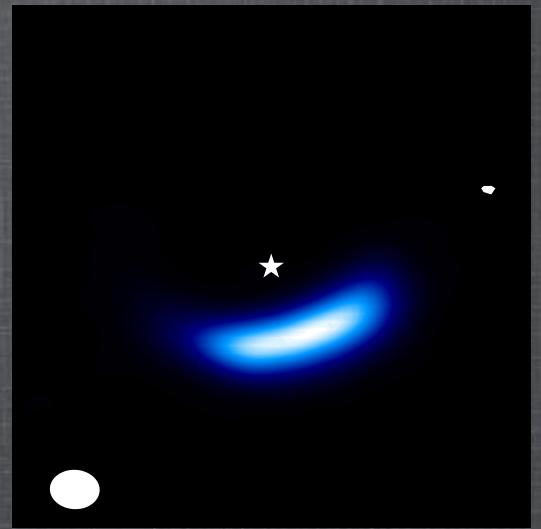
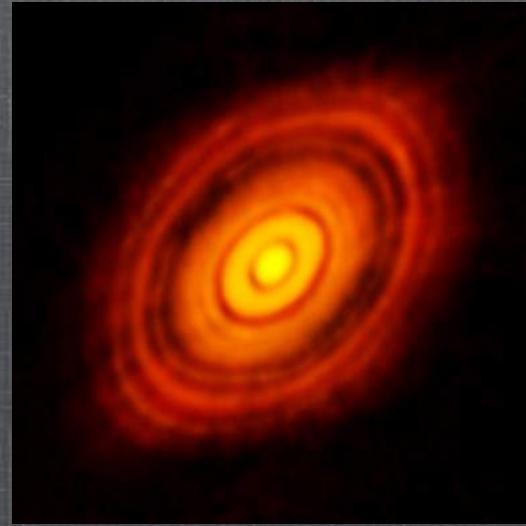




*Dust and gas in SPH
(part I)*

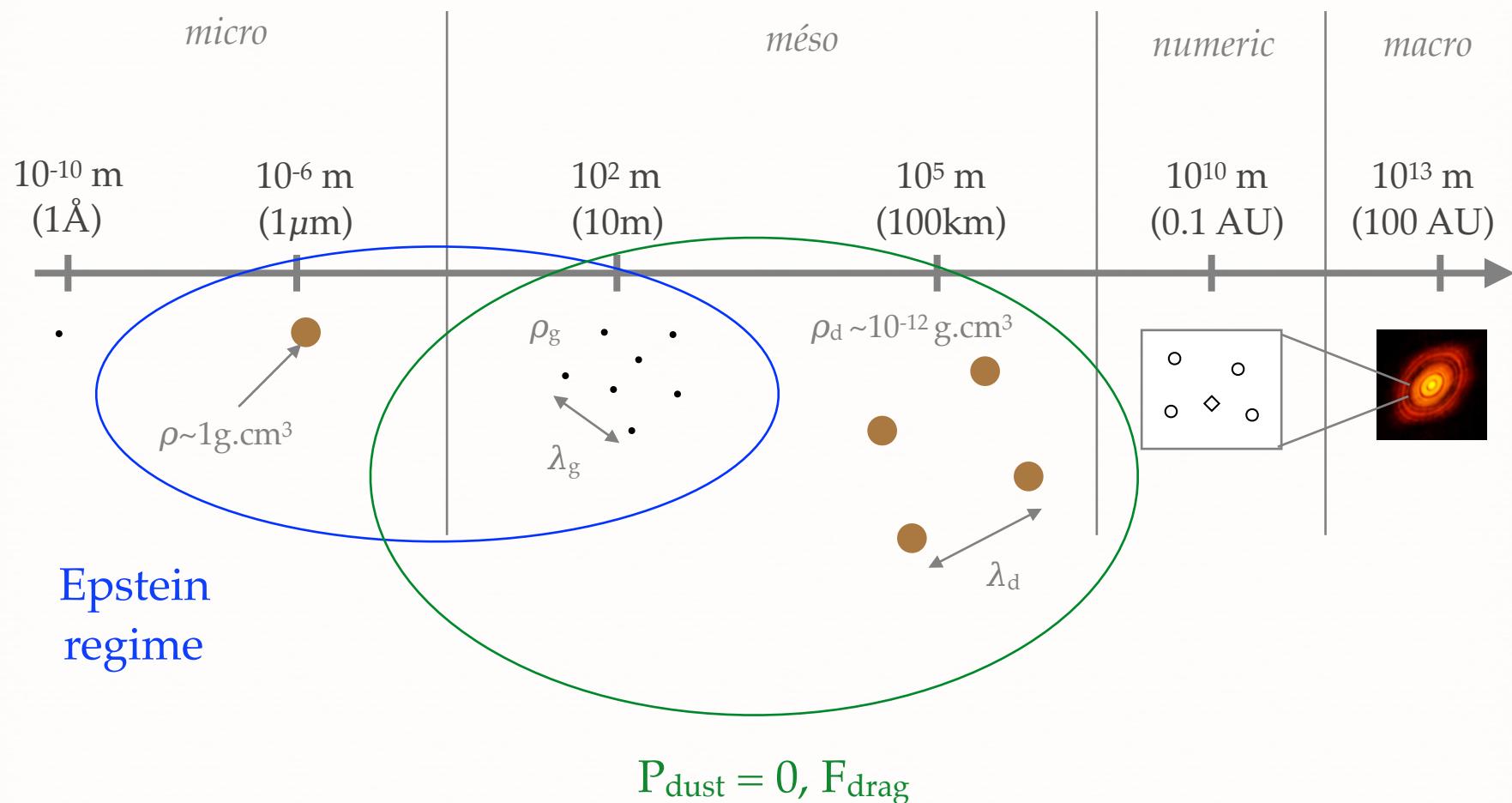


Guillaume Laibe
and the “dustbusters” consortium



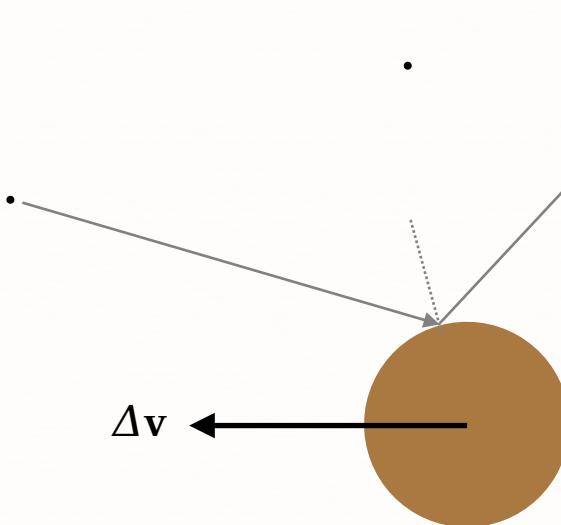
Scales

In a protoplanetary disc :



Force on a grain

Spherical homogeneous massive grain, specular reflexions :



Epstein drag force:

$$\mathbf{F}_d = \frac{dp}{dt} = \frac{\langle \mathbf{p}_{1c} \rangle}{t_{1c}}$$

$$\mathbf{p}_{1c} = -\frac{4}{3} \times m_g \Delta \mathbf{v}$$

$$t_{1c} = \left(n_g \underbrace{\left(\pi s^2 \right)}_{\sigma_{coll}} \underbrace{\sqrt{\frac{8}{\pi \gamma}} c_s}_{v_{th}} \right)^{-1}$$

$$\boxed{\mathbf{F}_d = -\frac{4}{3} \pi \rho_g s^2 \sqrt{\frac{8}{\pi \gamma}} c_s \Delta \mathbf{v}}$$

correction if
 Δv supersonic

Force balance on a grain:

$$\frac{d\mathbf{v}_d}{dt} = -\frac{\Delta \mathbf{v}}{t_{s,d}},$$

$$m_d \frac{d\mathbf{v}_d}{dt} = \mathbf{F}_d \quad \longrightarrow$$

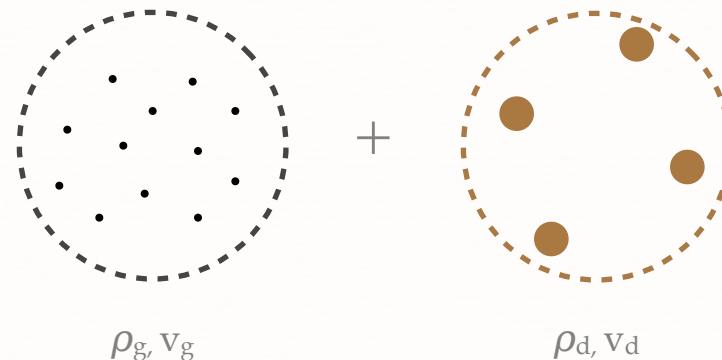
$$t_{s,d} \equiv \sqrt{\frac{\pi \gamma}{8}} \underbrace{\rho s}_{\text{circled}} \propto \frac{\sigma_d}{m_d}$$

Two fluids description

Mass conservation:

$$\frac{\partial \rho_g}{\partial t} + \nabla \cdot (\rho_g \mathbf{v}_g) = 0,$$

$$\frac{\partial \rho_d}{\partial t} + \nabla \cdot (\rho_d \mathbf{v}_d) = 0,$$



Momentum conservation:

$$\rho_g \left(\frac{\partial \mathbf{v}_g}{\partial t} + \mathbf{v}_g \cdot \nabla \mathbf{v}_g \right) = \nabla P + \rho_g \mathbf{g} + \{ \dots \} + K (\mathbf{v}_d - \mathbf{v}_g),$$
$$\rho_d \left(\frac{\partial \mathbf{v}_d}{\partial t} + \mathbf{v}_d \cdot \nabla \mathbf{v}_d \right) = \underbrace{\nabla P_d}_{0} + \rho_d \mathbf{g} + \{ \dots \} - K (\mathbf{v}_d - \mathbf{v}_g),$$

∇P : differential force

drag: exchange of momentum

differential advection

Energy conservation:

$$\rho_g \frac{du_g}{dt} = -P \nabla \cdot \mathbf{v}_g + \rho_g K \Delta \mathbf{v}^2.$$

Two fluids SPH equations

bell-shaped kernel

$$\rho_a = \sum_b m_b W_{ab}(h_a); \quad h_a = h_{\text{fact}} \left(\frac{m_a}{\rho_a} \right)^{1/3}$$

$$\left(\frac{d\mathbf{v}_a}{dt} \right)_{\text{drag}} = -3 \sum_j m_j \frac{\mathbf{v}_{aj} \cdot \hat{\mathbf{r}}_{aj}}{(\rho_a + \rho_j)t_{aj}^s} \hat{\mathbf{r}}_{aj} D_{aj}(h_a),$$

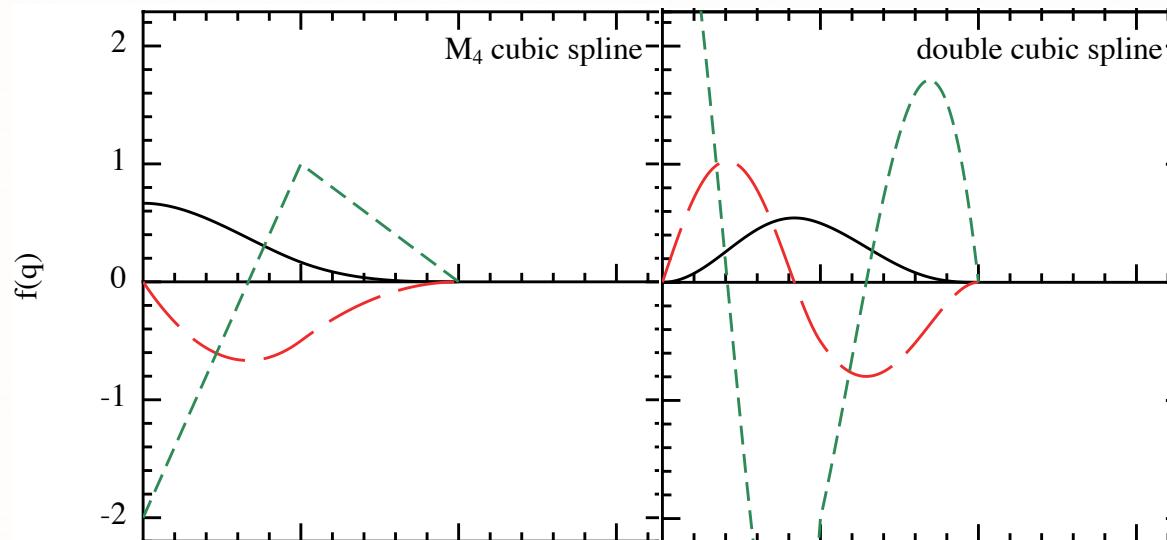
$$\rho_i = \sum_j m_j W_{ij}(h_i); \quad h_i = h_{\text{fact}} \left(\frac{m_i}{\rho_i} \right)^{1/3}$$

$$\left(\frac{d\mathbf{v}_i}{dt} \right)_{\text{drag}} = -3 \sum_b m_b \frac{\mathbf{v}_{ib} \cdot \hat{\mathbf{r}}_{ib}}{(\rho_i + \rho_b)t_{ib}^s} \hat{\mathbf{r}}_{ib} D_{ib}(h_b)$$

neighbours of
same type

own smoothing
length

double hump
drag kernel



$$D(r, h) = \frac{\sigma}{h^3} g(q),$$

$$g(q) = q^2 f(q)$$

Angular momentum conservation

Conservation of angular momentum:

$$\begin{aligned}
 \frac{d\mathbf{L}}{dt} &= \frac{d}{dt} \left(\sum_a m_a \mathbf{r}_a \times \mathbf{v}_a + \sum_i m_i \mathbf{r}_i \times \mathbf{v}_i \right) = \sum_a m_a \mathbf{r}_a \times \frac{d\mathbf{v}_a}{dt} + \sum_i m_i \mathbf{r}_i \times \frac{d\mathbf{v}_i}{dt} \\
 &= -3 \sum_a m_a \mathbf{r}_a \times \left\{ \sum_j \frac{m_j}{(\rho_a + \rho_j) t_{s,aj}} (\mathbf{v}_{aj} \cdot \hat{\mathbf{r}}_{aj}) \hat{\mathbf{r}}_{aj} D_{aj}(h_a) \right\} + \leftrightarrow \\
 &= -3 \sum_a \sum_j \underbrace{\frac{m_a m_j}{(\rho_a + \rho_j) t_{s,aj}}}_{S} \left(\underbrace{\mathbf{v}_{aj} \cdot \hat{\mathbf{r}}_{aj}}_A \right) \underbrace{\frac{\mathbf{r}_a \times \mathbf{r}_j}{r_{aj}}}_A D_{aj}(h_a) + \leftrightarrow, \\
 &= 0.
 \end{aligned}$$

Why not the simpler

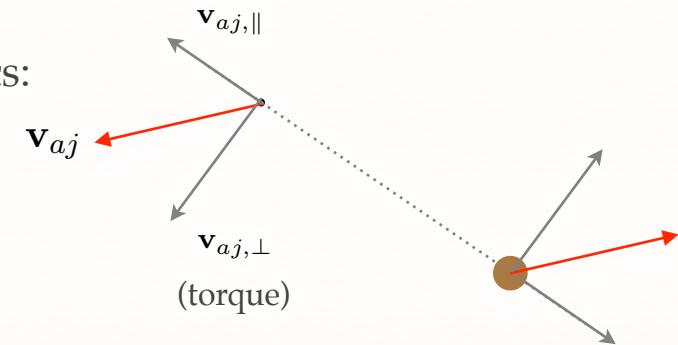
$$\frac{d\mathbf{v}_a}{dt} = - \sum_j \frac{m_j}{(\rho_a + \rho_j) t_{s,aj}} \mathbf{v}_{aj} D_{aj}(h_a)$$

maths:

$$\mathbf{v}_{aj} = \underbrace{(\mathbf{v}_{aj} \cdot \hat{\mathbf{r}}_{aj}) \hat{\mathbf{r}}_{aj}}_{\mathbf{v}_{aj,||}} + \underbrace{\hat{\mathbf{r}}_{aj} \times (\mathbf{v}_{aj} \times \hat{\mathbf{r}}_{aj})}_{\mathbf{v}_{aj,\perp}}$$

gives symmetric terms

physics:



Consistency - the factor 3 and approximations

Continuous limit:

$$\begin{aligned}
 I &= \sum_a \frac{m_a}{\rho_a} (\mathbf{v}_{aj} \cdot \hat{\mathbf{r}}_{aj}) \hat{\mathbf{r}}_{aj} D_{aj}(h_a) \simeq \int d\mathbf{r}' (\mathbf{v}_g(\mathbf{r}) - \mathbf{v}_d(\mathbf{r}')) \cdot \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|} \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|} D(\mathbf{r}' - \mathbf{r}) \\
 &\simeq \iiint dx' dy' dz' \left\{ \frac{\Delta v_x(\mathbf{r})(x-x')^2 + \Delta v_y(\mathbf{r})(y-y')(x-x') + \Delta v_z(\mathbf{r})(z-z')(x-x')}{(x-x')^2 + (y-y')^2 + (z-z')^2} \right\} D(\mathbf{r}' - \mathbf{r}) \hat{\mathbf{x}} \\
 &\quad + () \hat{\mathbf{y}} + () \hat{\mathbf{z}} - \iiint d\mathbf{r}' [(\mathbf{r}' - \mathbf{r}) \cdot \nabla_{\mathbf{r}'=\mathbf{r}} \mathbf{v}_d] \cdot \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|} \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|} D(\mathbf{r}' - \mathbf{r})
 \end{aligned}$$

drag kernel

$$\begin{aligned}
 &\simeq \Delta v_x(\mathbf{r}) \iiint dx' dy' dz' \left\{ \frac{(x-x')^2}{(x-x')^2 + (y-y')^2 + (z-z')^2} \right\} D(\mathbf{r}' - \mathbf{r}) \hat{\mathbf{x}} + () \hat{\mathbf{y}} + () \hat{\mathbf{z}} \\
 &\simeq \frac{\Delta v_x(\mathbf{r})}{3} \iiint dx' dy' dz' \left\{ \frac{(x-x')^2 + (y-y')^2 + (z-z')^2}{(x-x')^2 + (y-y')^2 + (z-z')^2} \right\} D(\mathbf{r}' - \mathbf{r}) \hat{\mathbf{x}} + () \hat{\mathbf{y}} + () \hat{\mathbf{z}} \\
 &\simeq \frac{\Delta \mathbf{v}(\mathbf{r})}{3}.
 \end{aligned}$$

Note: Projection and velocity gradient issues avoided with reconstruction

Dustybox

Initially: homogeneous mixture $\rho_d = \rho_{d,0}$, $\rho_g = \rho_{g,0}$

$$\begin{aligned}\frac{\partial v_g}{\partial t} &= \frac{K}{\rho_{g,0}} (v_g - v_d), \\ \frac{\partial v_d}{\partial t} &= -\frac{K}{\rho_{d,0}} (v_g - v_d).\end{aligned}$$

reach barycentric velocity

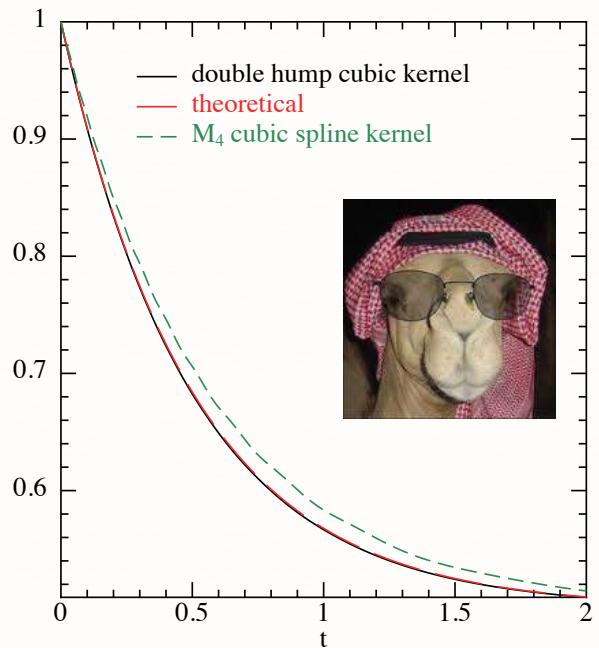
$$\begin{aligned}v_d &= v_0 - \frac{\rho_{g,0}}{\rho_{d,0} + \rho_{g,0}} \Delta v_0 e^{-t/t_s}, \\ v_g &= v_0 + \frac{\rho_{d,0}}{\rho_{d,0} + \rho_{g,0}} \Delta v_0 e^{-t/t_s}.\end{aligned}$$

barycentric stopping time

damps differential velocity

$$t_s \equiv \frac{K(\rho_{d,0} + \rho_{g,0})}{\rho_{d,0}\rho_{g,0}}$$

$$v_0 \equiv \frac{\rho_{g,0}v_{g,0} + \rho_{d,0}v_{d,0}}{\rho_{g,0} + \rho_{d,0}}$$



$$\Delta v_0 \equiv v_{d,0} - v_{g,0}$$

Let diagonalise the system:

$$\frac{\partial}{\partial t} \begin{pmatrix} v \\ \Delta v \end{pmatrix} = \begin{pmatrix} 0 & 0 \\ 0 & 1/t_s \end{pmatrix} \begin{pmatrix} v \\ \Delta v \end{pmatrix} \quad \longrightarrow$$

$$v = \text{cste}$$

$$\Delta v = \Delta v_0 e^{-t/t_s}$$

One fluid description

One fluid, two phases:

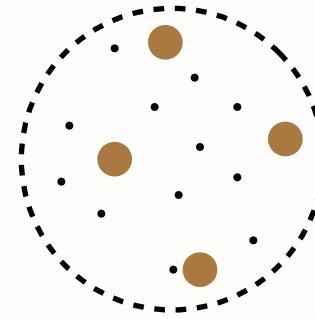
$$\rho \equiv \rho_g + \rho_d$$

$$\epsilon \equiv \rho_d / \rho$$

$$\tilde{u} = u(1 - \epsilon)$$

$$\mathbf{v} \equiv \frac{\rho_g v_g + \rho_d v_d}{\rho_g + \rho_d}$$

$$\Delta \mathbf{v} \equiv \mathbf{v}_d - \mathbf{v}_g$$



Conservation equations:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\rho \left(\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right) = \nabla P + \rho \mathbf{g} - \nabla (\epsilon (1 - \epsilon) \rho \Delta \mathbf{v} \Delta \mathbf{v})$$

$$\rho \frac{d\epsilon}{dt} = -\nabla (\epsilon (1 - \epsilon) \rho \Delta \mathbf{v})$$

$$\frac{d\Delta \mathbf{v}}{dt} = -\frac{\Delta \mathbf{v}}{t_s} + \frac{\nabla P}{(1 - \epsilon) \rho_g} - (\Delta \mathbf{v} \cdot \nabla) \mathbf{v} + \frac{1}{2} \nabla ((2\epsilon - 1) \Delta \mathbf{v} \Delta \mathbf{v})$$

$$\rho \frac{d\tilde{u}}{dt} = P \nabla (\mathbf{v} - \epsilon \Delta \mathbf{v}) + \epsilon (1 - \epsilon) \frac{\Delta \mathbf{v}^2}{t_s}$$

$$\rho, \mathbf{v} \quad \frac{d}{dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla$$

one advection velocity

Infinite drag limit

When $t_s = 0$, $\Delta v = 0$.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

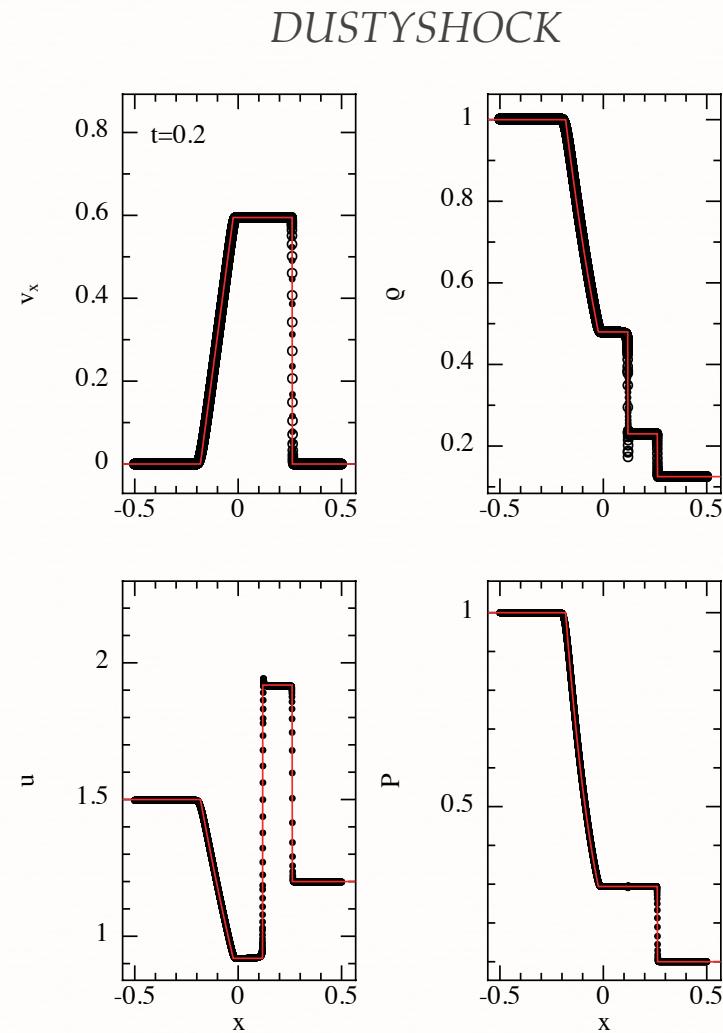
$$\rho \left(\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right) = \nabla P + \rho \mathbf{g}$$

$$\longrightarrow \tilde{c}_s = c_s \left(1 + \frac{\rho_d}{\rho_g} \right)^{-1/2}$$

Physically:

$$\tilde{c}_s = \sqrt{\frac{\text{stiffness}}{\text{inertia}}}$$

$$\rho_g \rightarrow \rho = \rho_g / (1 - \epsilon)$$



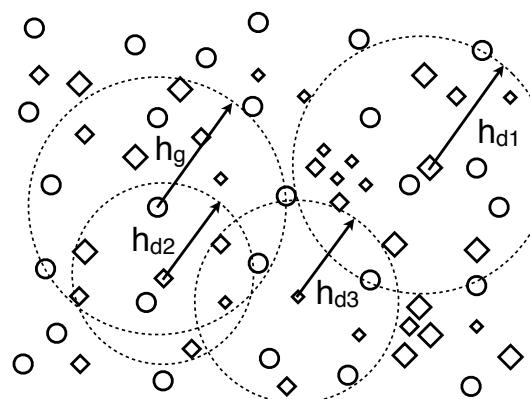
Gas accounts for the mass of the dust, transmitted instantaneously by the drag

Some comments

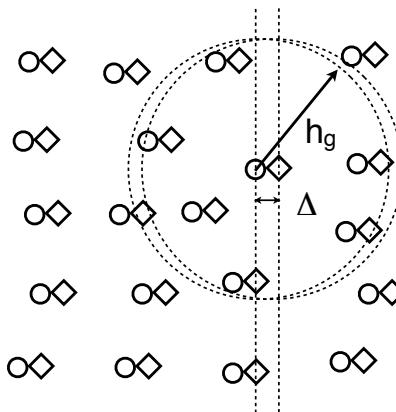
Main advantages of two fluid dust with SPH:

- Exact orbits in the zero-drag limit
- Track the history of the particle
- Allows dust interpenetration
- Sharp dust-gas discontinuities

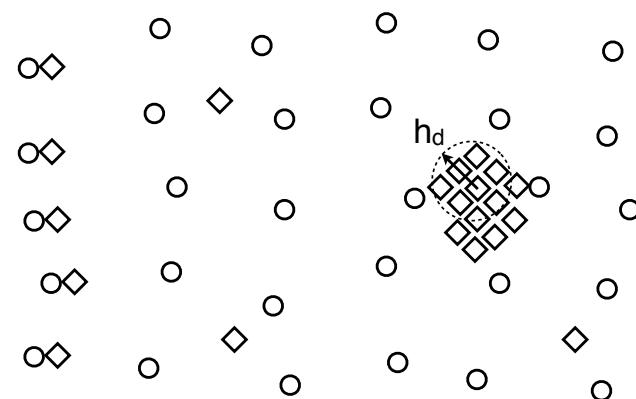
But:



interpolation issues
for multiple sizes



$h > c_s t_s ?$



↳ numerical artefacts !