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CALCULATED RADIOACTIVITY OF MSRE FUEL SALT

M. J. Bell

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### CALCULATED RADIOACTIVITY OF MSRE FUEL SALT

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### ABSTRACT

Calculations have been made of the inventory and radioactivity of the fission product and transuranium isotopes present in the MSRE fuel salt. The calculations have included operation with both <sup>235</sup>U and <sup>233</sup>U fuels, the effect of stripping of noble gases, and fluorination of the fuel salt after the period of <sup>235</sup>U operation. Results are presented which give the inventory and radioactivity of individual isotopes in the salt up to January 1, 1975.

### INTRODUCTION

The Molten Salt Reactor Experiment at ORNL was first operated at full power in May 1966. Since that time the reactor has been operated for over 100,000 Mwhr with both  $^{235}$ U and  $^{233}$ U fuels.  $^2$  In August 1968 the fuel salt was processed by fluorination to remove the 235 U fuel originally charged, and the reactor was then fueled with 233U prepared at the TURF facility at ORNL. In October 1968 the MSRE became the first reactor to operate with  $^{233}\mathrm{U}$  fuel. Power operation with  $^{233}\mathrm{U}$ fuel began in January 1969, and operation of the reactor was terminated on December 12, 1969. The fuel salt was drained and is being stored prior to permanent disposal. Estimates of the composition and radioactivity of the fission products present in the fuel salt drain tank are required to provide for safe storage and disposal of the salt. Such estimates should take into account, in as much detail as possible. the operating history and chemical processing history of the fuel salt. These estimates were made using a modification of the ORIGEN isotope generation and depletion code which took into account continuous chemical processing. Calculated results are presented which describe the composition and radioactivity of the fuel salt after 235U operation and after operation with <sup>233</sup>U.

### COMPUTATIONAL PROCEDURE

Estimates of the composition and radioactivity of the MSRE fuel salt were made using a modification of the ORIGEN isotope generation and depletion code which took into account continuous stripping of the noble gases Xe and Kr. 3 During periods of power operation, it was assumed that noble gas stripping took place on a 487-sec cycle with an efficiency of 38%. It was also assumed that tritium was removed at the same rate. In the calculations the power history of the fuel salt was approximated by the series of increments of constant average power shown in Table 1. Between periods of operation the fuel salt was drained on a number of occasions and a "heel" of approximately 10% of the total salt volume remained in the drain tank every time the salt was returned to the reactor. This behavior was taken into account using the same "flux-dilution" technique applied to the circulating fuel salt, i.e., the entire salt inventory was assumed to be exposed to a proportionately lower neutron flux. Nuclear data used for the calculation was that compiled for the MATADOR steady state material balance code.  $^{ extstyle l}$ Three group spectral constants were derived from the data of Prince. 5,6

During the period of operation of the MSRE additions of uranium were made to the fuel salt which amounted to approximately 2% of the uranium inventory. These additions were neglected in the present calculations. This approximation has the effect of raising the neutron flux required to maintain the fission rate at the specified level by less than 2%, and is expected to have a negligible effect on the radioactivity of the fuel salt.

During a six-day period in August 1968 the MSRE fuel salt was fluorinated to remove <sup>235</sup>U before beginning operation with <sup>233</sup>U. This processing also removed all those fission products having stable volatile fluorides and any Np present in the salt. In addition, the remaining noble gases and the halogens, Br and I, would also be expected to leave the salt. Accordingly, 100% of the elements H, He, Se, Br, Kr, Nb, Mo, Tc, Ru, Te, I, Xe, U and Np were removed from the salt 157 days after the end of power operation with <sup>235</sup>U.

Table 1. Approximate Power History of MSRE Fuel Salt

Period Ending	Time Elapsed (days)	Avg. Power This Period (Mw)	Cumulative Burnup (Mwhr)	Comments
4/11/66	0	0	0	First approach to full power
10/13/66	185	1.76	7823	
11/17/66	220	4.51	11611	
12/14/66	247	0	11611	
1/14/67	278	7.81	17420	
1/28/67	292	0	17420	
5/8/67	392	7.49	35385	
6/22/67	437	0	35385	
9/18/67	494	6.56	44362	
10/21/67	528	0	<b>Ա</b> 4362	
3/25/68	714	6.10	71580	End of <sup>235</sup> U operation
9/29/68	871	0	71580	End of <sup>235</sup> U processing
1/14/69	1009	0	71580	Beginning of <sup>233</sup> U full power operation
5/31/69	1146	6.19	91944	
9/22/69	1229	0	91944	
10/1/69	1268	4.20	95877	
11/2/69	1301	7.44	101770	
11/25/69	1324	0	101770	
12/12/69	1341	7.61	104816	End of <sup>233</sup> U operation

### COMPUTATIONAL RESULTS

The calculated inventories of fission products and transuranium elements present in the MSRE fuel salt after the termination of operation with  $^{235}\text{U}$  fuel are shown in Tables 2 and 3. The inventories at 157 days after shutdown reflect the removal of noble gases, halogens, and elements with volatile stable fluorides by fluorination in August 1968. It was assumed that 100% of these elements was removed. The remaining times past 157 days cooling correspond to the period before power operation with  $^{233}\text{U}$  fuel. The radioactivity of these isotopes for the same period is given in Tables 4 and 5. The computed activity of the fuel salt prior to the start of  $^{233}\text{U}$  operation is 0.289 x  $10^6$  curies.

The  $^{233}$ U charged to the MSRE for the second period of power operation had been purified by solvent extraction and ion exchange in 1964 and 1965. The isotopic composition of this material after purification was 84.6%  $^{233}$ U, 6.93%  $^{234}$ U, 2.44%  $^{235}$ U, 0.15%  $^{236}$ U, 5.87%  $^{238}$ U, and the uranium contained approximately 225 parts per million  $^{232}$ U. Table 6 shows the increase in radioactivity of this material during the period that elapsed between purification of the uranium and power operation of the MSRE with  $^{233}$ U fuel. The radioactivity of the uranium reaches a level of  $1.53 \times 10^3$  curies as a result of the presence of  $^{228}$ Th and its daughters.

Tables 7 and 8 give the transuranium element and fission product inventories in the fuel salt at the end of  $^{233}\text{U}$  power operation and as a function of time after shutdown. The radioactivity corresponding to these isotopes is given in Tables 9 and 10. The results indicate that 5.88 x  $10^{14}$  curies of radioactivity will remain in the fuel salt after 5 years cooling time. About 1% of the long lived radioactivity will result from transuranium elements, in particular, from  $^{232}\text{U}$  and its daughters. Of the fission product activity, greater than 98% is due to isotopes which form very stable fluoride salts. Approximately 1% of the fission product radioactivity is the result of isotopes of noble metals which would not be expected to remain dissolved in the salt.

Table 2. Fission Product Inventory of MSRE Fuel Salt After Period of  $$^{235}\!\text{U}$$  Operation as a Function of Time After Shutdown

POWER=	4.18 M	IW BURN	UP= 29	83. MWD	FLUX=	2.35E 12	N/CM**2-SEC
NUCLID		RATIONS, G	_	30.5		157 0	205 D
C		DISCHARGE	3.0 D			157. D	
SE 80 BR 81	0.0 0.0				0 1.06E 00 0 1.51E 00		0.0
SE 82	0.0				3.48E 00		0.0
RB 87	0.0				4.67E 00		
SR 88	0.0				3.37E 00		
SR 89	0.0				2.06E 00		
Y 89	0.0				1 4.47E 01		
SR 90	0.0				1 6.48E C1		
ZR 90	0.0				1.69E 00		
Y 91	0.0				3.97E 00		
ZR 91	0.0				6.60E 01		
ZR 92	0.0	7.34E 01	7.35E 01	7.35E 0	1 7.35E C1	7.35E 01	7.35E 01
ZR 93	0.0	7.95E 01	7.97E 01	7.97E 0	1 7.97E 01	7.97E 01	7.97E 01
ZR 94	0.0	7.99E 01	7.99E 01	7.99E 0	L 7.99E 01	7.99E 01	7.99E 01
ZR 95	0.0	1.41E 01	1.36E 01	1.02E 0	1 5.40E 00	2.64E 00	6.06E-01
NB 95	0.0				4.74E 00		5.07E-01
MO 95	0.0				6.83E 01		1.53E 00
ZR 96	0.0				8.08E 01		
MO 97	0.0		-		1 7.89E 01		0.0
MO 98	0.0				7.56E 01		0.0
TC 99	0.0				8.20E 01		0.0
MO100	0.0				1 8.42E 01		0.0
RU101	0.0 0.0				1 6.75E 01 1 5.62E 01		0.0
RU102 RU103	0.0				9.97E-01		0.0
RH103	0.0				4.03E 01		
RU104	0.0				2.58E 01		0.0
PD105	0.0				1.34E 01		
RU106	0.0				3.32E 00		0.0
PD106	0.0				3.19E 00		
PD107	0.0				3.42E 00		
PD1 08	0.0	1.46E 00	1.46E 00	1.46E 00	1.46E 00	1.46E 00	1.46E 00
1127	0.0	2.18E 00	2.20E 00	2.23E 00	2.27E 00	0.0	0.0
TE128	0.0	7.18E 00	7.19E 00	7.19E 00	7.19E 00	0.0	0.0
1129	0.0				1.40E 01		0.0
TE130	0.0				3.48E 01		0.0
XE1 31	0.0				1.25E 00		0.0
CS135	0.0				2.66E 00		
CS137	0.0				8.75E 01		
BA137	0.0				2.13E 00 4.93E 01		
BA138 LA139	0.0				1.17E 02		
CE140	0.0				1.36E 02		
CE141	0.0				1.67E 00		
PR141	0.0				1.18E 02		
CE142	0.0				1.14E 02		
PR143	0.0				5.13E-02		
ND143	0.0				1.13E 02		
CE144	0.0				4.67E 01		

Table 2 (Continued)

POWER =	4.13 M	W BUF	NUP= 29	83. MWD	FLUX=	2.35E 12	N/CM**2-SEC
NUCLID		RATIONS, ( DISCHARGE		30.C [	90. D	157. (	295.0
ND144	0.0	5.07F 01	5.11E 01	5.48E C1	6.21E 01	6.92E 0	8.05E 01
ND145	0.0	7.65F 01	7.66E 01	7.66E 01	7.66E 01	7.66E 01	7.66E 01
ND145	0.0	5.99E 01	5.99E 01	5.99E 01	5.99E 01	5.99E 0	1 5.99E 01
PM147	0.0	3.70E 01	3.71F 01	3.74E 01	3.61E 01	3.43E 0	3.11E 01
SM147	0.0	8.155 00	9.23E 00	8.97E 00	1.06E 01	1.23E 0	1.55E 01
ND148	0.0	3.38F 01	3.38F 01	3.38E 01	3.38E 01	3.38E 0	1 3.38E 01
SM148	0.0	1.34E 00	1.35E CC	1.39E 00	1.40E 00	1.40E 0	1.40E 00
SM149	0.0	3.63E 00	3.73E 00	3.79E 00	3.79E 00	3.79E 00	3.79E 00
NC150	0.0	1.35E 01	1.35E 01	1.35E 01	1.35E C1	1.35E 0	1 1.35E 01
SM150	0.0	1.92E 01	1.925 01	1.92E 01	1.92E 01	1.92E 0	1.92E 01
SM151	0.0	7.21E 00	7.24E 00	7.24E 00	7.23E 00	7.22E 00	7.20E 00
SM152	0.0	7.41E 00	7.41E 00	7.41F 00	7.41E 00	7.415 00	7.41E 00
EU153	0.0	3.68F 00	3.69F 00	3.70E 00	3.70E 00	3.70E 0	3.70E 00
SM154	0.0	1.65E 00	1.65E 00	1.65E 00	1.65E 00	1.65E 00	1.65E 00
SUBTOT	0.0	2.30E 03	2.30E 03	2.31E 03	2.31E 03	1.70E 0	3 1.70E 03
TOTALS	0.0	2.32E 03	2.32E C3	2.32E 03	2.32E 03	1.70E 0	3 1.70E 03

Table 3. Transuranium Isotope Inventory of MSRE Fuel Salt After Period of  $^{235}\text{U}$  Operation as a Function of Time After Shutdown

POWER=	4.18	3 MV		PURNUP=	29	83. MWD	F	LUX=	2.35E	12	N/CM**2-SEC	
NUCLIDE	CONCE	ENTF	RATION!	S. GRAMS								
			-	RGE 3.		30.0	D '	90. D	157	• D	295. D	
U234				02 7.76	-	-					1.54E-04	
U2 35				04 7.098			_				6.52E-03	
U236	. •			03 1.038							1.06E-03	
U238				05 1.488							1.24E-08	
	•••	0)		00 3.548							4.30E-05	
NP237	0.0											
PU239	0.0		6.13E	02 6.168	02	6.18E 0	2 6.1	BE 02	6.18E	02	6.18E 02	
PU240	0.0		2.77E	01 2.776	01	2.77E 0	1 2.7	7E 01	2.77E	Cl	2.77E 01	
PU241	0.0		1.478	00 1.476	00	1.46E 0	0 1.4	5E 00	1.44E	00	1.41E GO	
SUBTOT	2.25E	05	2-22F	05 2-22	0.5	2.22F 0	5 2.2	2E 05	6.47F	02	6.47E 02	
555151				~ <b></b>								
ZOTALS	2 - 25E	05	2.226	05 2.228	- 05	2.22F 0	5 2.2	2F 05	6.47F	02	6.47E 02	

Table 4. Fission Product Radioactivity of MSRE Fuel Salt After Period of  $^{235}\text{U}$  Operation as a Function of Time After Shutdown

POWER=	4.18 M	8UR	NUP=	2983	B. MWE	:	FLUX=	2.35E 12	N/CM**2-SEC
NUCLIDE		TIVITY, C		n	30.0	. n	90. D	157	D 295. D
SR 89	0.0								4 3.78E 03
									3 9.04E 03
	0.0								3 9.04E 03
	0.0								4 8.65E 03
ZR 95	0.0								4 1.28E 04
NB 95M	0.0						2.43E 03		2.72E 02
NB 95	0.0						1.86E 05		1.99E 04
	0.0						6.12E-05		0.0
TC 99M							5.85E-C5		0.0
	0.0						1.40E 00		Q.0
	0.0						3.19E 04		
RH1 03M							3.20E 04		
	0.0 6.0		-				1.11E 04 1.11E 04		0.0 3.0.0
	0.0								4 1.87E-09
CD115M									0 3.12E-01
SN119M	-						8.60E-01		0.0
SN123M							3.67E 01		0.0
	0.0	2.09E 00	2.02E	00 1	.48E	00	7.41E-01	0.0	0.0
SN125	0.0						9.85E-C1		0.0
SB125	0.0	3.33E 02	3.34E	02 3	. 34E	02	3.21E 02	0.0	0.0
TE125M	0.0						1.22E 02		0.0
	0.0						8.37E 00		0.0
SB127							7.88E-04		0.0
TE127M							8.04E 02		0.0
	0.0						7.95E 02		0.0
TE129M							2.44E 03		0.0
	0.0						1.56E C3		0.0
I131 XE131M	0.0						6.69E 01 1.23E 01		0.0 0.0
TE132							1.03E-03		0.0
	0.0						1.07E-C3		0.0
	0.0						5.14E-01		0.0
	0.0								0 9.64E-01
C S 1 3 6	0.0								1 7.64E-05
CS137	0.0	7.66E 03	7.66E	03 7	7. 64E	03	7.61E C3	7.58E 0	3 7.52E 03
BA137M	0.0	7.16E 03	7.16E	03 7	.15E	03	7.12E 03	7.09E 0	3 7.03F 03
BA140	0.0	3.20E 05	2.72E	C5 6	.31E	04	2.45E 03	6.50E 0	1 3.72E-02
	0.0								1 4.28E-02
CE141									4 5.93E 02
	0.0								2 1.07E-01
	0.0								5 9.04E 04
_	0.0								5 9.04E 04 0 1.21E-03
	0.0								4 2.89E 04
PM147									1 4.14E 00
	0.0								0 3.33E-01
<del>-</del>	0.0						3.44E-08		
-	0.0								2 1.96E 02

# Table 4 (Continued)

POWER=	4.18 M	W BUR	NUP= 29	983. MWD	FLUX=	2.35E 12	N/CM**2-SEC
NUCLIDE		TIVITY, CO		30.0 D	90. D	157. D	295. D
EU152	0.0	1.15E 00	1.15E 00	1.15E 00	1.14E 00	1.13E 00	1.10E 00
EU154	0.0			1 1.26E 01			
EU155	0.0	4.69E 02	4.68E C	2 4.55E 02	4.27E 02	3.98E 02	3.45E 02
EU156	0.0			3 4.74E 02			
GD162	0.0	2.15E 00	2.14E 00	2.03E 00	1.81E CO	1.59E 00	1.23E 00
T8162M	0.0	2.15E 00	2.14E 00	2.03E 00	1.81E 00	1.59E 00	1.23E 00
SUBTOT	0.0	4.52E 06	3.79E C	6 1.87E 06	9.73E 05	4.74E 05	2.89E 05
TOTALS	0-0	2.645 07	3.97F 04	5 1.87E 06	9.73E 05	4.74F 05	2.89F 05

Table 5. Transuranium Isotope Radioactivity of MSRE Fuel Salt After Period of  $^{235}\text{U}$  Operation as a Function of Time After Shutdown

POWER=	4.18	3 M	A !	BURI	NUP=	298	3. MW	)	FLUX=	2.35E	12	N/CM**2-SEC
NUCLID				•		_					_	
						_		_			• D	295 D
U2 34	4.87E	90	4.80E	ÇO	4.60E	CO	4.80E	00	4.80E C	0.0		9.55E-07
U237	Ŭ•O		9.55E	С3	7.02E	03	4.39E	02	9.25E-0	1 0.0		0.0
NP239	0.0		1.11E	06	4.60E	05	1.60E	02	3.30E-0	5 0.0		1.59E-05
PU239	0.0		3.76E	01	3.785	01	3.795	01	3.79E 0	1 3.798	01	3.79E 01
PU240	0.0		6.12E	GO	6.12E	00	6.12E	00	6.12E 0	6.12E	00	6.12E 00
PU241	0.0		1.685	02	1.68E	C2	1.67E	02	1.66E 0	2 1.64E	02	1.61E 02
CM242	0.0		1.45E	00	1.46E	00	1.30E	CO	1.01E C	7.57E	-01	4.22E-01
SUBTOT	4.87E	00	1.12E	06	4.67E	05	8.16E	02	2.16F 0	2 2.09E	02	2.05E 02
TOTALS	4.94E	00	2.225	06	4.68F	05	8.17E	02	2.18E 0	2 2.10E	02	2.06E 02

Table 6. Radioactivity of Enriching <sup>233</sup>U Used to Fuel MSRE as a Function of Postpurification Time

# MSRE 233-U FUEL COMPOSITION AFTER PURIFICATION

NUCLID	E RADIOAC	TIVITY, C	URIES			
	INITIAL	366.0 D		1098. D	1464. D	1830. D
TL208	0.0	1.97E 01	3.33E 01	4.25E 01	4.87E C1	5.29E 01
PB212	0.0	5.48E 01	9.24E 01	1.19E 02	1.35E 02	1.47E 02
B1212	0.0	5.48E 01	9.24E 01	1.18E C2	1.35E 02	1.47E 02
P0212	0.0	3.51E C1	5.92E 01	7.56E 01	8.66E 01	9.4CE 01
P0216	0.0	5.485 01	9.24E 01	1.18E 02	1.35E 02	1.47E 02
RN220	0.0			1.18E 02		
R A2 24	0.0			1.18E C2		
TH228	0.0	5.48E 01	9.24E 01	1.18E 02	1.35E C2	1.47E 02
TH229	0.0	3.10E-G2	6.20E-02	9.31E-02	1.24E-01	1.55E-01
U2 32	1.81E 02	1.798 02	1.77E C2	1.76E C2	1.74E C2	1.72E 02
U233	3.26E 02	3.26E 02	3.26E 02	3.26E C2	3.26E C2	3.26E 02
U234	1.74E 01	1.74E C1	1.74E C1	1.74E 01	1.74E 01	1.74E 01
U2 36	3.87E-03	3.87F-03	3.87E-03	3.97E-03	3.87E-03	3.87E-03
SUBTOT	5.24E G2	9.07E 02	1.17E 03	1.35E 03	1.47E 03	1.54E 03
TOTALS	5.248 02	9.07E 02	1.17E 03	1.35E 03	1.47E C3	1.54E 03

Table 7. Fission Product Inventory of MSRE Fuel Salt After Period of <sup>233</sup>U Operation as a Function of Time After Shutdown

FLUX= 3.89E 12 N/CM\*\*2-SEC POWER = 4.18 MW **BURNUP=** 1387. MWD NUCLIDE CONCENTRATIONS, GRAMS CHARGE DISCHARGE 384.0 C 749.C D 1115. D 1480. D 1845. D **RB 37** 4.67E 00 8.48E 00 8.48E 00 8.48E 00 8.48E 00 8.48E 00 8.48E 00 SR 88 3.37E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 Y 89 4.66E 01 6.66E 01 7.23E 01 7.24E 01 7.24E 01 7.24E 01 7.24E 01 6.39E 01 9.55E 01 9.31E 01 9.08E 01 8.86E 01 8.65E 01 8.44E 01 SR 90 2.58E 00 4.44E 00 5.91E 00 9.18E 00 1.14E 01 1.36E 01 1.57E 01 6.96E 01 9.73E 01 1.05E 02 1.05E 02 1.05E 02 1.05E 02 1.05E 02 7.35E 01 1.1CE 02 1.10F 02 1.10E 02 1.10E 02 1.10E 02 1.10E 02 7.97E 01 1.19E 02 1.19E 02 1.19E 02 1.19E 02 1.19E 02 1.19E 02 ZR 90 ZR 91 ZR 92 ZR 93 7.99E 01 1.18E 02 1.18E 02 1.18E 02 1.18E 02 1.18E 02 1.18E 02 ZR 94 1.53E 00 2.44E 01 3.92F 01 3.97E 01 3.97E 01 3.97E 01 3.97E 01 MO 95 3.08E 01 1.14E 02 1.14E 02 1.14E 02 1.14E 02 1.14E 02 1.14E 02 ZR 96 MO 97 0.0 3.25E 01 3.25F 01 3.25E 01 3.25E 01 3.25E 01 3.25E 01 MO 98 3.16E 01 3.16E 01 3.16E 01 3.16E 01 3.16E 01 3.16E 01 0.0 2.98F 01 2.99E 01 2.99E 01 2.99E 01 2.99E 01 2.99F 01 TC 99 0.0 MO100 2.85E C1 2.85E C1 2.85E C1 2.85E C1 2.85E C1 2.85E O1 0.0 1.95E 01 1.95E C1 1.95E 01 1.95E 01 1.95E 01 1.95E 01 **RU101** 0.0 0.0 1.56E 01 1.56F 01 1.56E 01 1.56E 01 1.56E 01 1.56E 01 4.10E 01 5.07E 01 5.30E 01 5.30E 01 5.30E 01 5.30E 01 5.30E 01 0.0 7.88E 00 RU102 **RH103 RU104** 1.34E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01 PD105 3.58E 00 4.61E 00 5.76E 00 6.30E 00 6.57E 00 6.71E 00 6.77E 00 PD106 3.41E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 5.64E 00 PD107 0.0 9.46E 00 9.47E 00 9.47E 00 9.47E 00 9.47E 00 9.47E 00 TE128 1.49E 01 1.58E 01 1.58E 01 1.58E 01 1.58E 01 1.58E 01 1129 0.0 **TE130** 2.09E 01 2.09E 01 2.09E 01 2.09E 01 2.09E 01 2.09E 01 0.0 8.63E 01 1.28E 02 1.25E 02 1.23E 02 1.20E 02 1.17E 02 1.14E 02 CS137 3.26E CO 5.56F OO 8.65F OC 1.15E O1 1.43E C1 1.70F O1 1.97F O1 **BA137** 4.93E 01 7.44E 01 7.44E 01 7.44E 01 7.44E 01 7.44E 01 7.44E 01 **BA138** 1.17E 02 1.70E C2 1.70E 02 1.70E 02 1.70E C2 1.70E 02 1.70E 02 1.36E 02 1.89E C2 1.90E C2 1.90E 02 1.90E 02 1.90E 02 1.90E 02 1.90E 02 1.90E 02 1.84E 02 1.84E 02 1.84E 02 1.84E 02 1.84E 02 1.73E 02 1.73E 02 1.73E 02 1.73E 02 1.73E 02 1.73E 02 LA139 CE 140 PR141 CE142 1.13E 02 1.67E 02 1.73E 02 1.73E 02 1.73E 02 1.73E 02 1.73E 02 ND143 2.84E 01 3.98E 01 1.56E 01 6.40E 00 2.62E CC 1.07E 00 4.41E-01 **CE144** ND144 8.05E 01 1.13F 02 1.37E 02 1.46E 02 1.50E 02 1.52E 02 1.52E 02 7.66E 01 1.07E 02 1.07E 02 1.07E 02 1.07E 02 1.07E 02 1.07E 02 ND145 5.99E 01 8.41E 01 8.41F 01 8.41F C1 8.41E C1 8.41E 01 8.41E 01 ND146 3.10E 01 4.01E 01 3.16E 01 2.42E 01 1.86E 01 1.43E 01 1.10E 01 PM147 1.56E 01 2.39E 01 3.40E 01 4.14E 01 4.70E 01 5.13E 01 5.46F 01 SM147 3.37E 01 4.63E 01 4.63E 01 4.63E 01 4.63E 01 4.63E 01 4.63E 01 ND148 1.35E 01 1.90F 01 1.90E 01 1.90E 01 1.90E 01 1.90E 01 1.90E 01 ND150 SM150 1.92E 01 2.71E 01 2.71E 01 2.71E 01 2.71E 01 2.71E 01 2.71E 01 7.20E 00 5.39E 00 5.38E 00 5.33E 00 5.29E 00 5.25E 00 5.21E 00 SM151 7.42E 00 1.46E 01 1.46E 01 1.46E 01 1.46E 01 1.46E 01 1.46E 01 SM152 3.70E CO 5.45E CO 5.49E CO 5.49E CO 5.49E CO 5.49E CO 5.49E OO EU153 SUBTOT 1.685 03 2.66E 03 2.71E 03 2.71E 03 2.71E 03 2.71E 03 2.71E 03

TOTALS 1.70E 03 2.76E C3 2.76E C3 2.76E C3 2.76E C3 2.76E C3 2.76E C3

Table 8. Transuranium Isotope Inventory of MSRE Fuel Salt After Period of <sup>233</sup>U Operation as a Function of Time After Shutdown

```
BURNUP=
                                                                                                                     1387. MWD
                                                                                                                                                                         FLUX = 3.89E 12 N/CM**2-SEC
POWER=
                                 4.18 MW
NUCLIDE CONCENTRATIONS, GRAMS
                              CHARGE DISCHARGE 384.0 D 749.C D 1115. D 1480. D 1845. D
                           8.05E 00 7.86E 00 7.78E 00 7.71E 00 7.64E 00 7.56E 00 7.49E 00
    U232
    U233 3.45E 04 3.30E 04 3.30E 04 3.30E C4 3.30E 04 3.30E 04 3.30E 04
                       2.81E 03 2.94E 03 2.94E 03 2.94E 03 2.94E 03 2.94E 03 2.94E 03 9.94E 02 9.86E 02 9.8
   U234
    U235
   U236
   U238
                        7.48E 02 6.31E 02 6.31E 02 6.31E 02 6.31E 02 6.31E 02 6.31E 02
PU239
PU240 3.62E 01 7.74E 01 7.74E 01 7.74E 01 7.74E 01 7.74E 01 7.74E 01
PU241 1.41E 00 7.89E 00 7.46E 00 7.08E 00 6.71E CO 6.36E 00 6.03E 00
SUBTOT 4.15E 04 4.01E 04 4.01E 04 4.01E 04 4.01E 04 4.01E 04 4.01E 04
TOTALS 4.15E 04 4.01E 04 4.01F 04 4.01E 04 4.01E 04 4.01E 04 4.01E 04
```

Table 9. Fission Product Radioactivity of MSRE Fuel Salt After Period of <sup>233</sup>U Operation as a Function of Time After Shutdown

FLUX= 3.89E 12 N/CM\*\*2-SEC POWER= 4.18 MW BURNUP= 1387. MWC NUCLIDE RADIOACTIVITY, CURIES 384.0 D 749.0 D 1115. D 1480. D 1845. D CHARGE DISCHARGE 3.77E 03 1.62F 05 9.72F 02 3.00E C1 9.12E-01 2.81E-02 8.67E-04 9.04E C3 1.35E 04 1.32F C4 1.28E 04 1.25E 04 1.22E 04 1.19E 04 SR 90 Y 90 9.06E 03 1.36E 04 1.32E 04 1.28E 04 1.25E 04 1.22E 04 1.19E 04 8.64E 03 1.83E C5 1.99E C3 5.38E 01 2.88E C0 1.56E-01 8.43E-03 Y 91 1.28E 04 2.00F C5 3.33F 03 1.36E 02 1.10E 01 8.96E-01 7.31E-02 ZR 95 NB 95M 2.72E 02 4.15E 03 7.08E C1 1.44E 00 1.17E-C1 9.51E-03 7.76E-04 1.99E 04 1.72E 05 8.30F 03 1.78E 02 1.29E 01 1.05E 00 8.56E-02 7.40E 04 9.92E 01 5.99E-01 3.96E-03 2.66F-05 1.79E-07 7.40E 04 8.92E 01 3.00E-01 1.98E-03 1.33E-05 8.94E-08 7.49E 03 3.63E 03 1.82E 03 9.12E 02 4.58F 02 2.30E 02 8.95E 03 3.63E 03 1.82E 03 9.12E 02 4.58E 02 2.30F 02 1.39E 02 1.65F 01 2.18E 00 2.86E-01 1.51E-01 7.99E-02 RU103 0.0 RH103M 0.0 RU106 0.0 RH106 0.0 SN123M 0.0 SB125 0.0 6.38E 02 5.12E 02 3.96E 02 3.06E 02 2.37E 02 1.83E 02 1.97E 02 2.11E 02 1.85E 02 1.45E 02 1.12E 02 8.70E 01 TE125M 0.0 TE127M 0.0 3.94F 03 3.70E 02 3.63E 01 7.08E 00 2.78E 00 1.09E 00 3.28E 04 3.65E 02 3.59E 01 3.50E 00 1.37E 00 5.39F-01 TE127 0.0 2.67E 04 2.15E 01 5.06E-02 1.16E-04 2.73E-07 6.40E-10 TE129M 0.0 9.79F 04 6.91F 00 1.62E-02 3.73E-C5 8.74E-08 2.05E-10 TE129 0.0 CS134 9.63E-01 5.52E 0C 3.87E 0C 2.76E 0D 1.97E CD 1.40E 0C 1.00E 0D CS137 7.51E 03 1.12F 04 1.09E 04 1.07E C4 1.04E C4 1.02E 04 9.95E 03 BA137M 7.03E 03 1.05E 04 1.02F 04 9.97E 03 9.74E C3 9.52E 03 9.30E 03 CE141 5.93E 02 4.10E 05 2.23E 02 3.63E-01 5.77E-04 9.37E-07 1.52E-09 9.06E 04 1.27E 05 4.98E 04 2.04E 04 8.37E 03 3.43E 03 1.41F 03 CE144 9.05E 04 1.28E 05 4.98E 04 2.04E 04 8.37E 03 3.43E 03 1.41E 03 PR144 PM147 2.88E 04 3.72F C4 2.93E 04 2.25E C4 1.73E 04 1.33E 04 1.02E 04 PM148M 4.14E 00 1.05E 03 1.86E 00 1.80E-02 1.72E-04 1.66E-06 1.61E-08 SM151 1.96E 02 1.47E 02 1.46E 02 1.45E 02 1.44E 02 1.43F 02 1.42E 02 1.10E 00 5.38E CO 5.06E CO 4.78E 00 4.51E CO 4.26E 00 4.02E 00 EU152 EU154 1.22E 01 3.52E 01 3.36E 01 3.22E 01 3.08E 01 2.95E 01 2.83E 01 EU155 3.44E 02 3.55E 02 2.38F 02 1.62E 02 1.10E 02 7.53E 01 5.14E 01 GD162 1.23E 00 2.74E 00 1.32E 00 6.61E-01 3.30E-01 1.65E-01 8.27E-02 TB162M 1.23E 00 2.74E 00 1.32F 00 6.61E-01 3.30E-01 1.65E-01 8.27E-02 SUBTOT 2.89E 05 1.80E 06 2.01E 05 1.15E 05 8.18E 04 6.58E 04 5.71E 04 TOTALS 2.89E 05 3.10E 07 2.01E C5 1.15E 05 8.18E C4 6.58E 04 5.71E 04

Table 10. Transuranium Isotope Radioactivity of MSRE Fuel Salt After Period of <sup>233</sup>U Operation as a Function of Time After Shutdown

```
BURNUP=
                                         1387. MWD
                                                          FLUX= 3.89E 12 N/CM**2-SEC
POWER=
            4.18 MW
NUCLIDE RADIOACTIVITY, CURIES
          CHARGE DISCHARGE 384.0 D 749.0 D 1115. D 1480. D 1845. D
TL208
         5.29E 01 5.49E 01 5.66E 01 5.76E 01 5.80E 01 5.81E 01 5.82E 01
        1.47E 02 1.53E 02 1.57F 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02
PB212
        1.47E 02 1.53E 02 1.57F 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02 9.40E 01 9.76E 01 1.01E 02 1.60E 02 1.61E 02 1.62E 02 1.03E 02 1.47E 02 1.53E 02 1.57E 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02 1.47E 02 1.53E 02 1.57E 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02 1.47E 02 1.53E 02 1.57E 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02 1.47E 02 1.53E 02 1.57E 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02
BI212
P0212
P0216
RN220
RA224
        1.47E 02 1.53E 02 1.57E 02 1.60E 02 1.61E 02 1.62E 02 1.62E 02
TH228
        1.72E 02 1.68E 02 1.67E 02 1.65E 02 1.64E 02 1.62E 02 1.60E 02
 U232
 U233
         3.27E 02 3.13E 02 3.13E 02 3.13E 02 3.13E 02 3.13E 02 3.13E 02
         1.74E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01 1.82E 01
 U234
         9.00E-01 1.00E 00 1.10E 00 1.11E 00 1.10E 00 1.10E 00 1.09E 00
PU238
         4.59E 01 3.87E 01 3.87E 01 3.87E 01 3.87E 01 3.87E 01 3.87E 01
PU239
         7.99E 00 1.71E 01 1.71E 01 1.71E 01 1.71E 01 1.71E 01 1.71E 01
PU240
         1.61E 02 9.01E 02 8.52E 02 8.08E 02 7.66E 02 7.26E 02 6.88E 02 2.94E-01 9.59E-01 2.35E 00 3.60E 00 4.79E 00 5.91E 00 6.97E 00
PU241
AM241
         4.22E-01 2.45E 01 4.88E 00 1.05E 00 2.34E-01 6.30E-02 3.81E-02
SUBTOT 1.76E 03 2.55E C3 2.51E C3 2.48E 03 2.45E 03 2.41E 03 2.37E 03
TOTALS 1.76E 03 7.84E 04 2.51E C3 2.48E C3 2.45E 03 2.41E 03 2.38E 03
```

Table 11 presents the photon spectrum produced by radioactive decay of the fission products in the fuel salt. The photon energy group structure for the calculation is the same as that used in the PHOEBE code. The most important fission product gamma ray sources in each of these groups are summarized in Table 12.

The photon spectrum produced by radioactive decay of the transuranium isotopes is shown in Table 13. In this table the 0.3 MeV mean energy group has been subdivided into seven low energy groups to include the x-radiation accompanying  $\alpha$ -decay of the actinides. The greatest shielding problem presented by these isotopes is the 2 x  $10^{12}$  photons/sec of 2.62 MeV energy generated by radioactive decay of  $^{208}$ Tl, a daughter of  $^{232}$ U. At the end of five years storage the radioactivity of  $^{208}$ Tl will determine the  $\gamma$ -ray shielding required to ship the fuel salt. At this time the entire decay chain of  $^{232}$ U and its daughters will be in secular equilibrium and will be disappearing with the 72 year half-life of the former.

An estimate has also been made of the neutron production rate in the fuel salt by  $\alpha$ -n reactions with  $^9\mathrm{Be}$  and  $^{19}\mathrm{F}$ . Using values given by Arnold  $^8$  for neutron production rates in thick absorbers and for dependence of neutron yield on energy, a neutron source strength of  $4.5 \times 10^9$  neutrons/sec was obtained. This neutron production rate is sufficiently high that the neutron dose rate will be the controlling radiation through a lead shield.

Table 11. Photon Spectrum of Fission Products in MSRE Fuel Salt After Period of <sup>233</sup>U Operation as a Function of Time After Shutdown

MSRE OPERATION WITH 233-U FUEL
POWER: 4.18 MW BURNUP: 1387. MWD FLUX: 3.89E 12 N/CM\*\*2-SEC

TWELVE GROUP PHOTON RELEASE RATES, PHOTONS/ SEC

EMEAN			TIM	E AFTER DI	SCHARGE						
(MEV)	DISCHARGE	200.0 D	384.0 D	566.0 D	749.0 D	930.0 D	1115. D	1297. D	1480. D	1662. D	1845. D
3.00E-01	2.11E 17	4.14E 14	2.01E 14	1.26E 14	8.21E 13	5.40E 13	3.56E 13	2.39E 13	1.62E 13	1.12E 13	7.91E 12
6.30E-01	3.41E 17	3.66E 15	9.60E 14	4.90E 14	4.06E 14	3.81E 14	3.66E 14	3.55E 14	3.47E 14	3.41E 14	3.35E 14
1.10E 00	1.59E 17	2.52E 13	1.64E 13	1.18E 13	8.58E 12	6.35E 12	4.74E 12	3.62E 12	2.81E 12	2.24E 12	1.82E 12
1.55E 00	1.09E 17	1.19E 13	7.34E 12	4.95E 12	3.36E 12	2.32E 12	1.61E 12	1.14E 12	8.22E 11	6.10E 11	4.66E 11
1.99E 00	1.62E 16	3.31E 13	2.12E 13	1.37E 13	8.80E 12	5.69E 12	3.64E 12	2.35E 12	1.52E 12	9.81E 11	6.34F 11
2.38E 00	1.99E 16	1.32E 12	9.12E 11	6.47E 11	4.58E 11	3.25E 11	2.29E 11	1.63E 11	1.15E 11	8.16E 10	5.78E 10
2.75E 00	8.24E 15	3.80E 10	2.68E 10	1.90E 10	1.35E 10	9.57E 09	6.75E 09	4.78E 09	3.39E 09	2.40E 09	1.70E 09
3.25E 00	4.25E 15	6.37E 08	5.99E 04	6.29E 00	6.25E-04	6.92E-08	0.0	0.0	0.0	0.0	0.0
3.70E 00	5.22E 15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22E 00	1.97E 15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.70E 00	6.89E 15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	9.82F 17	4-15E 15	1.215 15	6.47E 14	5.09F 14	4.49F 14	4.12F 14	3.97F 14	3.60F 14	3.56E 14	3.45E 14

MEV/ SEC 7.97E 17 2.55E 15 7.39E 14 3.96E 14 3.14E 14 2.79E 14 2.57E 14 2.42E 14 2.31E 14 2.23E 14 2.17E 14

### TWELVE GROUP ENERGY RELEASE RATES, MEV/WATT-SEC

EMEAN			TIM	E AFTER DI	SCHARGE						
(MEV)	DISCHARGE	200.0 D	384.0 D	566.0 D	749.0 D	930.0 D	1115. D	1297. D	1480. D	1662. D	1845. D
3.00E-01	1.52E 10	2.97E 07	1.45E 07	9.08E 06	5.89E 06	3.88E 06	2.56E 06	1.72E 06	1.17E 06	8.07E 05	5.68E 05
6.30E-01	5.14E 10	5.52E 08	1.45E 08	7.39E 07	6.13E 07	5.74E 07	5.52E 07	5.36E 07	5.24E 07	5.14E 07	5.05E 07
1.10E 00	4.17E 10	6.64E 06	4.32E 06	3.10E 06	2.26E 06	1.67E 06	1.25E 06	9.53E 05	7.40E 05	5.89E 05	4.80E 05
1.55E 00	4.04E 10	4.4CE 06	2.72E 06	1.84E 06	1.25E 06	8.60E 05	5.96E 05	4.22E 05	3.05E 05	2.26E 05	1.73E 05
1.99E 00	7.71E 09	1.58E 07	1.01E 07	6.52E 06	4.19E 06	2.71E 06	1.74E 06	1.12E 06	7.23E 05	4.67E 05	3.02E 05
2.38E 00	1.13E 10	7.50E 05	5.20E 05	3.69E 05	2.61E 05	1.85E 05	1.31E 05	9.27E 04	6.56E 04	4.65E 04	3.29E 04
2.75E 00	5.43E 09	2.5CE 04	1.77E 04	1.25E 04	8.87E 03	6.30E 03	4.44E 03	3.15E 03	2.23E 03	1.58E C3	1.12E 03
3.25E 00	3.31E 09	4.96E 02	4.66E-02	4.89E-06	4.86E-10	5.38E-14	0.0	0.0	0.0	0.0	0.0
3.70E 00	4.62E 09	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22E 00	1.99E 09	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.70E 00	7.75E C9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	G• 0	0.0	0.0
TOTAL	1.91E 11	6.10E 08	1.77E 08	9.48E 07	7.51E 07	6.67E 07	6.14E 07	5.79E 07	5.54E 07	5.35E 07	5.20E 07
WATTS	1.28E 05	4.08E 02	1.18E 02	6.34E 01	5.03E 01	4.47E 01	4.11E 01	3.88E 01	3.71E 01	3.58E C1	3.48E C1

Table 12. Summary of Important Fission Product Gamma Ray Sources in MSRE Fuel Salt

	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY = 0.300MEV	GROUP 1, MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
CE144 3.38E 07	2.07E 07 1.32E 07 8.49E	06 5.43E 06 3.49E 06	2.22E 06 1.43E 06	9.12E 05 5.85E 05 3.74E 05
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY * 0.630MEV	GROUP 2, MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
ZR 95 1.29E 09	1.52E 08 2.14E 07 3.07E 3.16E 08 5.64E 07 8.44E		7.05E 04 2.02E 04 8.74E 04 2.51E 04	5.75E 03 1.65E 03 4.69E 02 7.13E 03 2.05E 03 5.82E 02
NB 95 1.17E 09 BA137M 5.53E 07	3.16E 08		5.15E 07 5.09E 07	5.03E 07 4.98E 07 4.92E 07
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY = 1.100MEV	GROUP 3, MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
RH106 9.81E 06	5.63E 06 3.97E 06 2.82E	06 1.99E 06 1.42E 06	9.99E 05 7.09E 05	5.02E 05 3.56E 05 2.52E 05
EU154 2.64E 05	2.58E 05 2.52E 05 2.47E	05 2.41E 05 2.36E 05	2.31E 05 2.26E 05	2.21E 05 2.17E 05 2.12E 05
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY = 1.550MEV	GROUP 4, MEV/WATT-SEC		,
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 C 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
RH106 2.47E 06 PR144 4.20E 06	1.42E 06  1.0CE 06  7.10E 2.57E 06  1.64E 06  1.05E		2.52E 05 1.78E 05 2.76E 05 1.77E 05	1.26F 05 8.96E 04 6.34E 04 1.13E 05 7.25E 04 4.64E 04
PK144 4.20E 00	2.572 00 1.042 00 1.052	00 01142 05 44352 05	20100 05 10110 05	10150 05 10250 04 40040 04
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY # 1.990MEV	GROUP 5, MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
PR144 2.47E 07	1.51E 07 9.66E 06 6.20E	06 3.96E 06 2.55E 06	1.62E 06 1.04E 06	6.66E 05 4.27E 05 2.73E 05
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY = 2.380MEV	GROUP 6, MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0		1115. D 1297. D	1480. D 1662. D 1845. D
RH106 1.28E 06	7.36E 05 5.20E 05 3.69E	05 2.61E 05 1.85E 05	1.31E 05 9.27E 04	6.56E 04 4.65E 04 3.29E 04
	PRINCIPAL PHOTON SOURCES IN MEAN ENERGY = 2.750MEV	GROUP 7. MEV/WATT-SEC		
NUCLIDE		TIME AFTER DISCHARGE		
DISCHARGE	200.0 D 384.0 D 566.0	D 749.0 D 930.0 D	1115. D 1297. D	1480. D 1662. D 1845. D
RH106 4.36E 04	2.50E 04 1.77E 04 1.25E	04 8.87E 03 6.30E 03	4.44E 03 3.15E 03	2.23E 03 1.58E 03 1.12E 03

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Table 13. Photon Spectrum of Transuranium Isotopes in MSRE Fuel Salt After Period of <sup>233</sup>U
Operation as a Function of Time After Shutdown

MSRE OPERATION WITH 233-U FUEL
POWER= 4.18 MW BURNUP= 1387. MWD FLUX= 3.89E 12 N/CM\*\*2-SEC

### ACTINIDE PHOTON RELEASE RATES, PHOTONS/ SEC

EMEAN			MIT	E AFTER DI	SCHARGE						
(MEV)	DISCHARGE	200.0 D	384.0 D	566.0 D	749.0 D	930.0 D	1115. D	1297. D	1480. D	1662. D	1845. D
3.00E-02	9.88E 13	1.82E 09	2.52E 09	3.20E 09	3.87E 09	4.50E 09	5.14E 09	5.74E 09	6.34E 09	6.91E 09	7.48E 09
4.00E-02	3.67E 14	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11	1.73E 11
6.00E-02	5.07E 14	6.36E 11	6.45E 11	6.53E 11	6.61E 11	6.69E 11	6.77E 11	6.84E 11	6.92E 11	6.99E 11	7.06E 11
1.00E-01	7.78E 14	1.82E 12	1.85E 12	1.86E 12	1.87E 12	1.88E 12	1.89E 12				
1.50E-01	3.59E 14	1.09E 11	1.09E 11	1.10E 11	1.10E 11	1.10E 11	1.10E 11	1.11E 11	1.11E 11	1.11E 11	1.11E 11
2.00E-01	2.86E 14	5.92E 12	6.00E 12	6.05E 12	6.10E 12	6.13E 12	6.15E 12	6.16E 12	6.16E 12	6.16E 12	6.17E 12
3.00E-01	1.91E 14	5.09E 11	5.14E 11	5.18E 11	5.20E 11	5.22E 11	5.24E 11	5.24E 11	5.24E 11	5.25E 11	5.25E 11
6.30E-01	2.95E 13	4.68E 12	4.74E 12	4.79E 12	4.82E 12	4.85E 12	4.86E 12	4.87E 12	4.87E 12	4.87E 12	4.88E 12
1.10E 00	2.02E 12	1.38E 12	1.40E 12	1.41E 12	1.42E 12	1.43E 12	1.43E 12	1.44E 12	1.44E 12	1.44E 12	1.44E 12
1.55E 00	7.45E 1C	7.58E 10	7.68E 10	7.75E 10	7.81E 10	7.84E 10	7.87E 10	7.89E 10	7.89E 10	7.89E 10	7.89E 10
1.99E 00	3.59E 10	3.66E 10	3.71E 10	3.74E 10	3.77E 10	3.79E 10	3.80E 10	3.81E 10	3.81E 10	3.81E 10	3.81E 10
2.38E 00	2.78E 01	2.97E 01	3.04E 01	3.07E 01	3.07E 01	3.07E 01	3.06E 01	3.05E 01	3.04E 01	3.03E 01	3.C2E 01
2.75E 00	1.93E 12	1.97E 12	1.99E 12	2.01E 12	2.02E 12	2.03E 12	2.04E 12	2.05E 12	2.05E 12	2.05E 12	2.05E 12
3.25E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.70E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	2.62E 15	1.73E 13	1.75E 13	1.77E 13	1.78E 13	1.79E 13	1.80E 13	1.808 13	1.80E 13	1.80E 13	1.81E 13
MEV/ SEC	3.21E 14	1.17E 13	1.18E 13	1.19E 13	1.20E 13	1.21E 13					

ACTINIDE ENERGY RELEASE RATES, MEV/WATT-SEC

WATTS

EMEAN			TIM	E AFTER DI	SCHARGE						
(MEV)	DISCHARGE	200.0 D	384.0 D	566.0 D	749.0 D	930.0 D	1115. D	1297. D	1480. D	1662. D	1845. D
3.00E-02	7.09E 05	1.31E 01	1.81E 01	2.30E 01	2.78E 01	3.23E 01	3.69E 01	4.13E 01	4.55E Cl	4.97E 01	5.37E 01
4.00E-02	3.52E 06	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03	1.66E 03
6.00E-02	7.28E 06	9.13E 03	9.26E 03	9.38E 03	9.50E 03	9.61E 03	9.72E 03	9.83E 03	9.94E 03	1.00E 04	1.01E 04
1.00E-01	1.86E 07	4.37E 04	4.42E 04	4.46E 04	4.49E 04	4.51E 04	4.52E 04	4.53E 04	4.53E 04	4.53E C4	4.53E 04
1.50E-01	1.29E 07	3.92E 03	3.93E 03	3.94E 03	3.95E 03	3.96E 03	3.97E 03	3.97E 03	3.98E 03	3.99E 03	3.99E 03
2.00E-01	1.37E 07	2.84E 05	2.97E 05	2.90E 05	2.92E 05	2.93E 05	2.94E 05	2.95E 05	2.95E 05	2.95E 05	2.95E 05
3.00E-01	1.38E 07	3.65E 04	3.69E 04	3.72E 04	3.74E 04	3.75E 04	3.76E 04	3.77E 04	3.77E 04	3.77E C4	3.77E 04
6.30E-01	4.45E 06	7.07E 05	7.16E 05	7.22E 05	7.27E 05	7.31E 05	7.33E 05	7.35E 05	7.35E 05	7.35E 05	7.35 E 05
1.10E 00	5.32E 05	3.64E 05	3.69E 05	3.72E 05	3.75E 05	3.77E 05	3.78E 05	3.79E 05	3.79E 05	3.79E 05	3.79E 05
1.55E 00	2.76E 04	2.81E 04	2.85E 04	2.88E 04	2.90E 04	2.91E 04	2.92E 04	2.93E 04	2.93E 04	2.93E 04	2.93E 04
1.99E 00	1.71E 04	1.74E 04	1.77E 04	1.78E 04	1.79E 04	1.80E 04	1.81E 04	1.81E 04	1.81E 04	1.81E 04	1.82E 04
2.38E 00	1.58E-05	1.69E-05	1.738-05	1.75E-05	1.75E-05	1.75E-05	1.74E-05	1.74E-05	1.73E-05	1.73E-05	1.72E-05
2.75E 00	1.27E 06	1.29E 06	1.31E 06	1.32E 06	1.33E 06	1.34E 06	1.34E 06	1.35E 06	1.35E 06	1.35E C6	1.35E 06
3.25E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.70E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.22E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.70E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5.25E OC	C• 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	7.67E 07	2.79E 06	2.82E 06	2.85E 06	2.87E 06	2.89E 06	2.89E 06	2.90E 06	2.90E 06	2.90E 06	2.90E 06

5.14E 01 1.87E 00 1.89E 00 1.91E 00 1.92E 00 1.93E 00 1.94E 00 1.94E 00 1.94E 00 1.94E 00 1.94E 00

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