

# Comparison of discrete fiber and asymptotic homogenization methods for modeling of fiber-reinforced materials deformations

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Multiscale and high-performance computing for multiphysical problems 2019

June 24 - 25

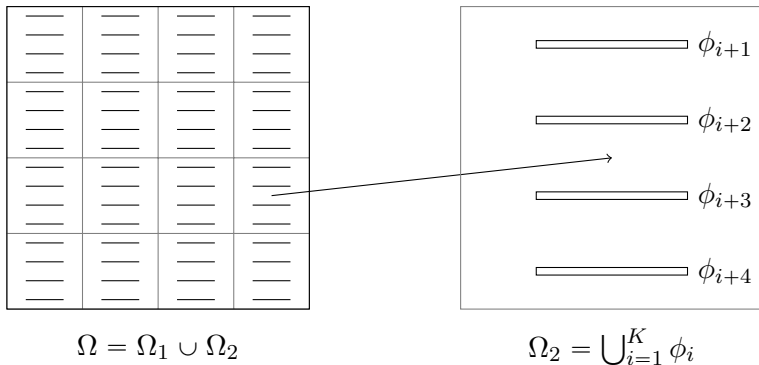
# Content

- 1 Introduction
- 2 Model problem
- 3 Approximations
- 4 Numerical simulations
- 5 Conclusion

# Introduction

- Fiber-reinforced materials are recommended as most of the strongest composite materials
- Numerical modeling of fiber-reinforced materials leads to huge grid size due to fiber size and count
- Discrete fiber method (discerte fracture method): one dimensional fibers
- Asymptotic homogenization method: averaged coarse problem

# Model problem



- $\Omega_1$  is the main material
- $\Omega_2$  is the fibers

# Stress-strain state

$$\nabla \cdot \boldsymbol{\sigma} = \boldsymbol{f}, \quad \boldsymbol{x} \in \Omega,$$

- $\boldsymbol{\sigma} = \boldsymbol{C}\boldsymbol{\varepsilon}$  is the stress tensor
- $\boldsymbol{C}$  is the elastic tensor
- $\boldsymbol{\varepsilon}$  is the strain tensor
- $\boldsymbol{f}$  is the force source

# Voigt notation

## Stress and elastic tensors

$$\boldsymbol{\sigma} = \begin{pmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{pmatrix}, \quad \boldsymbol{C} = \begin{pmatrix} C_{1111} & C_{1122} & C_{1112} \\ C_{2211} & C_{2222} & C_{2212} \\ C_{1211} & C_{1222} & C_{1212} \end{pmatrix}$$

## Strain tensor

$$\boldsymbol{\varepsilon} = \begin{pmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{pmatrix} = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} \\ \frac{\partial u_2}{\partial x_2} \\ \frac{\partial u_2}{\partial x_1} + \frac{\partial u_1}{\partial x_2} \end{pmatrix}.$$

# Lame parameters

Isotropic materials elastic tensor

$$\mathbf{C}_i = \begin{pmatrix} \lambda_i + 2\mu_i & \lambda_i & 0 \\ \lambda_i & \lambda_i + 2\mu_i & 0 \\ 0 & 0 & \mu_i \end{pmatrix}, \quad \mathbf{x} \in \Omega_i, \quad i = 1, 2.$$

$$\lambda_i = \frac{E_i \nu_i}{(1 + \nu_i)(1 - 2\nu_i)}, \quad \mu_i = \frac{E_i}{2(1 + \nu_i)}, \quad \mathbf{x} \in \Omega_i, \quad i = 1, 2.$$

- $E_i$  is the Young modulus
- $\nu_i$  is the Poisson coefficient

# Boundary conditions



Dirichlet condition on the left border

$$\mathbf{u} = (0, 0), \quad \mathbf{x} \in \Gamma_L.$$

Neumann condition on the right border

$$\boldsymbol{\sigma}_n = \mathbf{g}, \quad \mathbf{x} \in \Gamma_R.$$

$\boldsymbol{\sigma}_n = \boldsymbol{\sigma} \mathbf{n}$  and  $\mathbf{n}$  is the normal vector to the border



# Finite element approximation

Bilinear form

$$a(\mathbf{u}, \mathbf{v}) = \int_{\Omega_1} \mathbf{C}_1 \boldsymbol{\varepsilon}(\mathbf{u}) : \boldsymbol{\varepsilon}(\mathbf{v}) \, d\mathbf{x} + \int_{\Omega_2} \mathbf{C}_2 \boldsymbol{\varepsilon}(\mathbf{u}) : \boldsymbol{\varepsilon}(\mathbf{v}) \, d\mathbf{x},$$

Linear form

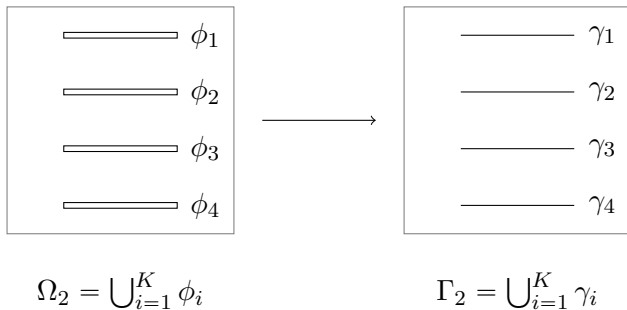
$$L(\mathbf{v}) = \int_{\Omega} \mathbf{f} \mathbf{v} \, d\mathbf{x} + \int_{\Gamma_R} \mathbf{g} \mathbf{v} \, d\mathbf{s},$$

Trial and test function spaces

$$V = \hat{V} = \{\mathbf{v} \in H^1(\Omega) : \mathbf{v} = (0, 0), \mathbf{x} \in \Gamma_L\},$$

$H^1$  is the Sobolev function space

# Discrete fiber approximation



## Discrete fiber approximation (2D)

Bilinear form

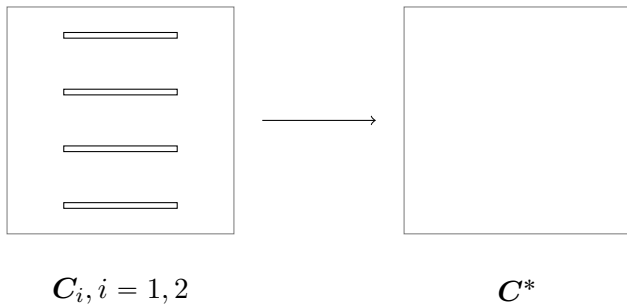
$$a(\mathbf{u}, \mathbf{v}) = \int_{\Omega} \mathbf{C}_1 \boldsymbol{\varepsilon}(\mathbf{u}) : \boldsymbol{\varepsilon}(\mathbf{v}) \, d\mathbf{x} + \int_{\Gamma_2} d (\lambda_2 + 2\mu_2 - \lambda_1 - 2\mu_1) (\nabla \mathbf{u}_{\boldsymbol{\tau}} \boldsymbol{\tau}) (\nabla \mathbf{v}_{\boldsymbol{\tau}} \boldsymbol{\tau}) \, ds,$$

Linear form

$$L(\mathbf{v}) = \int_{\Omega} \mathbf{f} \mathbf{v} \, d\mathbf{x} + \int_{\Gamma_R} \mathbf{g} \mathbf{v} \, d\mathbf{x},$$

- $d$  is thickness of fibers
- $\mathbf{u}_{\boldsymbol{\tau}} = \mathbf{u} \boldsymbol{\tau}$  and  $\boldsymbol{\tau}$  is the tangent vector to a fiber line
- Function spaces same as in FEM

# Asymptotic homogenization approximation



$C^*$  is the effective elastic tensor

# Asymptotic homogenization approximation

Average of the stress tensor

$$\langle \boldsymbol{\sigma} \rangle = \langle \mathbf{C} \boldsymbol{\varepsilon} \rangle = \mathbf{C}^* \langle \boldsymbol{\varepsilon} \rangle,$$

Average

$$\langle \psi \rangle = \frac{\int_{\omega} \psi \, d\mathbf{x}}{\int_{\omega} d\mathbf{x}},$$

$\omega$  is a periodic domain.

## Periodic problems

$\mathbf{u}^k$  is the solution with  $\mathbf{f}^k, k = 1, 2, 3$

- $\mathbf{f}^1 = -\nabla \cdot \mathbf{C} \boldsymbol{\varepsilon}((x_1, 0)),$
- $\mathbf{f}^2 = -\nabla \cdot \mathbf{C} \boldsymbol{\varepsilon}((0, x_2)),$
- $\mathbf{f}^3 = -\nabla \cdot \mathbf{C} \boldsymbol{\varepsilon}((x_2/2, x_1/2)).$

The effective elastic tensor

- $C_{ij11}^* = \langle \sigma_{ij}^1 \rangle, \quad ij = 11, 22, 12,$
- $C_{ij22}^* = \langle \sigma_{ij}^2 \rangle, \quad ij = 11, 22, 12,$
- $C_{ij12}^* = \langle \sigma_{ij}^3 \rangle, \quad ij = 11, 22, 12.$

$$\boldsymbol{\sigma}^k = \mathbf{C} \boldsymbol{\varepsilon}(\mathbf{u}^k), \quad k = 1, 2, 3$$

# Coarse problem

Bilinear form

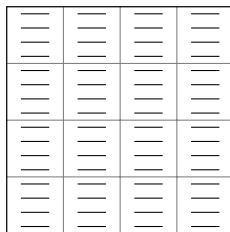
$$a(\mathbf{u}, \mathbf{v}) = \int_{\Omega} \mathbf{C}^* \boldsymbol{\varepsilon}(\mathbf{u}) : \boldsymbol{\varepsilon}(\mathbf{v}) \, \mathrm{d}\mathbf{x}$$

Linear form

$$L(\mathbf{v}) = \int_{\Omega} \mathbf{f} \mathbf{v} \, \mathrm{d}\mathbf{x} + \int_{\Gamma_R} \mathbf{g} \mathbf{v} \, \mathrm{d}\mathbf{s}.$$

We don't compute a higher order solution of the asymptotic homogenization method

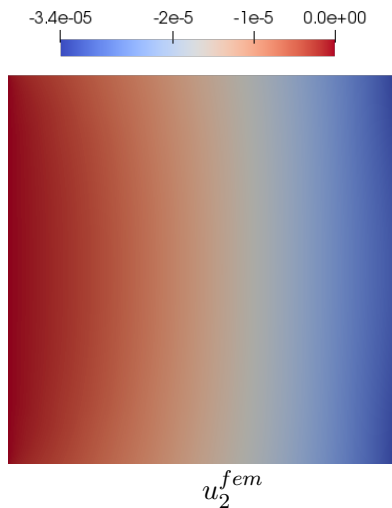
# Numerical simulations



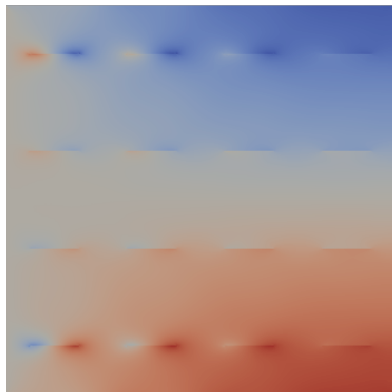
- $\Omega$  contains  $n \times n$  equal subdomains  $\omega$  ( $n = 4$ )
- Each  $\omega$  contains uniformly distributed  $k = K/n^2$  fibers ( $k = 4$ )
- Fibers size  $l \times d$ , where  $l = 1/2n$ ,  $d$  is the thickness ( $l = 1/8$ )
- $d$  thickness correlates with grid size
- $\mathbf{g} = (0, -10^{-5})$



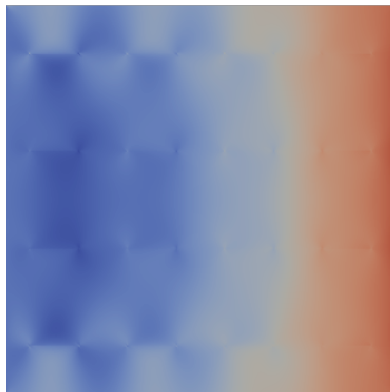
# FEM solution



## DFM error

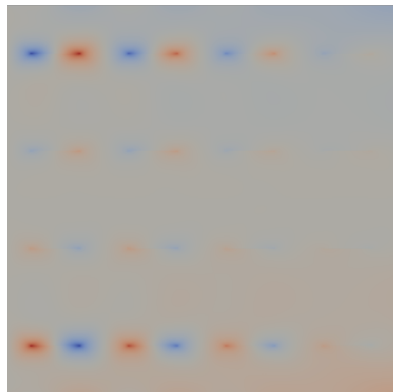


$$u_1^{dfm} - u_1^{fem}$$

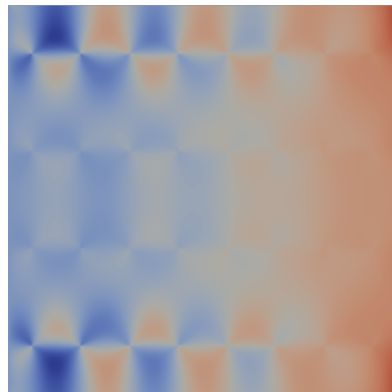
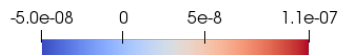


$$u_2^{dfm} - u_2^{fem}$$

## AHM error



$$u_1^{ahm} - u_1^{fem}$$



$$u_2^{ahm} - u_2^{fem}$$

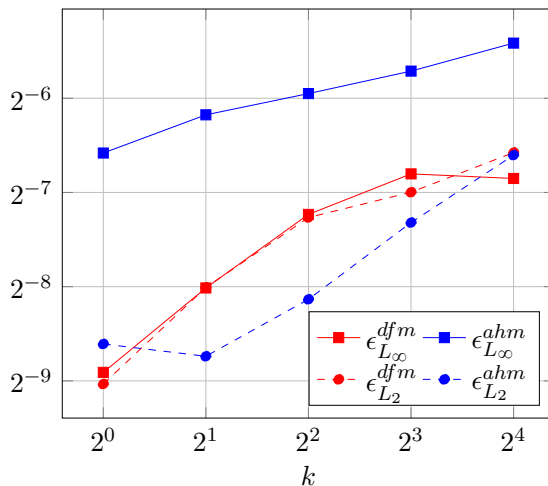
# Relative errors

## DFM relative error

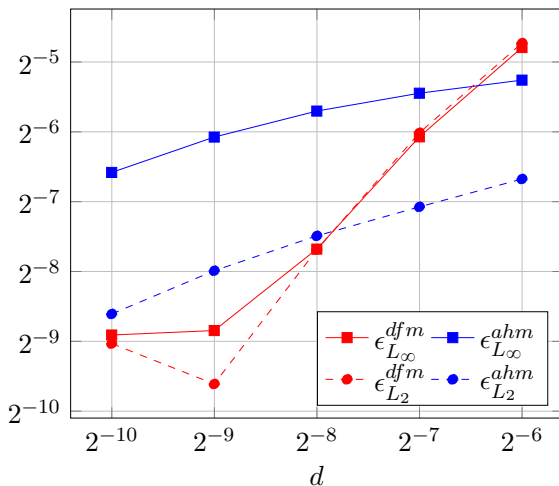
$$\epsilon_{L_\infty}^{dfm} = \frac{\|\mathbf{u}^{dfm} - \mathbf{u}^{fem}\|_{L_\infty}}{\|\mathbf{u}^{fem}\|_{L_\infty}}, \quad \epsilon_{L_2}^{dfm} = \frac{\|\mathbf{u}^{dfm} - \mathbf{u}^{fem}\|_{L_2}}{\|\mathbf{u}^{fem}\|_{L_2}},$$

## AHM relative error

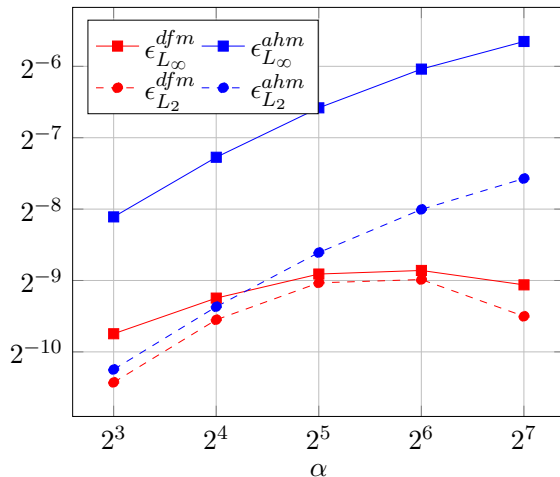
$$\epsilon_{L_\infty}^{ahm} = \frac{\|\mathbf{u}^{ahm} - \mathbf{u}^{fem}\|_{L_\infty}}{\|\mathbf{u}^{fem}\|_{L_\infty}}, \quad \epsilon_{L_2}^{ahm} = \frac{\|\mathbf{u}^{ahm} - \mathbf{u}^{fem}\|_{L_2}}{\|\mathbf{u}^{fem}\|_{L_2}},$$

Number of fibers in  $\omega$ 

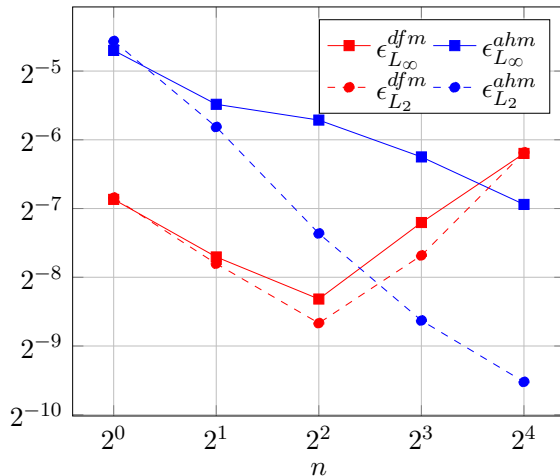
## Thickness of fibers



# Ratio of Young modulus

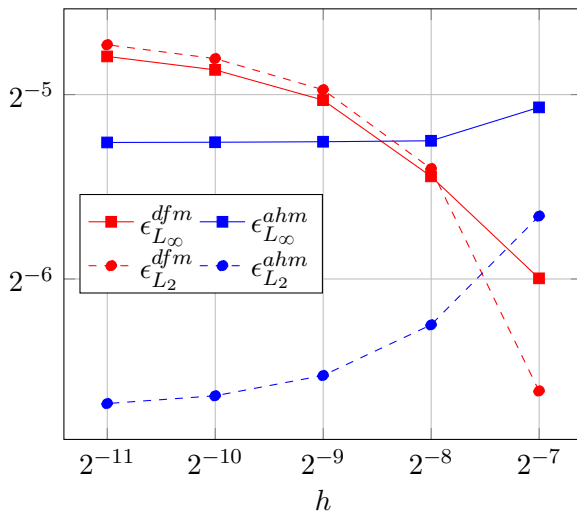


# Number of subdomains in one direction





Grid step ( $d = 1/64, l = 1/8$ )



# Conclusion

- DFM comparing to AHM showed better accuracy for a large ratio of Young modulus
- DFM is more convenient for thick fibers
- AHM solution is better for a large number of equal subdomains
- Using DFM we can solve on more coarse meshes

# Thank you

Thank you for your attention!