (COB), see Fig. 10. The first generation RCE used in the HPS Test Run consisted of a Virtex 5 FPGA with 1 GB of DDR3 RAM. A schematic overview of the system is shown in Fig. 11. The analog outputs of up to 12 SVT half-modules (60 APV25 ASICs) are digitized on the Rear-Transition-Module (RTM), a custom board on the back side of the ATCA crate, interfacing the HPS-specific readout to the generic DAQ components on the COB. A pre-amplifier converts the APV25 differential current output to a different voltage output scaled to the sensitive range of a 14-bit ADC operating at the system clock of 41.667 MHz. The RTM is organized into four sections with each section supporting three SVT half-module hybrids (15 APV25 ASICs). The RTM also includes a 4-channel fiber optic module and supporting logic which is used to interface to the JLab trigger system supervisor. Each section of the RTM is input to a DPM which apply thresholds for data reduction and organizes the sample data into UDP datagrams. The DPM also hosts an I<sup>2</sup>C controller used to configure and monitor the APV25 ASICs. A single ATCA crate with two COB cards was used, one supporting four DPMs and one supporting 3 DPMs and one DPM that is configured as the trigger and data transmission module. The

two COB cards and their DPMs are interconnected with a 10 Gb/s switch card [14] which also hosts two 1Gb/s Ethernet interfaces to the external SVT DAQ PC.

The external PC supports three network interfaces; two standard 1 Gb/s Ethernet and one custom low latency data reception card. The first is used for slow control and monitoring of the 8 DPM modules and the second serves as the interface to the JLAB data acquisition system. The third custom low latency network interface is used to receive data from the ATCA crate and supports a low latency, reliable TTL trigger acknowledge interface to the trigger DPM. This PC hosts the SVT control and monitoring software as well as the Read Out Controller application used to interface with the JLab DAQ.

In order to minimize cable length for the analog APV25 output signal the ATCA crate was located approximately 1 m from the beam line, next to our cable vacuum feed-troughs. Before shielding with lead-blankets was arranged, we observed two failures of normally reliable ATCA crate power supplies, time-correlated to beam instabilities.

While trigger rates during the HPS Test Run was significantly lower this system was tested at trigger rates up to 20 kHz and 50 MB/s.

### 6.3. General Data Acquisition and Online Computing

Every crate participating in the readout process contains a Readout Controller (ROC) that collects digitized information, processes it, and sends it on to the event builder. For the ECal, both VXS crates run ROC applications in a single blade Intel-based CPU module running CentOS Linux OS. For the SVT DAQ, the ROC application runs on the external PC under RHEL. The event builder assembles information from the ROCs into a single event which is passed to the event recorder that writes it to a RAID5-based data storage system capable of handling up to 100 MB/s. The event builder and other critical components run on multicore Intel-based multi-CPU servers. The DAQ network system is a network router providing 10 Gb/s high-speed connection to the JLab computing facility for long-term storage. For the HPS Test Run, both the SVT and ECal ROC had a 1 Gb/s link to the network router.

## 7. Reconstruction and Performance

### 7.1. SVT Performance

For the duration of the HPS Test Run all SVT modules and APV25 chips were configured to their nominal operating points [15] with all sensors reverse-biased at

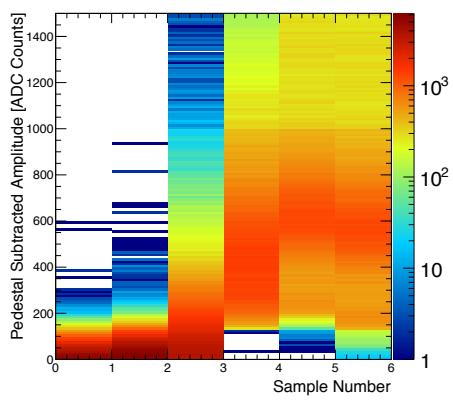


Figure 12: Accumulation of six pedestal-subtracted samples from individual SVT channels associated with hits on tracks.

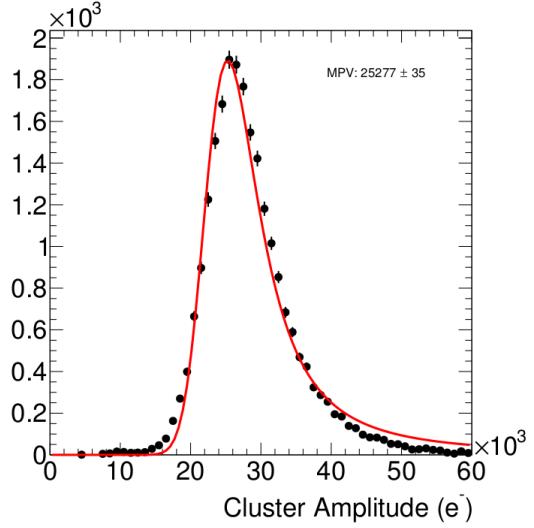


Figure 13: The cluster charge distribution for hits associated with track follow the characteristic Landau shape.

598 180 V. The sensors were operated within a temperature  
 599 range of 20 – 24°C. Approximately 97% of the 12,780  
 600 SVT channels were found to be operating normally; the  
 601 fraction of dead or noisy channels varied from 2.4%  
 602 to 4.7% throughout the HPS Test Run. Most of these  
 603 losses were due to 2-4 misconfigured APV25 ASICs, a  
 604 known noisy half-module and problems in two particu-  
 605 lar APV25 ASICs.

#### 606 7.1.1. Cluster and Hit Reconstruction

607 After a trigger is received, the amplitude of every  
 608 APV25 analogue output is sampled and digitized in  
 609 six consecutive time bins, separated by roughly 25 ns.  
 610 The typical, pedestal subtracted, pulse shape obtained  
 611 is shown in Fig. 12. As the figure demonstrates, the  
 612 SVT was well timed-in to the trigger with the rise of the  
 613 pulse at the 3rd sampling point. In order to find the time,  
 614  $t_0$ , and amplitude of each hit, the six samples from each  
 615 channel are fitted to an ideal  $CR - RC$  function. Note that  
 616 in the HPS Test Run the APV25 ASICs were operating  
 617 with a 50 ns shaping time. These hits are passed through  
 618 a simple clustering algorithm which forms clusters by  
 619 grouping adjacent strips with the position of a cluster on  
 620 the sensor determined by the amplitude-weighted mean.  
 621 With a linear gain up to  $\approx 3$  MIPs, the cluster charge  
 622 for hits associated with a track follow the characteristic  
 623 Landau shape. A noise level between  $1.1 - 1.5 \times 10^3$   
 624 electrons was established through multiple calibration  
 625 runs giving a signal to noise ratio of 21 – 25. Lab-  
 626 based radioactive source tests was used to provide the  
 627 absolute charge normalization. After clustering hits on  
 628 a sensor, the hit time for each cluster is computed as  
 629 the amplitude-weighted average of the individually fit-

630 ted  $t_0$  on each channel. The  $t_0$  resolution is studied by  
 631 comparing the cluster hit time with the average of all  
 632 cluster hit times on the track shown in Fig. 14. After  
 633 correcting for offsets from each sensor (time-of-flight  
 634 and clock phase) and accounting for the correlation be-  
 635 tween the  $t_0$  and track time, the extracted  $t_0$  resolution is  
 636 2.6 ns. This is somewhat worse than the approximately  
 637 2 ns resolution expected for S/N 25 which we attribute  
 638 to the true pulse shape differing from our idealized fit  
 639 function which will be improved in the future. Reduc-  
 640 ing the APV25 ASIC pulse shaping time to 35 ns will  
 641 also improve time resolution. These results show that  
 642 we can operate with the six sample readout mode of the  
 643 APV25 chip and achieve time resolution adequate for  
 644 pileup rejection during electron running in HPS.

645 Good agreement between observed and simulated oc-  
 646 cupancies after taking into account dead or noisy chan-  
 647 nels. The hit reconstruction efficiency was estimated by  
 648 measuring the number of good tracks with a hit close to  
 649 the extrapolated intersection of a given sensor that was  
 650 excluded from the track fit itself. Tracks which inter-  
 651 sect regions with known bad channels or very close to  
 652 in the edge region are excluded. The hit reconstruction  
 653 efficiency, see Fig. 15, was measured to be above 98%  
 654 and fairly uniform across the SVT.

655 The spatial resolution of similar microstrip sensors is  
 656 well established by test beam data, against which the  
 657 charge deposition model in the simulation is validated.  
 658 This resolution can be parameterized as a function of the  
 659 total signal to single-strip noise and the crossing angle

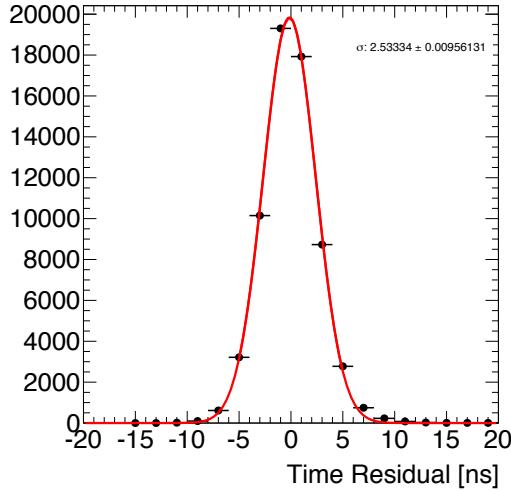


Figure 14: The residual of individual cluster times with the average of all clusters on the track.

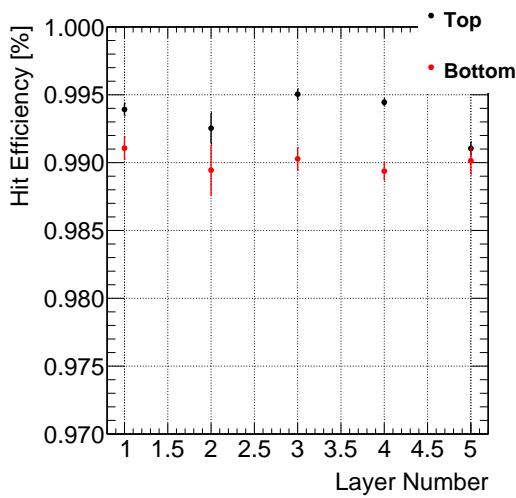


Figure 15: The hit reconstruction efficiency as a function of detector layer.

of tracks through the sensor. The single-hit resolution for charged particles with signal to noise ratio above 20, as demonstrated here, is relatively constant at approximately 6  $\mu\text{m}$  for tracks that enter approximately normal to the sensors as in HPS.

### 7.1.2. Momentum and Vertexing Resolution

By selecting  $e^+e^-$  pairs from the triggered events we are able to study basic distributions of pair production kinematics. Pairs of oppositely charged tracks, one in the top and one in the bottom half of the SVT, with momentum larger than 400 MeV were selected. The pair production kinematics are relatively well reproduced as shown in Fig. 16.

The expected momentum resolution from simulation is between 4-5% for tracks in the momentum range of the HPS Test Run. By comparing the shapes of the kinematic distributions for single- and two track events between data and simulation we estimate an agreement with the nominal scale and resolution to within 10%.

In the HPS Test Run, as well as in electron running with HPS, the dominant source of uncertainty in the tracking and vertexing is multiple Coulomb scattering. For the vertexing performance the foremost difference compared to electron beam running is that the target was located approximately 67 cm upstream from our nominal target position; giving almost collinear tracks in the detector. The increased lever arm over which tracks are extrapolated widens the resolution with up to a factor of eight (depending on momentum) compared to what is achieved at the nominal electron target position for HPS. Figure 17 shows the horizontal and vertical positions of the extrapolated track at the converter position. While residual alignment show small shifts, the good agreement between data and simulated events of the widths indicates a good understanding of the material budget and distribution in the SVT. Having the dominant contribution to the vertex resolution approximately right demonstrates that the resolution in HPS, with a target at 10 cm, will be as calculated.

### 7.2. ECal Performance

The integrated pulse of each FADC channel was converted to energy by subtracting a pedestal and applying a conversion factor to convert ADC counts to energy. The pedestals are measured using special runs where each trigger records 100 samples of signals from the APDs with 4 ns between each sample. The pedestals were extracted from the part of the window before the

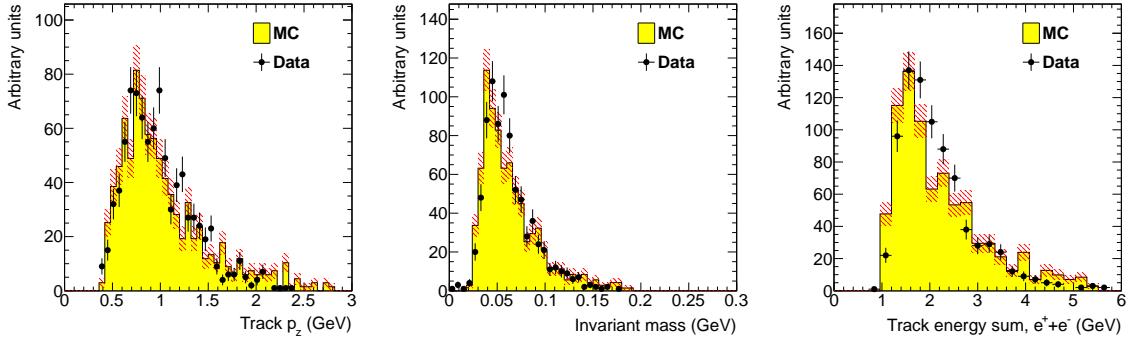


Figure 16: Kinematic distributions for  $e^+e^-$  pairs selected by opposite charged tracks in the top and bottom half of the tracker: track momentum in the top half of the SVT (left), invariant mass (middle) and the sum of the track momentum for the pair (right).

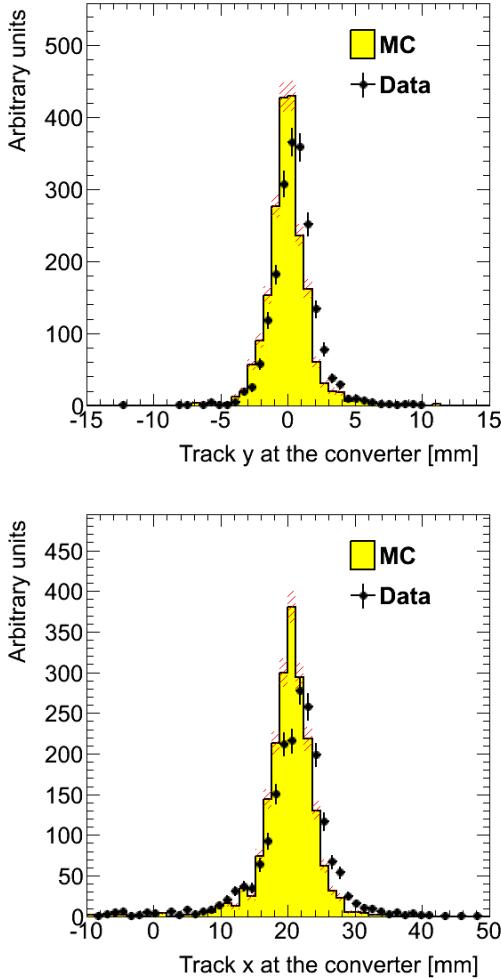


Figure 17: Vertical (top) and horizontal (bottom) extrapolated track position at the converter taking into account the measured fringe field.

708 actual hit in the calorimeter. Modules with signal above  
 709 the threshold are clustered using a simple algorithm  
 710 similar to the one deployed for the trigger (see Sec. 6.1).  
 711 Due to the high effective readout threshold of 73 MeV  
 712 the average number of crystals in a cluster was  $\sim 3$  and  
 713 the simple clustering algorithm worked well for recon-  
 714 struction of the detected shower energy. An average  
 715 noise level of approximately 15 MeV was measured in  
 716 special pedestal runs.

717 The ratio of the ECal cluster energy  $E$  to the momen-  
 718 tum  $p$  of a matched track in the SVT was used to de-  
 719 termine the conversion factors from ADC counts to en-  
 720 ergy. To compare data and simulation, all inoperable or  
 721 noisy channels in the SVT and ECal were disabled in  
 722 both data and simulation so that any efficiency or bias  
 723 that affect the data should be reflected in the simulation.  
 724 Iteratively, conversion coefficients for each crystal were  
 725 adjusted until the  $E/p$  ratio in data and simulation were  
 726 similar. The distribution of the  $E/p$  ratio in data and  
 727 simulation are compared in Fig. 18. The peak position  
 728 of the distribution indicates the sampling fraction  
 729 of the ECal, the fraction of the incident particle energy  
 730 measured in the cluster. The width and tails of the distri-  
 731 bution in data indicates imperfect calibration and noise  
 732 of the ECal modules. This level of calibration and the  
 733 agreement with simulation was found to be sufficient to  
 734 study normalized event rates in the HPS Test Run.

### 735 7.3. Trigger Performance

736 As described above in Sec. 6, the energy from each  
 737 crystal is measured differently in the trigger and what  
 738 is readout from the ECal. The trigger performance  
 739 was studied by simulating the trigger for each event  
 740 and comparing to how the events were actually trig-  
 741 gered. To eliminate trigger bias, we use a tag and probe  
 742 method: to study the trigger performance in one half

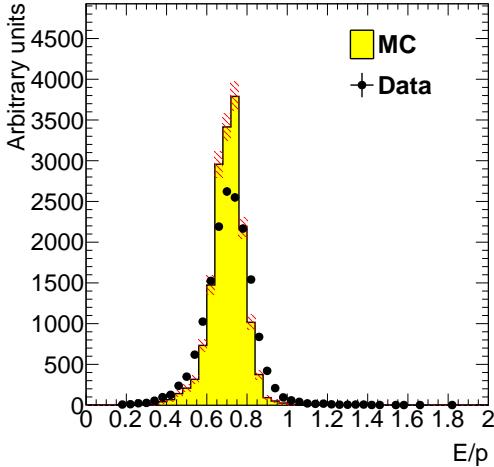


Figure 18: The ECal energy over track momentum ratio ( $E/p$ ) comparing data and simulation for single cluster triggers in the top half of the ECal.

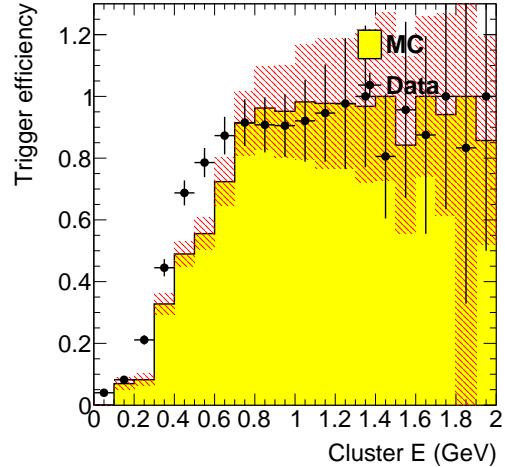


Figure 19: Trigger efficiency in both halves of the ECal for data and simulation as a function of cluster energy.

Converter (% $X_0$ )	<b>1.60</b>	<b>0.45</b>	<b>0.18</b>
EGS5	$1162 \pm 112$	$255 \pm 28$	$94 \pm 17$
GEANT4	$2633 \pm 250$	$371 \pm 38$	$114 \pm 18$
Observed	$1064 \pm 2$	$196 \pm 1$	$92 \pm 1$

Table 4: Observed and predicted event rate (in Hz) normalized to 90 nA for three different converter thicknesses. The uncertainty on the prediction includes systematic uncertainties from ECal alignment, background normalization, beam current normalization and limited statistics in the simulation.

of the ECal, we select events which triggered the other half and where there was exactly one probe cluster in the ECal half under study. We then measure trigger efficiency as the fraction of tagged events that fired the trigger in the probe half as a function of the probe cluster energy, shown in Fig. 19. The trigger turn-on is slow and reaches an uneven plateau just below 1 GeV for two reasons; gain variations between different crystals lead to the threshold variations and the nonlinearity of the time-over-threshold integral means that the effective threshold is higher for clusters that span multiple crystals. The effective trigger threshold is therefore dependent on position and energy of the particle as well as cluster multiplicity.

As a cross-check we simulate the FADC trigger path by converting from readout hits (with fixed-size window integration) to trigger hits (time-over-threshold integration). The CTP clustering algorithm and the trigger decision from the SSP is simulated before we compare the trigger decision and trigger time to what was reported by the actual trigger. For every event, the trigger reports the trigger decision as a bit mask (top half, bottom half or both) and the time the trigger fired. The turn-on from the trigger threshold was measured to be 1280 in units of ADC counts as expected. The threshold was not perfectly sharp because of uncertainties in the conversion from readout to trigger hits described above, but based on comparisons with simulation we found that the trigger worked exactly as specified.

#### 7.4. Trigger Rate Comparisons

Trigger rates observed in the HPS Test Run are dominated by multiple Coulomb scattered  $e^+e^-$  pairs in the converter. In simulated events, the rate of triggers depend on the modeling of the pairs angular distribution and the subsequent multiple Coulomb scattering in the converter. Rates from different converter thicknesses are used to study the varying multiple Coulomb scattering contribution (pair production angle is constant). Restricting clusters to a well calibrated region of the ECal and subtracting the "no converter" background we see agreement with the rates predicted by the EGS5 simulation program, see Tab. 7.4. This gives further confidence that the dominant source of background occupancy for HPS, multiple Coulomb scattered beam electrons, is well described [16, 17, 18].

## 8. Summary and Outlook

The HPS Test Run experiment, using a simplified version of the apparatus planned for the full HPS ex-

periment in a parasitic photon beam, demonstrated the feasibility of the detector technologies proposed for the silicon vertex tracker, electromagnetic calorimeter, and data acquisition systems. Performance from each of these subsystems has been shown to be adequate to conduct the full experiment successfully. Studies of multiple Coulomb scattering tails of electrons and positrons from photon conversions further backs expectations from simulation, giving credence to estimates of the detector backgrounds expected in electron beam running for HPS.

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