

Microelectronic Circuits Assignment 1

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1 Question 1

Value of components (resistor/capacitor) present in the circuit:

Table 1: Calculated values for question 1

Sl. No.	Component Name	Value
1	R1(k Ω)	15k Ω
2	C1 (nF)	1nF

1.1 Circuit as on LT SPICE

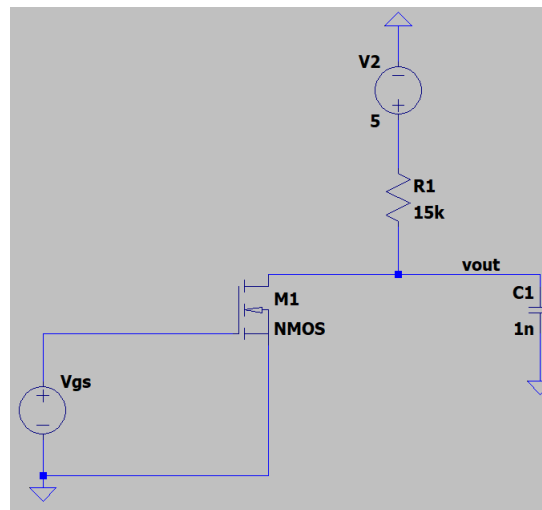


Figure 1: Circuit for question 1

1.2 Graphs

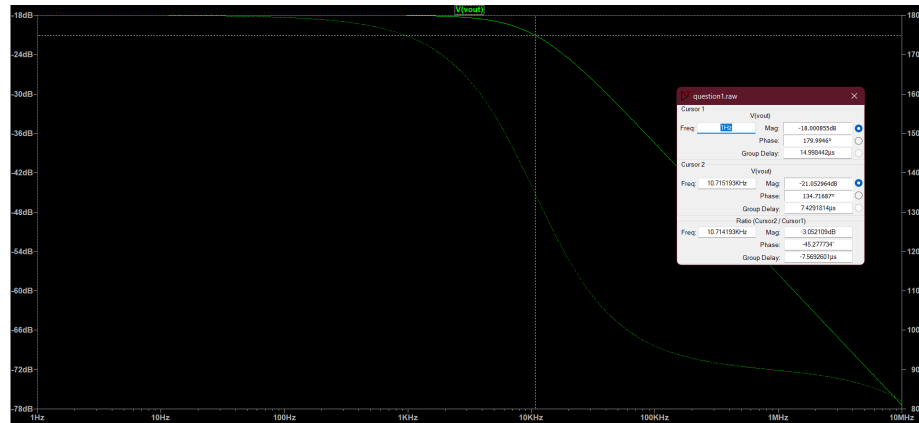


Figure 2: Frequency Response

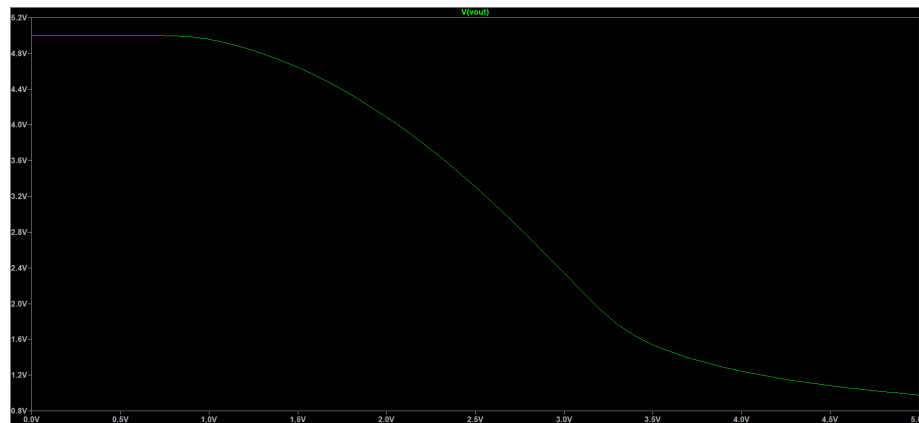


Figure 3: Voltage transfer characteristics

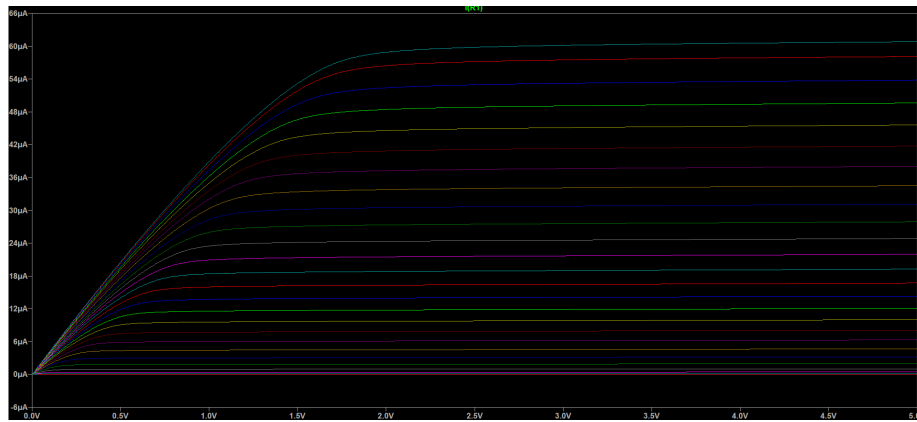


Figure 4: Graph of i_{DS} vs V_{DS}

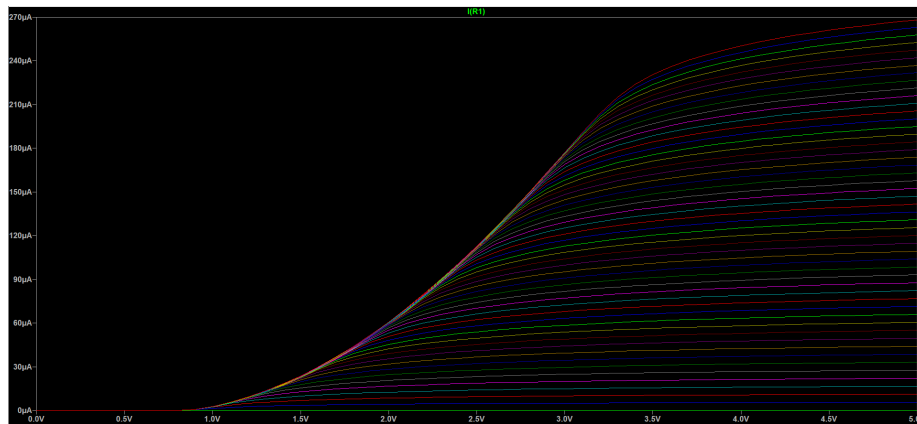


Figure 5: Graph of i_{DS} vs V_{GS}

In figure 2 on the preceding page, for an approximate 3dB change in frequency (as shown by both cursors), we see the phase shift by approximately 45° .

1.3 Miscellaneous calculations

1.3.1 DC operating point

Given the overdrive voltage of the MOSFET as 0.2V and the threshold voltage as 0.6696061V, to calculate the DC operating point, we must take $V_{GS} = V_{TH} + V_{OV} = 0.8696061\text{V}$. With this value of V_{GS} , the simulation yields the following values:

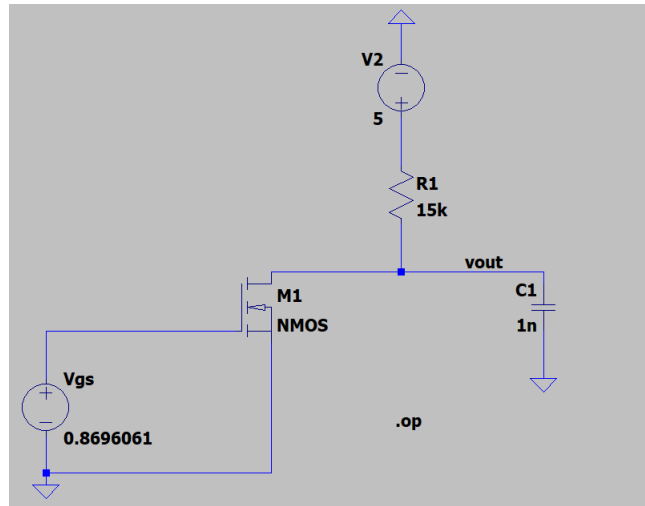


Figure 6: DC operating point circuit

--- Operating Point ---		
V(n002) :	0.869606	voltage
V(n001) :	5	voltage
V(vout) :	4.99329	voltage
Id(M1) :	4.47302e-007	device_current
Ig(M1) :	0	device_current
Ib(M1) :	-5.00329e-012	device_current
Is(M1) :	-4.47297e-007	device_current
I(C1) :	-4.99329e-021	device_current
I(R1) :	4.47302e-007	device_current
I(V2) :	-4.47302e-007	device_current
I(Vgs) :	0	device_current

Figure 7: DC operating point parameters

1.3.2 Small signal calculations

Transconductance g_m is given by:

$$g_m = \frac{2I_D}{V_{OV}}$$

Using the values found above from the DC operating point calculations, we can calculate the transconductance to be

$$g_m = \frac{2 \times 4.47302 \times 10^{-7}}{0.2} = 4.47302 \times 10^{-6} \text{ A/V}$$

The value of the output resistance r_o corresponding to the early effect/channel length modulation is given by:

$$r_o = \left(\frac{\partial i_D}{\partial V_{DS}} \right)^{-1} \bigg|_{V_{GS}=\text{constant}}$$

This can be found out from the simulation by setting $V_{GS} = V_{TH} + V_{OV}$ and finding the value of the inverse of the differential at $V_{DS} = 5\text{V}$.

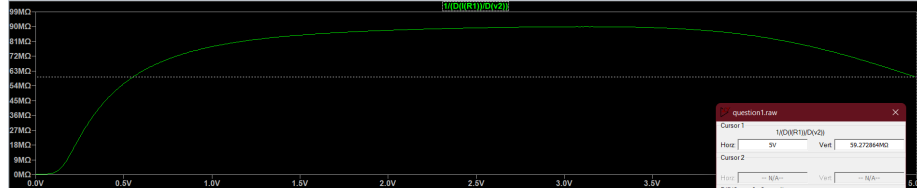


Figure 8: Output resistance for small signal calculations

The value of r_o we get from this graph is $r_o = 59.272865\text{M}\Omega$. Collectively, we get the small signal model as below:

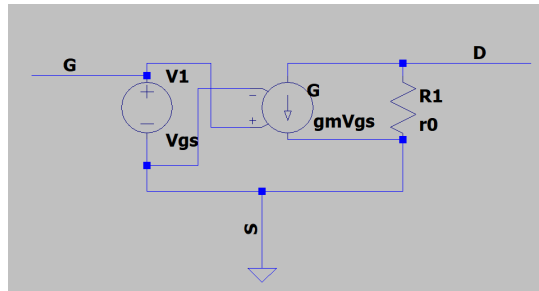


Figure 9: Small signal model

2 Question 2

Value of components (resistors/gain) present in the circuit

Table 2: Calculated values for question 2

Sl. No.	Component Name	Value
1	$R_1(k\Omega)$	$30k\Omega$
2	$R_2(k\Omega)$	$17k\Omega$
3	$R_3(k\Omega)$	$30k\Omega$
4	$R_4(k\Omega)$	$50k\Omega$
5	k	18 V/V

2.1 Circuit as on LT SPICE

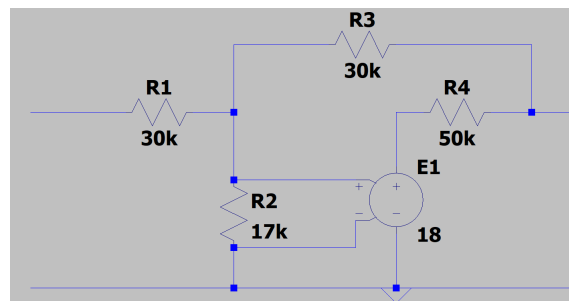


Figure 10: Original 2 port network simulated on LT SPICE

2.2 Z, Y and H Parameters

2.2.1 Z parameters

Z parameters as obtained from LT SPICE

$$Z = \begin{bmatrix} 23.492822k\Omega & -4.0669856k\Omega \\ -47.99043k\Omega & -11.24402k\Omega \end{bmatrix}$$

2.2.2 Y parameters

Y parameters as obtained from LT SPICE

$$Y = \begin{bmatrix} 24.479166\mu\text{S} & -8.8541665\mu\text{S} \\ -104.47916\mu\text{S} & -51.145835\mu\text{S} \end{bmatrix}$$

2.2.3 H parameters

$$H = \begin{bmatrix} 40.851062k\Omega & 361.70211mV/V \\ -4.268085A/A & -88.936169\text{S} \end{bmatrix}$$

2.3 Calculations

2.3.1 Z parameters

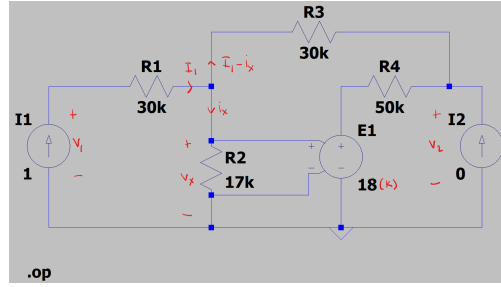


Figure 11: Z parameter circuit 1 (for z_{11} and z_{21})

Assume the convention in the above circuit for the calculations that follow

$$\begin{aligned}
 -(I_1 - i_x)(R_3 + R_4) - kV_x + V_x &= 0 \\
 (i_x - I_1)(R_3 + R_4) &= V_x(k - 1) \\
 (i_x - I_1)(R_3 + R_4) &= i_x R_2(k - 1) \\
 i_x(R_3 + R_4 - R_2(k - 1)) &= I_1(R_3 + R_4) \\
 \implies i_x &= I_1 \frac{(R_3 + R_4)}{R_3 + R_4 - R_2(k - 1)} \\
 V_1 &= I_1 R_1 + V_x \\
 V_1 &= I_1 R_1 + i_x R_2 \\
 V_1 &= I_1 \left[R_1 + \frac{R_2(R_3 + R_4)}{R_3 + R_4 - R_2(k - 1)} \right] \\
 \implies \frac{V_1}{I_1} &= z_{11} = R_1 + \frac{R_2(R_3 + R_4)}{R_3 + R_4 - R_2(k - 1)}
 \end{aligned}$$

Also :

$$\begin{aligned}
 V_2 &= (I_1 - i_x)R_4 + kV_x \\
 V_2 &= (I_1 - i_x)R_4 + k i_x R_2 \\
 V_2 &= i_x(kR_2 - R_4) + I_1 R_4 \\
 V_2 &= I_1 \left[R_4 + \frac{(kR_2 - R_4)(R_3 + R_4)}{R_3 + R_4 - R_2(k - 1)} \right] \\
 \implies \frac{V_2}{I_1} &= z_{21} = R_4 + \frac{(kR_2 - R_4)(R_3 + R_4)}{R_3 + R_4 - R_2(k - 1)}
 \end{aligned}$$

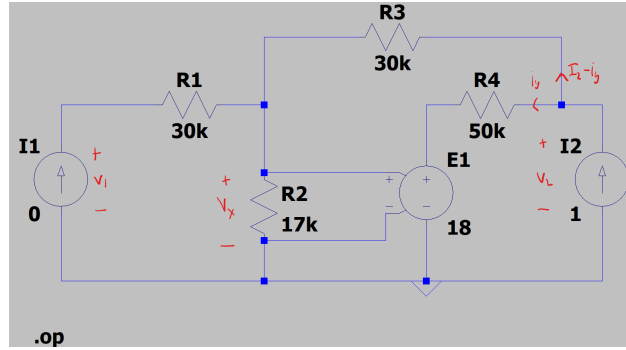


Figure 12: Z parameter circuit 2 (for z_{12} and z_{22})

Assume the convention in the above circuit for the calculations that follow

$$\begin{aligned}
 -R_3(I_2 - i_y) - V_x + kV_x + i_y R_4 &= 0 \\
 i_y R_4 - R_3(I_2 - i_y) &= (1 - k)V_x \\
 i_y R_4 - R_3(I_2 - i_y) &= (1 - k)(I_2 - i_y)R_2 \\
 i_y R_4 &= (I_2 - i_y)[(1 - k)R_2 + R_3] \\
 (R_4 + R_3 + (1 - k)R_2)i_y &= I_2[(1 - k)R_2 + R_3] \\
 \implies i_y &= I_2 \frac{(1 - k)R_2 + R_3}{(1 - k)R_2 + R_3 + R_4} \\
 V_2 &= i_y R_4 + kV_x \\
 V_2 &= i_y R_4 + k(I_2 - i_y)R_2 \\
 V_2 &= i_y[R_4 - kR_2] + KI_2 R_2 \\
 V_2 &= I_2 \left[\frac{(R_4 - kR_2)\{(1 - k)R_2 + R_3\}}{(1 - k)R_2 + R_3 + R_4} + kR_2 \right] \\
 \implies \frac{V_2}{I_2} &= \boxed{z_{22} = \frac{(R_4 - kR_2)\{(1 - k)R_2 + R_3\}}{(1 - k)R_2 + R_3 + R_4} + kR_2}
 \end{aligned}$$

Also :

$$\begin{aligned}
 V_1 &= V_x = (I_2 - i_y)R_2 \\
 V_1 &= I_2 R_2 \left[1 - \frac{(1 - k)R_2 + R_3}{(1 - k)R_2 + R_3 + R_4} \right] \\
 \implies \frac{V_1}{I_2} &= \boxed{z_{12} = R_2 \left[1 - \frac{(1 - k)R_2 + R_3}{(1 - k)R_2 + R_3 + R_4} \right]}
 \end{aligned}$$

Using the corresponding values taken from table 2 on page 6 into the above equations, we get the matrix for the Z parameters:

$$Z = \begin{bmatrix} 23.49282297k\Omega & -4.066985646k\Omega \\ -47.99043062k\Omega & -11.244041914k\Omega \end{bmatrix}$$

Which is in accordance with the values obtained from the simulation.

2.3.2 Y parameters

From the above matrix for Z parameters, we can calculate the Y parameters as follows:

$$\begin{aligned} \Delta Z &= z_{11}z_{22} - z_{12}z_{21} \\ \Rightarrow \Delta Z &= [(23.49282297 \times -11.244041914) - \\ &\quad (-47.99043062 \times -4.066985646)] \times 10^3 \\ \Delta Z &= -459.326 \times 10^6 \\ Y &= \begin{bmatrix} \frac{z_{22}}{\Delta Z} & -\frac{z_{12}}{\Delta Z} \\ -\frac{z_{21}}{\Delta Z} & \frac{z_{11}}{\Delta Z} \end{bmatrix} \end{aligned}$$

Simplifying the above matrix, we get the Y parameters:

$$Y = \begin{bmatrix} 2.448 \times 10^{-5} \mu\mathcal{U} & -8.8541 \times 10^{-6} \mu\mathcal{U} \\ -1.104480 \times 10^{-4} \mu\mathcal{U} & -5.11 \times 10^{-5} \mu\mathcal{U} \end{bmatrix}$$

2.3.3 H parameters

Similarly, we can calculate the H parameters as follows:

$$H = \begin{bmatrix} \frac{\Delta Z}{z_{22}} & -\frac{z_{12}}{z_{22}} \\ -\frac{z_{21}}{z_{22}} & \frac{1}{z_{22}} \end{bmatrix}$$

Simplifying the above matrix, we get the H parameters:

$$H = \begin{bmatrix} 40.8507k\Omega & -0.3617V/V \\ -4.2681A/A & -88.9363\mathcal{U} \end{bmatrix}$$

2.4 Load resistance value at port 2

Varying the output resistance at the terminals of port 2 and by calculating the voltage and current across the resistance, we can calculate the maximum power dissipated across the resistance. This can be seen in the following figure:

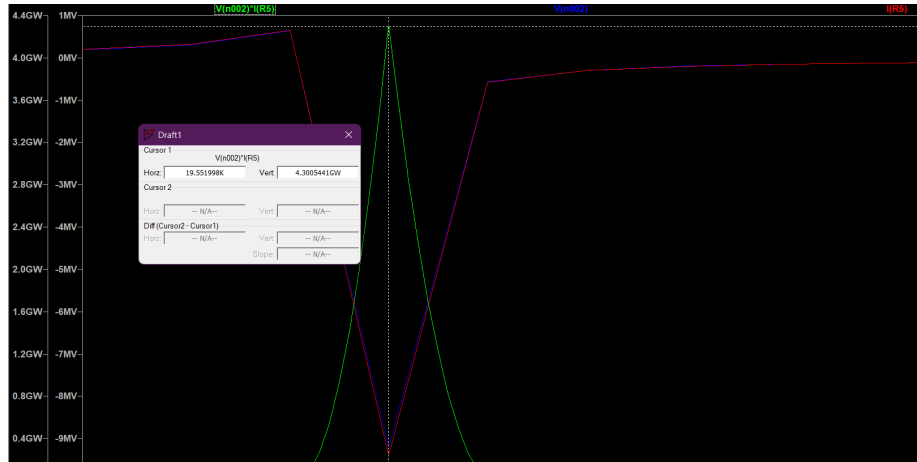


Figure 13: Load resistance value at port 2

According to the simulation results shown above, the value for the resistance at which maximum power transfer occurs is $19.551998k\Omega$ and the maximum power transferred is $4.3005441GW$. The circuit used to determine the above graph is shown below:

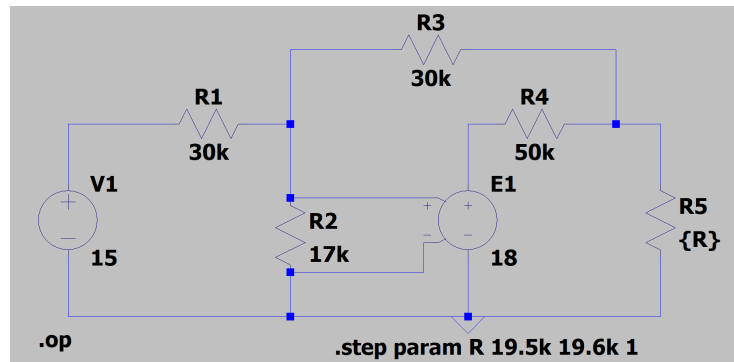


Figure 14: Circuit used to calculate the maximum power transfer point

The values through which the resistance is varied, is deduced through trial and error to get a clear graph.