

# Stress singularities of some common kernel transformed viscoelastic models

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## Abstract

The kernel conformation tensor is a powerful generic transformation for a large class of differential constitutive models. We derive its stress singularity associated with the stretching solution of the viscoelastic extra-stress tensor. This is relevant to re-entrant corner flows in contraction/expansion flows and the separation of a free-surface from a solid surface at the die lip in extrudate swell. The theoretical asymptotic results are compared to the numerical scheme results for the two common particular kernel conformation cases of natural logarithm and square-root. These results are presented for the viscoelastic models in which the asymptotic stress-tensor singularity is currently known.

*Keywords:*

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sec:1

## 1. Introduction

We will be concerned here with deriving the stress singularities of the kernel-conformation tensor for the common viscoelastic models of UCM, Oldroyd-B [4, 11], simplified PTT [5, 2, 12] and Giesekus [9] relevant to steady planar contraction/expansion and extrudate swell flows. In these situations, the local asymptotic behaviour of the viscoelastic extra-stress has been determined to take the generic form

$$\mathbf{T} \sim \lambda(\psi)\mathbf{u}\mathbf{u}^T \quad \text{as } r \rightarrow 0, \quad (1) \quad \text{eq:T}$$

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where  $r$  denotes the radial distance to the singularity,  $\psi$  is the planar streamfunction,  $\mathbf{u}$  the velocity field and the scalar function  $\lambda$  is constant along streamlines. Near to the above mentioned singularities, the velocity and stress is self-similar, taking separable forms

$$\psi = C_0 r^m f(\theta), \quad \lambda(\psi) = C_1 \left( \frac{\psi}{C_0} \right)^n, \quad (2)$$

where the amplitudes  $C_0, C_1$  and exponents  $m, n$  are all constant. These give the estimates

$$\mathbf{T} = O(\lambda |\mathbf{u}|^2) = O(r^{m(n+2)-2}), \quad \nabla \mathbf{v} = O(r^{m-2}) \quad \text{as } r \rightarrow 0. \quad (3)$$

Results for the re-entrant corner [10, 13, 6, 7] and extrudate-swell [**<empty citation>**] are summarised in Table 1. The angle of flow is  $\pi/\alpha$  in both cases, where  $\alpha \in (1/2, 1)$  for re-entrant corners and  $\alpha \in (2/3, 1)$  for extrudate-swell. These implicitly assume an absence no of vortices at the boundaries, such as lip vortices.

In the re-entrant corner case, UCM and Oldroyd-B take the same potential flow solutions. The elastic stress dominates the solvent stress for all corner angles greater than  $180^\circ$ . Thus the effect of adding a solvent viscosity to UCM does not change the nature of the singularity. However, this is not the same for sPTT and Giesekus, where currently results are known only when a solvent viscosity is present.

The transcendental equations to determine the  $\lambda_0$  eigenvalue are

$$\sin \left( \frac{\lambda_0 \pi}{\alpha} \right) = -\lambda_0 \sin \left( \frac{\pi}{\alpha} \right) \quad (4) \quad \boxed{\text{eq:terc}}$$

for the re-entrant corner and

$$\sin \left( \frac{2\lambda_0 \pi}{\alpha} \right) = \lambda_0 \sin \left( \frac{2\pi}{\alpha} \right) \quad (5) \quad \boxed{\text{eq:tees}}$$

for extrudate-swell.

The dimensionless model equations we are considering are

$$\begin{aligned} \nabla \cdot \mathbf{u} &= 0, & \text{Re} \frac{D\mathbf{u}}{Dt} &= -\nabla p + \beta \nabla^2 \mathbf{u} + (1 - \beta) \nabla \cdot \mathbf{T}, \\ \mathbf{T} + \text{Wi} \left( \overset{\nabla}{\mathbf{T}} + \mathbf{g}(\mathbf{T}) \right) &= 2\mathbf{D}, & \mathbf{g}(\mathbf{T}) &= \begin{cases} \mathbf{0}, & \text{UCM/Oldroyd-B,} \\ \epsilon \text{tr}(\mathbf{T}) \mathbf{T}, & \text{PTT,} \\ \hat{\alpha} \mathbf{T}^2, & \text{Giesekus,} \end{cases} \end{aligned} \quad (6) \quad \boxed{\text{GovEq}}$$

with pressure  $p$ ,  $D/Dt$  denoting the material or substantive derivative and the upper convective stress derivative in the elastic constitutive equation. The usual dimensionless parameters are the Reynolds number  $\text{Re} = \rho U L / \eta_0$ , Weissenberg number  $\text{Wi} = \lambda_p U / L$ , solvent viscosity fraction  $\beta = \eta_s / \eta_0$  and model parameters  $\epsilon$  in PTT and  $\hat{\alpha}$  in Giesekus. Here,  $U$  and  $L$  are characteristic velocity and length scales,  $\eta_s$  is the solvent viscosity,  $\eta_p$  the polymer viscosity,

Model	$\psi$ m	$\lambda(\psi)$ n	$\mathbf{T}$ p=m(n+2)-2	$\mathbf{D}$ q=m-2	p
UCM/Oldroyd-B	$\alpha(3 - \alpha)$	$-\frac{2(1-\alpha)}{(3-\alpha)}$	$-2(1 - \alpha)$	$-(1 - \alpha)(2 - \alpha)$	
sPTT (with solvent)	$1 + \lambda_0$	$-\frac{2(2+\lambda_0)}{(5+\lambda_0)}$	$-\frac{4((1-\lambda_0))}{(5+\lambda_0)}$	$-(1 - \lambda_0)$	
Giesekus (with solvent)	$1 + \lambda_0$	$-\frac{(3+\lambda_0)}{4}$	$-\frac{(1-\lambda_0)(3-\lambda_0)}{4}$	$-(1 - \lambda_0)$	

Table 1: Summary by model of singularity exponents for re-entrant corners of angle  $\pi/\alpha$  with  $1/2 < \alpha < 1$ . The benchmark case of  $270^\circ$  is  $\alpha = 2/3$ . For sPTT and Giesekus,  $\lambda_0$  is the smallest positive root of the transcendental equation (4). The sPTT and Giesekus results also hold for extrudate-swell, where  $\pi/\alpha$  now represents the angle of separation with  $1/3 < \alpha < 1$  and  $\lambda_0$  is the smallest positive root of (5).

Table1

$\eta_0 = \eta_s + \eta_p$  the total viscosity and  $\rho$  the density. The dimensional pressure, solvent and elastic stresses have been scaled with  $\eta_0 U/L$ ,  $\eta_s U/L$  and  $\eta_p U/L$  respectively.

The Weissenberg number is usually scaled from the local singularity problems and set to unity. The results in Table 1 hold not only for Weissenberg order one, but large as well. As regards the Reynolds number, the results hold generally for order one values, although the main application is the creeping flow regime with Reynolds number small.

sec:2

## 2. Kernel-conformation singular behaviour

We begin by remarking that the dyadic product  $\mathbf{u}\mathbf{u}^T$  has eigenvalues 1 and 0 with associated eigenvectors in the directions parallel and perpendicular to  $\mathbf{u}$  respectively. This affords the diagonalisation

$$\mathbf{u}\mathbf{u}^T = \mathbf{O} \begin{pmatrix} |\mathbf{u}|^2 & 0 \\ 0 & 0 \end{pmatrix} \mathbf{O}^T \quad (7)$$

with

$$\mathbf{O} = \frac{1}{|\mathbf{u}|} \begin{bmatrix} u & -v \\ v & u \end{bmatrix}, \quad (8)$$

being composed of the unitary eigenvectors, the one in the velocity direction we denote by  $\hat{\mathbf{u}} = \mathbf{u}/|\mathbf{u}|$ . As long as the velocity does not vanish, then  $\mathbf{O}$  is proper orthogonal.

For stabilisation reasons, numerical simulations are performed with the kernel-conformation tensor [1], which can be any continuous, invertible and differentiable matrix transformation function  $\mathbb{k}(\mathbf{A})$  of the conformation tensor  $\mathbf{A}$ . The extra-stress tensor is related by

$$\mathbf{A} = \text{Wi}\mathbf{T} + \mathbf{I}, \quad (9)$$

and we take  $Wi = 1$  without loss of generality. Consequently, the form (1) becomes

$$\mathbf{A} = \mathbf{O} \begin{pmatrix} \lambda|\mathbf{u}|^2 + 1 & 0 \\ 0 & 1 \end{pmatrix} \mathbf{O}^T, \quad (10)$$

and for the kernel-conformation

$$\mathbb{k}(\mathbf{A}) = \mathbf{O} \begin{pmatrix} \mathbb{k}(1 + \lambda|\mathbf{u}|^2) & 0 \\ 0 & \mathbb{k}(1) \end{pmatrix} \mathbf{O}^T. \quad (11)$$

Near singularities  $\lambda|\mathbf{u}|^2$  grows unboundedly and hence we have the asymptotic behaviour

$$\mathbb{k}(\mathbf{A}) \sim \mathbb{k}(\lambda|\mathbf{u}|^2) \mathbf{O} \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} \mathbf{O}^T = \mathbb{k}(\lambda|\mathbf{u}|^2) \hat{\mathbf{u}}\hat{\mathbf{u}}^T \quad \text{as } r \rightarrow 0. \quad (12)$$

Consequently

$$\mathbb{k}(\mathbf{A}) = O(\mathbb{k}(r^p)) \quad \text{as } r \rightarrow 0, \quad (13)$$

eq:kA

where  $p = m(n + 2) - 2$  is negative. The common transformations for  $\mathbb{k}$  of natural logarithm [8] and square-root [3] have the effect of significantly reducing the singularity of  $\mathbb{k}(\mathbf{A})$  compared to  $\mathbf{A}$ . This gives an additional computational benefit to the kernel transformed conformation formulation.

sec:3

### 3. Numerical verification

Here we verify (13) with exponent  $p$  in Table 1 for the natural log and square-root transformations.

#### 3.1. Re-entrant corner

We take the standard benchmark case of  $270^\circ$ , so that  $\alpha = 2/3$  with corner angle  $\pi/\alpha = 3\pi/2$ . Table 2 summarises the theoretical singular radial behaviours for UCM/Oldroyd-B, sPTT and Giesekus. The sPTT and Giesekus results require the presence of a solvent viscosity and hold for  $0 < \beta < 1$ , with any non-zero value of the extensibility parameter  $\epsilon$  for sPTT or non-zero value of the mobility parameter  $\hat{\alpha}$  (and bounded by unity) for Giesekus.

Figure 1 shows the results for the three models in the parameter case  $\beta = 0.5$  and  $\epsilon = \hat{\alpha} = 0.1$ . These are plotted along the ray  $\theta = \pi/2$ , where  $\theta = 0$  is the upstream wall and  $\theta = 3\pi/2$  is the downstream wall.

#### 3.2. Extrudate-swell

The separation angle has to be estimated as the tangent angle of the free-surface. This will vary with model,  $\beta$ ,  $Wi$  and model parameter  $\epsilon$  or  $\hat{\alpha}$ .

sPTT:  $Wi=1$ ,  $\epsilon=0.1$ ,  $\beta = 0.5$ :  $\lambda_0 \approx 0.440$  (from estimated separation angle),  $p=-0.412$

Giesekus:  $Wi=1$ ,  $\hat{\alpha} = 0.1$ ,  $\beta = 0.5$ :  $\lambda_0 \approx 0.442$  (from estimated separation angle),  $p=-0.357$

Model	$\mathbf{A}$	$\ln \mathbf{A}$	$\mathbf{A}^{\frac{1}{2}}$
UCM/Oldroyd-B	$r^{-\frac{2}{3}}$	$-\frac{2}{3} \ln r$	$r^{-\frac{1}{3}}$
sPTT (with solvent)	$r^{-0.3286}$	$-0.3286 \ln r$	$r^{-0.1643}$
Giesekus (with solvent)	$r^{-0.2796}$	$-0.2796 \ln r$	$r^{-0.1398}$

Table 2: Summary by model of singularity exponents for re-entrant corners of angle  $\pi/\alpha$  with  $1/2 < \alpha < 1$ . For sPTT and Giesekus,  $\lambda_0$  is the smallest positive root of the transcendental equation (4).

Table2

Model	$\mathbf{A}$	$\ln \mathbf{A}$	$\mathbf{A}^{\frac{1}{2}}$		
sPTT (with solvent)	$r^{-0.3286}$	$-0.3286 \ln r$	$r^{-0.1643}$		
Giesekus (with solvent)	$r^{-0.2796}$	$-0.2796 \ln r$	$r^{-0.1398}$		

Table 3

Table3

#### 4. Discussion

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#### References

- fonso2011 [1] A.M. Afonso, F.T. Pinho, and M.A. Alves. “The kernel-conformation constitutive laws”. In: *Journal of Non-Newtonian Fluid Mechanics* Not available (Oct. 2011), Not available. ISSN: 0377-0257. DOI: 10.1016/j.jnnfm.2011.09.008. URL: <https://dx.doi.org/10.1016/j.jnnfm.2011.09.008>.
- Alves2003 [2] Manuel A. Alves, Paulo J. Oliveira, and Fernando T. Pinho. “Benchmark solutions for the flow of Oldroyd-B and PTT fluids in planar contractions”. In: *Journal of Non-Newtonian Fluid Mechanics* 110 (Feb. 2003), pp. 45–75. ISSN: 0377-0257. DOI: 10.1016/s0377-0257(02)00191-x. URL: [https://dx.doi.org/10.1016/s0377-0257\(02\)00191-x](https://dx.doi.org/10.1016/s0377-0257(02)00191-x).

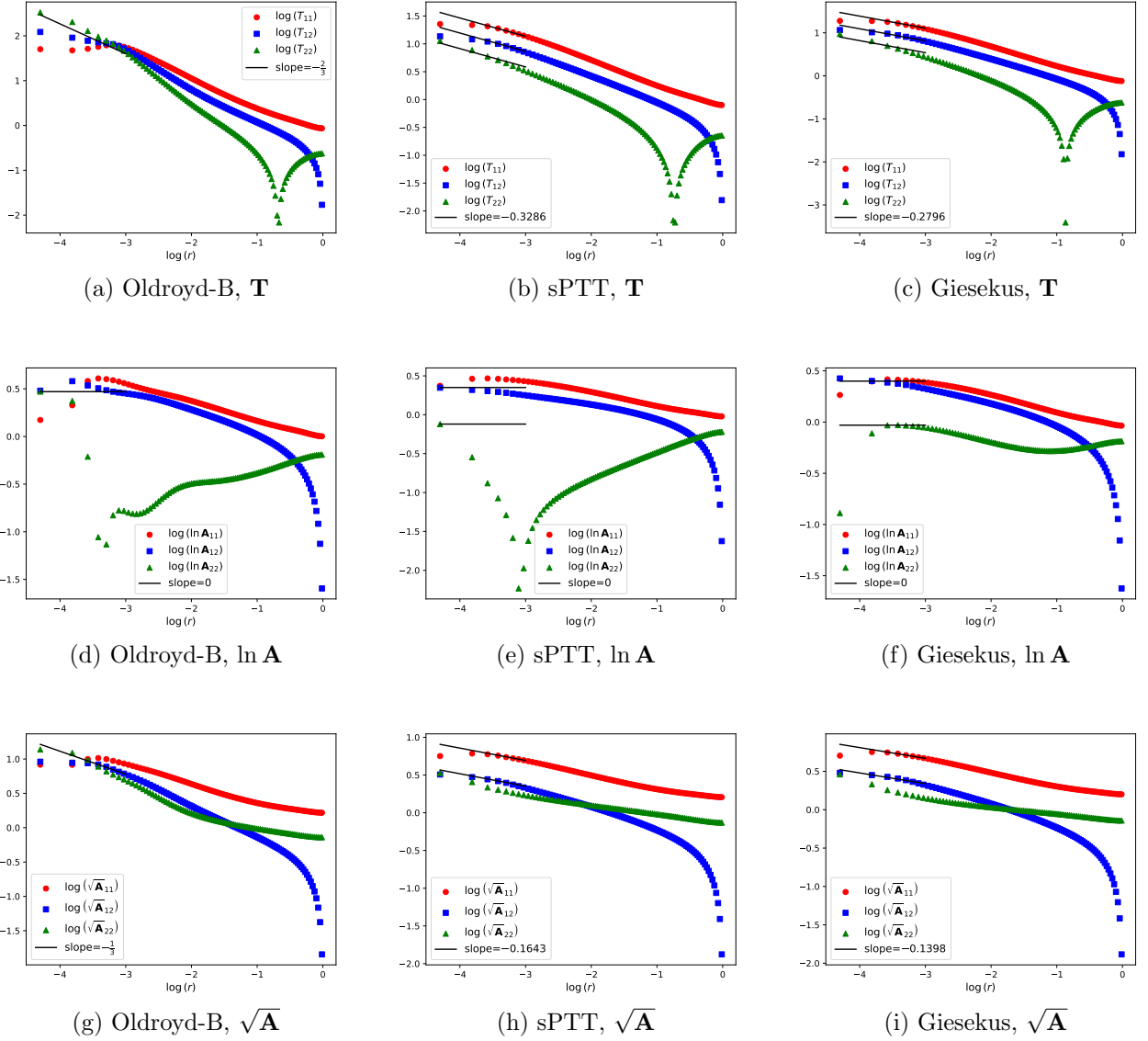


Figure 1: Numerical verification of the asymptotic results for the 4:1 contraction flow along  $\theta = \frac{\pi}{2}$ .

- [3] Nusret Balci et al. “Symmetric factorization of the conformation tensor in viscoelastic fluid models”. In: *Journal of Non-Newtonian Fluid Mechanics* 166 (June 2011), pp. 546–553. ISSN: 0377-0257. DOI: 10.1016/j.jnnfm.2011.02.008. URL: <https://dx.doi.org/10.1016/j.jnnfm.2011.02.008>.
- [4] R. B. Bird, R. C. Armstrong, and O. Hassager. *Dynamics of polymeric liquids. Vol.1, Fluid mechanics*. 2nd ed. New York, 1987.
- [5] Mahdi Davoodi, Konstantinos Zografos, and Robert J. Poole. “On the similarities of the sPTT and FENE-P models for polymeric fluids”. In: *Science Talks* 2 (June 2022), p. 100015. ISSN: 2772-5693. DOI: 10.1016/j.sctalk.2022.100015. URL: <https://dx.doi.org/10.1016/j.sctalk.2022.100015>.

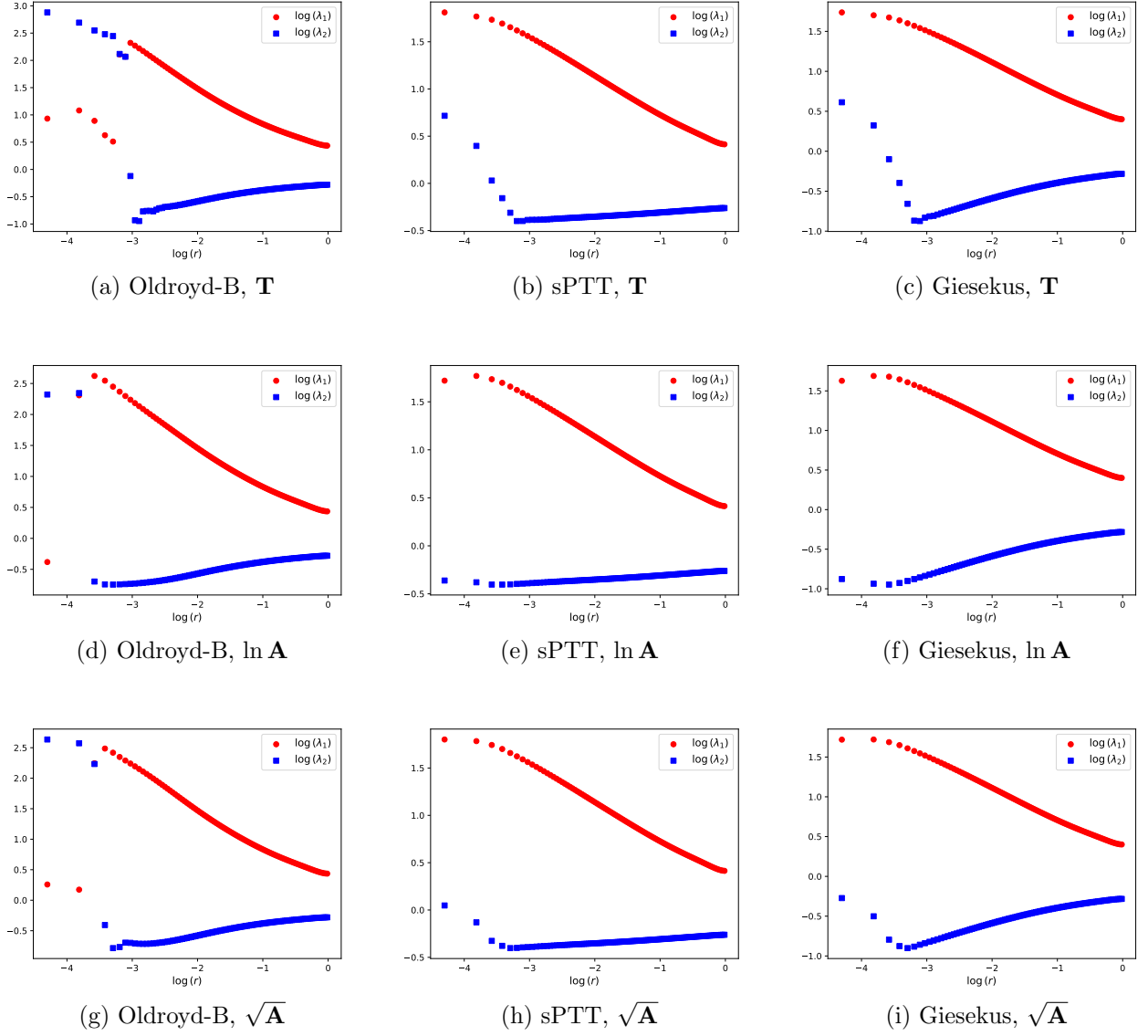


Figure 2: Numerical verification of the asymptotic results for the 4:1 contraction flow along  $\theta = \frac{\pi}{2}$ .

contraction

Evans2005

- [6] J. D. Evans. “Re-entrant corner flows of the upper convected Maxwell fluid”. In: *Proc. R. Soc. A* 461 (2053 Jan. 2005), pp. 117–142. DOI: 10.1098/rspa.2004.1335.

Evans2005b

- [7] J.D Evans. “Re-entrant corner flows of Oldroyd-B fluids”. In: *Proceedings of the Royal Society A: Mathematical, Physical and Engineering Sciences* 461 (June 2005), pp. 2573–2603. ISSN: 1364-5021, 1471-2946. DOI: 10.1098/rspa.2004.1410. URL: <https://dx.doi.org/10.1098/rspa.2004.1410>.

Fattal2004

- [8] Raanan Fattal and Raz Kupferman. “Constitutive laws for the matrix-logarithm of the conformation tensor”. In: *Journal of Non-Newtonian Fluid Mechanics* 123 (Nov. 2004), pp. 281–285. ISSN: 0377-0257. DOI: 10.1016/j.jnnfm.2004.08.008. URL: <https://dx.doi.org/10.1016/j.jnnfm.2004.08.008>.

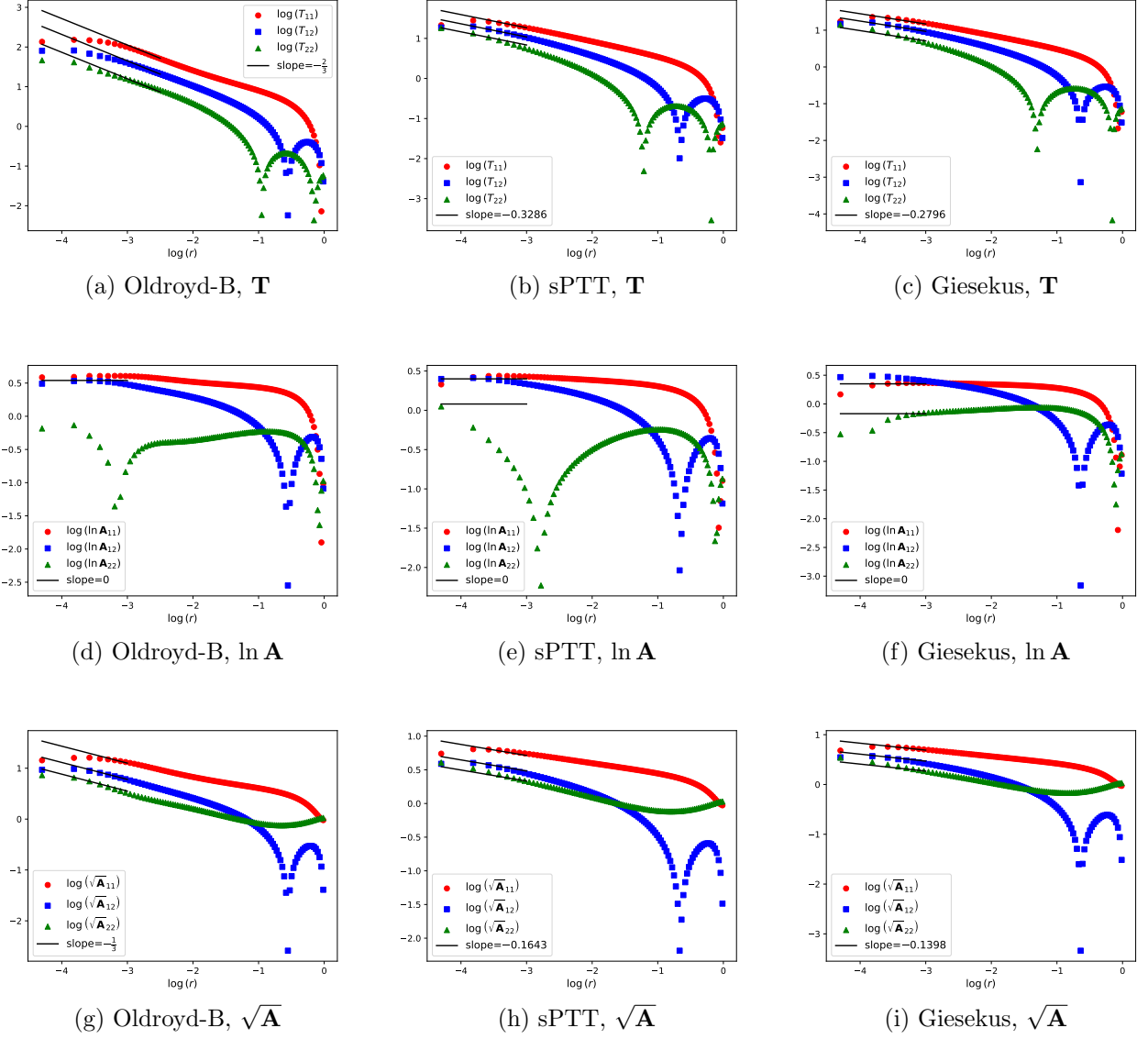


Figure 3: Numerical verification of the asymptotic results for the 1:4 expansion flow along  $\theta = \frac{\pi}{2}$ .

Expansion

Giesekus1982

- [9] H. Giesekus. “A simple constitutive equation for polymer fluids based on the concept of deformation-dependent tensorial mobility”. In: *Journal of Non-Newtonian Fluid Mechanics* 11 (Jan. 1982), pp. 69–109. ISSN: 0377-0257. DOI: 10.1016/0377-0257(82)85016-7. URL: [https://dx.doi.org/10.1016/0377-0257\(82\)85016-7](https://dx.doi.org/10.1016/0377-0257(82)85016-7).

Hinch1993

- [10] E.J. Hinch. “The flow of an Oldroyd fluid around a sharp corner”. In: *Journal of Non-Newtonian Fluid Mechanics* 50 (2 Dec. 1993), pp. 161–171. ISSN: 0377-0257. DOI: 10.1016/0377-0257(93)80029-b. URL: [https://dx.doi.org/10.1016/0377-0257\(93\)80029-b](https://dx.doi.org/10.1016/0377-0257(93)80029-b).

Larson1988

- [11] R. G. Larson. *Constitutive Equations for Polymer Melts and Solutions*. Oct. 1988. ISBN: 9780409901191.



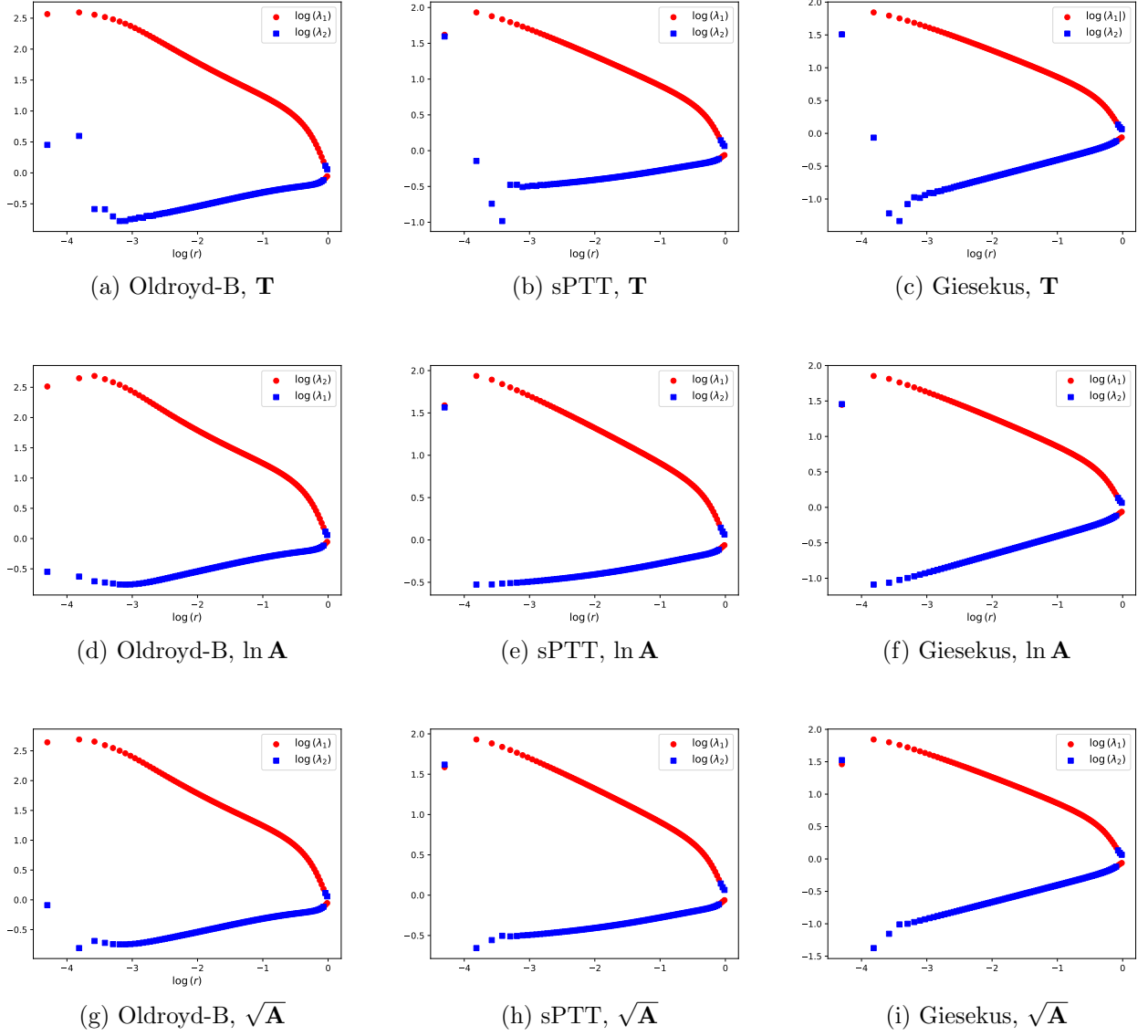


Figure 4: Numerical verification of the asymptotic results for the 1:4 expansion flow along  $\theta = \frac{\pi}{2}$ .

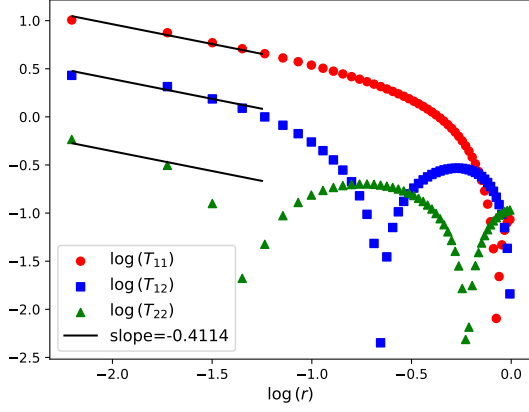
Expansion

Thien1977

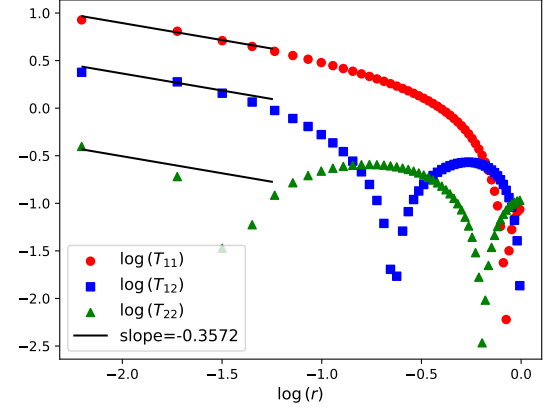
- [12] N. Phan-Thien and R. I. Tanner. “A new constitutive equation derived from network theory”. In: *Journal of Non-Newtonian Fluid Mechanics* 2.4 (1977), pp. 353–365. ISSN: 0377-0257. DOI: [https://doi.org/10.1016/0377-0257\(77\)80021-9](https://doi.org/10.1016/0377-0257(77)80021-9). URL: <https://www.sciencedirect.com/science/article/pii/0377025777800219>.

renardy1995

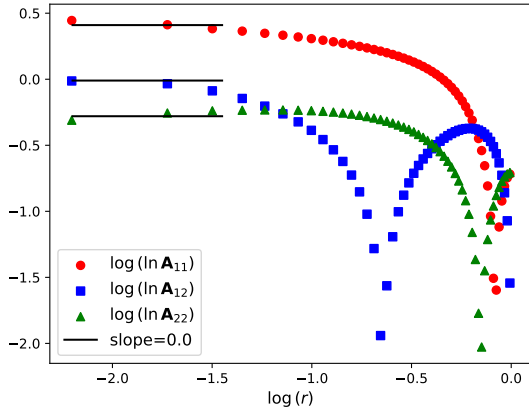
- [13] Michael Renardy. “A matched solution for corner flow of the upper convected Maxwell fluid”. In: *J. Non-Newton. Fluid Mech.* 58 (1 1995), pp. 83–89. ISSN: 0377-0257. DOI: [https://doi.org/10.1016/0377-0257\(94\)01339-J](https://doi.org/10.1016/0377-0257(94)01339-J).



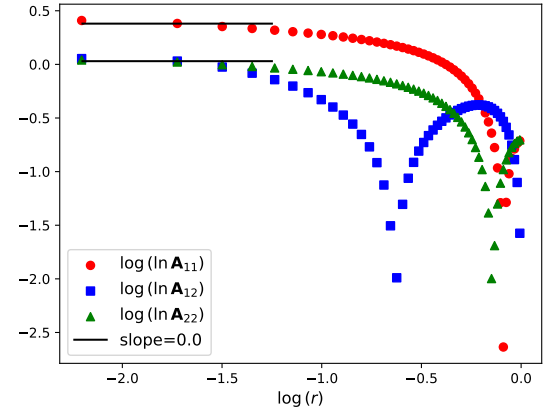
(a) sPTT,  $\mathbf{T}$



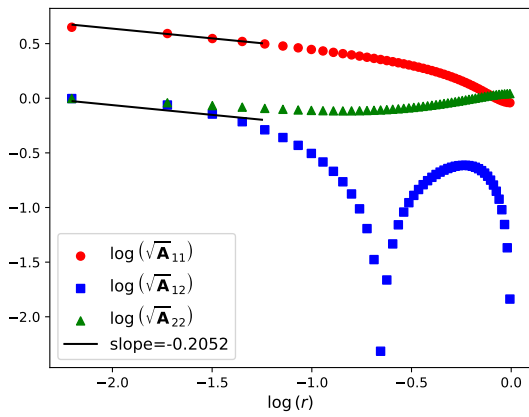
(b) Giesekus,  $\mathbf{T}$



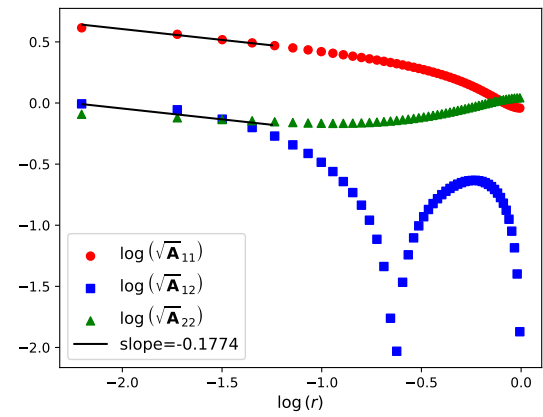
(c) sPTT,  $\ln \mathbf{A}$



(d) Giesekus,  $\ln \mathbf{A}$

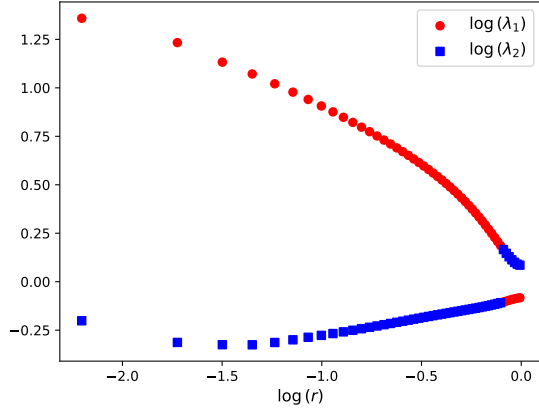


(e) sPTT,  $\sqrt{\mathbf{A}}$

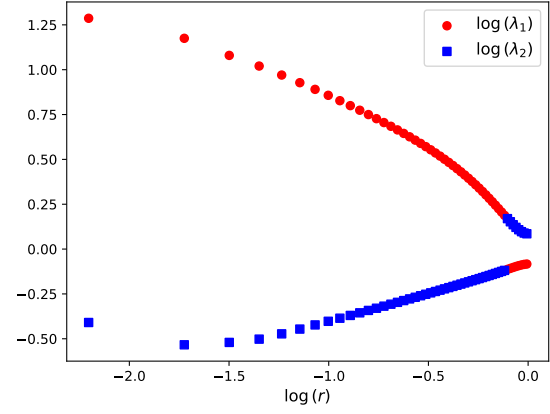


(f) Giesekus,  $\sqrt{\mathbf{A}}$

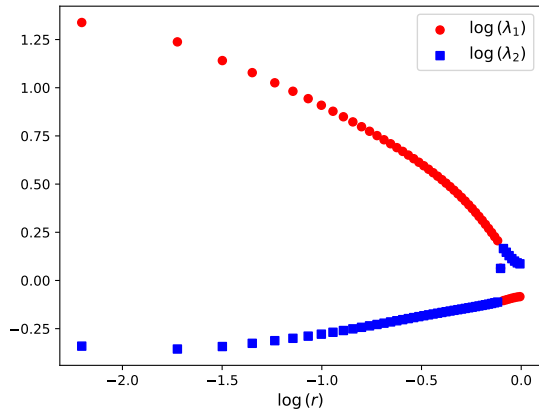
Figure 5: Numerical verification of the asymptotic results for the extrudate flow along  $\theta = \frac{\pi}{2}$ .



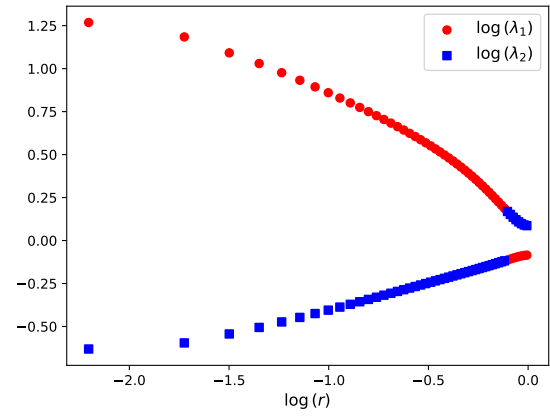
(a) sPTT,  $\mathbf{T}$



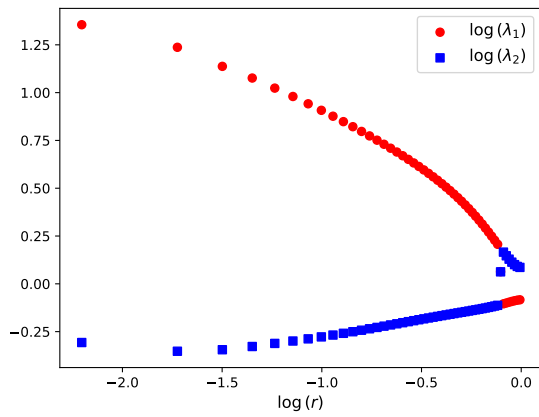
(b) Giesekus,  $\mathbf{T}$



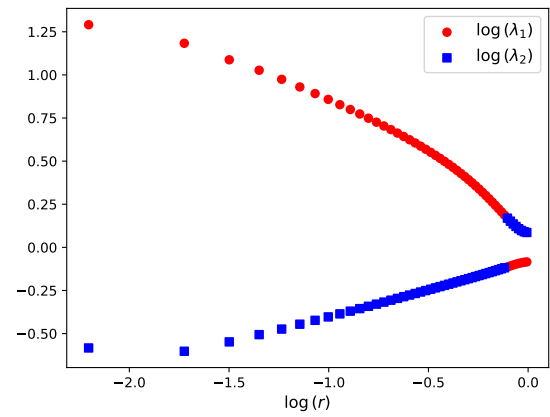
(c) sPTT,  $\ln \mathbf{A}$



(d) Giesekus,  $\ln \mathbf{A}$



(e) sPTT,  $\sqrt{\mathbf{A}}$



(f) Giesekus,  $\sqrt{\mathbf{A}}$

Figure 6: Numerical verification of the asymptotic results for the extrudate flow along  $\theta = \frac{\pi}{2}$ .