

Formal synthesis through set computation

With an application to adaptive cruise control

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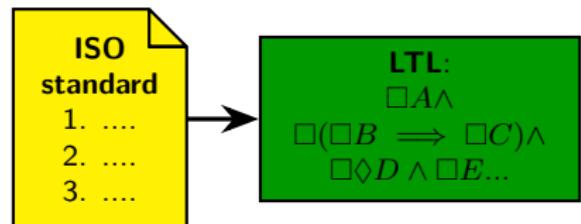
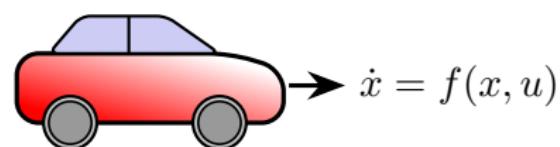
EECS Control Seminar, University of Michigan

December 11, 2015

Correct-by-construction: How to pose the problem?

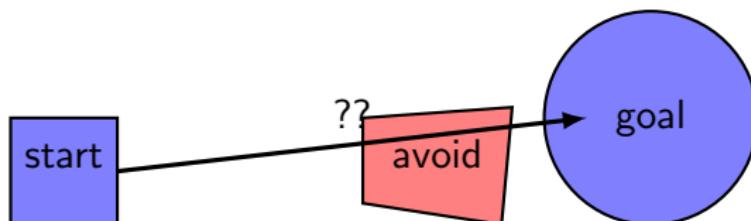
- Engineering: **system** and **textual specifications**
- Math: **system model** (e.g., controlled ODE's) and **formal specification** (e.g. in LTL)

We know that modeling can be difficult, and the same is true for specification “translation”



Correct-by-construction: How to solve the problem?

- Need guarantees on transient behavior (far from steady state)
- Reachability problem is undecidable in general
- Typically have to settle for conservative results



Outline

- 1 Introduction
- 2 Formal specifications and reachability
- 3 Application: Adaptive cruise control

Set-valued reachability operator

For a system $\Xi : \dot{x} = f(x, u)$, the **flow operator** $\phi_{\Xi}(t, y, u)$ satisfies

$$\phi_{\Xi}(0, y, u) = y, \quad \frac{d}{dt}\phi_{\Xi}(t, y, u) = f(\phi(t, y, u), u)$$

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For sets X, S , define a set-valued operator for **safe reachability**:

$$\text{Rch}_S^{\infty, \Xi}(X) = \{y : \exists \text{ control } u(x), T > 0 \text{ s.t.}$$
$$\phi_{\Xi}(t, y, u) \in S \text{ for } t \in [0, T] \text{ and } \phi_{\Xi}(T, y, u) \in X\}$$

Set-valued reachability operator

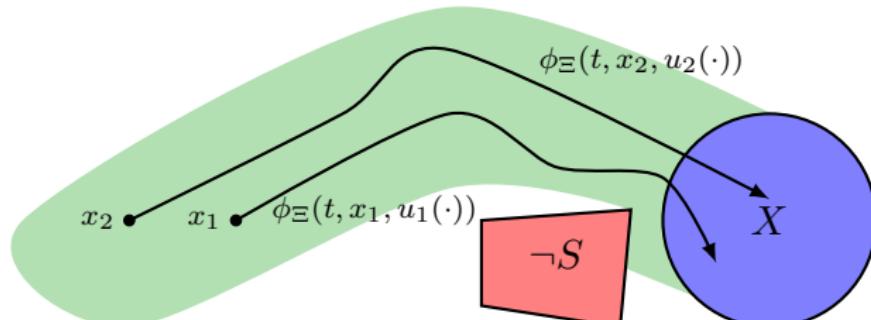
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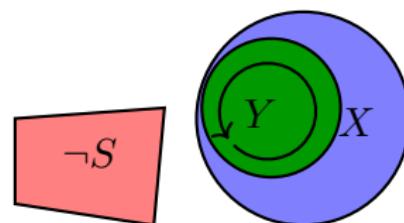
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Relation to formal specifications

Many LTL specs can be stated in terms of reachability

- Safety ($\square X$): Controlled invariance of X : find
 $Y : Y = \text{Rch}_X^{\infty, \exists}(Y)$

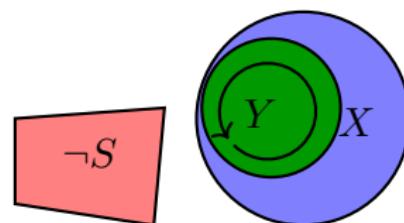


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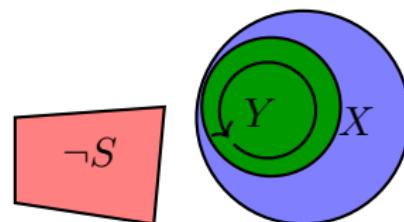
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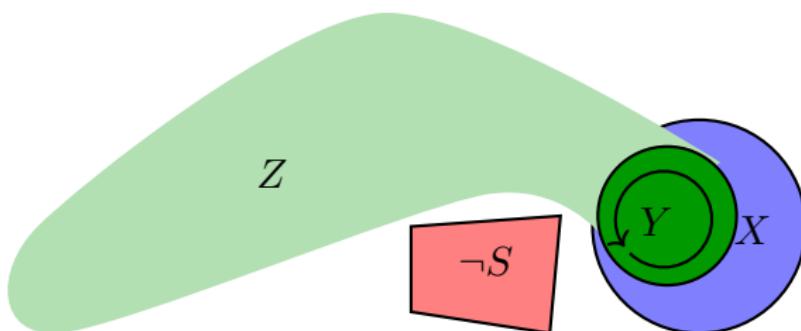
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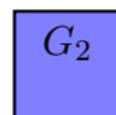
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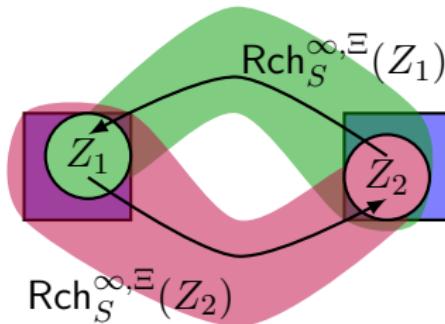
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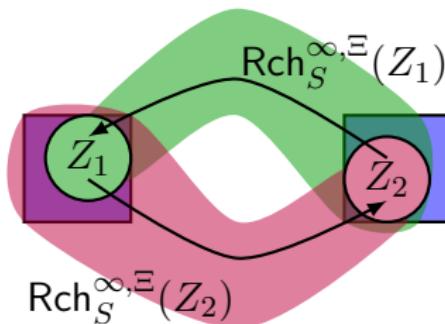
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- Difficulty: How to compute $\text{Rch}_S^{\infty, \Xi}??$

Some work related to reachability

- Zonotopes¹
- Occupation measures/positive polynomials²
- Reference governors³
- Bernstein methods⁴
- Hamilton-Jacobi equation⁵
- Polytopic reachability for discrete time linear systems

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Reachability for linear discrete-time dynamics

- Linear system: $\Sigma : x(t+1) = Ax(t) + Bu(t) + Ed(t)$
- Input restriction $u \in \mathcal{U} = \{u : H_u u \leq h_u\}$
- Disturbance assumption $d \in \mathcal{D} = \{d : H_d d \leq h_d\}$
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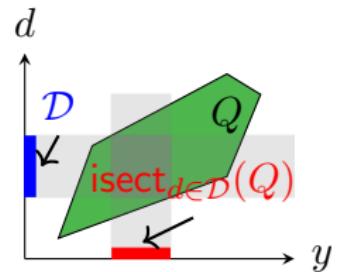
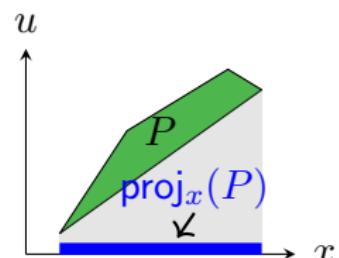
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Valid initial states:

$$\text{Rch}_S^{1,\Sigma}(X) = S \cap \text{proj}_x \circ \text{isect}_{d \in \mathcal{D}}(P)$$

Need only polyhedron **projection** and
intersection



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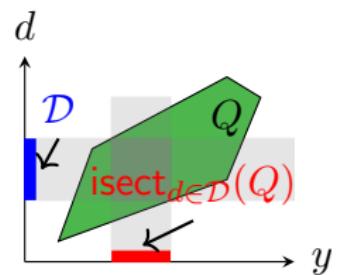
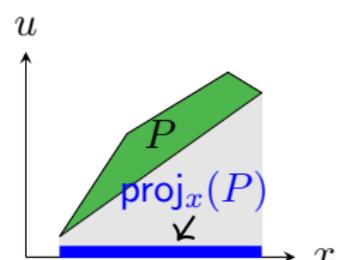
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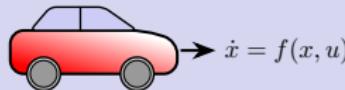
$$\text{Rch}_S^{\infty, \Sigma}(X) = \bigcup_{k \geq 0} \underbrace{\text{Rch}_S^{1,\Sigma} \circ \dots \circ \text{Rch}_S^{1,\Sigma}(X)}_{k \text{ times}}$$



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- ① Introduction
- ② Formal specifications and reachability
- ③ Application: Adaptive cruise control

Model: continuous dynamics



ACC car dynamics

$$m\dot{v} = F_w - F_r(v)$$

$$\dot{h} = v_L - v$$

$$\dot{v}_L = a_L$$

F_r polynomial drag term

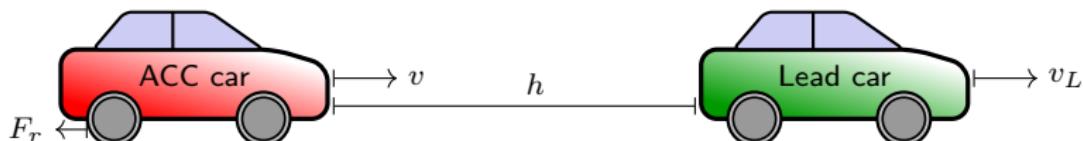
Input bound

$$F_w \in [-0.3mg, 0.2mg]$$

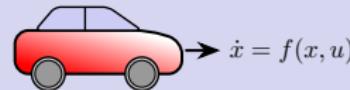
Lead car assumptions

$$v_L \in [v_L^-, v_L^+]$$

$$a_L \in [a_L^-, a_L^+]$$



Model: discrete dynamics



- Hybrid system

No lead car:

$$\begin{aligned} m\dot{v} &= F_w - F_r(v) \\ h &\equiv h^{max} \end{aligned}$$

$$R_{2,1} \quad \quad \quad R_{1,2}$$

Lead car:

$$\begin{aligned} m\dot{v} &= F_w - F_r(v) \\ \dot{h} &= v_L - v \\ \dot{v}_L &= a_L \end{aligned}$$

$$R_{2,2}$$

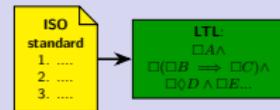
- Reset maps

$$R_{1,2}(v, h^{max}) = \{(v, \bar{h}, \bar{v}_L) : (\bar{h}, \bar{v}_L) \in \mathcal{H} \times \mathcal{V}_L\}$$

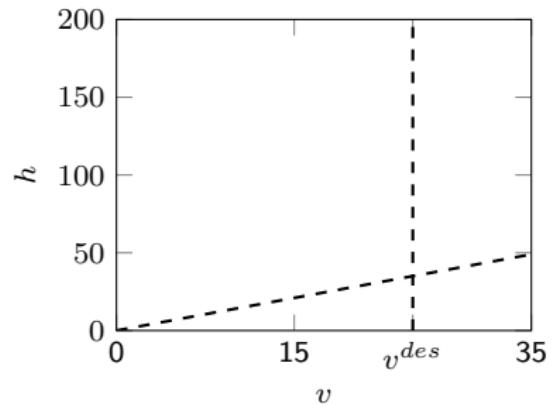
$$R_{2,1}(v, h, v_L) = \{(v, h^{max})\}$$

$$R_{2,2}(v, h, v_L) = \{(v, \bar{h}, \bar{v}_L) : (\bar{h}, \bar{v}_L) \in \mathcal{H} \times \mathcal{V}_L\}$$

Textual to formal specification

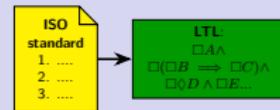


ISO: "When the ACC is active, the vehicle speed shall be controlled automatically either to maintain a time gap (h/v) to a forward vehicle, or to maintain the set speed v_{des} , whichever speed is lower."

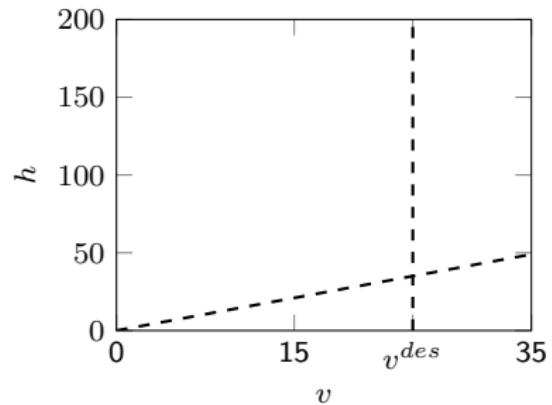


LTL :
$$\left(\bigwedge_{i=1}^2 (\quad \Rightarrow \quad) \right)$$

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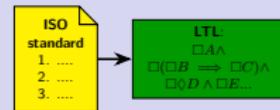


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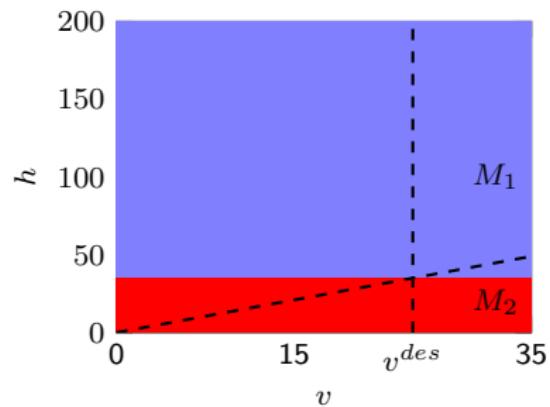


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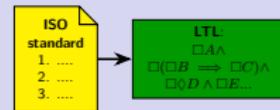


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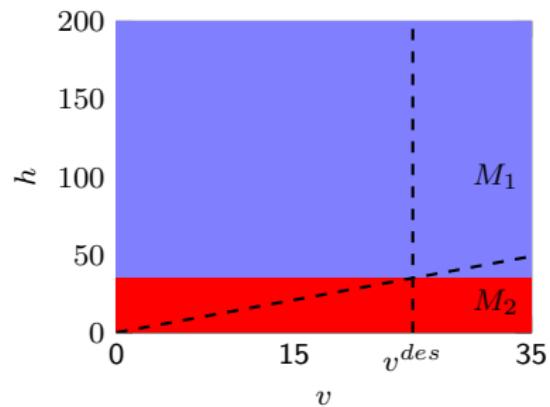
$$\left(\bigwedge_{i=1}^2 (\square M_i \Rightarrow \quad) \right)$$

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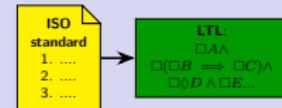


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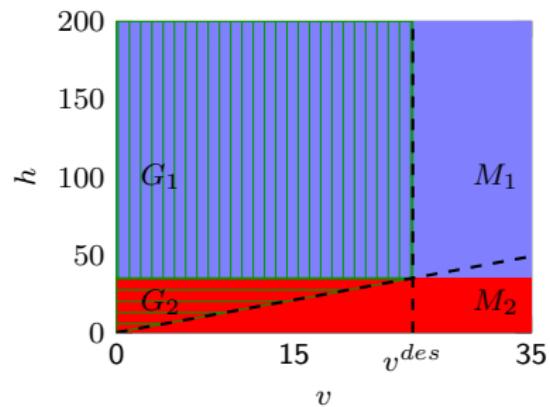
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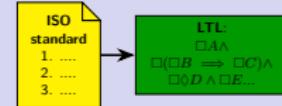


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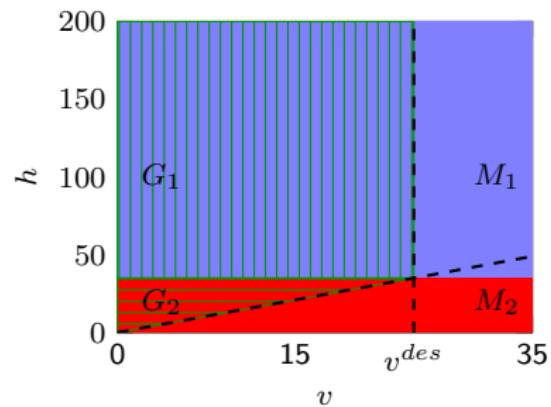
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$$\text{LTL} : \square S_U \wedge \square \left(\bigwedge_{i=1}^2 (\square M_i \Rightarrow \diamond \square G_i) \right)$$

- \square = “always”, \diamond = “eventually”
- Input constraint $S_U = \{F_w : F_w \in [-0.3mg, 0.2mg]\}$

Fixed point interpretation of specification

- Solve for specification of the form

$$\square ((\square M_1 \implies \diamond \square G_1) \wedge (\square M_2 \implies \diamond \square G_2))$$

For Inv^∞ controlled invariance operator, want sets C_1 and C_2 s.t.

$$C_1 \subset M_1 \cap \text{Rch}_S^\infty \underbrace{(\text{Inv}^\infty(G_1 \cap (C_1 \cup C_2)) \cup C_2)}_{D_1},$$

$$C_2 \subset M_2 \cap \text{Rch}_S^\infty \underbrace{(\text{Inv}^\infty(G_2 \cap (C_1 \cup C_2)) \cup C_1)}_{D_2}.$$

Correct control strategy if such C_1, C_2 are found:

- When in C_1 , make progress toward D_1
- When in C_2 , make progress toward D_2

Want to make C_1 and C_2 as large as possible to maximize controller domain

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Solution via Polyhedral Invariant Set Computation (PCIS)

- Set computations directly on the continuous state space of a linearized system
 - Conservative linearization
 - Reachability in linearized system implies reachability in original system

$$C_1^0 = M_1, \quad C_2^0 = M_2$$

$$C_1^{k+1} = M_1 \cap \text{Rch}_S^\infty \left(\text{Inv}^\infty \left(G_1 \cap (C_1^k \cup C_2^k) \right) \cup C_2^k \right)$$

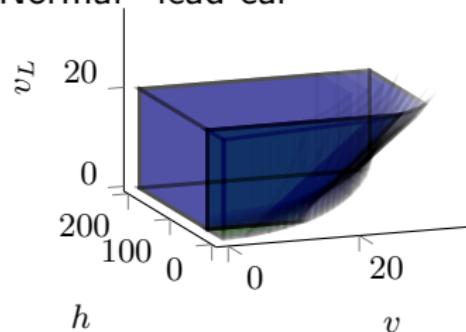
$$C_2^{k+1} = M_2 \cap \text{Rch}_S^\infty \left(\text{Inv}^\infty \left(G_2 \cap (C_1^k \cup C_2^k) \right) \cup C_1^k \right)$$

- Use approximations to keep sets simple
- Iterations converge after one step

PCIS: Computations

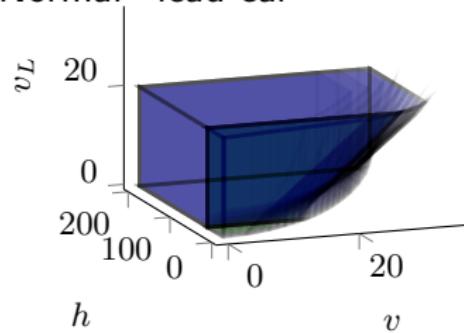
PCIS: Domain

“Normal” lead car

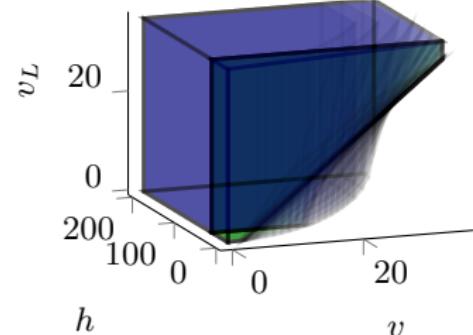


PCIS: Domain

“Normal” lead car

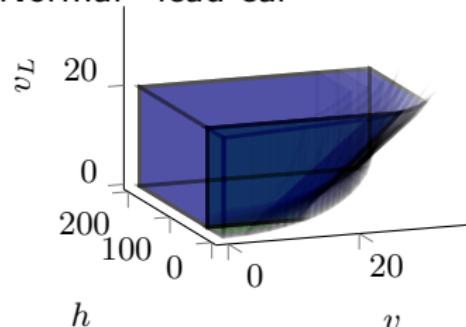


“Aggressive” lead car

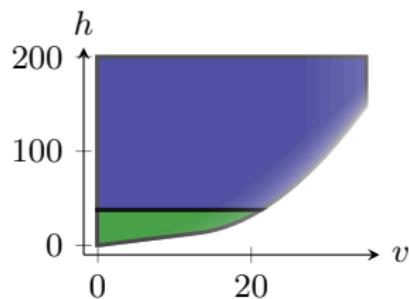


PCIS: Domain

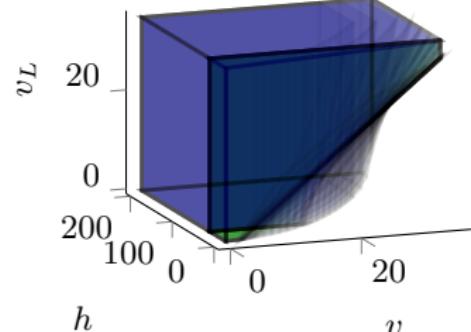
“Normal” lead car



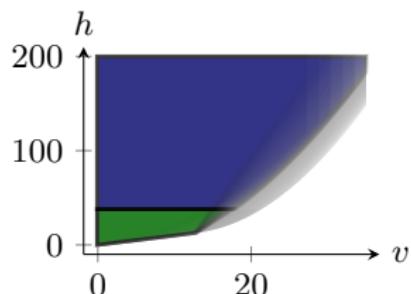
Cross section at $v_L = 10$ m/s



“Aggressive” lead car

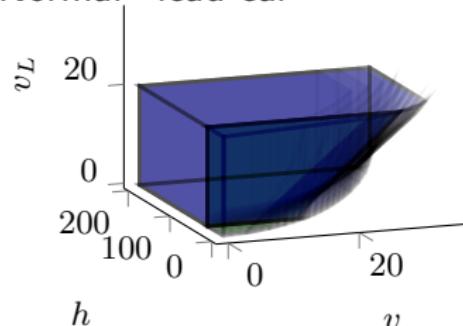


Cross section at $v_L = 10$ m/s

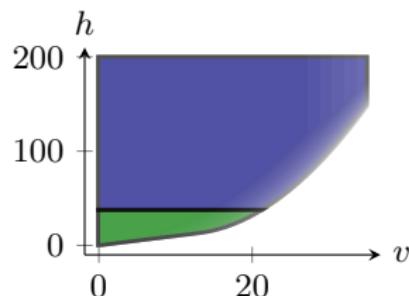


PCIS: Domain

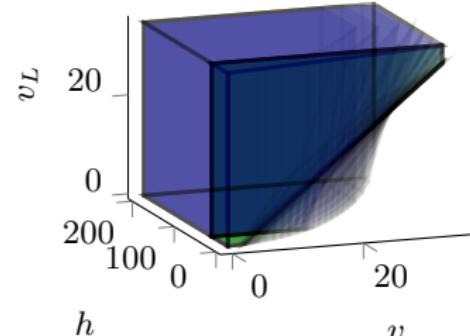
“Normal” lead car



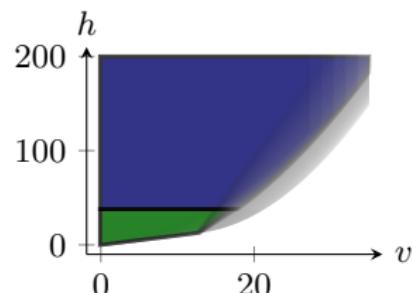
Cross section at $v_L = 10 \text{ m/s}$



“Aggressive” lead car



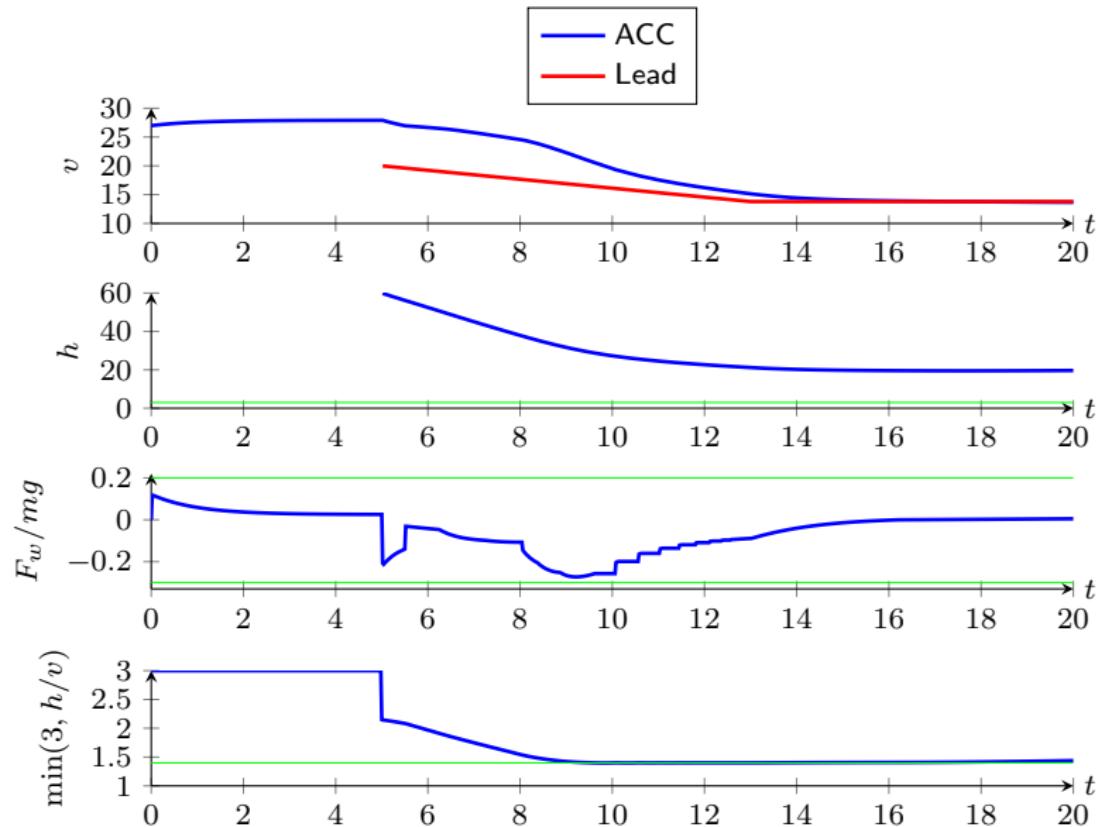
Cross section at $v_L = 10 \text{ m/s}$



- Implementation: use quadratic program with constraints to move between sets

Simulations: video

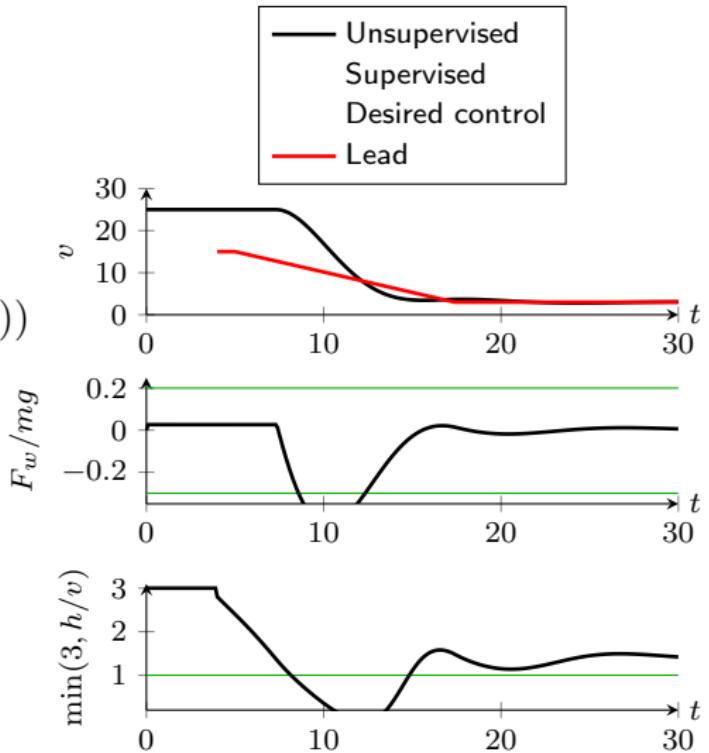
Simulations: plots



Controller supervision

Naive controller:

$$F_r(v) - k(v - \min(v^{des}, h/\omega_{des}))$$



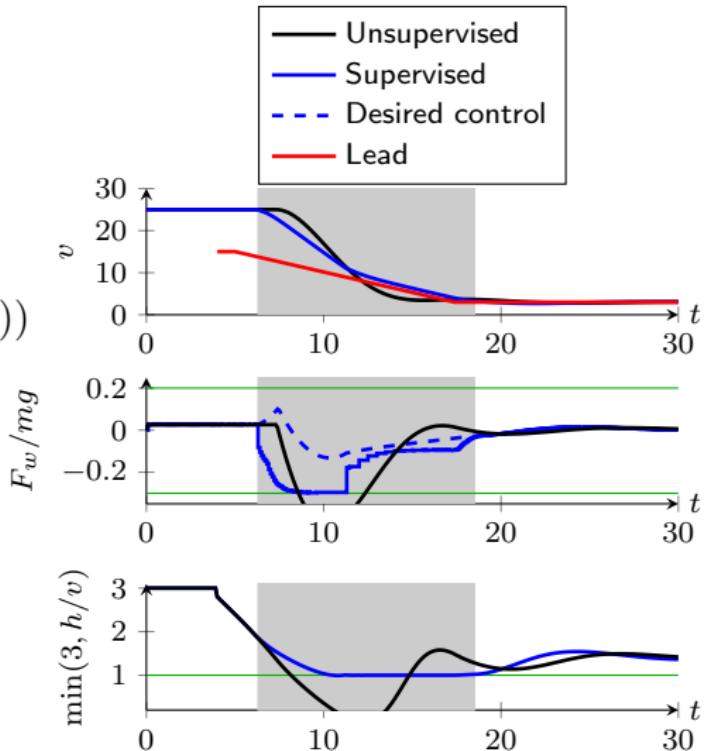
Controller supervision

Naive controller:

$$F_r(v) - k(v - \min(v^{des}, h/\omega_{des}))$$

Supervision:

- Guarantees safety
- Minimally intrusive



Summary

- Partially automated formal synthesis

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- Explicitly computed “safe set”: enables supervision/alerts

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- Partially automated formal synthesis
- Explicitly computed “safe set”: enables supervision/alerts
- Test reasonableness of specification and model instead of performance
 - May be unrealizable
 - May result in unintended behavior (e.g., satisfy $A \implies B$ by making A false)

Thank you for your attention!

Next speaker: Yuxiao Chen



Extra: Method comparison

	PCIS	Pessoa	Barrier fun.
Complex Specifications	Not yet	Yes	TBD
Automation	For LTI	Yes	Not yet
Approximation bounds	For LTI	For IS ⁶	Maybe
Parameter tuning	Yes	Some	Yes
Non-linear	Not now	Yes	Yes
High-dimensional	Not now	Not now	Yes
Termination guarantees	Approximate	Yes	N/A

⁶Incrementally Stable Systems