

## # Final 4312 F24

### # Q3

$$C_c = 15.5e-12$$

$$R_c = 0$$

$$C_L = 35e-12$$

$$C_1 = 0.9e-12$$

### ## DC Bias Point

$$I_1 = 100e-6$$

$$I_3 = I_1$$

$$I_5 = 6 * 50e-6 \Rightarrow 0.0003$$

$$g_{moverIn} = 10$$

$$g_{moverIp} = 8$$

$$\lambda_{bdn} = 1 / (70e3 * I_1)$$

$$\lambda_{bdp} = 1 / (70e3 * I_3)$$

$$C_{gs5} = 10 * 90 * 1e-15 \Rightarrow 9e-13$$

$$g_{m1} = 10 * I_1 \Rightarrow 0.001$$

$$g_{o2} = \lambda_{bdn} * I_1$$

$$1/g_{o2} \Rightarrow 70,000$$

$$g_{o4} = \lambda_{bdp} * I_3$$

$$1/g_{o4} \Rightarrow 70,000$$

$$g_{m5} = g_{moverIp} * I_5 \Rightarrow 0.0024$$

$$g_{o5} = \lambda_{bdp} * I_5$$

$$1/g_{o5} \Rightarrow 23,333.3333$$

$g_{o6} = \lambda_{mbd} \cdot I_5$   
 $1/g_{o6} \Rightarrow 23,333.3333$

## ## Open Loop Small-Signal Analysis

### ### DC Gain

$A_1 = g_{m1} / (g_{o2} + g_{o4}) \Rightarrow 35$   
 $A_2 = g_{m5} / (g_{o5} + g_{o6}) \Rightarrow 28$   
 $ADC = A_1 \cdot A_2 \Rightarrow 980$   
 $20 \cdot \log_{10}(ADC) \Rightarrow 59.8245$

### ### Poles

- Current Mirror

$g_{m3} = 800e-6$   
 $C_{gs3} = 0.3e-12$   
 $f_{cm} = 1/2/\pi \cdot g_{m3}/2/C_{gs3} \Rightarrow 212,206,590.7892$

- Dominant, unity-gain, non-dominant

$f_1 = 1/2/\pi \cdot (g_{o2} + g_{o4}) / (C_{gs5} + (1 + A_2) \cdot C_c) =$   
 $f_{1a} = 1/2/\pi \cdot (g_{o2} + g_{o4}) / ((1 + A_2) \cdot C_c) \Rightarrow 10,1$

$f_u = ADC \cdot f_1 \Rightarrow 9,894,179.4107$   
 $f_{ua} = 1/2/\pi \cdot g_{m1} / C_c \Rightarrow 10,268,060.8446$

$f_2 = 1/2/\pi \cdot g_{m5} / (C_L + C_{gs5} + C_L \cdot C_{gs5} / C_c) \Rightarrow 10$   
 $f_{2a} = 1/2/\pi \cdot g_{m5} / (C_L + C_{gs5}) \Rightarrow 10,639,884$   
 $f_{2b} = 1/2/\pi \cdot g_{m5} \cdot C_c / (C_c + C_{gs5}) / C_L \Rightarrow 10,314$

$f_z = 1/2/\pi \cdot g_{m5} / C_c \Rightarrow 24,643,346.0271$

## ## Loop Gain

$$\beta = 200 / (200 + 200) \Rightarrow 0.5$$

$$TDC = \beta * ADC \Rightarrow 490$$

$$f_uT = f_{ua} * \beta \Rightarrow 5,134,030.4223$$

$$P_{lag2} = \text{atan}(f_uT/f_2) \text{ in degrees} \Rightarrow 27.0144 \text{ deg}$$

$$P_{lagz} = \text{atan}(f_uT/f_z) \text{ in degrees} \Rightarrow 11.7683 \text{ deg}$$

$$PM = 90 \text{ degrees} - P_{lag2} - P_{lagz} \Rightarrow 51.2173 \text{ deg}$$

- using an Rc and LHP zero

$$R_c = 2/gm_5 \Rightarrow 833.3333$$

$$f_{LHPz} = 1/2\pi / (R_c - 1/gm_5) / C_c \Rightarrow 24,643,346.027$$

$$P_{leadLHPz} = \text{atan}(f_uT/f_{LHPz}) \text{ in degrees} \Rightarrow 11.7$$

$$PM = 90 \text{ degrees} - P_{lag2} + P_{leadLHPz} \Rightarrow 74.7539$$

- putting LHP zero on second pole

$$R_c = 1/2\pi / C_c / f_2 + 1/gm_5 \Rightarrow 1,436.351$$

$$f_{LHPz} = 1/2\pi / (R_c - 1/gm_5) / C_c \Rightarrow 10,069,842.474$$

$$P_{leadLHPz} = \text{atan}(f_uT/f_{LHPz}) \text{ in degrees} \Rightarrow 27.0$$

$$PM = 90 \text{ degrees} - P_{lag2} + P_{leadLHPz} \Rightarrow 90 \text{ degr}$$

## ## Step response

- step

$$R_F = 200e3$$

$$I_{in} = 2.5e-6$$

$$V_{out} = -R_F * I_{in} \Rightarrow -0.5$$

## ## Dominant-Pole Compensation

$\text{atan}(1/3)$  in degrees  $\Rightarrow$  18.4349 degrees

ratio = 3

$f2\_DP = 1/2/\pi * (go5 + go6) / CL \Rightarrow$  389,767.2

$fuT\_DP = f2\_DP/ratio \Rightarrow$  129,922.4025

$f1\_DP = fuT\_DP/beta/ADC \Rightarrow$  265.1478

$CG = (go2+go4)/(2*\pi*f1\_DP) \Rightarrow$  1.715e-8

$f1\_DP\_check = 1/2/\pi * (go4 + go2) / (CG + Cgs$

$fuT\_DP\_check = beta * ADC * f1\_DP\_check \Rightarrow$  129

$Plag\_DP = \text{atan}(fuT\_DP\_check/f2\_DP)$  in degrees

$PM\_DP = 90 \text{ degrees} - Plag\_DP \Rightarrow$  71.566 degrees