

# Killer Yeast Vs. Sensitive Yeast

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MATH 445 - Statistical, Dynamical, and Computational Modeling

December 2, 2013

## Proposal

The differential equation we may use for modeling the growth of yeast is the same as that used for bacterial growth in a chemostat:

$$\begin{aligned}\frac{dN}{dt} &= k(C)N - \frac{FN}{V}, \\ \frac{dC}{dt} &= -\alpha k(C)N - \frac{FC}{V} + \frac{FC_0}{V},\end{aligned}$$

with initial conditions  $C(0) = C_i$  and  $N(0) = N_i$ ,  $N$  is the number of yeast in the chamber in units number/volume,  $C$  is the concentration of nutrient in the chamber with units mass/volume,  $C_0$  is the concentration of nutrient in the reservoir,  $F$  is the in/out flow rate with units volume/time,  $V$  is the volume of the chamber,  $\alpha$  is a unitless inverse of the yield constant, and  $k(C)$  is the reproduction rate for yeast in units 1/time with possible formula chosen such that  $\lim_{C \rightarrow \infty} k(C) = k_{max}$ , and  $k_{max}$  represents the maximum possible reproduction rate:

$$k(C) = \frac{k_{max}C}{k_n + C}.$$

where  $k_n$  is chosen such that  $k(k_n) = k_{max}/2$ . The quantitative measurement for fitness is a measurement of optical density at steady state (equilibrium) at a given flow rate ( $F$ ) in volumes/hr.

Because the data is collected in density form, we propose solving for density  $\rho = N/V$ :

$$\begin{aligned}\frac{d\rho}{dt} &= k(C)\rho - \frac{F\rho}{V}, \\ \frac{dC}{dt} &= -\alpha k(C)\rho - \frac{FC}{V} + \frac{FC_0}{V},\end{aligned}$$

with initial conditions  $\rho(0) = \rho_i$  and  $C(0) = C_i$ , and all other constants are identical as before.

In order to find the steady states, we have to find the intersections of the null-clines at equilibrium points  $(\bar{\rho}, \bar{C})$ , i.e.  $d\bar{\rho}/dt = 0$  and  $d\bar{C}/dt = 0$ :

$$\begin{aligned}\frac{d\rho(\bar{\rho}, \bar{C})}{dt} &= k(\bar{C})\bar{\rho} - \frac{F\bar{\rho}}{V}, \\ &= \bar{\rho} \left( k(\bar{C}) - \frac{F}{V} \right) = 0,\end{aligned}$$

which is zero for  $\bar{\rho} = 0$  or  $k(\bar{C}) = F/V$ . Solving the other equation gives us the other steady-states:

$$\frac{dC(\bar{\rho}, \bar{C})}{dt} = -\alpha k(\bar{C})\bar{\rho} - \frac{F\bar{C}}{V} + \frac{FC_0}{V} = 0,$$

which is zero for  $\alpha k(\bar{C})\bar{\rho} + \frac{F\bar{C}}{V} = \frac{FC_0}{V}$ .

In order to evaluate these null-clines, we need to evaluate the non-trivial cases, here for  $\dot{\rho} = 0$ ,

$$\begin{aligned} k(\bar{C}) &= \frac{k_{max}\bar{C}}{k_n + \bar{C}} = \frac{F}{V} \\ k_{max}\bar{C} &= \frac{F}{V}(k_n + \bar{C}) \\ k_{max}\bar{C} - \frac{F}{V}\bar{C} &= \frac{F}{V}k_n \\ \bar{C} \left( k_{max} - \frac{F}{V} \right) &= \frac{F}{V}k_n \\ \bar{C} &= \frac{Fk_n}{V(k_{max} - \frac{F}{V})} \\ \bar{C} &= \frac{Fk_n}{V k_{max} - F}. \end{aligned} \tag{1}$$

Likewise, for  $\dot{C} = 0$ ,

$$\begin{aligned} \alpha k(\bar{C})\bar{\rho} + \frac{F\bar{C}}{V} &= \frac{FC_0}{V} \\ \alpha \left[ \frac{k_{max}\bar{C}}{k_n + \bar{C}} \right] \bar{\rho} + \frac{F\bar{C}}{V} &= \frac{FC_0}{V} \\ \alpha k_{max}\bar{C}\bar{\rho} + \frac{F\bar{C}}{V}(k_n + \bar{C}) &= \frac{FC_0}{V}(k_n + \bar{C}) \\ \alpha k_{max}\bar{C}\bar{\rho} + \frac{F\bar{C}}{V}(k_n + \bar{C}) &= \frac{FC_0}{V}(k_n + \bar{C}) \\ \alpha k_{max}\bar{C}\bar{\rho} + \frac{F\bar{C}k_n}{V} + \frac{F\bar{C}^2}{V} &= \frac{FC_0k_n}{V} + \frac{FC_0\bar{C}}{V} \\ \alpha k_{max}\bar{C}\bar{\rho} &= \frac{FC_0k_n}{V} + \frac{FC_0\bar{C}}{V} - \frac{F\bar{C}k_n}{V} - \frac{F\bar{C}^2}{V} \\ \bar{\rho} &= \frac{FC_0k_n}{V(\alpha k_{max}\bar{C})} + \frac{FC_0\bar{C}}{V(\alpha k_{max}\bar{C})} - \frac{F\bar{C}k_n}{V(\alpha k_{max}\bar{C})} - \frac{F\bar{C}^2}{V(\alpha k_{max}\bar{C})} \\ \bar{\rho} &= \frac{FC_0k_n}{V\alpha k_{max}\bar{C}} + \frac{FC_0}{V\alpha k_{max}} - \frac{Fk_n}{V\alpha k_{max}} - \frac{F\bar{C}}{V\alpha k_{max}} \\ \bar{\rho} &= \frac{F}{V\alpha k_{max}} \left( \frac{C_0k_n}{\bar{C}} + C_0 - k_n - \bar{C} \right). \end{aligned} \tag{2}$$

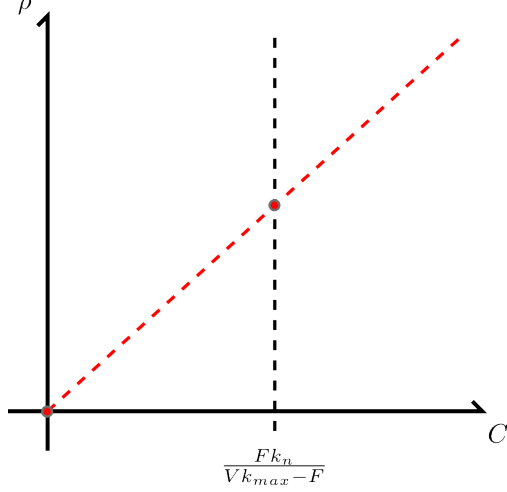


Figure 1: The  $\dot{C} = 0$  nullcline (red) intersecting with the  $\dot{\rho} = 0$  nullcline (black). The trivial steady-state  $(0,0)$  and non-trivial steady-state  $(\bar{\rho}, \bar{C})$  are shown as red dots.

By placing Eq. (1) inside Eq. (2), we can find the intersection of the null-clines:

$$\begin{aligned}\bar{\rho}(\bar{C}) &= \frac{F}{V\alpha k_{max}} \left( \frac{C_0 k_n}{\bar{C}} + C_0 - k_n - \bar{C} \right) \\ &= \frac{F}{V\alpha k_{max}} \left( \frac{C_0 k_n}{\frac{F k_n}{V k_{max} - F}} + C_0 - k_n - \frac{F k_n}{V k_{max} - F} \right) \\ &= \frac{F}{V\alpha k_{max}} \left( \frac{C_0 (V k_{max} - F)}{F} + C_0 - k_n - \frac{F k_n}{V k_{max} - F} \right).\end{aligned}$$

The unknowns in this are  $\alpha$ ,  $k_{max}$ , and  $k_n$ . First, assume  $\alpha = 1$ . With this assumption we can then minimize the difference between the equilibrium solution of the differential equations  $\dot{\rho}$  and  $\dot{C}$  (determined numerically) and the observed optical density for a given  $F$  to provide an estimate for  $\bar{C}$ , which we can then plug into equations (1) and (2) to get  $k_{max}$  and  $k_n$ .

The data we are provided with include two sets of two separate runs, along with the concentration of nutrient in the reservoir,  $C_0 = 0.02$ :

## 1 K1 Run

### Vessel One :

Volumes/Hr	0.028	0.099	0.142	0.207	0.269	0.287	0.352	0.403
Optical Density at Steady State	0.144	0.151	0.099	0.069	0.045	0.02	0.003	0

### Vessel Two :

Volumes/Hr	0.054	0.11	0.141	0.199	0.257	0.296	0.348	0.397	0.41
Optical Density at Steady State	0.164	0.151	0.11	0.092	0.072	0.023	0.006	0.002	0.004

## 2 Sensitive Run

### Vessel One :

Volumes/Hr	0.041	0.099	0.167	0.223	0.266	0.328	0.356	0.401	0.462
Optical Density at Steady State	0.54	0.494	0.459	0.395	0.229	0.019	0.006	0.003	0

### Vessel Two :

Volumes/Hr	0.0571	0.126	0.196	0.263	0.313	0.383
<sup>a</sup> Optical Density at Steady State	0.385	0.456	0.363	0.197	0.044	0.004

