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OPERATION OF THE AIRCRAFT REACTOR EXPERIMENT

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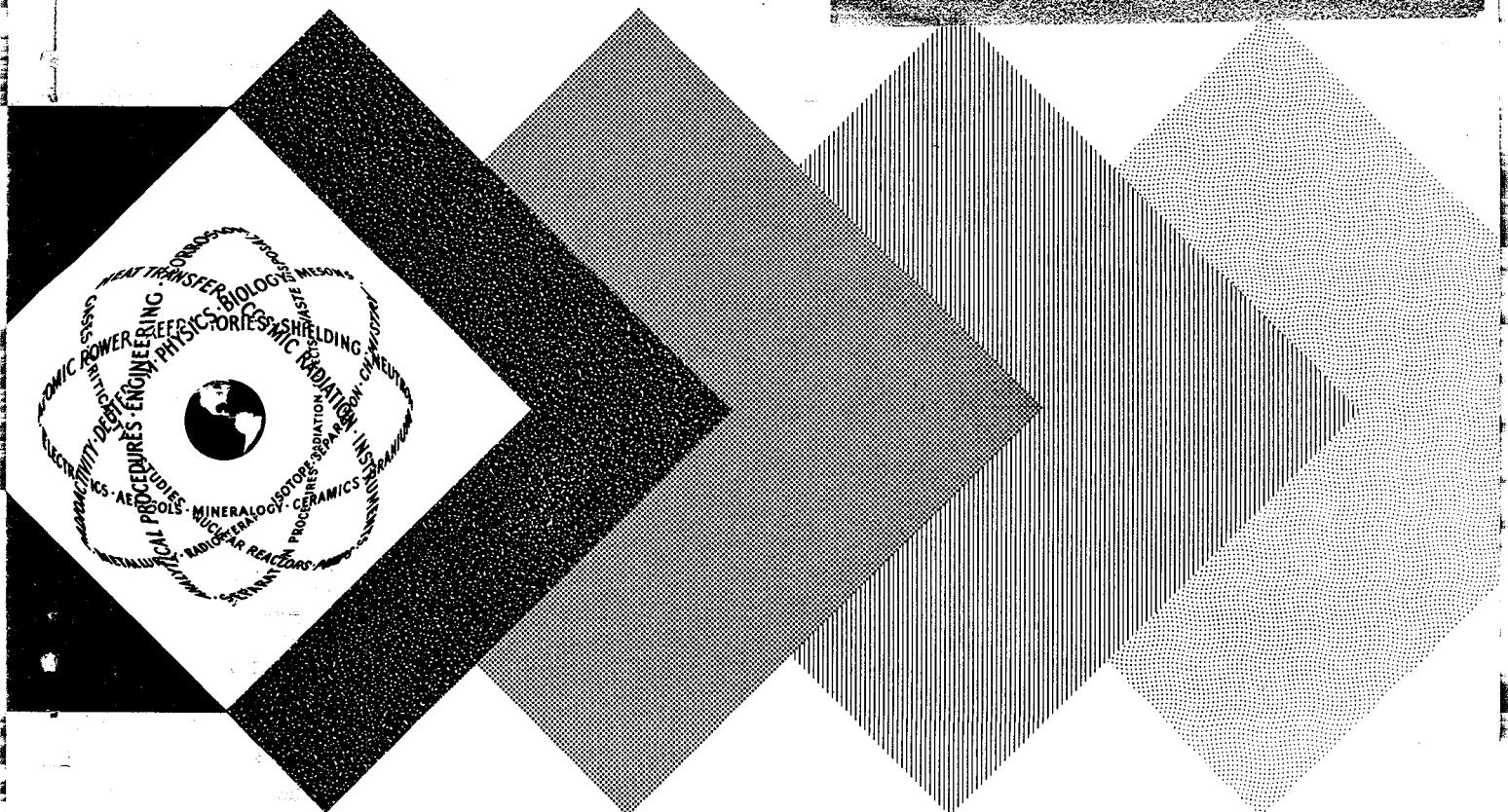
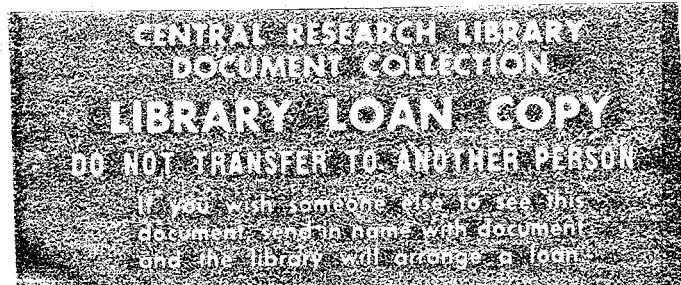
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September 6, 1955

Oak Ridge National Laboratory
Oak Ridge, Tennessee



UNITED STATES ATOMIC ENERGY COMMISSION

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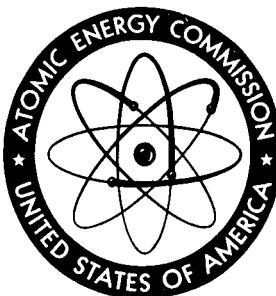
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By

W. B. Cottrell
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J. L. Meem

September 6, 1955

Work performed under Contract No. W-7405-Eng-26

Oak Ridge National Laboratory
Oak Ridge, Tennessee

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ACKNOWLEDGMENTS

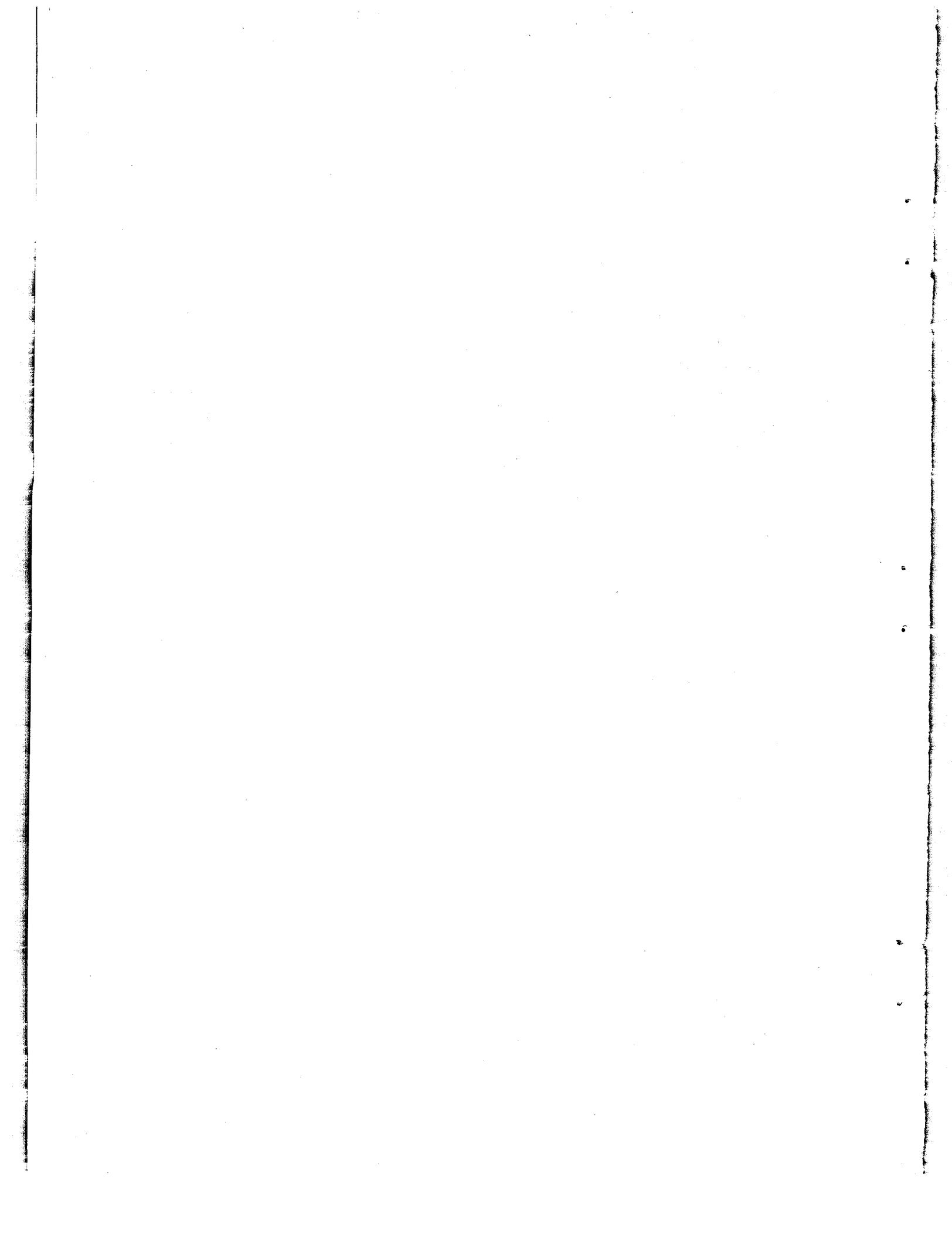
The experiment described herein was performed by the ARE Operations Group under the immediate supervision of E. S. Bettis and J. L. Meem, with frequent support from other groups in the ANP Project. In particular, W. R. Grimes and his crew effected the carrier and concentrate loading operation, as well as the fluoride sampling; C. P. Coughlen and his crew effected the sodium loading and sampling; a group from the Analytical Chemistry Division, under the supervision of J. C. White, performed all analyses of fluoride and sodium samples; and E. B. Johnson obtained a reactor power calibration from analysis of a fuel sample. Craft foremen B. H. Webster and J. C. Packard are both to be commended for the excellent craftsmanship in the construction and maintenance of the system, which made the operation of the system such a success; and all who were in the building during the operation are appreciative of the concern of the Health Physics Group under R. L. Clark.

The bulk of this report was prepared by the authors, but considerable assistance was received from W. K. Ergen in the analysis of the nuclear data. The work of numerous others is referred to in the various analyses which are presented in the text and in the appendixes. In addition, the constructive criticism of W. H. Jordan, S. J. Cromer, and E. S. Bettis, each of whom reviewed this report, is gratefully acknowledged.

FOREWORD

The operation of the Aircraft Reactor Experiment (ARE) culminated four years of endeavor at ORNL in the field of nuclear propulsion of aircraft. The final success of the experiment is a tribute to the efforts of the 300-odd technical and scientific personnel who constitute the ANP Project at ORNL, as well as those others who were less prominently engaged in the fabrication, assembly, and installation of the experiment. The project was capably directed toward this goal during its formative years by Dr. R. C. Briant (now deceased), and subsequently by W. H. Jordan and S. J. Cromer, currently Director and Co-Director, respectively.

This is the second in a series of three reports which summarize the ARE experience and is concerned primarily with the nuclear operation of the reactor. The experiment is described, and the data obtained during the time from the start of the critical experiment until the reactor was shut down for the last time are analyzed. The material is presented in essentially chronological order, and frequent reference is made to appended material which includes important detailed data and information that may not be of general interest.



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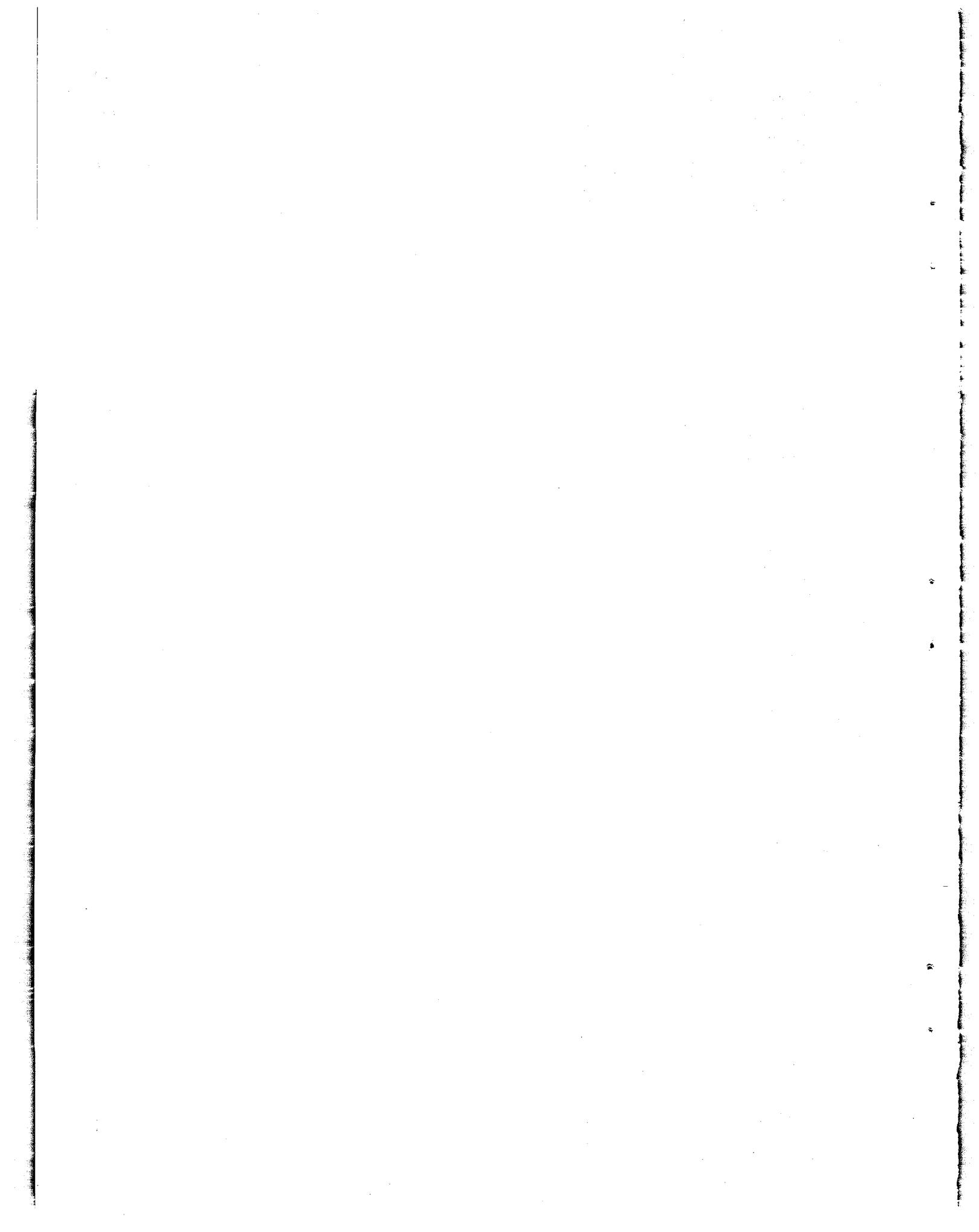
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OPERATION OF THE AIRCRAFT REACTOR EXPERIMENT

SUMMARY

The Aircraft Reactor Experiment (ARE) was operated successfully and without untoward difficulty in November 1954. The following statements summarize the notable information obtained from the experiment.

1. The reactor became critical with a mass of 32.8 lb of U^{235} , which gave a concentration of 23.9 lb of U^{235} per cubic foot of fluoride fuel. For operation at power, the U^{235} content of the fuel mixture was increased to 26.0 lb/ft³, and thus the final composition of the fuel mixture was 53.09 mole % NaF, 40.73 mole % ZrF_4 , and 6.18 mole % UF_4 .

2. The maximum power level for sustained operation was 2.5 Mw, with a temperature gradient of 355°F; the maximum fuel temperature at this level was 1580°F. Temperatures as high as 1620°F were recorded during transients.

3. From the time the reactor first went critical until the final shutdown, 221 hr had elapsed, and for the final 74 hr the power was in the megawatt range (0.1 to 2.5 Mw). The total integrated power was about 96 Mw-hr.

4. While at power the reactor exhibited excellent stability and it was easily controlled because of its high negative temperature coefficient of reactivity, which made the reactor a slave to the

load placed upon it. The fuel temperature coefficient was $-9.8 \times 10^{-5} (\Delta k/k)/^{\circ}F$, and the overall coefficient for the reactor was -6.1×10^{-5} .

5. Practically all the gaseous fission products and probably some of the other volatile fission products were removed from the circulating fuel. In a 25-hr run at 2.12 Mw the upper limit of the reactor poisoning due to xenon was 0.01% $\Delta k/k$. No more than 5% of the xenon stayed in the molten fluoride fuel.

6. The total time of operation at high temperature (1000 to 1600°F) for the sodium circuit was 635 hr, and, for the fluoride fuel system, 462 hr. During most of the operating period the sodium was circulated at 150 gpm and the fuel at 46 gpm.

7. The fabricability and compatibility of the materials system, i.e., fluoride fuel, sodium coolant, and Inconel structure, were demonstrated, at least for the operating times, temperatures, and flux levels present.

8. All components and, with few exceptions, all instrumentation performed according to design specifications. The performance of the pumps was particularly gratifying, and the low incidence of instrumentation failure was remarkable in view of the quantity and complexity of the instruments used.

1. INTRODUCTION

The Aircraft Nuclear Propulsion (ANP) project at the Oak Ridge National Laboratory was formed in the fall of 1949, at the request of the Atomic Energy Commission, to provide technical support to existing Air Force endeavors in the field. The ORNL effort gradually expanded and, following the recommendation of the Technical Advisory Board in the summer of 1950, was directed toward the construction and operation of an aircraft reactor experiment. A complete description of the ARE falls naturally into three categories that correspond to the three phases of the project: (1) design and installation, (2) operation, and (3) postoperative examination. Each of these phases is covered by a separate report, ORNL-1844, ORNL-1845, and ORNL-1868, respectively. Much detailed information pertaining to the selection of the reactor type and to the design, construction, and pre-nuclear operation of the reactor experiment will be presented in ORNL-1844. As the title of this report (ORNL-1845) indicates it is concerned primarily with the operation of the experiment, and only insofar as they are necessary or useful to the understanding or evaluation of the nuclear operation are design and preliminary operational data included herein. The third report (ORNL-1868) will describe the aftermath of the experiment, with particular reference to corrosion, radiation effects, and the decay of activity - effects that cannot be evaluated at this time because of the high level of the radioactivity of the equipment.

The specific operating objectives were to attain a fuel temperature of 1500°F, with a 350°F temperature rise across the reactor, and to operate the system for approximately 100 Mw-hr. Other objectives of the experiment were to obtain as much experimental data as possible on the reactor operational characteristics. The extent to which each of these objectives was fulfilled is described herein, and a measure of the success of the program is thus provided.

Although it was initially planned to use a

sodium-cooled, solid-fuel-element reactor, the reactor design evolved first to that of a sodium-cooled, stationary-liquid-fuel reactor and, finally, to that of a circulating-fuel reactor employing sodium as a reflector coolant. These evolutionary processes left their mark on the experiment, particularly in that the reactor had to incorporate a moderator geometry that was originally specified and ordered for the sodium-cooled reactor. The adaptation of this moderator geometry to the circulating-fuel reactor resulted in a reactor in which the fuel stream was divided into six parallel circuits, each of which made numerous passes through the core. These fuel passages were not drainable - a condition which caused considerable concern throughout the course of the experiment.

Although it is not the purpose of this report to give a detailed history of the design, construction, or preliminary testing of the reactor system, the final design and pertinent prenuclear operation are briefly described. The bulk of the report concerns the operation of the experiment from the time uranium was added to the fuel system on October 30 until the evening of November 12, when the reactor was shut down for the last time. In addition to the description of the various experiments and analyses of the data which are presented in the body of the report, the entire nuclear operation, as recorded in the "Nuclear Log," is given in Appendix T. The report also includes a number of recommendations based on the operating experience, and much detailed supporting data and information not appropriate for inclusion in the body of the report are given in the other appendices.

The various experiments that were performed on the ARE were designated as E, L, or H series, depending upon whether they occurred during the critical experiment, low-power operation, or high-power operation, respectively. Each of these experiments, as listed below, is discussed in this report.

Experiment Series No.	Type of Experiment
E-1	Critical experiment
E-2	Subcritical measurement of reactor temperature coefficient
L-1	Power determination at 1 w (nominal)
L-2	Regulating rod calibration vs fuel addition
L-3	Fuel system characteristics
L-4	Power determination at 10 w (nominal)
L-5	Regulating rod calibration vs reactor period
L-6	Calibration of shim rod vs regulating rod
L-7	Effect of fuel flow on reactivity
L-8	Low-power measurement of reactor temperature coefficient
L-9	Adjustment of chamber position
H-1	Approach to power: 10-kw run
H-2	Test of off-gas system
H-3	Approach to power: 100-kw to 1-Mw runs
H-4	High-power measurement of the fuel temperature coefficient
H-5	High-power measurement of the reactor temperature coefficient
H-6	Reactor startup on temperature coefficient
H-7	Sodium temperature coefficient
H-8	Effect of a dollar of reactivity
H-9	High-power measurement of reactor temperature coefficient
H-10	Moderator temperature coefficient
H-11	Xenon run at full power
H-12	Reactivity effects of sodium flow
H-13	Xenon buildup at one-tenth full power
H-14	Operation at maximum power

2. DESCRIPTION OF THE REACTOR EXPERIMENT

The ARE consisted of the circulating-fuel reactor and the associated pumps, heat transfer equipment, controls, and instrumentation required for its safe operation. A schematic arrangement of the reactor system is shown in Fig. 2.1. The major functional parts of the system are discussed briefly below. The physical plant is described in Appendix U. A detailed description of the reactor and the associated system may be found in the design and installation report.¹ A summary of the design and operational data, including a detailed flow sheet of the experiment, is given in Appendix B.

REACTOR

The reactor assembly consisted of a 2-in.-thick Inconel pressure shell in which beryllium oxide moderator and reflector blocks were stacked around fuel tubes, reflector cooling tubes, and control assemblies. Elevation and plan sections of the reactor are shown in Figs. 2.2 and 2.3. The innermost region of the lattice assembly was the core, which was a cylinder approximately 3 ft in diameter and 3 ft long. The beryllium oxide was machined into small hexagonal blocks which were split axially and stacked to effect the cylindrical core and reflector. Each beryllium oxide block in the core had a 1.25-in. hole drilled axially through

its center for the passage of the fuel tubes. The outer 7.5 in. of beryllium oxide served as the reflector and was located between the pressure shell and the cylindrical surface of the core. The reflector consisted of hexagonal beryllium oxide blocks, similar to the moderator blocks, but with 0.5-in. holes.

The fuel stream was divided into six parallel circuits at the inlet fuel header, which was located above the top of the core and outside the pressure shell. These circuits each made 11 series passes through the core, starting close to the core axis, and progressing in serpentine fashion to the periphery of the core, and finally leaving the core through the bottom of the reactor. The six circuits were connected to the outlet header. Each tube was of 1.235-in.-OD seamless Inconel tubing with a 60-mil wall. The combination of parallel and series fuel passes through the core was largely the result of the need for assuring turbulent flow in a system in which the fluid properties and tube dimensions were fixed.

The reflector coolant, i.e., sodium, was admitted into the pressure shell through the bottom. The sodium then passed up through the reflector tubes, bathed the inside walls of the pressure shell, filled the moderator interstices, and left from the plenum chamber at the top of the pressure shell. The sodium, in addition to cooling the reflector and pressure shell, acted as a heat transfer medium

¹Design and Installation of the Aircraft Reactor Experiment, ORNL-1844 (to be issued).

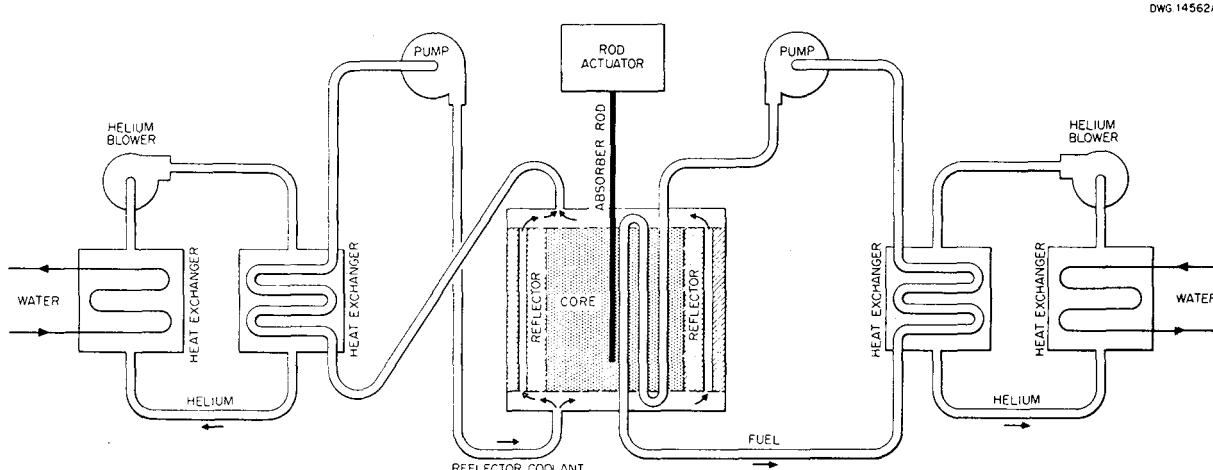


Fig. 2.1. Schematic Diagram of the Aircraft Reactor Experiment.

in the core by which moderator heat was readily transmitted to the fuel stream.

FUEL SYSTEM

The fuel was a mixture of the fluorides of sodium and zirconium, with sufficient uranium fluoride added to make the reactor critical. While the fuel ultimately employed for the experiment was the $\text{NaF-ZrF}_4\text{-UF}_4$ mixture with a composition of

53.09-40.73-6.18 mole %, respectively, most preliminary experimental work (i.e., pump tests, corrosion tests) employed a fuel containing somewhat more UF_4 . The fuel was circulated around a closed loop from the pump to the reactor, to the heat exchanger, and back to the pump. An isometric drawing of the fuel system is given in Fig. 2.4.

The fuel pump was a centrifugal pump with a vertical shaft and a gas seal, as shown in Fig. 2.5.

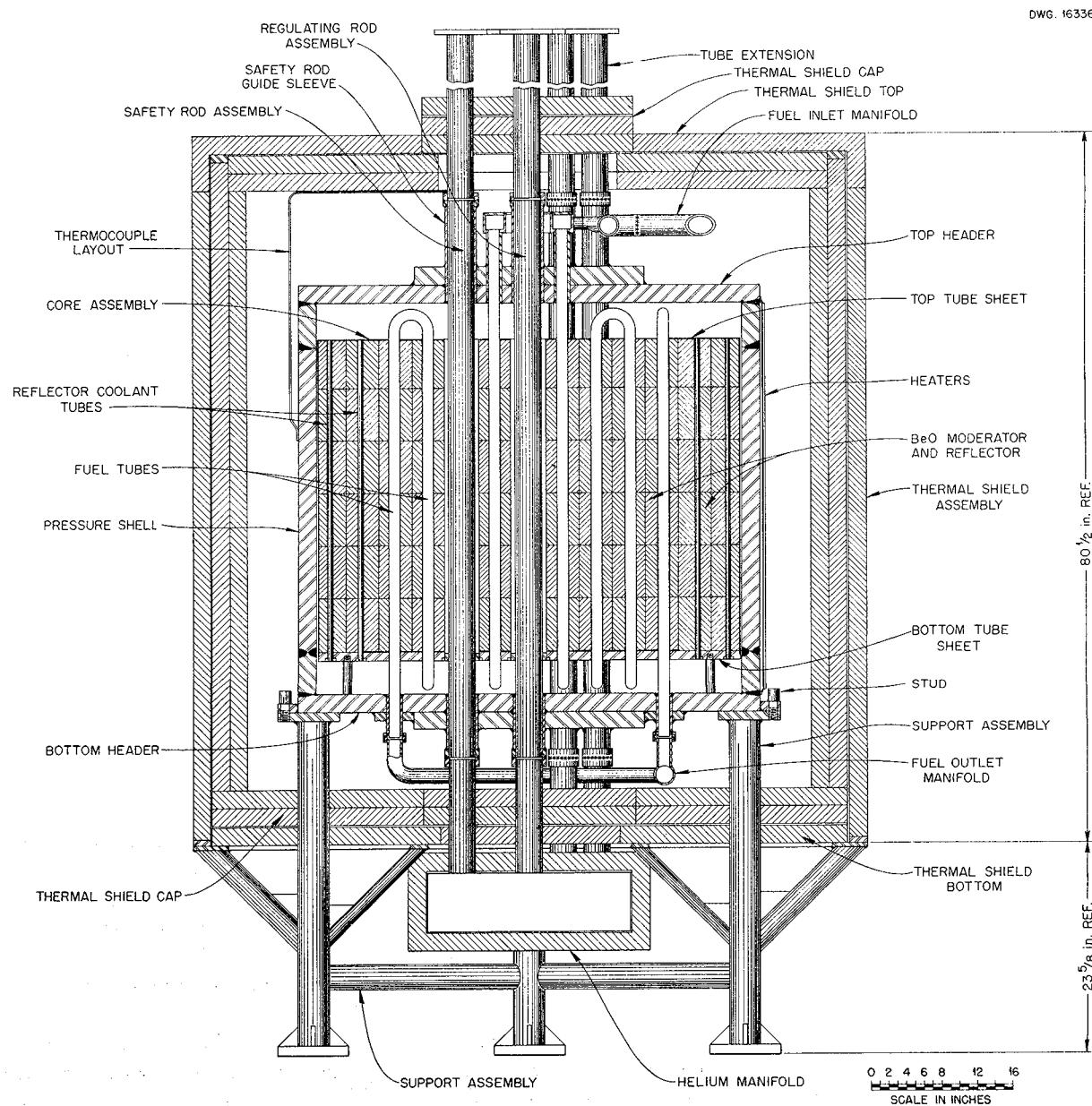


Fig. 2.2. The Reactor (Elevation Section).

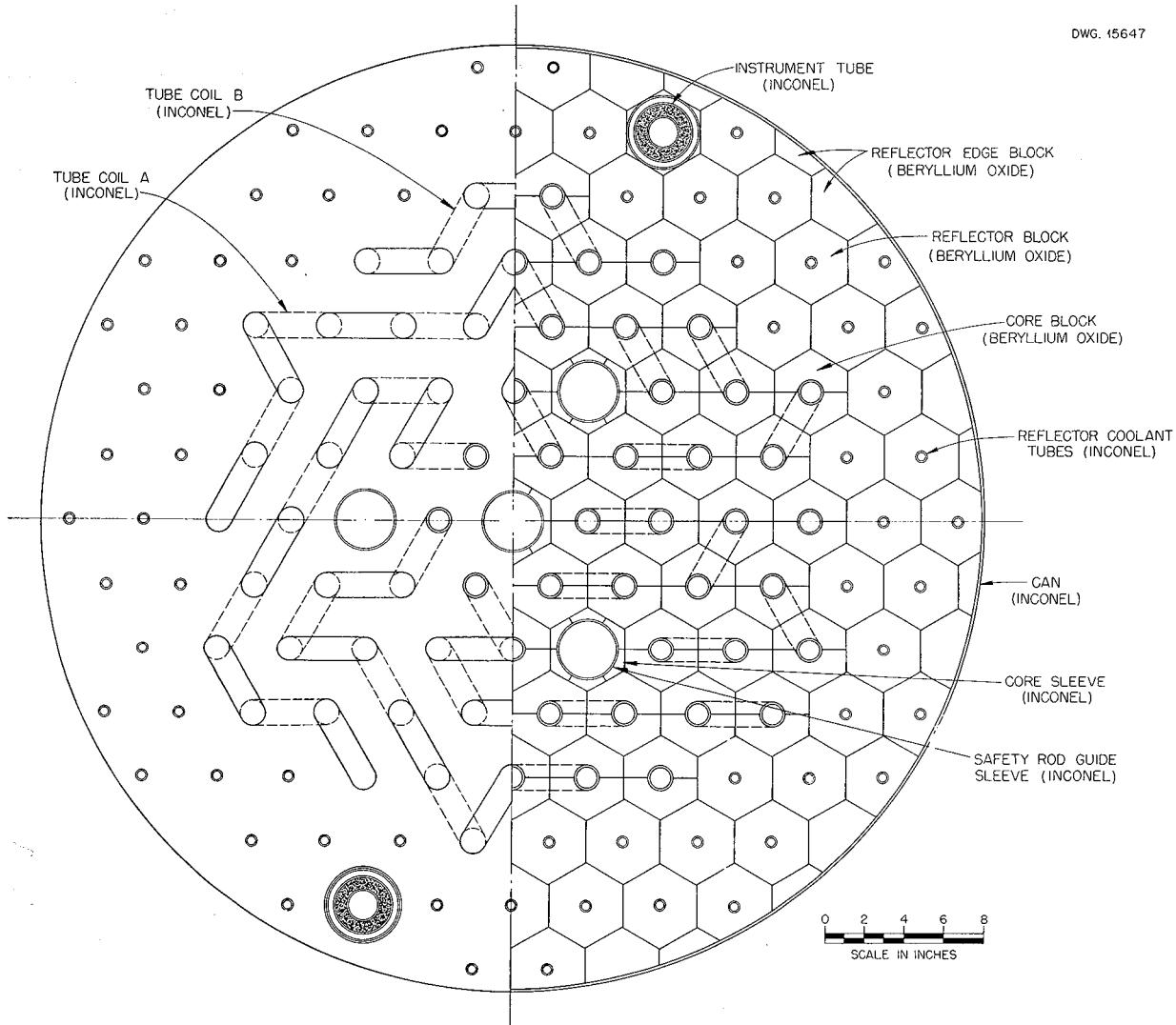


Fig. 2.3. The Reactor (Plan Section).

The fuel expansion volume around the impeller cavity provided the only liquid-to-gas interface in the fuel system. While speeds up to 2000 rpm could be attained with the 15-hp d-c pump motor, the desired fuel flow of 46 gpm was attained at a speed of 1080 rpm. Although only one pump was used in the experiment, a spare fuel pump, isolated from the operating pump and in parallel with it, was provided.

From the pump the fuel flowed to the reactor, where it was heated, then to two parallel fuel-to-helium heat exchangers, and back to the pump. The cycle time was about 47 sec at full flow, of

which approximately 8 sec was the time required for the fuel to pass through the core. The two fuel-to-helium heat exchangers were each coupled to a helium-to-water heat exchanger. The heat extracted from the fuel was transferred via the helium to water, and the water — the ultimate heat sink — was discharged. The helium flow rate in the fuel-to-helium heat exchanger loop was controlled through a magnetic clutch that coupled the blower to a 50-hp motor. Control of the helium flow rate in this manner permitted smooth control at any reactor power at which the heat generation was great enough for the temperature coefficient to be the controlling factor.

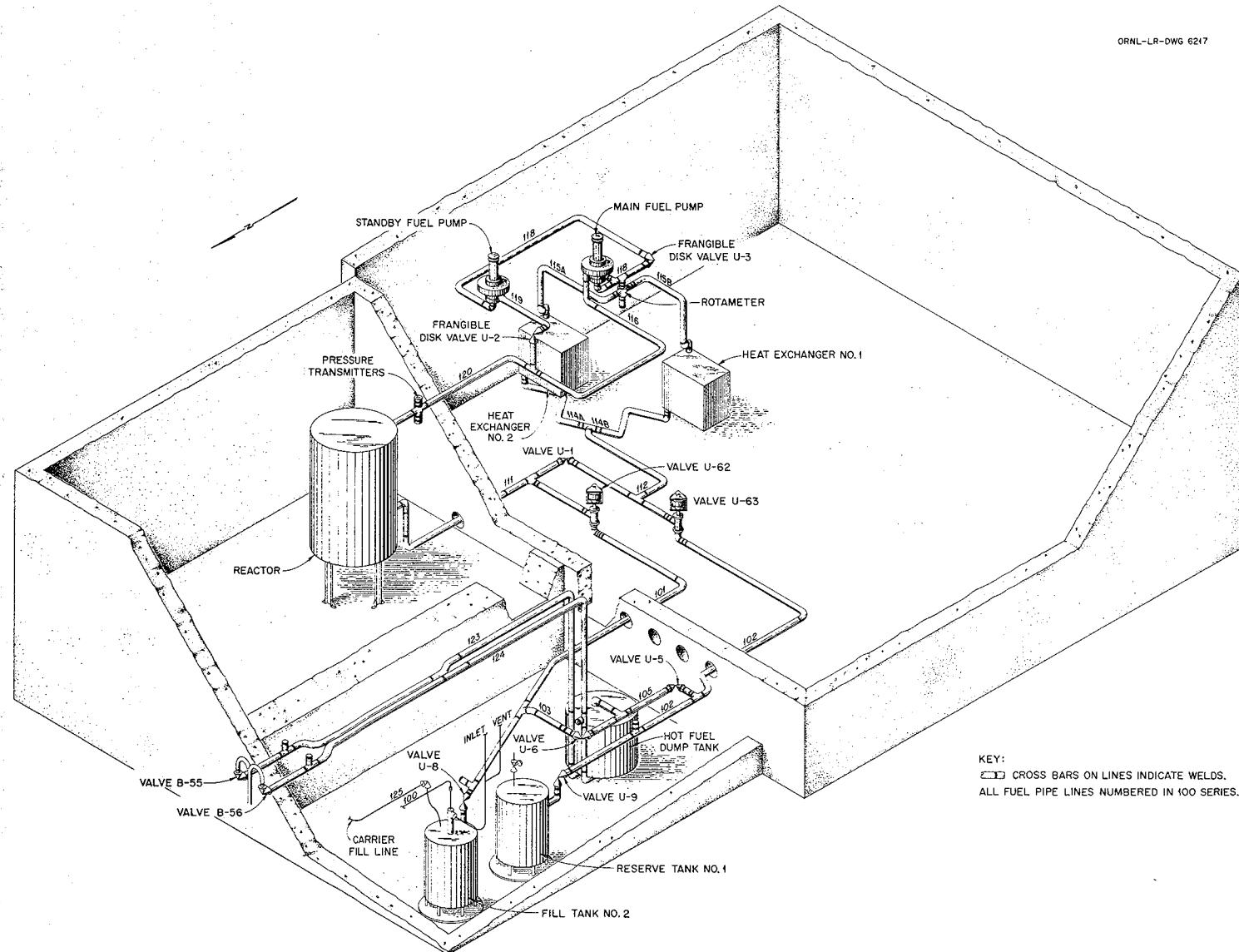


Fig. 2.4. Isometric Drawing of Fuel System.

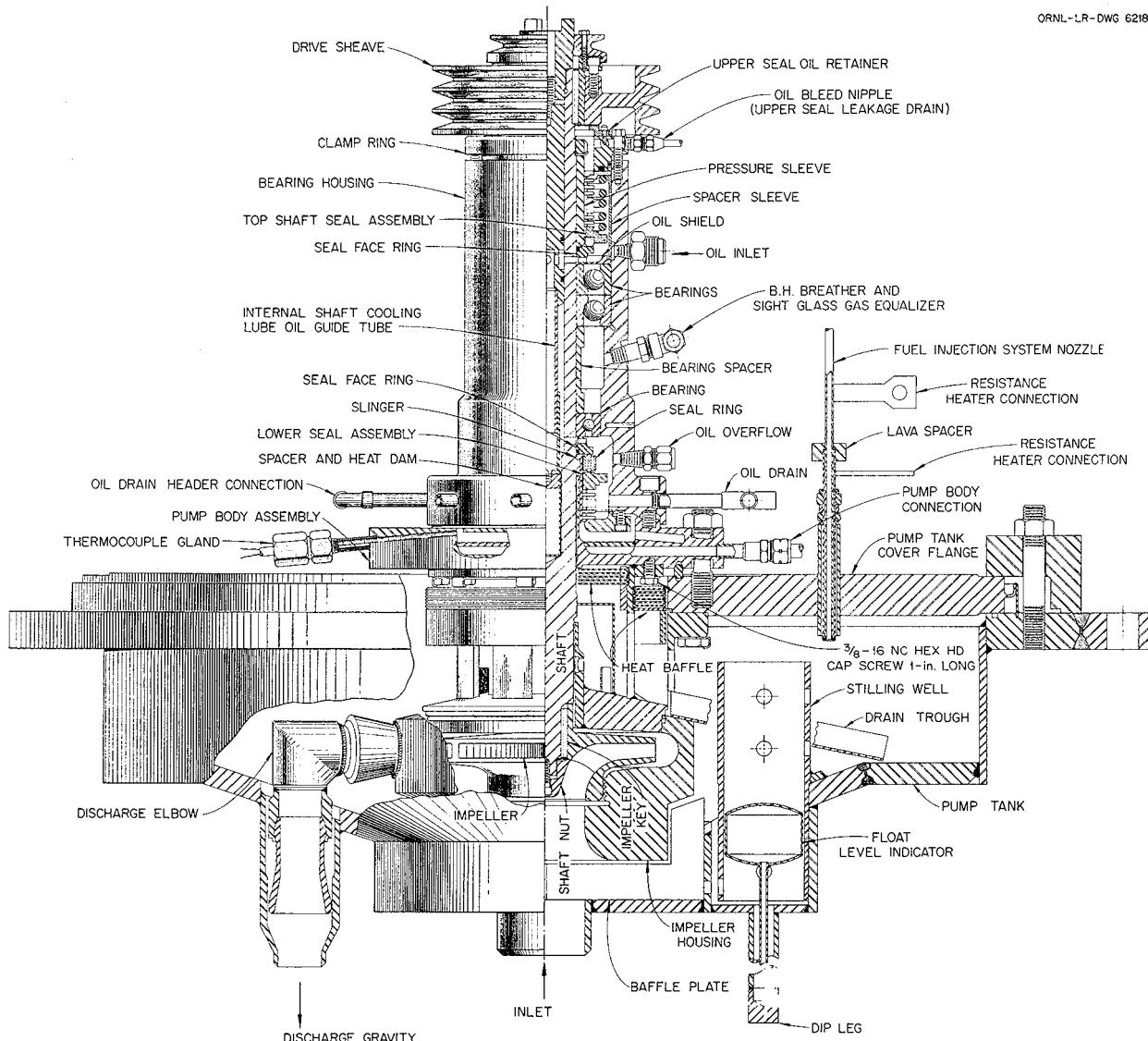


Fig. 2.5. Fuel Pump.

As shown in Fig. 2.4, the fuel system was connected with two fill tanks (only one of which was used) and one dump tank which had provisions for removing the afterheat from the fuel.

The relatively high melting point of the circulating fuel (about 1000°F for the NaF-ZrF₄-UF₄ fuel containing 6.18% UF₄) required that all equipment within which it was circulated be heated sufficiently to permit loading, unloading, and low-power operation. This heating was accomplished by means of electrical heaters attached to all components of the fuel and sodium systems; i.e., pressure shell, heat exchanger, pumps, and tanks, as well as all fuel and sodium piping.

In addition to the heaters and insulation, all fuel and sodium piping was surrounded by a 1- to 1½-in. annulus (inside the heaters) through which helium was circulated. The helium circulated through the annuli was monitored at various stations around the system for evidence of leaks and was, in addition, a safety factor in that it could be expected to keep hot any spots at which heater failures occurred.

SODIUM SYSTEM

The sodium circuit external to the reactor, shown in Fig. 2.6, was similar to that of the fuel. The sodium flowed from pump to reactor, to heat

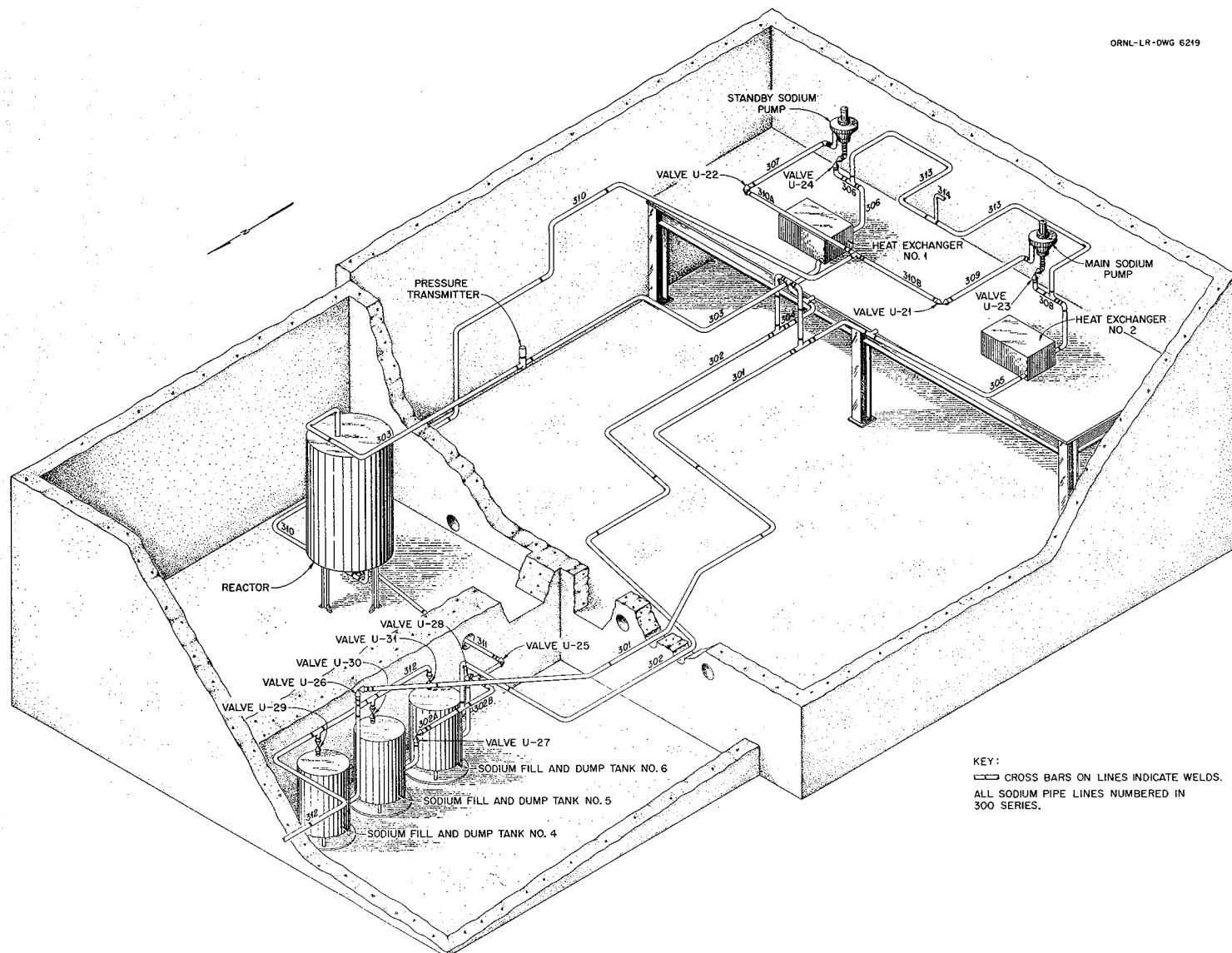


Fig. 2.6. Isometric Drawing of Sodium System.

exchanger, to pump. The sodium pumps were gas-sealed centrifugal pumps of the same design as the fuel pump, except that a smaller expansion volume was provided. Again, there were two sodium pumps, one of which was a spare in parallel with the operating pump.

The sodium was circulated through the two parallel sodium-to-helium heat exchangers after being heated in the reactor. Again the heat was transferred via the helium to water in two helium-to-water heat exchangers. The sodium system was equipped with heaters, as was the fuel system, and all piping was surrounded with the helium annulus for leak monitoring and heat distribution.

PROCESS INSTRUMENTATION

Since a basic purpose of the ARE was the acquisition of experimental data, the importance of complete and reliable instrumentation could not be overemphasized. Therefore there were 27 strip temperature recorders (mostly multipoint), 5 circular temperature recorders, 7 indicating flow controllers, 9 temperature indicators (with up to 96 points per instrument), about 50 spark-plug level indicators, 20 ammeters, 40 pressure gages, 16 pressure regulators, and 20 pressure transmitters. In addition there were numerous flow recorders, indicators, alarms, voltmeters, tachometers, and assorted miscellaneous instruments.

Most ARE process instrumentation was installed to permit observing and recording rotational speeds, flow rates, temperatures, pressures, or liquid levels. The operating values of temperature, pressure, and flow at various stations around the ARE fluid circuits are given in Appendix B. Since most commercially available instruments for measuring flow and pressure are subject to temperature limitations considerably lower than the minimum operating temperature of the ARE and they employ open lines in which the ZrF_4 vapor could condense, they were not suitable for ARE applications. Therefore a bellows type of device was adapted for use as a pressure indicator, and a fluid-immersed inductance type of instrument was developed for measuring sodium and fuel liquid level and fuel flow.² Sodium flow was measured by an electromagnetic flowmeter. Conventional chromel-alumel thermocouples welded to the pipe walls were used to determine temperatures. The

instrumentation flow sheet is shown in Fig. 2.7. Most of the indicating and recording instruments were located in the control room. While numerous important temperatures were recorded in the control room, about 75% of the thermocouples were indicated (or recorded) only in the basement.

NUCLEAR INSTRUMENTATION AND CONTROLS

Detailed information on the important nuclear instrumentation and controls is presented in Appendix C. Briefly, the nuclear instrumentation (such as fission chambers and ion chambers), the electronic components (such as preamplifiers and power amplifiers), and the control features of the ARE were similar, and in many cases identical, to those of the MTR, the LITR, and other reactors now in operation. However, since the fission chambers were located in a high-temperature region within the reflector, it was necessary to develop special high-temperature chambers. Helium was used to cool them to below 600°F.

The locations of the two fission chambers in the reactor may be seen from examination of Fig. 2.3; the locations of the remaining ion chambers are shown on Fig. 2.8. Since the fission chambers moved through sleeves in the reactor which were parallel to those for the regulating and shim rods, it was convenient to group the drive mechanisms with those for the rods in an igloo outside the shielding above the reactor, as shown in Fig. 2.8. All other ion chambers were external to the reactor pressure shell; they viewed the reactor at mid-plane; and they were mounted so that they would move horizontally. These chambers included a BF_3 counter (for the critical experiment), two parallel circular plate (PCP) chambers, and two compensated chambers.

There were two separate elements to the control system — the single regulating rod and the three shim rods. The locations of these rods in the reactor may be seen from examination of Fig. 2.3. The regulating rod had a vertical movement of 12 in. about the center of the reactor and was fabricated of stainless steel. Several such regulating rods, with varying amounts of metal, were fabricated, and the one finally used in the experiment had a total value of 0.4% $\Delta k/k$ for the 12-in. movement and could be moved at a rate of 0.011% ($\Delta k/k$)/sec.

The three safety rods were located in the core on 120-deg points at a radius of 7.5 in. from the

²For greater detail see ANP Quar. Prog. Rep. Sept. 10, 1952, ORNL-1375, p 23.

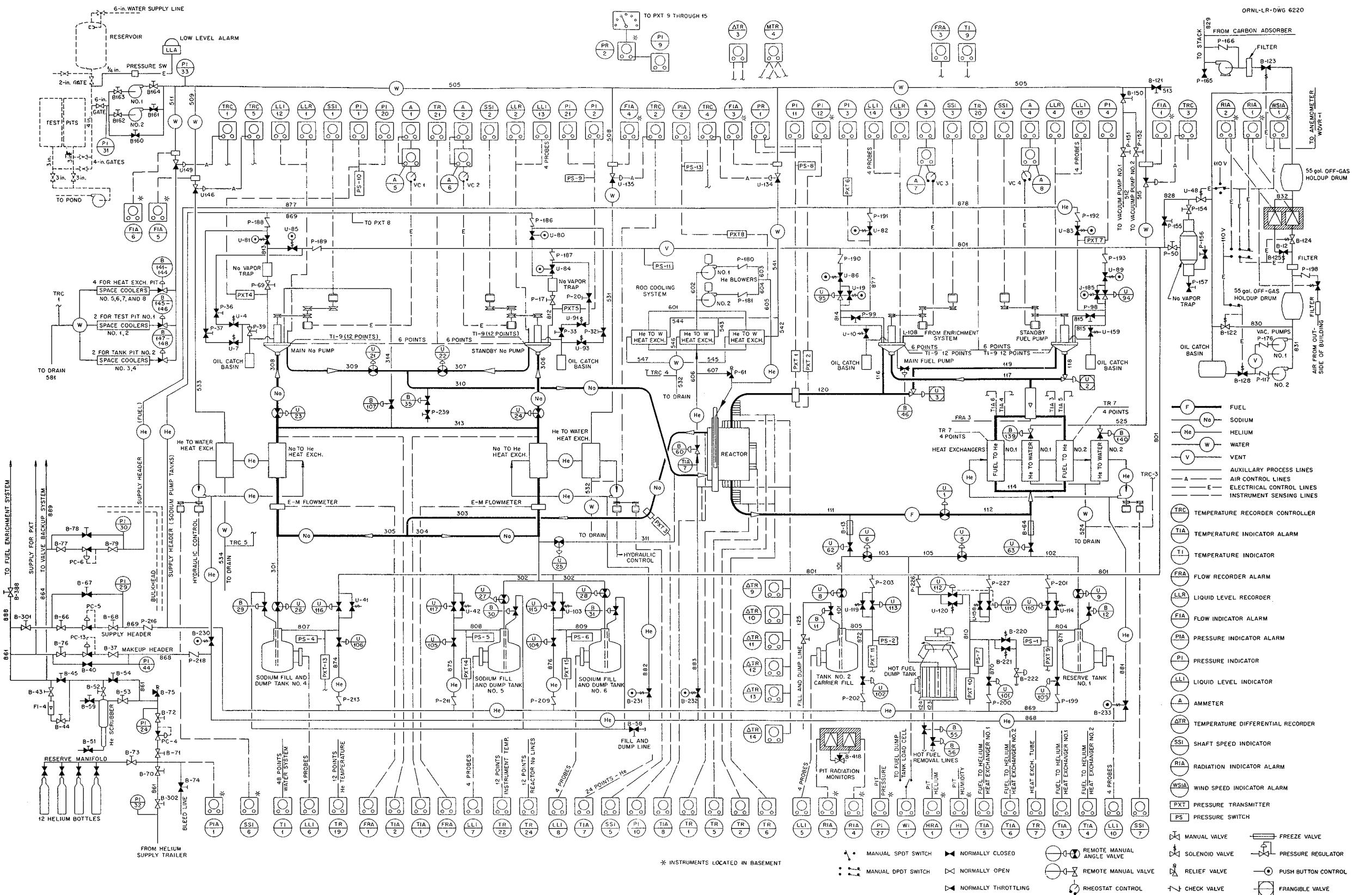
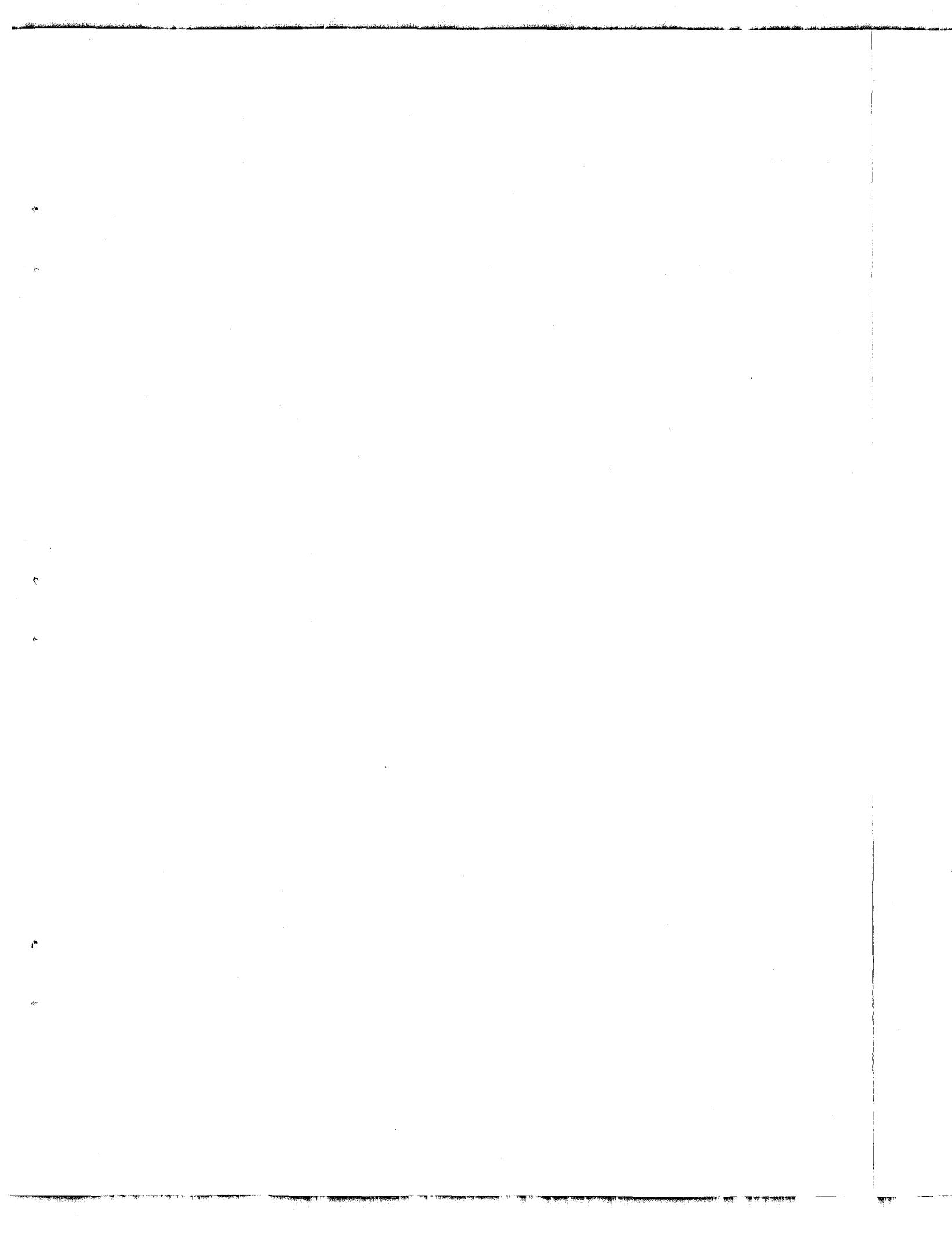


Fig. 2.7. Process Instrumentation.



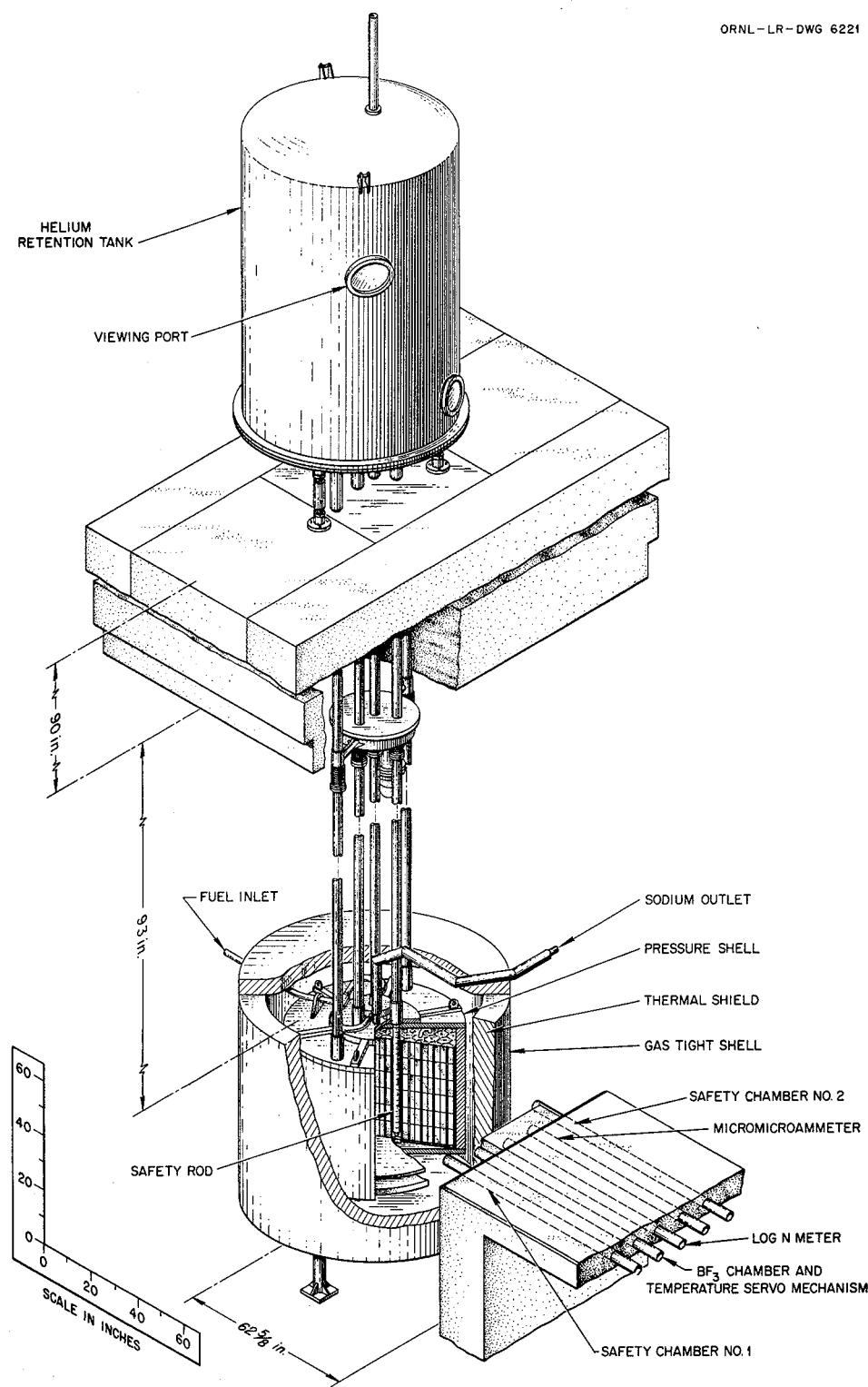


Fig. 2.8. Isometric Drawing of Control Rods and Nuclear Instrumentation.

center of the reactor. Each rod was made up of slugs of a hot-pressed mixture of boron carbide and iron; the slugs were canned in stainless steel. The canned sections were slipped over a flexible tube. The total rod travel was 36 in., and 13 min was required for withdrawal of the rod. Thus, the 5.8% $\Delta k/k$ in each rod (total for the three was approximately 17% $\Delta k/k$) could be withdrawn at a rate of 0.45% ($\Delta k/k$)/min per rod.

A small amount of the helium used to cool the fission chambers was directed through the shim and regulating rod holes, but the helium flow was so low that not much cooling was effected. This helium was circulated in an independent circuit, known as the rod cooling system, which had two two-speed helium blowers in parallel and three helium-to-water heat exchangers. The helium circulated from the blowers through the rod sleeves and fission chamber sleeves to the heat exchangers and back to the blowers, and it removed, in the process, up to 35 kw of reactor heat. Part of the helium returning from the reactor was diverted through pipe annuli before reaching the heat exchanger.

OFF-GAS SYSTEM

The off-gas system was designed to permit the collection, holdup, and controlled discharge of the radioactive fission products that were evolved as a consequence of reactor operation. Although only the gases above the fuel system were expected to have significant activity, the gas from the sodium system was also discharged through the off-gas system. As shown in Fig. 2.9, there was, in addition to the primary off-gas system, an auxiliary system for discharging gases from the pit through nitrogen-cooled charcoal tanks.

In the primary system the off gases from both the fuel and the sodium were directed to a common vent header. From this header, helium plus the volatile fission gases passed through a NaK scrubber, which removed bromine and iodine, and then into two holdup tanks, which were connected in series, to permit the decay of xenon and krypton. From these the gases were released up the stack. The release of gases to the stack was dependent

upon two conditions: (1) a wind velocity greater than 5 mph and (2) radioactivity of less than $0.8 \mu\text{c}/\text{cm}^3$. The activity was sensed by a monitor which was located between the two holdup tanks.

FUEL ENRICHMENT SYSTEM

The fluoride fuel used in the ARE was amenable to a convenient enrichment technique in which the fuel system was first filled with a mixture of the fluorides of sodium and zirconium. When this mixture, NaZrF_5 , had been circulated for a sufficient time to ascertain that the reactor was ready to be taken critical (no leaks, etc.), uranium in the form of molten Na_2UF_6 was added to the fluorides then in the system. The temperature contour diagram of the $\text{NaF-ZrF}_4\text{-UF}_4$ system is shown in Fig. 2.10. The melting point of Na_2UF_6 was 1200°F , and there were no mixtures of higher melting points on the join between Na_2UF_6 and NaZrF_5 , which is shown in Fig. 2.11. The addition of Na_2UF_6 raised the melting point of the mixture only slightly above that of NaZrF_5 (955°F).

It was initially intended that the enrichment operation would consist of the remote addition of Na_2UF_6 to the system from a large tank which contained all the concentrate. From the large tank, the concentrate was to pass through an intermediate transfer tank which would transfer about 1 qt or less at a time. The intermediate tank was suspended from a load beam so that the weight of the concentrate could be determined before each addition of enriched material. However, this system was discarded when preoperational tests proved the temperature control of the system to be inadequate; in addition, the accuracy of the weight-measuring instrumentation on the transfer tank was uncertain.

In lieu of the original enrichment system, a less elaborate, more direct method of concentrate addition was employed. The enrichment procedure actually used involved the successive connection of numerous small concentrate containers to an intermediate transfer pot, which, in turn, was connected to the fuel system by a line which injected the concentrate into the pump tank above the liquid level.

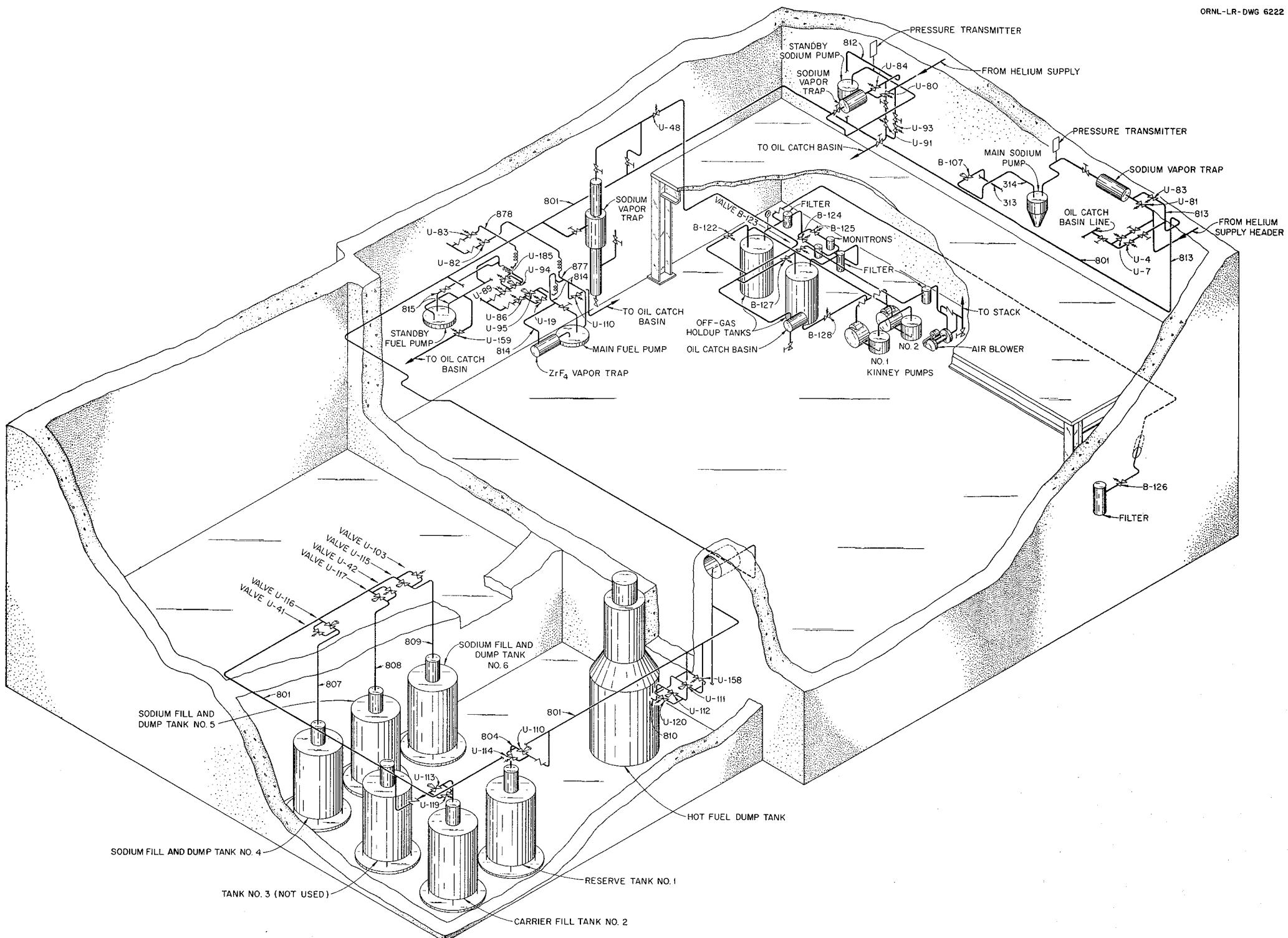
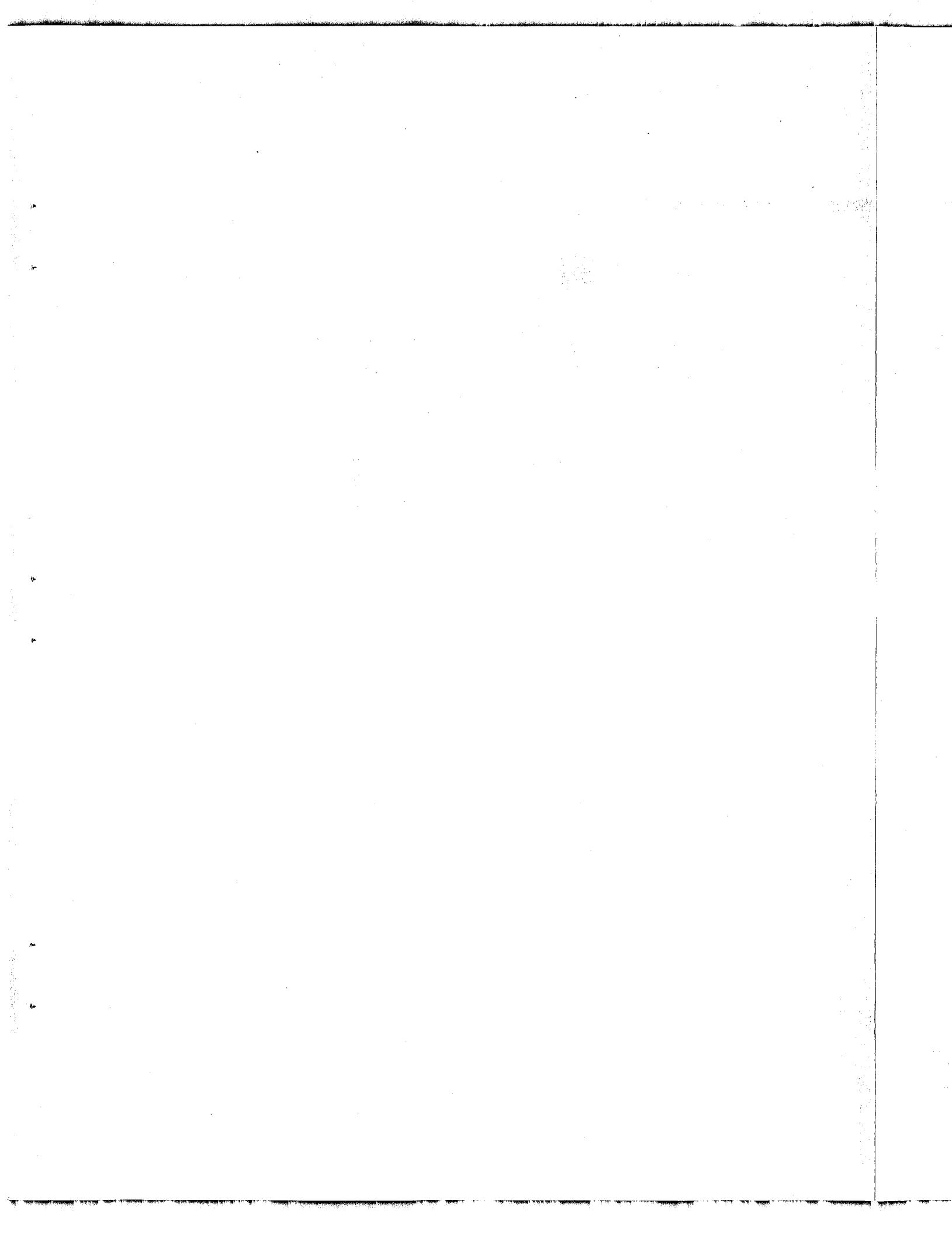


Fig. 2.9. Isometric Drawing of Off-Gas System.



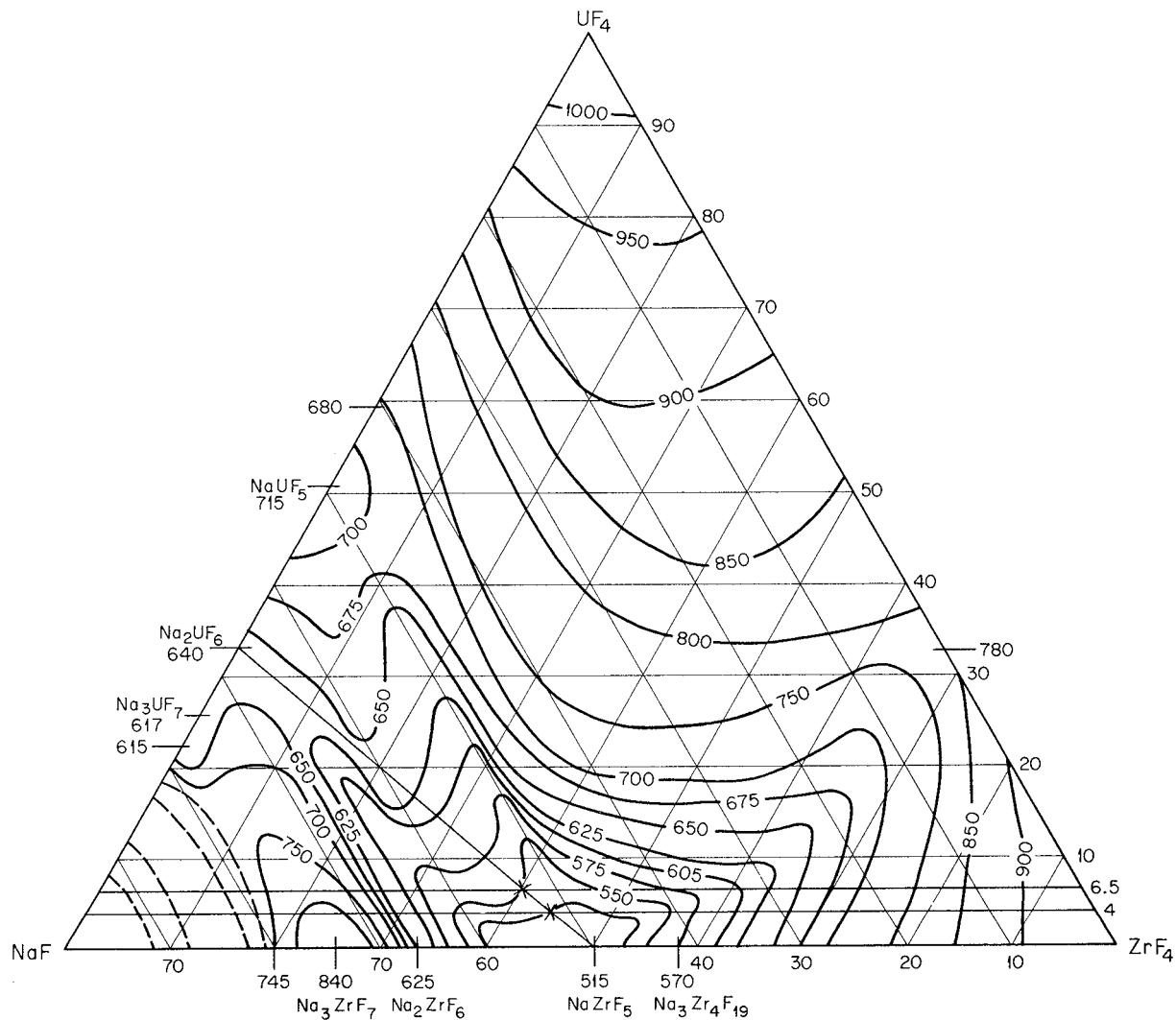


Fig. 2.10. The System NaF-ZrF₄-UF₄.

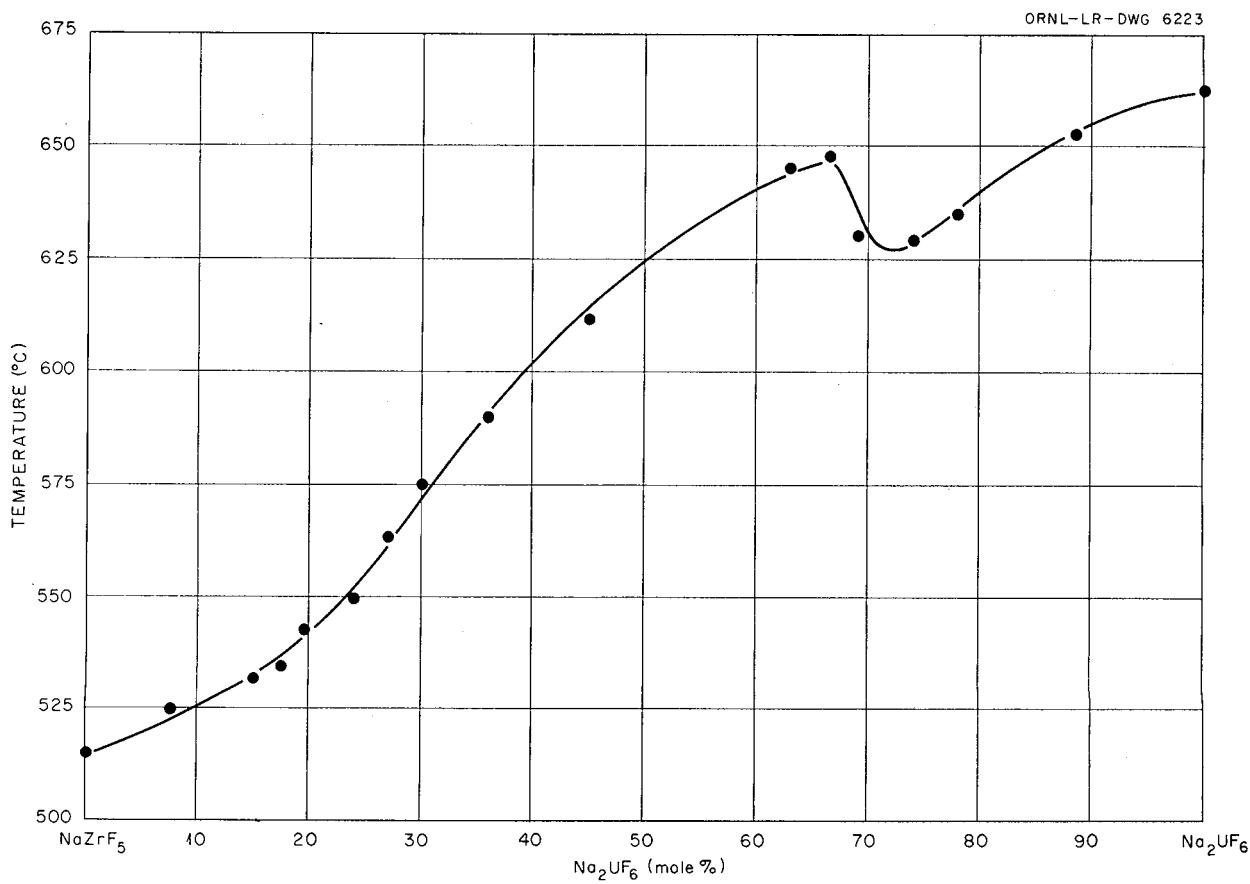


Fig. 2.11. The Pseudo-Binary System $\text{NaZrF}_5\text{-Na}_2\text{UF}_6$.

3. PRENUCLEAR OPERATION

It is not the purpose here to describe in detail the preliminary checks and shakedown tests which preceded the nuclear operation of the system because this information is covered in the design and installation report.¹ However, some understanding of the scope and significance of these "preliminary" tests is desirable, particularly since at the conclusion of this phase of the operation the fuel and sodium systems were left filled with clean carrier and sodium, respectively, and the fuel system was ready for the fuel enrichment operation which comprised the critical experiment.

The preliminary tests accomplished many purposes, the more important being the cleaning and leak-checking of the systems, performance and functional testing of components, checking and calibrating of instruments, and the practicing of operational techniques. The system, as an integral unit, was sufficiently assembled by August 1 for the operating crews to be placed on a three-shift basis so that intensive tests on the various systems, initially with water as the circulating fluid, could be started. There were, however, frequent delays while changes and modifications that the testing indicated as being desirable or necessary were made. The operation with sodium, in particular, was responsible for major changes in the sodium vent system and the elimination of the sodium purification system. Tests with sodium and carrier in the systems were concluded on October 30, at which time the system was ready for the critical experiment.

CIRCULATION OF SODIUM

By the last week in September, all temperature tests preliminary to operation of the sodium system had been completed. It was necessary to operate the sodium system before operating the fuel system because the sodium was used to heat the reactor to above the fuel melting point. In preparation for filling the sodium system, the temperature of the entire system was brought to 600°F and sodium was transferred from portable drums into the system fill tanks. The sodium used had been carefully filtered to minimize the oxygen content, which at the time of the filling averaged about 0.025 wt %.

¹*Design and Installation of the Aircraft Reactor Experiment, ORNL-1844 (to be issued).*

The system was filled with sodium on the morning of September 26. No particular difficulties were encountered during the filling or when the sodium pumps were operated at design speed, although there was evidence of trapped gas in the system. The electromagnetic flowmeters, which were at first inoperative, functioned properly after sufficient time had elapsed for wetting of the pipe wall to occur. On the following afternoon a leak developed in a tube bend in the sodium purification system, so the sodium was dumped.

Subsequent analyses revealed that the leak occurred where a thermocouple pad had been heliarc welded to the tube. The excessive weld penetration which caused the leak was attributed to a lack of instruction to the welder that a variation in pipe wall thickness existed in this section.

As a consequence of this leak and difficulties experienced during draining of the sodium, a number of changes were made in the sodium system. The purification systems were eliminated and provisions were made for better heat control for all vent lines and valves to prevent freezing of the sodium and plugging of the lines. It was concluded that the sodium purification system could be removed without endangering the experiment because experience in operating the system had proved that the oxygen contamination was very low; furthermore, there was no danger of the oxide plugging the heat exchanger tubes because of the low temperature differential in the system and the large diameters of the tubes in the heat exchangers. It was felt, also, that the purification system represented the weakest link in the fluid circuit because thinner walled tubing had been used there than anywhere else in the system, except for the reactor tubes, which were assembled with extreme care. Even so, the thin-walled tubing in the purification system would probably not have presented a problem had the thermocouples been properly welded.

On October 16 the sodium was recharged into the system at 600°F, circulated, and dumped four times to thoroughly check the operability of the sodium system. Analyses of the sodium taken both at 600 and 925°F showed the oxygen content to be satisfactorily low (of the order of 0.026 wt %), and therefore the initial batch of sodium was not replaced. The sodium was circulated for several days at 1300°F before fuel carrier, NaZrF₅, was

added to the fuel tank. During the period of sodium circulation, the typical system characteristics were those given in Figs. 3.1 and 3.2. The data were comparable to those obtained during the water tests.¹ Such discrepancies as existed were within experimental error and could easily have been due to changes in the system that were made during the time between the two tests, such as the removal of the purification systems and the removal of the bypass around the reactor during the water tests.

During and after the second sodium loading operation the copper gauze in the helium stream was monitored and no evidence of sodium leakage was found. With helium in the fuel system the temperatures in the fuel and sodium systems were

then gradually raised (about 10°F/hr) to 1300°F. After the 1300°F temperature was reached, the helium pressure in the fuel system was reduced to 0.5 psig and sufficient krypton was added to bring the system pressure up to 5.0 psig. The helium in the annuli was then sampled and analyzed for krypton, and no evidence of a leak was found.

CIRCULATION OF FUEL CARRIER

With the system isothermal at 1300°F, the fuel carrier, NaZrF₅, was loaded into the fill tank at 1200°F, and the fuel system was evacuated to facilitate raising the fluoride into the system. This filling operation, which occurred on October 25, required only a few minutes once the desired vacuum was attained. During the filling operation it was possible to follow the progress of the fluoride through the system by watching the thermocouple indications along the pipe because of the 100°F temperature difference between the initial fluoride temperature and the system temperature. In contrast to the sodium system, there did not appear to be any gas trapped in the fuel system after loading; evidence of this was that there was no liquid level change when the pressure in the pump was changed, and the temperature differentials across the six parallel fuel passages in the reactor changed simultaneously when a temperature perturbation was put into the system.

Five samples of the carrier were taken, and the analytical results from each showed the concentrations of impurities and corrosion products given in Table 3.1.

There was twice as much carrier available as was required to fill the system, and if chemical analyses of samples of the carrier after it had been circulated for about 50 hr had indicated too high a corrosion-product buildup (as could have resulted if the system had not been adequately cleaned), the carrier in the system would have been dumped and replaced with the extra carrier. However, from the very favorable analyses of the first two samples it was apparent that replacing the carrier would not be necessary. (The chromium content would have had to have been 500 ppm to have necessitated the replacement. The corrosion mechanism that defines the upper limit of the chromium content is described in detail in ORNL-1844.¹)

During the time the carrier was being circulated and before the enrichment operation commenced, the system characteristics were determined. The

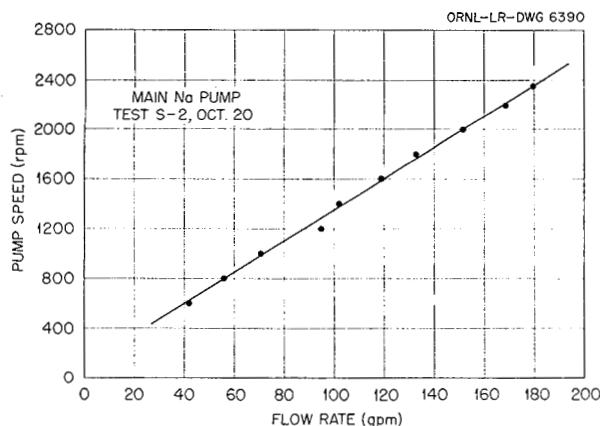


Fig. 3.1. Pump Speed vs Sodium Flow Rate.

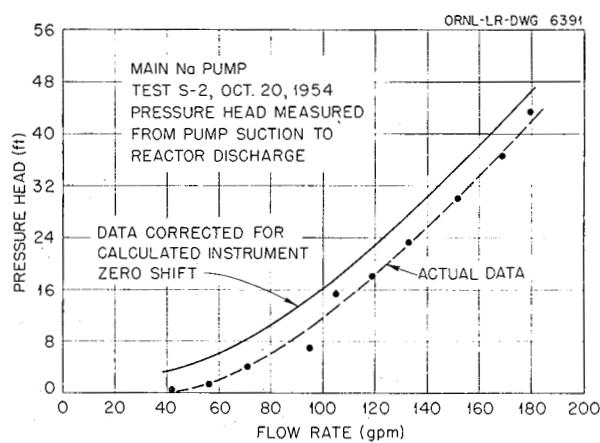


Fig. 3.2. Pressure Head vs Sodium Flow Rate.

TABLE 3.1. ANALYSES OF IMPURITIES AND CORROSION PRODUCTS IN CARRIER SAMPLES

Date	Time	Running Time (hr)	Impurities and Corrosion Products Found (ppm)		
			Cr	Fe	Ni
10/25	1650	9.7	90	<5	50
10/26	0214	19.1	81	<5	40
	1911	36.1	81	<5	6
10/27	1919	60.2	90	18	12
10/29	0935	98.5	102	30	20

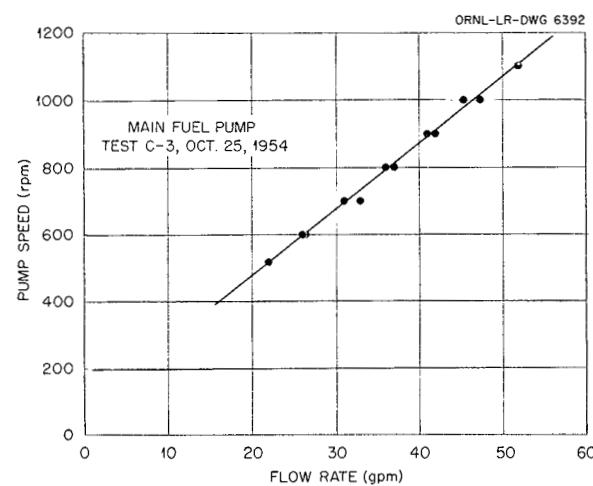


Fig. 3.3. Pump Speed vs Fuel Carrier Flow Rate.

data obtained in terms of pump speed vs flow and system head vs flow are given in Figs. 3.3 and 3.4, respectively. These data were considerably different from those to be expected from an extrapolation of the water data. The discrepancies are analyzed in more detail in ORNL-1844,¹ but the only completely satisfactory explanation is that the system head during the water test was too high, possibly due to the temporary water Rotameter installation or to one or more of the reactor tubes not being completely filled so that only partial flow was obtained through the reactor during the water test.

FINAL PREPARATIONS FOR NUCLEAR OPERATION

By this time the neutron source had been placed in the reactor and the nuclear instrumentation

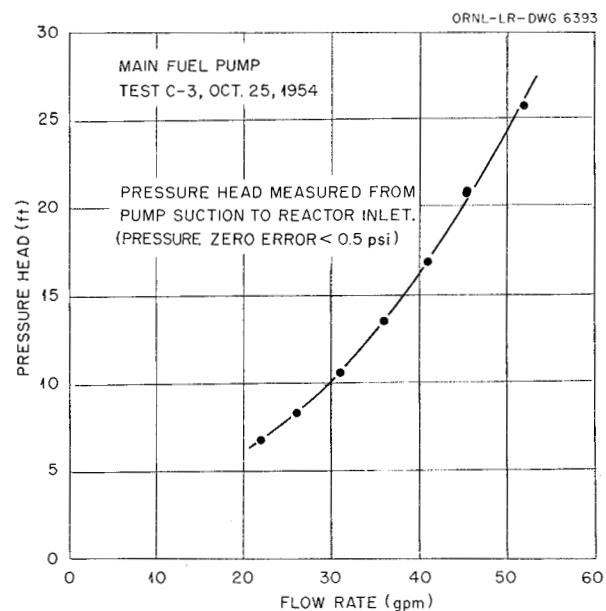


Fig. 3.4. Pressure Head vs Fuel Carrier Flow Rate.

checked out. A BF_3 counter was installed in one of the instrument holes external to the reactor in order to check the fission chambers during the critical experiment. Pulse height and voltage curves were measured on all three fission chambers (the two regulars plus a spare) in order to establish the operational plateau for each chamber.

The mechanical operation tests of the regulating rod and of the three safety (shim) rods were made; in all, over 25 rod drop tests were performed in order to ensure the reliability of the rod insertions at high (1200 to 1300°F) temperatures. The rod drives were also continuously cycled in order to check the performance of the gear trains and

motors. During this time the rod magnet faces were cleaned, and, in order to maintain more uniform drop currents, it was decided to keep the magnet faces engaged at all times when the rods were not in use.

Before the fuel concentrate (Na_2UF_6) was charged to the enrichment system, a number of practice operations were performed with carrier in the enrichment system. The temperature control of the system was inadequate and the operation of the weigh cell on the transfer tank was such that reproducible weights could not be obtained. Although the enrichment system probably could have been made to work, considerable time would have been required. Accordingly, the original enrichment system was abandoned, and a manually operated system was improvised. The concentrate was first batched down into a number of containers.

The concentrate in each of these containers was then added to the fuel system at the pump after first passing through an intermediate transfer pot. The amount of concentrate added was determined by weight measurements of the concentrate containers before and after use. While this system was being set up, the operating crews were engaged in leak testing the various auxiliary systems, determining operability of heater circuits, checking and reading thermocouples, establishing the performance of the pump lubrication and cooling systems, checking the operation of the annulus system helium blowers, monitoring the annulus helium for leaks, and checking the operability of the various off-gas systems, instrumentation, and the like. By the morning of October 30, these tests were sufficiently well in hand for the critical experiment to commence.

4. CRITICAL EXPERIMENT

On October 30 the sodium had been circulating 275 hr, and the fuel carrier about 110 hr. Both the sodium system and the fuel system were at an isothermal temperature of 1300°F, and the fuel system was ready for the addition of concentrate (Na_2UF_6) to the carrier (NaZrF_5). The addition of the concentrate was necessarily time-consuming because of the cautious manner in which each addition had to be made during the approach to criticality; however, this operation would have been completed more rapidly had it not been for unforeseen difficulties. The reactor did not reach criticality until 3:45 PM, November 3, some four days after the enrichment operation was started. Unfortunately, much of the four days was spent in removing plugs and in repairing leaks which occurred in the enrichment line. Since these leaks were largely the result of the improvised nature of the enrichment mechanism, they were not of serious consequence.

The chronology of the critical experiment is shown in Fig. 4.1, and a detailed description of the experiment, including a subcritical temperature coefficient measurement, is presented below. The critical experiment, as well as all nuclear operations, followed, in general, the pattern prescribed in the "ARE Operating Procedures, Part II, Nuclear Operation,"¹ which is included in this report as Appendix D.

ENRICHMENT PROCEDURE

By the afternoon of October 30 the chemists had installed and checked out the injection apparatus, and the systems were ready for the enrichment operation to commence. The loading station was located directly above the main fuel pump. The injection rig consisted of an oven into which the batch cans fitted, an intermediate, heated transfer pot capable of holding about 5.5 lb of concentrate, a resistance-heated transfer line connecting the batch can with the transfer pot, and the electrically heated injection line running from the transfer pot into the pump, as well as various auxiliary equipment, such as helium supply and vent lines, vacuum pump, pressure control, and electrical heating equipment. The resistance-heated transfer line was left exposed to the air so that blow

torches could be applied in case of a plug. A flow sketch of the injection system is shown in Fig. 4.2.

The fuel concentrate was batched into small cans prior to loading. The three batch sizes are given in the following tabulation:

Can Size	Approximate Concentrate Weight (lb)
A	30
B	10
C	0.5

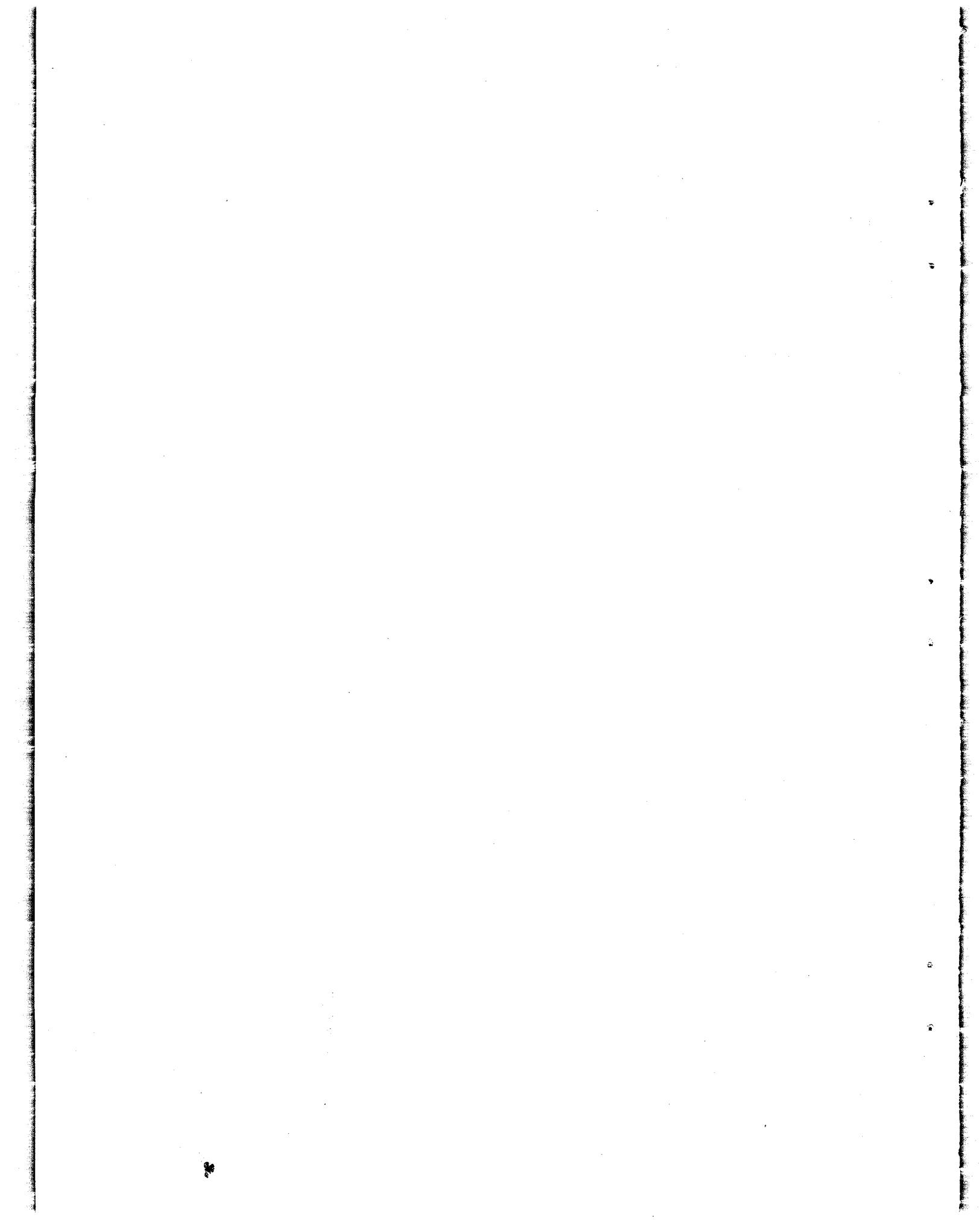
The A and B size cans were used during the critical experiment. The C size cans were held for use in calibrating the regulating rod. Table 4.1 lists the batch cans by numbers in the order in which the cans were used in the critical experiment, the net amount of concentrate and uranium added, and the U^{235} content.

Prior to an injection a batch can was selected, set in the oven, and heated to 1400°F. Meanwhile the transfer lines were being heated. When proper temperatures were reached, an injection was attempted. The intermediate transfer pot was filled from the batch can by pressurizing the batch can and venting the transfer pot. At the same time the pump pressure was maintained above that of the transfer pot so that there could not be an inadvertent transfer into the pump. When the spark plug probes indicated that the transfer pot was full, the pressure in the batch can was released, and the material in the transfer pot was forced into the pump by helium pressure. This method of transfer was used so that only a measured amount of concentrate (not more than 5.5 lb) could be added at a given time and the system pressures could be kept low. With low system pressures there was less need for venting and possibly clogging the vent lines. Figure 4.3 shows a photo of the chemists preparing for an injection during the critical experiment.

EARLY STAGES OF THE EXPERIMENT

At 1500 on October 30 the critical experiment was started. The main fuel pump was first trimmed to its minimum prime level and the shaft speed was reduced to 500 rpm (20-gpm flow). At this

¹J. L. Meem, *ARE Operating Procedures, Part II, Nuclear Operation*, ORNL CF-54-7-144 (July 27, 1954).



CHRONOLOGY OF THE CRITICAL EXPERIMENT

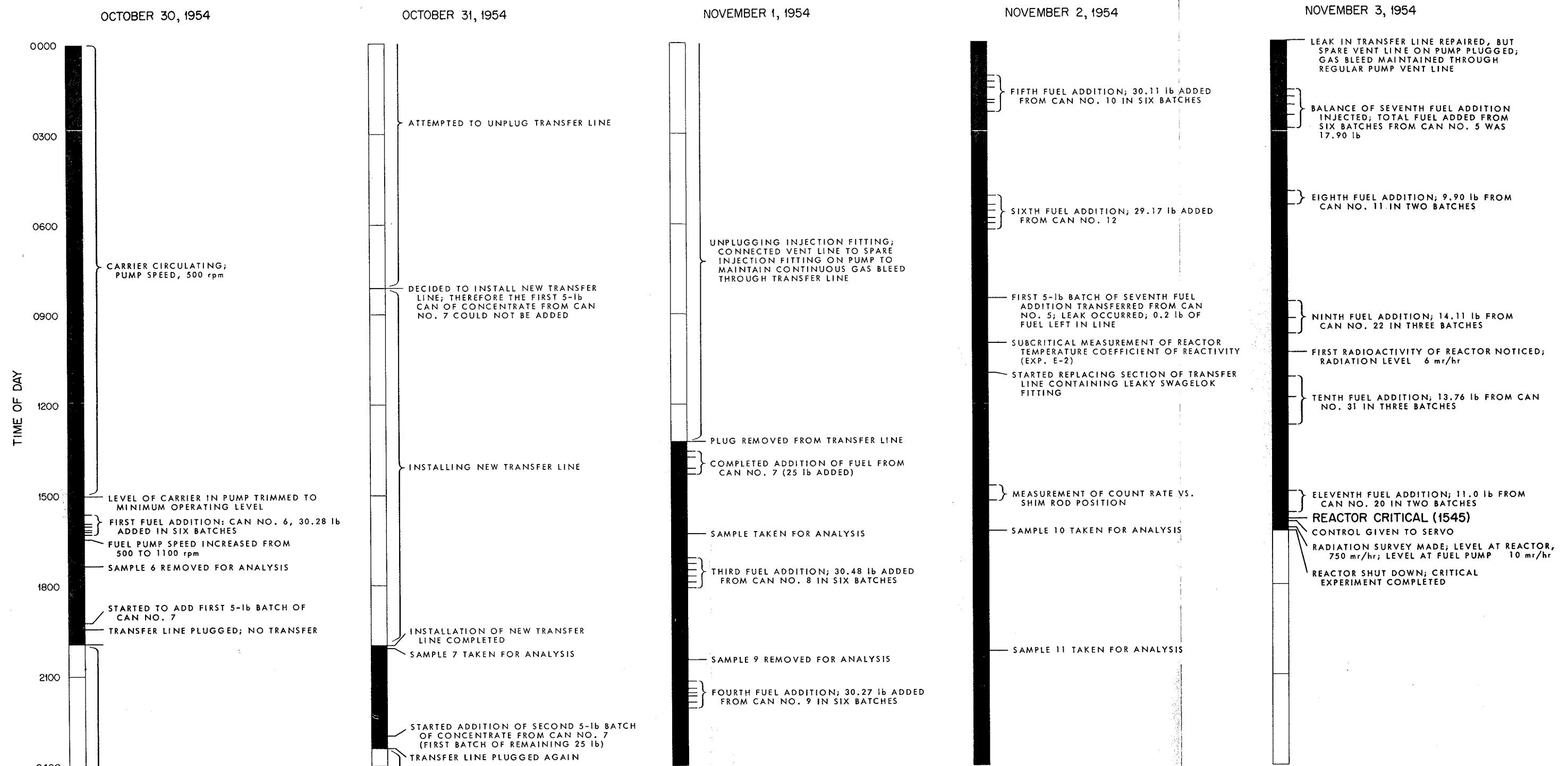
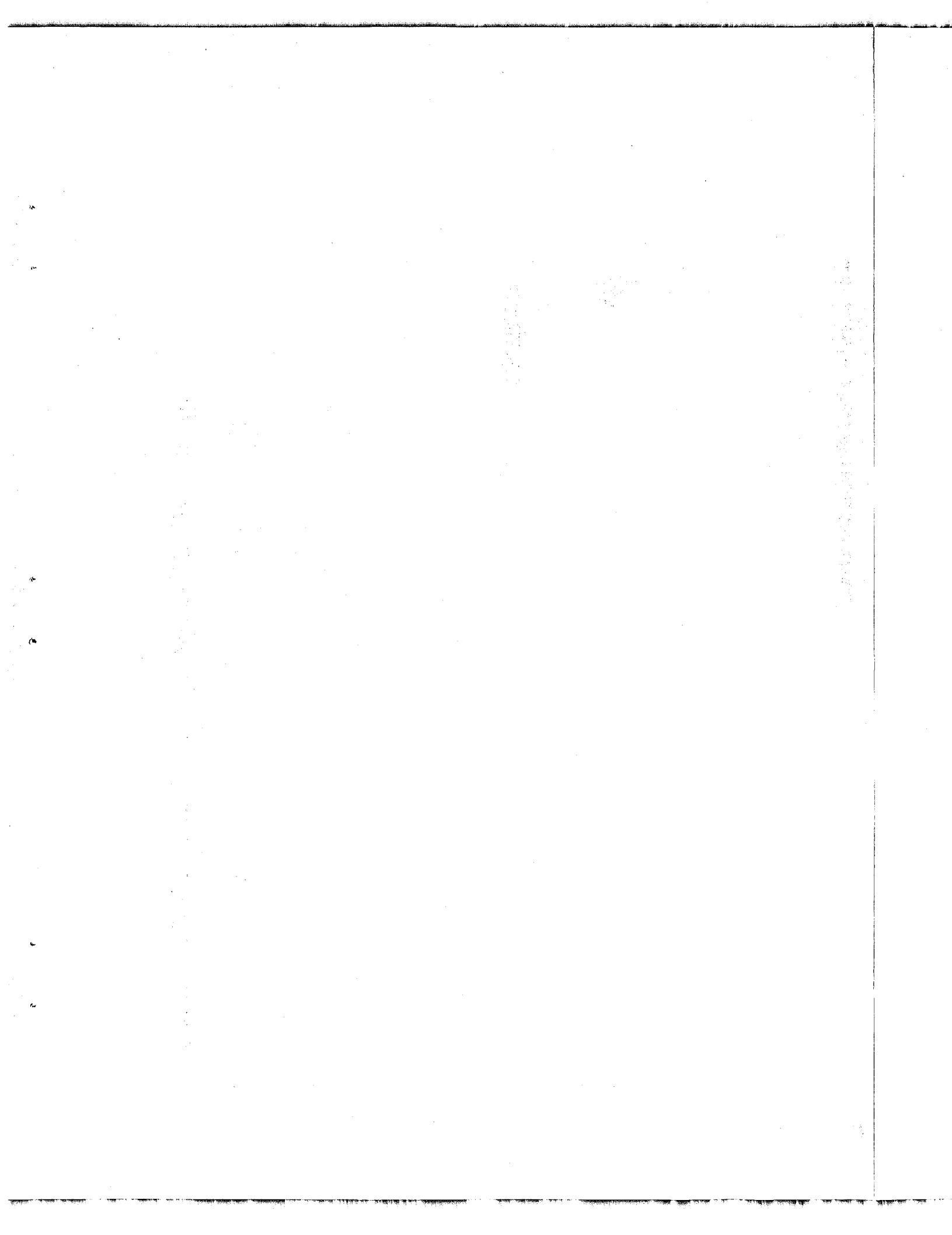


Fig. 4.1.



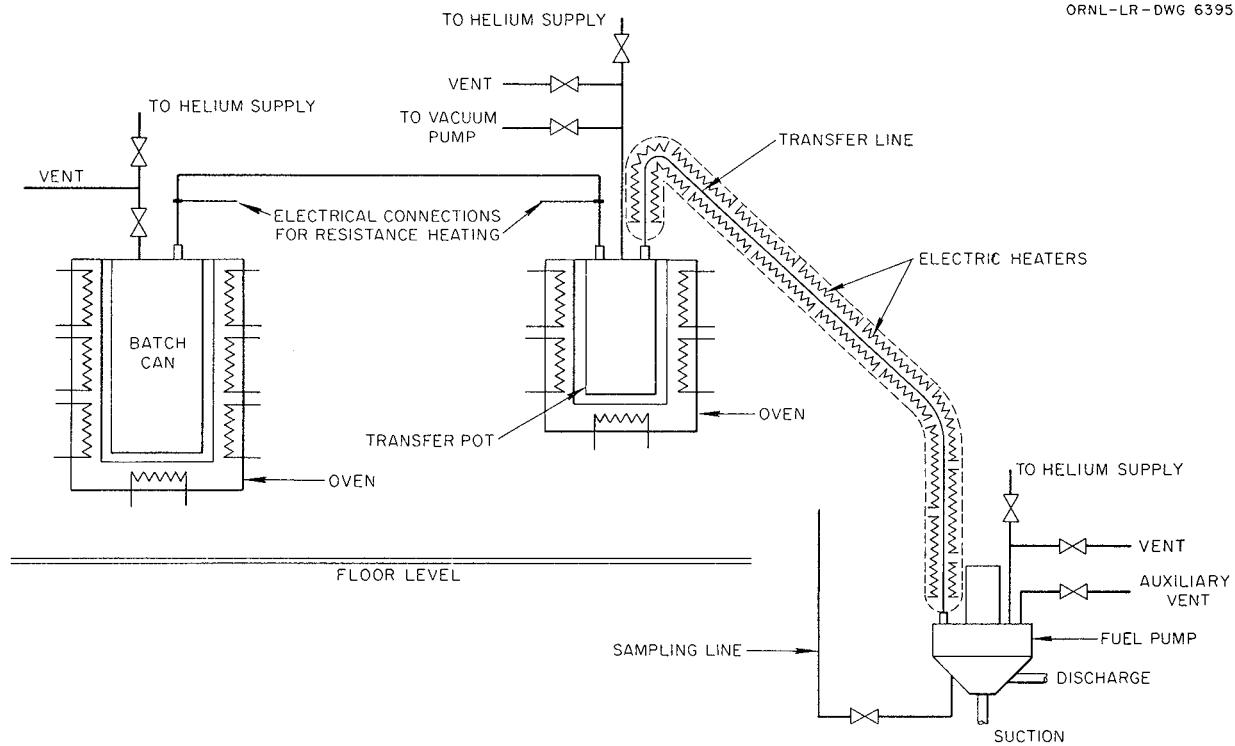


Fig. 4.2. Equipment for Addition of Fuel Concentrate to Fuel System.

TABLE 4.1. FUEL CONCENTRATE BATCHES ADDED DURING CRITICAL EXPERIMENT

Date	Time	Batch Can No.	Concentrate Added		Uranium Added		Weight of U ²³⁵ Added	
			g	lb	wt %	g	g	lb
10/30	1625	A-6	13,609	30.002	59.548	8104	7569	16.687
11/1	1415	A-7	11,510	25.375	59.513	6850	6398	14.105
	1804	A-8	13,852	30.538	59.530	8246	7702	16.980
	2203	A-9	13,806	30.437	59.587	8227	7684	16.940
11/2	0213	A-10	13,638	30.066	59.454	8108	7573	16.695
	0610	A-12	13,241	29.191	59.531	7882	7362	16.230
	0831	A-5	8,221	18.124	59.637	4903	4579	10.095
11/3	0523	A-11	4,505	9.932	59.671	2688	2511	5.536
	0941	B-22	6,432	14.180	59.702	3840	3587	7.908
	1245	B-31	6,312	13.915	59.637	3764	3516	7.751
	1536	B-20	4,567	10.068	59.529	2719	2540	5.600

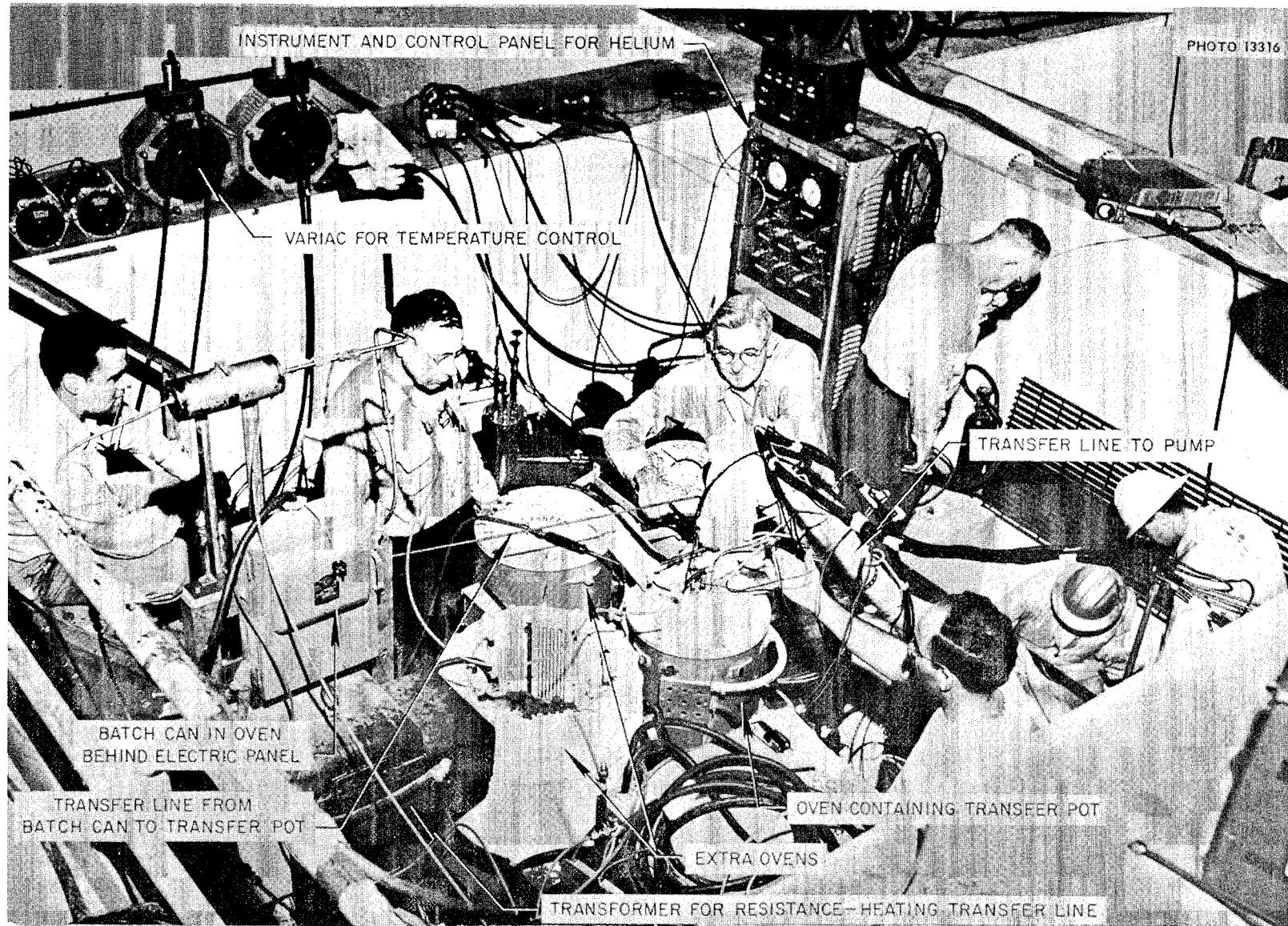


Fig. 4.3. Chemists Preparing for Enrichment Operation During Critical Experiment.

time the volume of carrier in the fuel system was calculated to be 4.82 ft^3 , and the weight was 927 lb. At 1507, concentrate transfer was started from batch can A-6 to the intermediate tank, and, at 1539, transfer of the first 5.5 lb of fuel to the system was accomplished. At 1554, the second 5.5 lb of fuel had been added. These fuel injections very noticeably affected the fission chamber recorders. Mixing of the concentrate with the carrier did not occur rapidly, and therefore each time the enriched slug entered the reactor it produced a multiplication that was observable on the fission chamber count-rate recorder. Figure 4.4 is a photograph of the trace of fission chamber No. 1; the pips that occurred during addition of the first and second slugs of fuel are readily observable. From the time interval between pips, which was almost

²The first five samples taken prior to this time were for carrier impurity analysis. These five analyses were discussed in chap. 3, "Prenuclear Operation."

exactly 2 min, and the volume of the fuel system,

a check on the rate of fuel flow was obtained:

$$f (\text{gpm}) = \frac{4.82 (\text{ft}^3) \times 7.48 (\text{gal}/\text{ft}^3)}{2 (\text{min})}$$

$$= 18.03 .$$

This checked fairly well with the value of about 20 gpm read from the fuel flow recorder.

The remaining four injections from can A-6 were accomplished smoothly. The pumps were speeded up to an observed fuel flow rate of 46 gpm to obtain better mixing of the fuel. At 1720, fuel sample 6 was removed for analysis.²

At 1920 the first 5.5-lb injection from can A-7 was started, but the transfer line from the intermediate pot to the pump clogged due to concentrate freezing in it. After several hours of unsuccessful attempts to free the line, a gas leak occurred in the transfer line at the intermediate tank pot, and

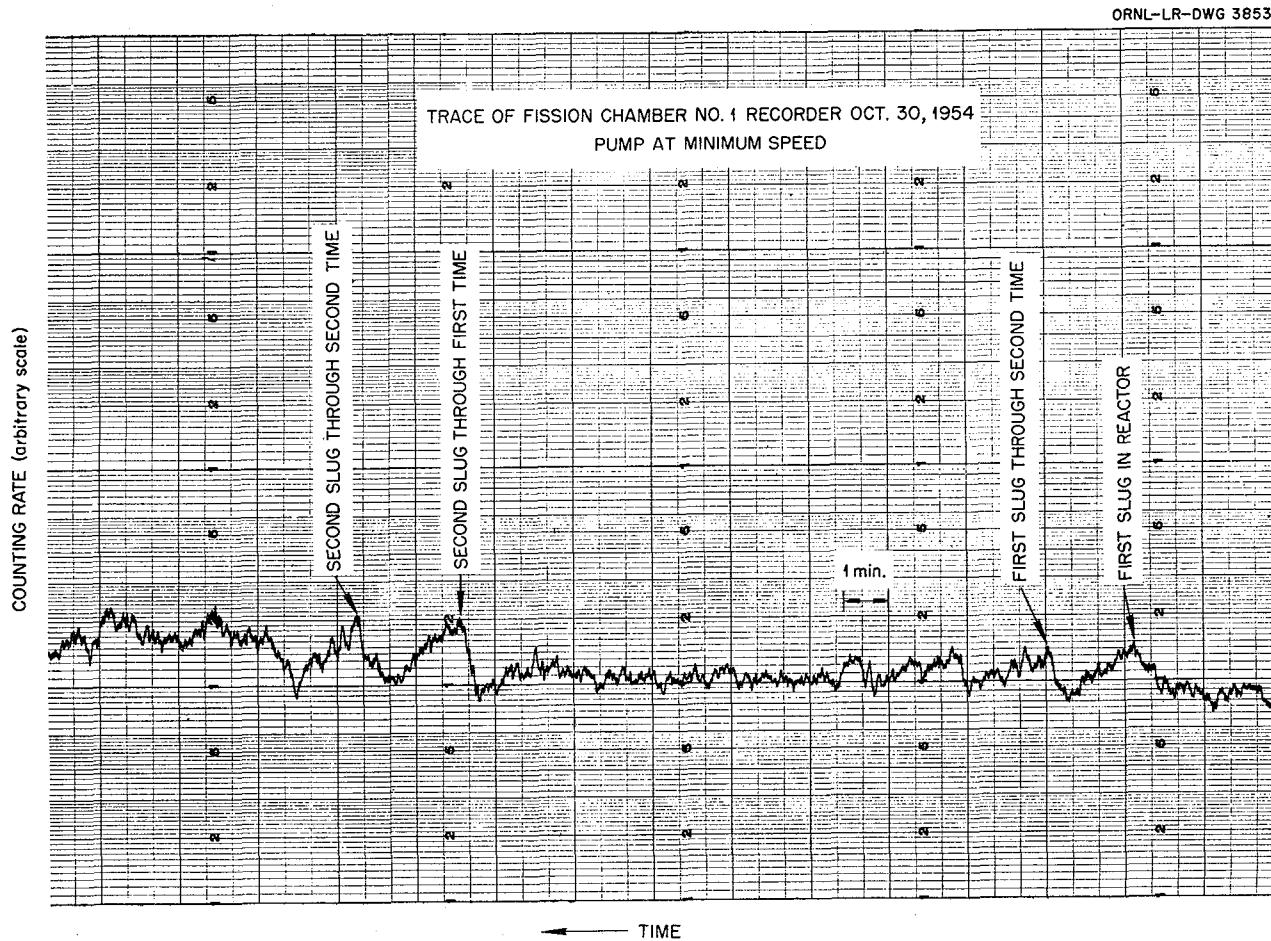


Fig. 4.4. Passage of Enriched Slugs Through Reactor.

it was then decided to install a new transfer line and transfer pot. At this time it was reported that no transfer of concentrate had been made to the pump from can A-7. The first 5.5 lb of can A-7 was lost to the experiment through the leaks and in the plugged line.

At 2000 on November 1, the new transfer line and tank were installed and checked out ready for use. At 2006, fuel sample 7 was drawn for analysis, and, at 2300, the critical experiment was resumed. When the first 5.5-lb slug was injected, periodic pips were again observed on the fission chamber recorder. These pips had a period of 47 sec which, together with a pump speed of 1080 rpm, yielded a calculated fuel flow of 46 gpm, which corresponded to the flow observed on the fuel flowmeter.

At 2315, while attempting the next 5.5-lb transfer, the line again froze. The line was disconnected and found to be plugged at the injection fitting through the pump flange. It was therefore decided to increase the current to the resistance-heated fitting and to add a separate vent line from the pump so that the chemists could continue to "blow through" the transfer line and out the new vent line without raising the system pressure.

By 1320 on November 1 the new vent line had been installed and the transfer system was again in operating condition. The transfer of the remaining 20 lb of concentrate in four batches from can A-7 took place with no difficulty, and the transfer was completed by 1415. At 1617, fuel sample 8 was taken for analysis, and, at 1707, the first batch from can A-8 was transferred into the system. The remaining 5 batches were transferred smoothly, and the transfer from can A-8 was completed by 1804. At 2028, fuel sample 9 was removed for analysis. The next three additions of fuel from cans A-9, A-10, and A-12 were accomplished with little difficulty.

At 0830 on November 2, while transferring the first 5-lb batch from can A-5, a leak occurred in the injection line just below the floor level of the loading station (see Fig. 4.3). Examination of the injection line showed the leak to have occurred at a Swagelok fitting. Approximately 0.2 lb of concentrate was lost from the experiment as a result of the leak. Since the line had clogged, it was necessary to install a new section of line. During the time the repairs were being made to the injection system, the original schedule was changed, and a subcritical measurement of the temperature coefficient of reactivity was made. In addition, samples 10 and 11 were taken for analysis.

SUBCRITICAL MEASUREMENT OF THE REACTOR TEMPERATURE COEFFICIENT

Approximately 100 lb of U^{235} (180 lb of Na_2UF_6) had been added at the time the leak occurred on November 2, at 0831, and it was estimated that this was about 80% of the total fuel needed. Although it had been planned to make a preliminary measurement of the temperature coefficient of reactivity with about 90% of the fuel added (see "Nuclear Operating Procedures," Appendix D), the plans were revised and the measurement was made at this time.

At the start of the experiment the reactor mean temperature was 1306°F. The fuel heat exchanger barrier doors were raised (at 1003); two minutes later the fuel helium blower was started and its speed increased to 275 rpm. The resultant cooling, with time, as traced by the reactor fuel mean temperature recorder, is shown in Fig. 4.5, with the counting rate from fission chamber No. 2 superimposed. The data for both fission chambers are given in Table 4.2. The counting rate of the fission chambers monitors the neutron flux.

The counting rate was observed to rise with decreasing temperature and thus indicated a negative temperature coefficient of reactivity. Counts were taken for 40 sec during every minute. At 1010, when the reactor temperature reached 1250°F, the helium blower was stopped, and soon thereafter the reactor temperature began to rise again, with a corresponding decrease in counting rate.

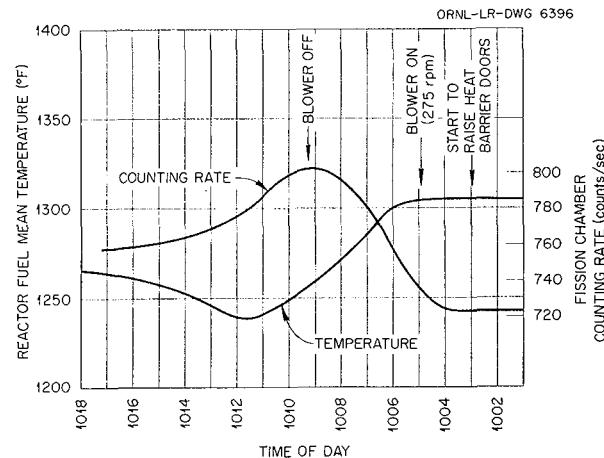


Fig. 4.5. Subcritical Measurement of the Reactor Temperature Coefficient. (Plot of fission chamber No. 2 counting rate superimposed on fuel mean temperature chart.)

TABLE 4.2. SUBCRITICAL MEASUREMENT OF THE REACTOR TEMPERATURE COEFFICIENT

Time	Reactor Mean Temperature (°F)	Fission Chamber No. 1 (counts/sec)	Fission Chamber No. 2 (counts/sec)
1004	1306	486.4	723
1005	1304	492.8	736
1006	1302	512.0	755
1007	1290	531.2	780.8
1008	1275	537.6	793.6
1009	1260	537.6	793.6
1010	1252	544.0	800.0
1011	1244	531.2	787.2
1012	1240	531.2	774.4
1013	1246	518.4	768.0
1014	1252	518.4	768.0
1015	1258	512	761.6
1154	1275	502	736.0
1319	1284	490.9	725.0
1422	1290	484	713.0

The reactor temperature coefficient, as estimated from the data presented in Fig. 4.5, was of the order of -5×10^{-5} ($\Delta k/k$)/ $^{\circ}\text{F}$. The data were adequate to show that the reactor would be easy to control; therefore the experiment was allowed to proceed. It will subsequently be observed that the temperature data recorded in the data room did not exhibit the full temperature drop across the reactor in any run where heat was being abstracted from the system. Consequently where the abstracted heat is one of the parameters of the experiment, as in the above temperature coefficient measurement, it would be expected that some temperature correction would be in order. The existing data for the case in question are, however, too meager to justify correction, although based on correlations (app. K) with data taken during the low- and the high-power runs, the control room temperature indications were lower than the actual temperature, and therefore the estimated temperature coefficient given above is too high.

It may also be noted from examination of Fig. 4.5 that the maximum counting rate and the temper-

ature minimum did not occur simultaneously. A lag of about 2.5 min in the response of the reactor temperature was observed. The reason for this time lag is not well understood, but it may have some connection with the fact that the thermocouples were outside the reactor and hence did not "see" the changes immediately. Details of this and later measurements of the fuel and reactor temperature coefficients are given in Appendix O.

APPROACH TO CRITICALITY

At 0130 on November 3, the injection system was again in operation, and the fuel additions during the remainder of the critical experiment occurred without mishap. The remaining portions of can A-7 and all of cans B-22, B-31, and B-20 were added during this time.

Throughout the course of the experiment, the progress toward criticality was observed on the neutron detectors. With every fuel injection the counting rates of the two fission chambers and the BF_3 counter were simultaneously clocked and recorded. The approach to criticality could readily be seen by plotting the reactivity, k , against the concentration of the fuel in the system. The reactivity was obtained from the relationship

$$k = 1 - \frac{1}{M},$$

where M is the subcritical multiplication, which is determined from the expression

$$M = \frac{N}{N_0},$$

where N is the counting rate after a fuel injection and N_0 is the initial counting rate. As criticality is approached, $1/M$ approaches zero, and therefore at criticality, $k = 1$.

Figure 4.6 shows a plot of k vs U^{235} concentration, where k is determined from three neutron detectors, i.e., two fission chambers and a BF_3 counter. The reactivity, as observed on the two fission chambers, showed a rapid increase during the early stages of the experiment and then leveled off as the critical condition was near. The BF_3 counter, on the other hand, showed a more uniform approach to criticality. The differences in the responses of the two types of detectors are discussed in Appendix E. Table 4.3 presents the data from which Fig. 4.6 was drawn.

A condensed, running uranium inventory during the critical experiment is given in Table 4.4. The

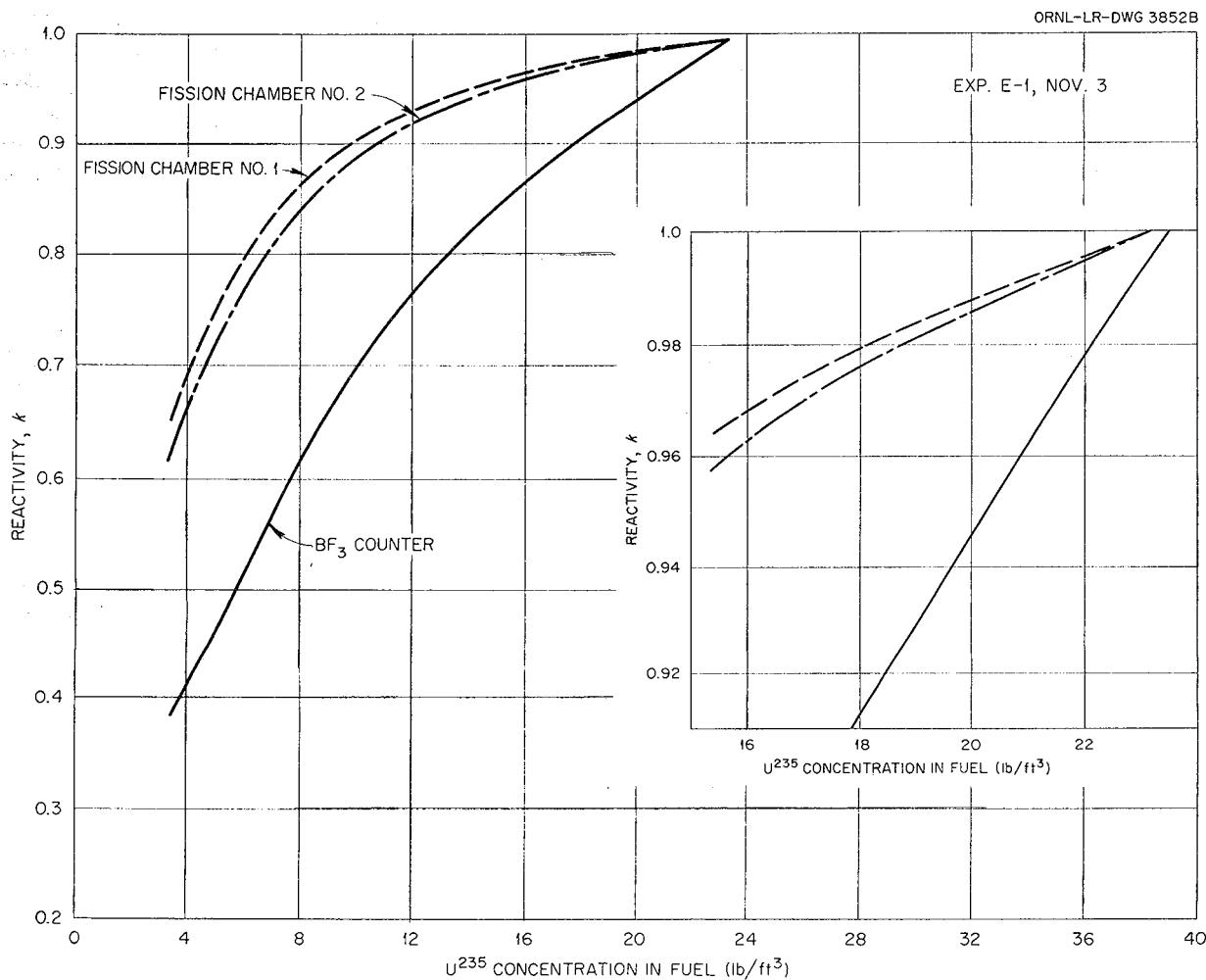


Fig. 4.6. Approach to Criticality: Reactivity vs Fuel Concentration.

figures of columns 4, 6, and 11 were supplied by the chemists.³

At 1545 on November 3 upon the addition of the second batch of fuel from can B-20, a sustaining chain reaction was attained — the reactor was critical. Figure 4.7 shows a photo of the control room just as the critical condition was reached.

At 1547 the reactor was given over to the servo mechanism at an estimated power of 1 watt, and during the next $\frac{1}{2}$ hr a brief radiation survey of the reactor and heat exchanger pits was made (cf., chap. 5, "Low-Power Experiments"). At 1604 the reactor was shut down, and thus the initial phase of the ARE operation program was completed.

³J. P. Blakely, *Uranium in the ARE*, ORNL CF-55-1-43 (Jan. 7, 1955).

The uranium inventory (Table 4.4) showed that the critical concentration of U^{235} was 23.94 lb/ft^3 , which corresponded to a total weight of 133.8 lb of U^{235} in the fuel system. At this time the total weight of the fuel was 1156 lb, and its volume was 5.587 ft^3 . The per cent by weight of U^{235} was calculated to be 11.57.

The critical mass of U^{235} in the reactor was calculated from the ratio of volumes:

$$M_r = M_s \frac{V_r}{V_s},$$

where

M_r = critical mass of U^{235} in reactor core,

M_s = mass of U^{235} in system,

V_r = critical volume of reactor,

TABLE 4.3. APPROACH TO CRITICALITY: REACTIVITY FROM VARIOUS NEUTRON DETECTORS vs FUEL CONCENTRATION

Log Run No.	U ²³⁵ Concentration (lb/ft ³)	Fission Chamber No. 1			Fission Chamber No. 2			BF ₃ Counter		
		Counting Rate, N (counts/sec)	Multiplication, M (N/N ₀)	Reactivity, k	Counting Rate, N (counts/sec)	Multiplication, M (N/N ₀)	Reactivity, k	Counting Rate, N (counts/sec)	Multiplication, M (N/N ₀)	Reactivity, k
1	0	9.46*	1	0	16.28*	1	0	4.49*	1	0
2	3.39	26.7	2.82	0.645	42.5	2.61	0.617	7.04	1.57	0.361
3	6.16	47.44	5.02	0.801	71.54	4.39	0.772	9.19	2.05	0.510
4	9.37	86.96	9.19	0.891	128.5	7.90	0.873	13.43	2.99	0.667
5	12.45	147.2	15.6	0.936	217.2	13.34	0.925	19.73	4.39	0.780
6	15.36	251.9	26.6	0.962	367.6	22.6	0.956	29.5	6.57	0.848
7	18.09	450.9	47.6	0.979	649.9	39.9	0.975	49.0	10.8	0.908
8	19.74	648.2	68.5	0.985	977.4	60.0	0.983	70.5	15.7	0.936
9	20.63	859.3	90.8	0.989	1317	80.9	0.988	93.7	20.9	0.952
10	21.88	1489	157.4	0.994	2316	142.3	0.993	161.3	35.9	0.972
11	23.08	4028	425.6	0.998	6730	413.5	0.998	442.0	98.5	0.990
12	23.94	Critical								

*Initial counting rate, N₀.

TABLE 4.4. URANIUM INVENTORY DURING CRITICAL EXPERIMENT

Date	Time	Run No.	Fuel Concentrate Added		Samples Removed for Analysis		Fuel Mixture			Uranium-235		
			Weight (lb)	Volume (ft ³)	Fuel Removed (lb)	U ²³⁵ Removed (lb)	Total Weight Concentrate Plus Carrier (lb)	Total Volume (ft ³)	Density (lb/ft ³)	Weight Added (lb)	Concentration lb/ft ³	wt %
10/30	1425	1					927.3	4.820	192.4	0		
	1625	2	30.00	0.1046			957.3	4.925	194.4	16.687	16.687	3.388 1.743
	1740				2.447	0.0427	954.8	4.912				16.644
10/31	2013				2.531	0.0441	952.3	4.900				16.600
	1415	3	25.37	0.0885			977.7	4.988	196.0	14.105	30.705	6.156 3.141
11/1	1635				2.286	0.0716	977.5	4.976				30.633
	1804	4	30.54	0.1065			1008	5.082	198.3	16.980	47.613	9.368 4.723
	2040				2.670	0.1261	1005	5.069				47.487
	2203	5	30.44	0.1062			1036	5.175	200.2	16.940	64.427	12.45 6.220
	0213	6	30.07	0.1049			1066	5.280	201.9	16.695	81.122	15.36 7.610
11/2	0610	7	29.19	0.1018			1095	5.382	203.5	16.230	97.352	18.09 8.890
	0831	8a	5.50	0.0192			1101	5.401	203.8	3.058	100.410	18.59 9.123
	1625				2.562	0.2337	1098	5.388				100.176
	2025				2.716	0.2478	1095	5.375				99.928
11/3	0256	8b	12.62	0.0440			1108	5.419	204.5	7.037	106.965	19.74 9.654
	0523	9	9.93	0.0346			1118	5.454	205.0	5.536	112.501	20.63 10.06
	0941	10	14.18	0.0495			1132	5.503	205.7	7.908	120.409	21.88 10.64
	1245	11	13.92	0.0486			1146	5.552	206.4	7.751	128.160	23.08 11.18
	1536	12	10.07	0.0351			1156	5.587	206.9	5.600	133.760	23.94 11.57
	1545		Criticality reached									
11/4	0910				2.679	0.3100	1153	5.574				133.450
	0915				2.718	0.3145	1151	5.561				133.135
	1310				2.482	0.2872	1148	5.549				132.848
	1315				0.732	0.0847	1147	5.545				132.763

PHOTO I3268



Fig. 4.7. Control Room at Criticality.

V_s = system volume.

Therefore

$$M_r = 133.8 \text{ lb} \left(\frac{1.37 \text{ ft}^3}{5.587 \text{ ft}^3} \right) = 32.8 \text{ lb} .$$

The calculated, cold, clean critical mass of the reactor, as obtained from the subsequent rod calibrations, was 32.75 lb (cf., app. F).

The reactor was not instrumented to permit the measurement of the flux or power distributions through the reactor, but measurements of these distributions were made on a critical mockup of the reactor at the ORNL Critical Experiment Facility about two years before the operation of the ARE.⁴ These measurements represent the best

⁴D. Callahan and D. Scott, *Preliminary Critical Assembly for the Aircraft Reactor Experiment*, ORNL-1634 (Oct. 28, 1953).

information that is available and, because of the general interest therein, typical axial and radial flux and power distribution curves are given in Appendix G.

ANALYSES OF FUEL SAMPLES

In addition to the fuel samples taken, as noted, during the critical experiment, four more samples were removed on November 4 after initial criticality was reached. A list of all samples taken and the results of the chemical analyses are presented in Table 4.5. Besides showing the analyses of the percentages of U and U²³⁵ by weight in the fuel system and a comparison with the U²³⁵ (wt %) content obtained from the criticality data, the table also lists the results of the analyses for the impurities and corrosion products Fe, Cr, and Ni to provide information on the purity of the fuel and the corrosion rate of the fuel system.

TABLE 4.5. CHEMICAL ANALYSES OF FUEL SAMPLES

Date	Time	Sample No.	Impurities and Corrosion Products (ppm)			Total Uranium (wt %)	U ²³⁵ from Chemical Analysis (wt %)	U ²³⁵ from Critical Experiment Data (wt %)
			Cr	Fe	Ni			
10/25	1650	1	90	200	50			
10/26	1414	2	81	<5	40			
	1911	3	81	<5	6			
10/27	1919	4	90	18	12			
10/29	0935	5	102	30	20			
10/30	1740	6	100	20	10	2.47 ± 0.01	2.31	1.74
	2013	7	150	15	10	1.84 ± 0.04	1.72	1.74
11/1	1635	8	190	15	15	3.45 ± 0.01	3.22	3.14
	2040	9	200	10	17	5.43 ± 0.01	5.07	4.72
11/2	1625	10	210			9.58 ± 0.08	8.95	9.12
	2025	11	205	20	20	9.54 ± 0.08	8.91	9.12
11/4	0910	12	310			12.11 ± 0.10	11.32	11.57
	0915	13	300			12.21 ± 0.12	11.41	11.57
	1310	14	320			12.27 ± 0.08	11.46	11.57
	1315	15	310			12.24 ± 0.12	11.43	11.57
11/5	1100	16	372	5	<5	12.54 ± 0.07	11.72	11.72
11/6		17				12.57 ± 0.07	11.75	11.79
	0535	18	420			12.59 ± 0.12	11.77	11.79
11/7	0423	19	445			13.59 ± 0.08	12.70	12.38

The first five samples were removed from the system prior to enrichment, and samples 16 through 19 were taken after the critical experiment and during the low power runs at the time of the calibration of the regulating rods against fuel addition.

For the most part, the U^{235} content as given by chemical analysis agreed to within a few per cent with that obtained from the running inventory. When the sample for analysis was withdrawn from the system too soon after a fuel addition, there was a tendency for the analysis to be low, undoubtedly, because of inadequate mixing of the additive with the bulk of the fuel. The chemical analysis of sample 1, however, was obviously in error, whereas that of sample 9 gave a uranium content that was about 7% higher than the inventory showed. The other sample analysis figures were within about 2% of the percentages given by the inventory. The analyses of samples 12, 13, and 14, which were taken after the critical experiment, agreed to within about 1% with the inventory calculation.

The increase in the buildup of chromium in the fuel system with time is shown in Fig. 4.8 to give an indication of the corrosion rate of the system. The initial corrosion rate was quite small, but after enriched fuel had been added to the system, the analyses showed a chromium content increase of about 50 ppm/day.

CALIBRATION OF THE SHIM RODS

As outlined in the "Nuclear Operating Procedures," Appendix D, during the first fuel additions the shim rods were withdrawn all the way out of the reactor to obtain the multiplication. After about 100 lb of U^{235} had been added to the system, the procedure was altered in order to obtain a shim rod calibration. After each fuel addition, all three rods were simultaneously withdrawn to positions of 20, 25, 30, and 35 in. out; total movement was 36 in. The counting rate of each of the neutron detectors was recorded for each rod position. Figure 4.9 shows the reciprocal multiplication and the reactivity as a function of U^{235} content of the fuel system for the various rod positions. The data used for plotting Fig. 4.9 were obtained from the BF_3 counter and are presented in Table 4.6. A cross-plot of reactivity vs shim rod position determined the rod calibration details, which are given in Appendix J. The rods

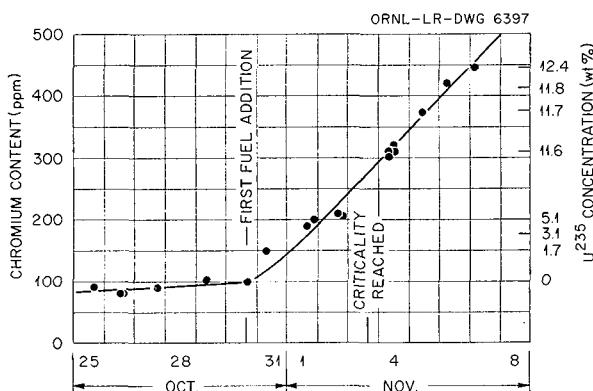


Fig. 4.8. Increase in Chromium Concentration in Fuel as a Function of Time.

were found to be nonlinear, with $(\Delta k/k)/in.$ and total $\Delta k/k$ varying in the manner shown in Appendix D. From the calibration it was found that each rod was worth a total of about 5.8% $\Delta k/k$.

As a check on the general shape of the reactivity curves of the shim rods, a series of counts were taken on the BF_3 counter and the fission chambers for various rod positions for two different uranium concentrations. These data are also discussed in Appendix J.

MEASUREMENT OF THE REACTIVITY-MASS RATIO

Prior to the ARE operation it had been estimated that when the critical mass (assumed to be 30 lb) was reached, the value of the ratio $(\Delta k/k)/(\Delta M/M)$ should be 0.232. This value was obtained from a calculation of the ratio for various amounts of U^{235} , as shown in Fig. D.1 of Appendix D. From the data taken during the critical experiment, it was possible to establish an experimental curve for the ratio and to verify the value given above for the ratio at the critical mass.

In order to find $(\Delta k/k)/(\Delta M/M)$ experimentally, use was made of the curve of Fig. 4.9 which gives k in terms of the U^{235} content of the fuel in the system for various shim rod positions; i.e., for any point,

$$\frac{\Delta k/k}{\Delta M/M} = \left(\frac{\Delta k}{\Delta M} \right) \left(\frac{M}{k} \right) = R ,$$

which is the reactivity-mass ratio. The value

TABLE 4.6. REACTIVITY vs U²³⁵ CONTENT OF FUEL SYSTEM FOR VARIOUS SHIM ROD POSITIONS

Experiment E-1 Run No.	U ²³⁵ in System (lb)	Shim Rod Positions* (in. out)	Counting Rate, BF ₃ Counter (counts/sec)	N ₀ /N	k = 1 - (N ₀ /N)
8 A	100.41	20	32.0	0.140	0.860
		25	38.4	0.117	0.883
		30	46.9	0.0956	0.904
		35	54.3	0.082	0.918
8 B	103.13	20	34.1	0.131	0.869
		25	40.5	0.111	0.889
		30	51.2	0.0877	0.912
		35	57.8	0.0774	0.923
8 C	106.18	20	36.3	0.123	0.877
		25	46.9	0.0954	0.905
		30	57.8	0.0774	0.923
		35	66.1	0.0676	0.932
8 D	106.97	20	36.3	0.123	0.877
		25	46.9	0.0954	0.905
		30	59.7	0.0749	0.925
		35	68.3	0.0655	0.935
9 A	110.14	20	38.4	0.117	0.883
		25	51.2	0.0874	0.913
		30	68.3	0.0655	0.934
		35	83.2	0.0538	0.946
9 B	112.50	20	40.5	0.111	0.889
		25	55.5	0.0808	0.919
		30	76.8	0.0582	0.942
		35	93.9	0.0479	0.952
10 A	115.58	20	44.8	0.0998	0.900
		25	59.7	0.0749	0.925
		30	83.2	0.0538	0.946
		35	110.9	0.0403	0.960
10 B	118.63	20	42.7	0.105	0.895
		25	68.3	0.0655	0.934
		30	93.3	0.0479	0.952
		35	136.5	0.0327	0.967
10 C	120.41	20	51.2	0.0873	0.913
		25	68.3	0.0655	0.934
		30	110.9	0.0403	0.960
		35	162.1	0.0276	0.972
11 A	123.43	20	51.2	0.0873	0.913
		25	85.3	0.0524	0.948
		30	128.0	0.0349	0.965
		35	213.3	0.0209	0.979

*Position of all three shim rods.

TABLE 4.6 (continued)

Experiment E-1 Run No.	U^{235} in System (lb)	Shim Rod Positions* (in. out)	Counting Rate, BF_3 Counter (counts/sec)	N_0/N	$k = 1 - (N_0/N)$
11 B	126.48	20	59.7	0.0749	0.925
		25	93.9	0.0476	0.952
		30	162.1	0.0275	0.973
		35	307.2	0.0145	0.985
11 C	128.16	20	59.7	0.0749	0.925
		25	93.9	0.0476	0.952
		30	196.3	0.0228	0.977
		35	443.7	0.0101	0.990
12 A	131.08	20	59.8	0.0748	0.925
		25	110.9	0.0403	0.960
		30	256.0	0.0175	0.983
		35	955.7	0.00468	0.995
12 B	133.76	20	68.3	0.0655	0.935
		25	136.5	0.0327	0.967
		30	375.5	0.0119	0.988
		35	Critical		

*Position of all three shim rods.

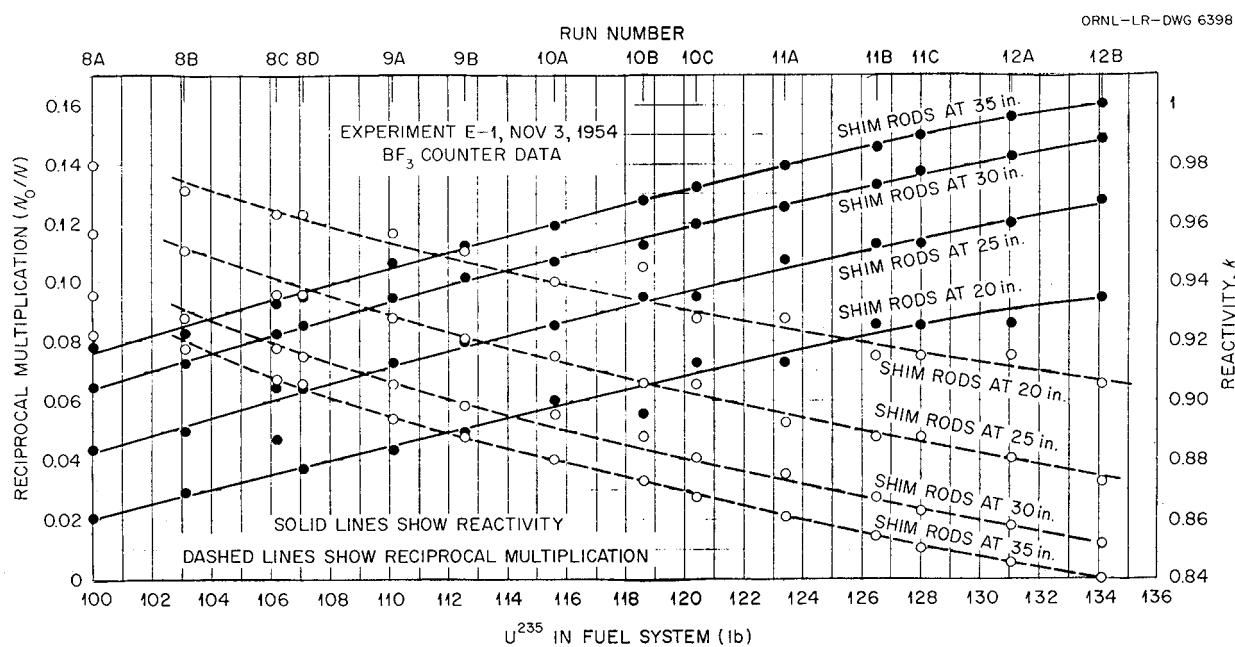


Fig. 4.9. Reactivity and Reciprocal Multiplication vs U^{235} Content of Fuel System for Various Shim Rod Positions.

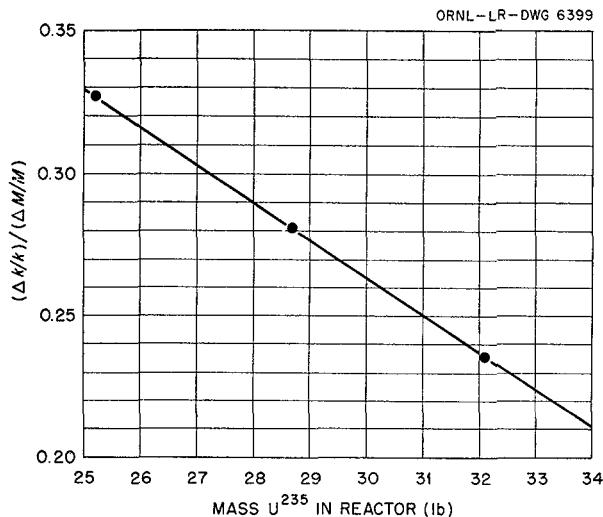


Fig. 4.10. Reactivity-Mass Ratio as a Function of the U²³⁵ Content of the Fuel in the Reactor.

TABLE 4.7. REACTIVITY-MASS RATIO AS A FUNCTION OF THE AMOUNT OF U²³⁵ IN THE REACTOR FOR VARIOUS SHIM ROD POSITIONS

Mass Range* (lb)	Shim Rod Position** (in.)	M_1 , Mass of U ²³⁵ in Reactor (lb)	ΔM (lb)	Reactivity, k	Δk	Reactivity-Mass Ratio, $\frac{\Delta k/k}{\Delta M/M}$
100 to 106	25	25.24	1.47	0.891	0.0172	0.331
	30	25.24	1.47	0.913	0.0175	0.329
	35	25.24	1.47	0.924	0.0174	0.322
				Average		0.327
114 to 120	25	28.66	1.47	0.929	0.0137	0.287
	30	28.66	1.47	0.951	0.0136	0.279
	35	28.66	1.47	0.963	0.0135	0.273
				Average		0.280
128 to 134	25	32.10	1.44	0.961	0.0110	0.257
	30	32.10	1.49	0.982	0.0100	0.219
	35	32.10	1.40	0.995	0.0100	0.231
				Average		0.236

*These mass ranges refer to the curves of Fig. 4.9 on which these calculations are based.

**Position of all three rods.

$(\Delta k/\Delta M)$ is the slope of the k vs M curves shown in Fig. 4.9. For various small sections of the curves the slopes approximated straight lines. From the average values of M and k over these increments of the curves and the measured slopes, the ratio R was determined for each increment. Figure 4.10 shows a plot of R vs the U²³⁵ content of the fuel in the system.

The value of R for the experimental critical mass (133.8 lb) was calculated to be

$$\frac{\Delta k/k}{\Delta M/M} = 0.236$$

for shim rod positions of 25, 30, and 35 in. Since this value (0.236) was in excellent agreement with the calculated value (0.232), it was used throughout the experiment. The data are tabulated in Table 4.7.

5. LOW-POWER EXPERIMENTS

The reactor was operated, after initial criticality was attained, for about 20 min at a nominal power of 1 w and then shut down. The next morning a series of low-power experiments was started. This series of experiments lasted from the morning of November 4 until the morning of November 8. The chronology of this low-power operation is given in Fig. 5.1.

Two of the early experiments, L-1 and L-4, were devoted to a determination of the reactor power from measurements of the fuel activation. These runs were each of 1 hr duration with the reactor at a nominal power of 1 and 10 w, respectively. After each of these runs, fuel samples were taken and the activity counts were made from which the reactor power was determined. The method was inaccurate, as subsequently evidenced by power calibrations from the extracted power, but did indicate that the nominal power estimates were low.

Radiation surveys of the entire experimental system were made during both the nominal 1- and 10-w runs except that a survey of the reactor pit was not attainable during the 10-w run because the pit was sealed at that time. Most of the equipment and many of the instruments were, however, located in the heat exchanger pits to which access was maintained throughout the low-power operation.

Most of the time of the low-power operation was devoted to calibration of the regulating and shim rods. The two essentially independent methods used to calibrate the regulating rods were calibration against fuel addition and calibration against reactor periods by using the inhour equation (app. I). The shim rods were then calibrated against the regulating rod.

Also as an integral part of the low-power operation the earlier measurement of the temperature coefficient was checked, and the fuel system performance characteristics were determined. Finally, in preparation for the high-power experiments, the ion chambers, which had been positioned close to the reactor during the critical and low-power experiments for greater sensitivity, were withdrawn so that they would register sensibly at the higher powers.

POWER DETERMINATION FROM FUEL ACTIVATION

Reactor power measurements are usually made by exposing gold or indium foils to the neutron

flux in a reactor soon after initial criticality is attained. In the ARE it was simpler to draw off a sample of the uranium-bearing fuel after operation and measure its activity with an ion chamber. Comparison with a similar sample of known activity gave a determination of the flux level and, hence, the power level. The procedure is described in Appendix H.

In run L-1, the reactor was operated for 1 hr at an estimated power level of 1 w, and a sample was drawn off for measurement of the activity. The specific activity was too low for a reliable determination and, accordingly, the experiment was repeated in run L-4 at a nominal 10-w power level.

It was subsequently found from the heat balance at high power that the actual power was 27 w during run L-4. However, the fuel sample activity was only on the order of one-half to two-thirds the activity to be expected from operation at 27 w. Apparently a considerable amount of the gaseous fission products was being given off from the fuel. A comparison of the data obtained from fuel activation with those obtained from heat balances is given in Appendix N.

RADIATION SURVEYS

The primary purpose of experiments L-1 and L-4 was to calibrate the estimated reactor power against the power determined from the radioactivity of fuel samples, but, at the same time, radiation dose levels were measured at various locations around the reactor and the tank and heat exchanger pits. These data will subsequently be of interest in evaluating the radiation damage to various components of the system.

Most of the radiation measurements were made with a "Cutie-Pie" (a gamma-sensitive ionization chamber), but a GM survey meter, a methane proportional counter, an electroscope, and a boron-coated electroscope were used for some measurements, in particular, those made close to the reactor. While the GM survey meter only provided a check on the gamma dose as measured by the "Cutie-Pie," the other instruments provided measurements of the fast- and thermal-neutron doses. The proportional counter measured the fast-neutron dose, and the thermal-neutron flux was calculated from the difference of the two electroscope readings.

CHRONOLOGY OF THE LOW-POWER EXPERIMENTS

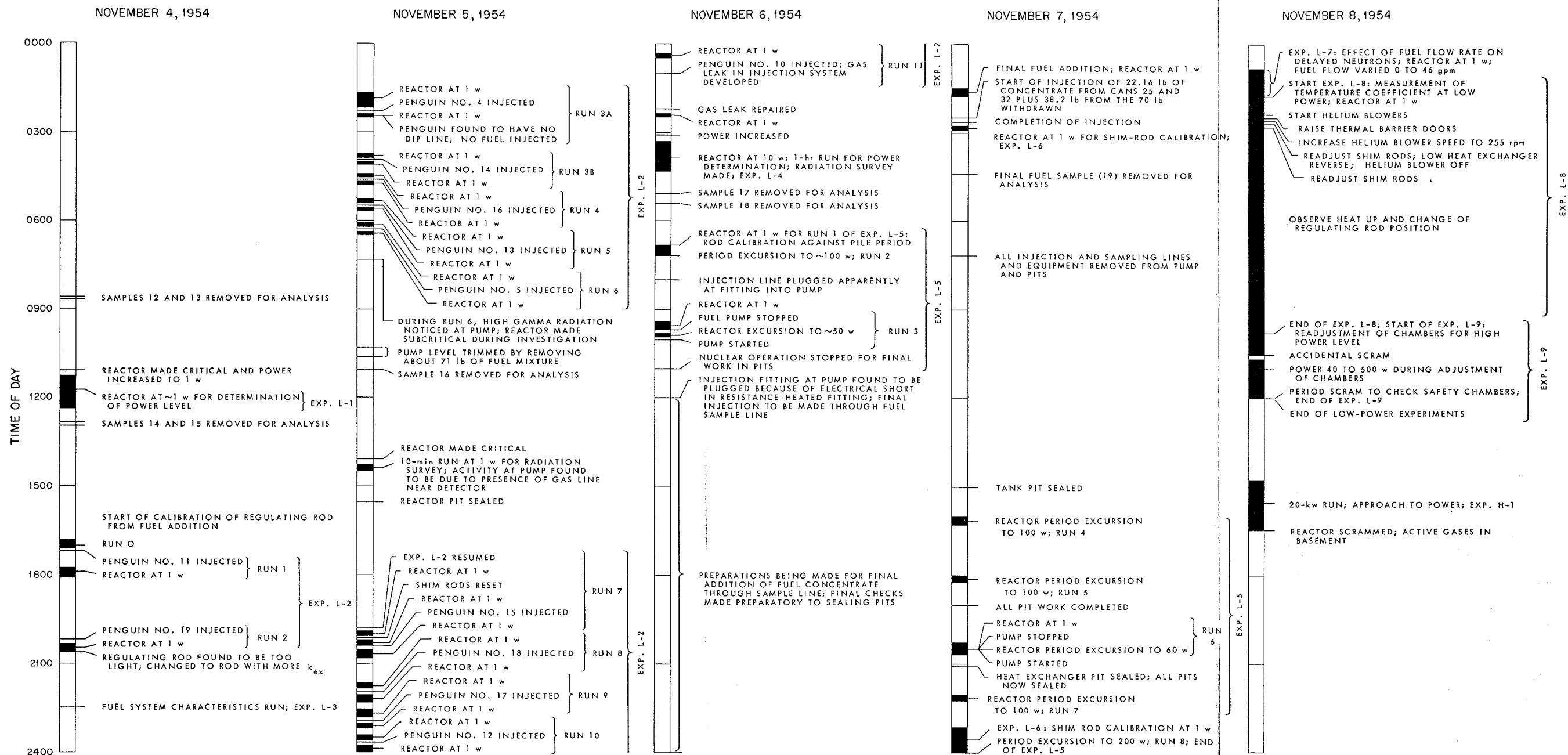
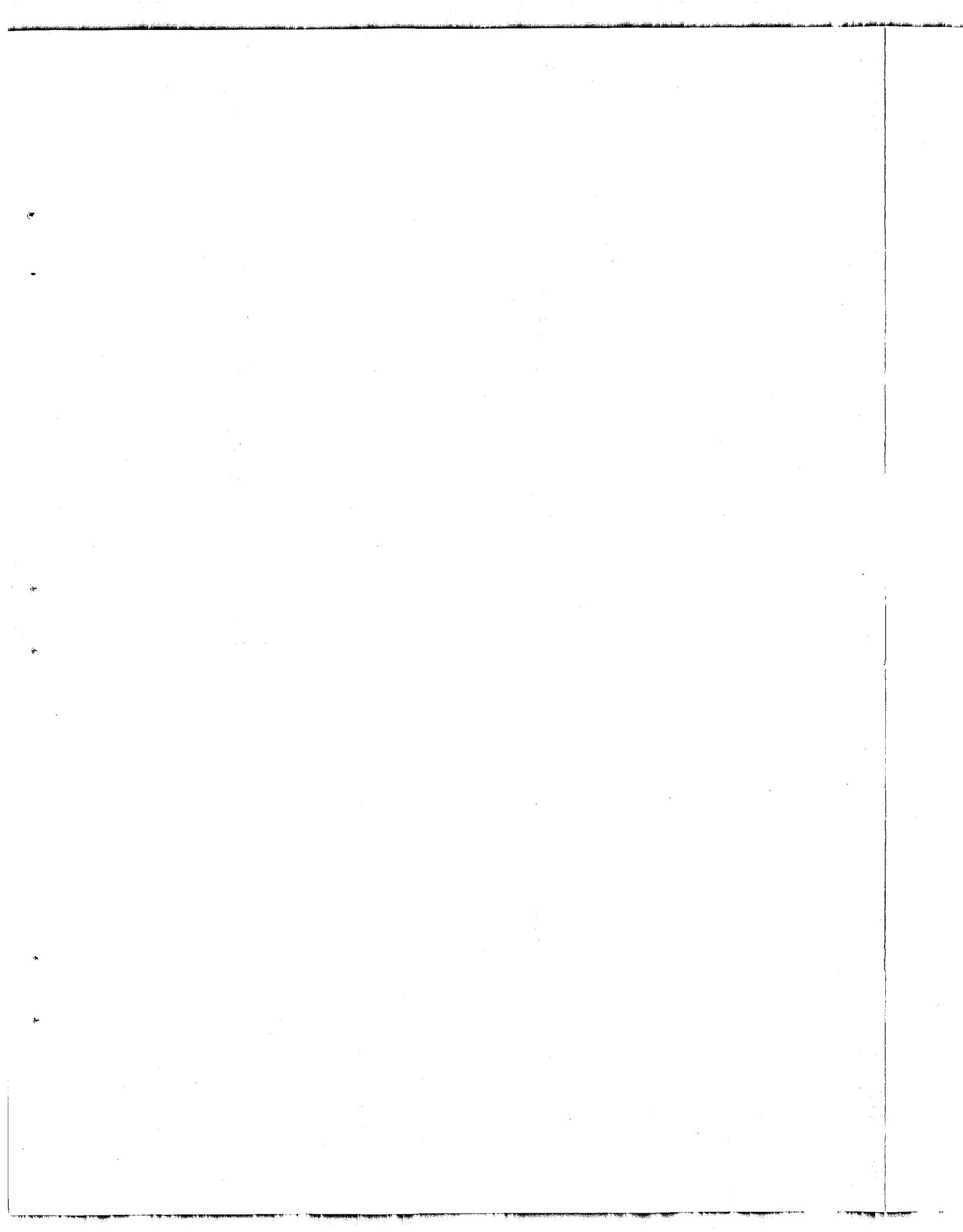


Fig. 5.1.



The radiation dose data from the two runs during which the dose in the pits was measured are presented in Tables 5.1 and 5.2. Table 5.1 gives the gamma and the fast- and thermal-neutron doses in the reactor pit during the 2.7-w run; Table 5.2 gives the gamma doses at various stations in the heat exchanger pit during both the 2.7- and 27-w runs. Within the accuracy of the measurements, there is excellent agreement between the doses per watt from the two runs.

REGULATING ROD CALIBRATION FROM FUEL ADDITIONS

Twelve small cans, or "penguins" (so-called because of their shape), had been prepared for adding small amounts of fuel to the system in order to calibrate the regulating rod (exp. L-2) after initial criticality had been reached. Each penguin contained from 0.2 to 0.5 lb of fuel concentrate (0.1 to 0.3 lb of U²³⁵). The contents of the penguins were injected directly into the pump rather than through the intermediate transfer pot that was used in the critical experiments. Table 5.3 lists the penguins in the chronological order in which they were used, together with the amount of uranium injected from each can.

The method used to calibrate the regulating rod was to note the difference between the position of the rod at criticality before and after each injection of fuel, with the shim rods held constant. Before each injection the reactor was brought from subcritical to a nominal power of 1 w, and the shim and regulating rod positions were recorded. The reactor was then brought subcritical on the regulating rod, with the shim rods in position, and the

fuel was injected from the penguin. Upon completion of the injection the reactor was again brought critical to 1-watt power with the regulating rod. The positions of the rods were again recorded. The worth of the rod was then obtained from the relation

$$\frac{\Delta k}{k} = 0.236 \frac{\Delta M}{M}$$

and the known increment of fuel added to the system; the proportionality factor, 0.236, was obtained experimentally during the critical experiment (cf. chap. 4).

The first run of experiment L-2 started at 1651 on November 4. After two injections had been completed, it was apparent that the worth of the 12 in. of vertical movement of the regulating rod in terms of $\Delta k/k$ was about 0.24%. It was desirable, for reasons of safety and also for convenience in conducting high-power transient experiments, to have a rod worth about one dollar of reactivity (which for the ARE was 0.4% rather than 0.76% as in stationary-fuel reactors, because of delayed-neutron loss in the circulating fuel). A number of spare rods of varying weights had been made up to take care of such a contingency, and one was selected and installed which had more nearly the desired weight. The original rod weighed 19.2 g/cm of length, and the new rod weighed 36 g/cm.

While the rod was being changed (a delay of about 5 hr), the fuel system characteristics of pressure head vs flow were obtained. These measurements are described in a following section of this chapter.

TABLE 5.1. RADIATION LEVELS IN REACTOR PIT DURING 2.7-w RUN

Position	Gamma Dose Rate (mr/hr per w)	Fast-Neutron Dose Rate (mrep/hr per w)	Thermal-Neutron Dose Rate (mrep/hr per w)	Total Dose Rate* (mr/hr)
Space cooler No. 1	48	67	8	760
Top center of reactor (1 in. above thermal shield)	280	280	35 (est.)	3200
Side of reactor at mid-plane (at surface of thermal shield)	440	180	22 (est.)	2350
Manhole into pits	12	10	2	130

*The total dose rate was obtained from the weighted sum of the preceding columns by using an RBE of 10 for fast neutrons and 5 for thermal neutrons.

TABLE 5.2. GAMMA-RAY DOSE IN TANK AND HEAT EXCHANGER PITS

	Doses per Watt During 2.7-w Run (mr/hr)	Doses per Watt During 27-w Run (mr/hr)
Locations Surveyed in Dump Tank Pit		
Motor for space cooler No. 3	0.3	0.3
Vent valve U-113 for tank No. 6	0.1	0.15
Motor for stack vent on hot fuel dump tank	0.2	0.15
Vent Valve U-112 for hot fuel dump tank	0.1	0.07
Helium inlet valve U-100	0.07	0.07
Motor for space cooler No. 4		0.07
Air-operated valve for tank No. 5		0.07
Locations Surveyed in Fuel-to-Helium Heat Exchanger Pit		
Operator's position at fuel sampler	6	4
Pressure transmitter PXT-6	22	
Top plate of main fuel pump	150	120
Top bearing of pump motor	45	80
V-belt at pump	7	6
V-belt at pump motor	7	4
Line 120 under valve U-3	110	12
Bend No. 2 of line 303	105	45
Motor for space cooler No. 6	10	
West side of heat exchanger No. 1	135	120
Bottom of fuel flowmeter	95	105
Line 112 between valves U-63 and U-1	220	200
Lubrication pump for pump	65	90
Top of fuel storage tank	4	
Helium analyzer dryers	0.3	1
East side of heat exchanger No. 1		230
West side of heat exchanger No. 2		200
Sheet metal can around pump		185
Locations Surveyed in Sodium-to-Helium Heat Exchanger Pits		
Top of standby sodium pump	1.5	1.4
V-belt above standby pump	1.5	1.7
Line 310 under valve B-141	13	15
Motor for space cooler No. 7	4	
Top of main sodium pump	1.5	0.7
V-belt above main pump	0.7	0.8
Line 309 at valve U-21	2.2	1.8
Line 313 at bend No. 5	1.5	1.5
Motor for space cooler No. 8	1.5	
North side of front heat exchanger	15	16
Kinney pump No. 1	4	4
Magnetic clutch on 50-hp motor	11	13
North side of back heat exchanger	1	6
North end of rod-coolant blower No. 1	6	7
EM flowmeter on line 305	3.7	5
Standby pump lubrication system		9
Main pump lubrication system		3

TABLE 5.3. FUEL CONCENTRATE BATCHES ADDED DURING LOW-POWER EXPERIMENTS

Date	Time	Penguin No.	Concentrate Added		Uranium Added		U^{235} Added	
			g	lb	wt %	g	g	lb
11/4	1710	C-11	227	0.5004	59.671	135	126	0.2778
	2009	C-19	722	1.5917	59.671	431	403	0.8885
11/5	0354	C-14	247	0.5445	59.671	147	137	0.3020
	0439	C-16	285	0.6283	59.671	170	159	0.3505
11/5	0529	C-13	131	0.2888	59.671	78.2	73.0	0.1609
	0619	C-5	123	0.2712	59.671	73.3	68.5	0.1510
11/5	2045	C-15	92	0.2028	59.671	55	51.4	0.1143
	2204	C-18	87	0.1918	59.671	52	48.6	0.1071
11/5	2258	C-17	457	1.0075	59.671	273	255	0.5622
	2345	C-12	84	0.1852	59.671	50	46.7	0.1030
11/6	0100	C-10	84	0.1852	59.671	50	46.7	0.1030
11/7	0231	120*	21,681	47.798	27.557	5975	5581	12.304

*Container No. 120 was not a penguin but a specially prepared batch of concentrate which provided the excess uranium required for the experiments and to compensate for burnup.

At 0142 on November 5 the installation of the second rod was completed and the experiment was resumed. Four more injections of fuel were made and the rod movement was noted. At 0630, during the sixth fuel injection, an unexpectedly high burst of gamma-ray activity (55 mr/hr) was observed on a "Cutie-Pie" monitoring the fuel addition at the injection station over the pump. Further fuel addition was stopped until the cause of the high gamma-ray reading could be ascertained. While investigation was under way the level of the pump was trimmed to avoid any possible hazard from the uranium held in the pump. About 71 lb of fuel was removed from the system. Later in the day the cause of the high gamma-ray activity was determined to be a vent line passing close to the position of the "Cutie-Pie." Apparently, the "Cutie-Pie" had been held close enough to the vent line to read the fission gases (evolved during operation) as they were discharged through the vent line.

At 1947 the experiment was resumed and five more injections were made uneventfully. A photograph of the control room taken during this time is presented in Fig. 5.2; it shows two members of the ARE operating group examining the fission chamber recorders after a fuel injection for rod calibration; other members of the evening crew are shown in

their nominal operating stations.

An inventory of the uranium added during this experiment is given in Table 5.4. The final large amount (47.8 lb) of concentrate containing 12.30 lb U^{235} that was added after the experiment is also shown in the table, as well as a record of the samples and withdrawals. The final amount of U^{235} in the system was 138.55 lb, with a system volume of 5.33 ft³.

The data obtained for calibration of the regulating rod as a function of fuel addition are given in Table 5.5, which lists the values of M , ΔM , $\Delta M/M$, the recorded movement of the rod during each fuel addition, the average position of the rod for each fuel addition, and the calculated value of $(\Delta k/k)/in.$

The results of the calibration are shown in Fig. 5.3, where $(\Delta k/k)/in.$ is plotted as a function of rod position. The movement of the rod for each point is shown as a horizontal line through the point. The values of $(\Delta k/k)/in.$ for both rods were used, the values of reactivity for rod No. 1 being corrected by the ratios of the weights of the two rods. From these data it is evident that there is no good reason for presuming that the value of $(\Delta k/k)/in.$ over the whole length of rod is not constant. Therefore, the average value taken over the first ten runs gives

$$(\Delta k/k)/in. = 0.033\%/in.$$



PHOTO 13344

Fig. 5.2. Typical Control Room Scene: Examining Charts During Rod Calibration Experiments.

TABLE 5.4. URANIUM INVENTORY DURING LOW-POWER EXPERIMENTS

Date	Time	Run No.	Fuel Concentrate Added		Samples Removed for Analysis		Fuel Mixture			Uranium-235			
			Weight (lb)	Volume (ft ³)	Fuel Removed (lb)	U ²³⁵ Removed (lb)	Total Weight Concentrate Plus Carrier (lb)	Total Volume (ft ³)	Density (lb/ft ³)	Weight Added (lb)	Total Weight in System (lb)	Concentration lb/ft ³	wt %
11/4	1315	0					1147.45	5.5454	206.9		132.763	23.94	11.57
	1710	1	0.5004	0.0017			1147.95	5.5471	206.9	0.2778	133.041	23.98	11.59
	2009	2	1.5917	0.0056			1149.54	5.5527	207.0	0.8885	133.930	24.12	11.65
11/5	0354	3	0.5445	0.0019			1150.08	5.5546	207.05	0.3020	134.232	24.17	11.67
	0439	4	0.6283	0.0012			1150.71	5.5558	207.1	0.3505	134.583	24.22	11.70
	0529	5	0.2888	0.0010			1151.00	5.5568	207.1	0.1609	134.744	24.25	11.71
	0619	6	0.2712	0.0009			1151.27	5.5577	207.1	0.1510	134.895	24.27	11.72
	1015				53.486*	6.269	1097.78	5.2944	207.1		128.626	24.27	11.72
	1020				17.523*	2.064	1080.26	5.2148	207.1		126.562	24.27	11.72
	1100				2.5807	0.291	1077.68	5.2023	207.1		126.271	24.27	11.72
	2045	7	0.2028	0.0007			1077.88	5.2030	207.2	0.1143	126.385	24.29	11.73
	2204	8	0.1918	0.0004			1078.07	5.2034	207.2	0.1071	126.492	24.31	11.73
	2258	9	1.0075	0.0020			1079.08	5.2054	207.3	0.5622	127.054	24.41	11.77
	2345	10	0.1852	0.0004			1079.27	5.2058	207.3	0.1030	127.157	24.43	11.78
11/6	0100	11	0.1852	0.0004			1079.45	5.2062	207.3	0.1030	127.260	24.44	11.79
	0530				2.686	0.317	1076.76	5.1932	207.3		126.943	24.44	11.79
	0535				2.839	0.335	1073.92	5.1795	207.3		126.608	24.44	11.79
11/7	0231	12	47.798**	0.1667			1121.72	5.3462	209.8	12.304	138.912	25.98	12.38
	0423				2.918	0.361	1118.80	5.3323	209.8		138.551	25.98	12.38

*Two large batches of fluoride mixture were removed from the system in order to trim the liquid level in the pump.

**Of this amount, only 15.419 lb was Na₂UF₆, the remainder being some of the fluoride mixture that was removed from the system when the pump level was trimmed.

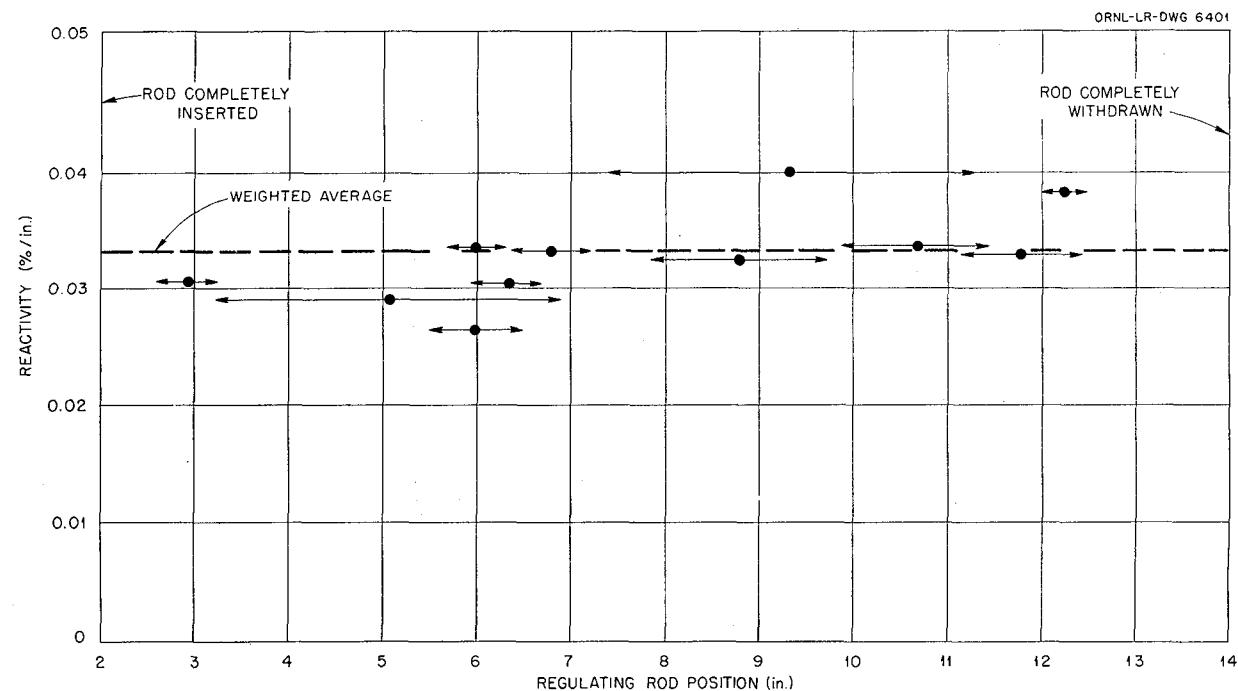


Fig. 5.3. Calibration of Regulating Rod from Fuel Addition.

TABLE 5.5. REGULATING ROD REACTIVITY CALIBRATION FROM FUEL ADDITION

(Exp. L-2)

Run No.	M , Weight of U^{235} in System (lb)	ΔM , Weight of U^{235} Added (lb)	$\Delta M/M$	$\Delta k/k$ (%)	Average Regulating Rod Position (in.)	Movement of Regulating Rod During Fuel Addition (in.)	Reactivity, $(\Delta k/k)/in.$ (%/in.)
1	133.041	0.2778	0.00209	0.0493	11.80	2.4	0.0308*
2	133.930	0.8885	0.00663	0.156	9.35	7.3	0.0400*
3	134.232	0.3020	0.00225	0.0531	10.70	1.6	0.0335
4	134.583	0.3505	0.00260	0.0614	8.80	1.9	0.0323
5	134.744	0.1609	0.00119	0.0281	6.80	0.85	0.0330
6	134.895	0.1510	0.00112	0.0264	6.00	1.0	0.0264
7	126.385	0.1143	0.000904	0.0213	6.35	0.7	0.0304
8	126.492	0.1070	0.000847	0.0200	6.00	0.6	0.0333
9	127.054	0.5622	0.00442	0.104	5.10	3.6	0.0289
10	127.157	0.1030	0.000810	0.0191	12.25	0.5	0.0383
11	127.260	0.1030	0.000809	0.0191	2.95	0.67**	0.0305**
Average reactivity, weighted according to rod movement 0.0331							

*Corrected by the ratio of the weight of the new rod to the weight of the original rod: $36/19.2 = 1.88$.

**Average of three readings.

The value from run 11 was not included in this average because three different values of rod final position were recorded in different places for this run.

REGULATING ROD CALIBRATION FROM REACTOR PERIODS

The calibration of the regulating rod by use of reactor periods (exp. L-5) utilized the inhour equation in a form in which reactivity is given in terms of the reactor period for a given rate of fuel flow. Figure 5.4 shows a plot of the reactivity $(\Delta k/k)$ as a function of reactor periods for 0- and 48-gpm fuel flow, as calculated from the inhour relation. Details of the calculational method used are presented in Appendix I.

In the experimental procedure followed, the regulating rod was suddenly withdrawn a known distance, while the shim rods were in a set position and the reactor was operating at a nominal power of about 1 w. The reactor was then allowed to rise in power on a constant period to a peak of 50 to 100 w, at which time it was manually

scrammed. From the induced period and the known flow, the excess reactivity introduced during the run was obtained from the inhour formula. This number was then divided by the travel of the regulating rod to find the value of $(\Delta k/k)/in.$ for the run. A total of eight reactor excursions of this nature were made, six at 48-gpm flow, and two at zero flow.

Some of the reactor excursions during this experiment are shown in Fig. 5.5, as recorded by the log N recorder. The straight lines that indicate the slope of the power increase reflect periods on the order of 20 to 25 sec. Figure 5.6 presents some of the period traces recorded on the period recorder during the experiment. The initial high peaks for each rod movement are due to the transient condition, the interpretation of which is given in Appendix S. In plotting the period for a particular rod motion, the average of the periods obtained from the log N and the period recorders was used.

A plot of $(\Delta k/k)/in.$ as a function of rod position as obtained from this experiment is shown in Fig. 5.7. The horizontal lines on each side of the

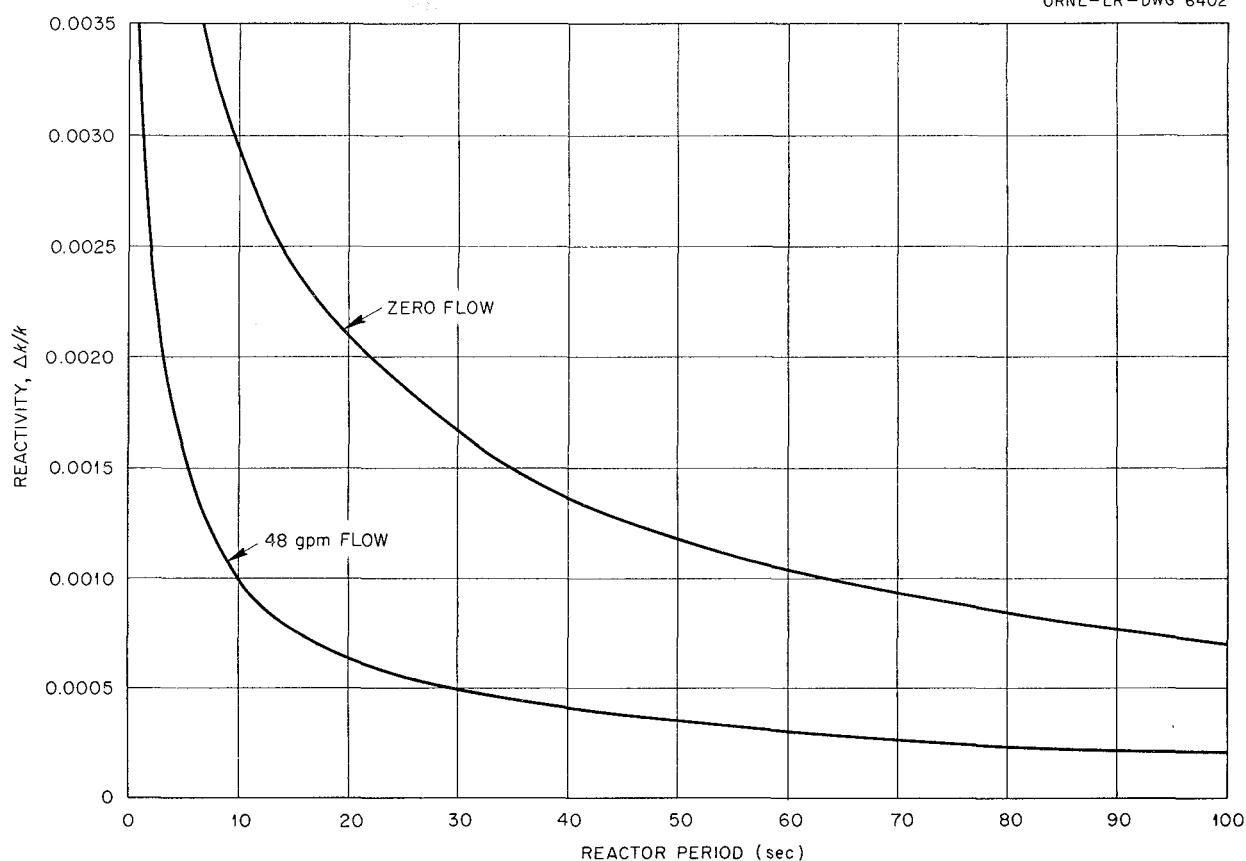


Fig. 5.4. Regulating Rod Reactivity vs Reactor Period for Fuel Flow Rates of 0 and 48 gpm.

experimental points show the extent of the rod movement for that point. Again, there is no conclusive evidence that the reactivity of the rod per unit length was not constant. Therefore, the average of the 48-gpm flow data weighted over the rod movement for each run gives

$$(\Delta k/k)/\text{in.} = 0.029\%/\text{in.}$$

For the two zero-flow points the rod was moved over the middle 10 in. of its 12-in. travel in two 6-in. overlapping runs covering the upper and lower halves of the rod, respectively. The weighted average of these points gave a value of

$$(\Delta k/k)/\text{in.} = 0.033\%/\text{in.},$$

which is in excellent agreement with the fuel addition calibration. This value was settled upon as the best value of reactivity per inch over the whole length of the regulating rod. The values for the reactivity vs rod position are given in Table 5.6.

CALIBRATION OF SHIM RODS VS REGULATING ROD

With the reactivity of the regulating rod known, the shim rods could be calibrated against it (exp. L-6). This calibration could then be compared with the previous calibration made during the fuel addition. It was assumed that the three shim rods were enough alike that a calibration of one rod would be representative, and rod No. 3 was chosen for the calibration.

The calibration procedure consisted of setting shim rods Nos. 1 and 2 in a fixed position, and then, with the reactor at a power level of 1 w on the servo mechanism, rod No. 3 was moved until a specified travel of the regulating rod was obtained. At the start of the experiment the rods were adjusted so that shim rod No. 3 was nearly all the way out (position indicator at 35 in.) and the regulating rod nearly all inserted (position indicator at 3 in.). After recording the position of all rods,

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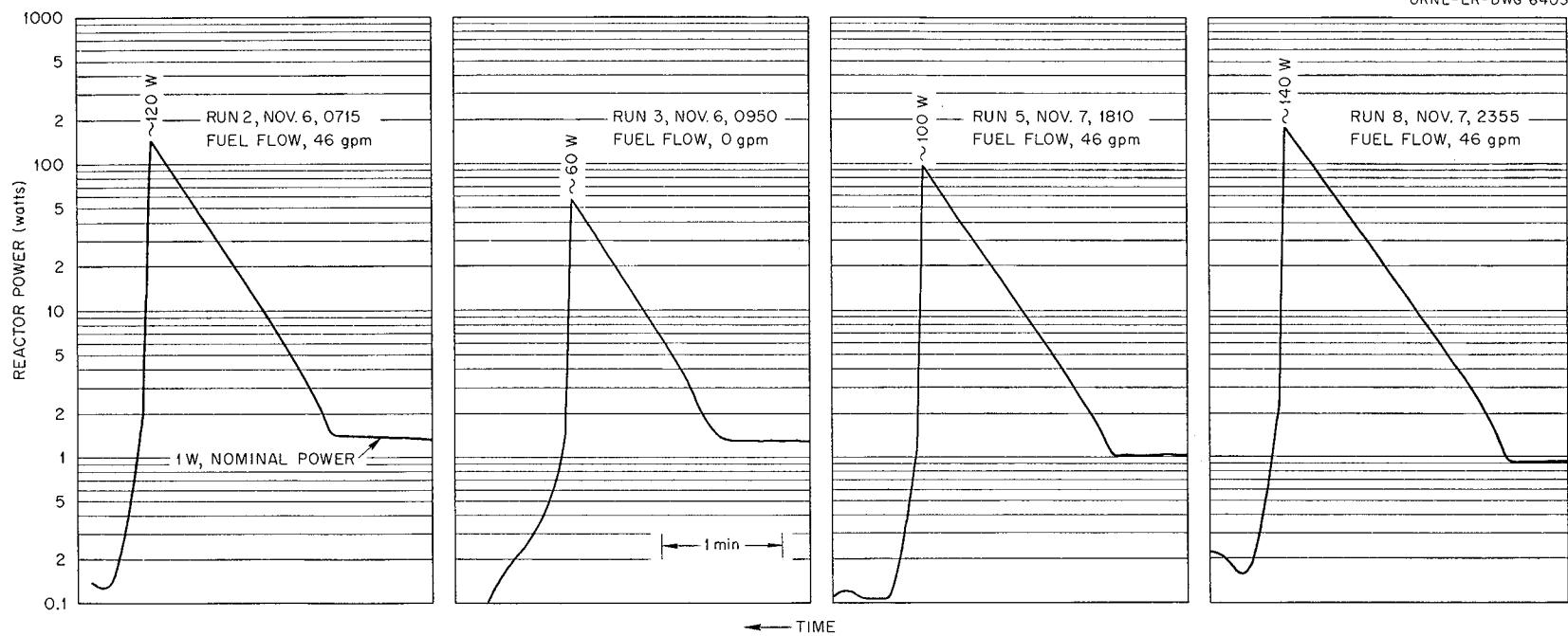


Fig. 5.5. Typical Reactor Excursions Recorded by Log N Recorder During Period Calibration of Regulating Rod. Experiment L-5.

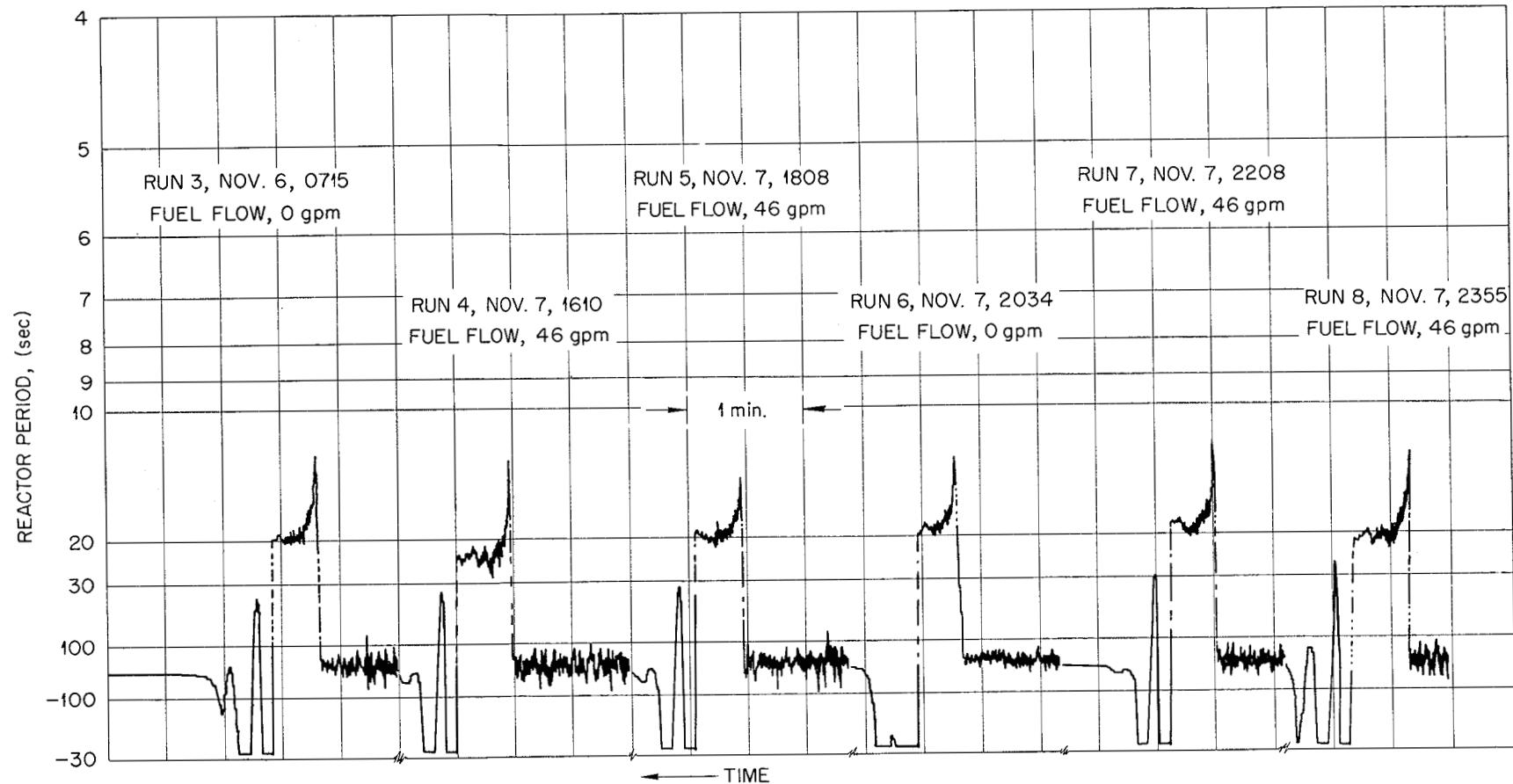


Fig. 5.6. Reactor Periods Recorded by the Period Recorder During Calibration of Regulating Rod. Experiment L-5.

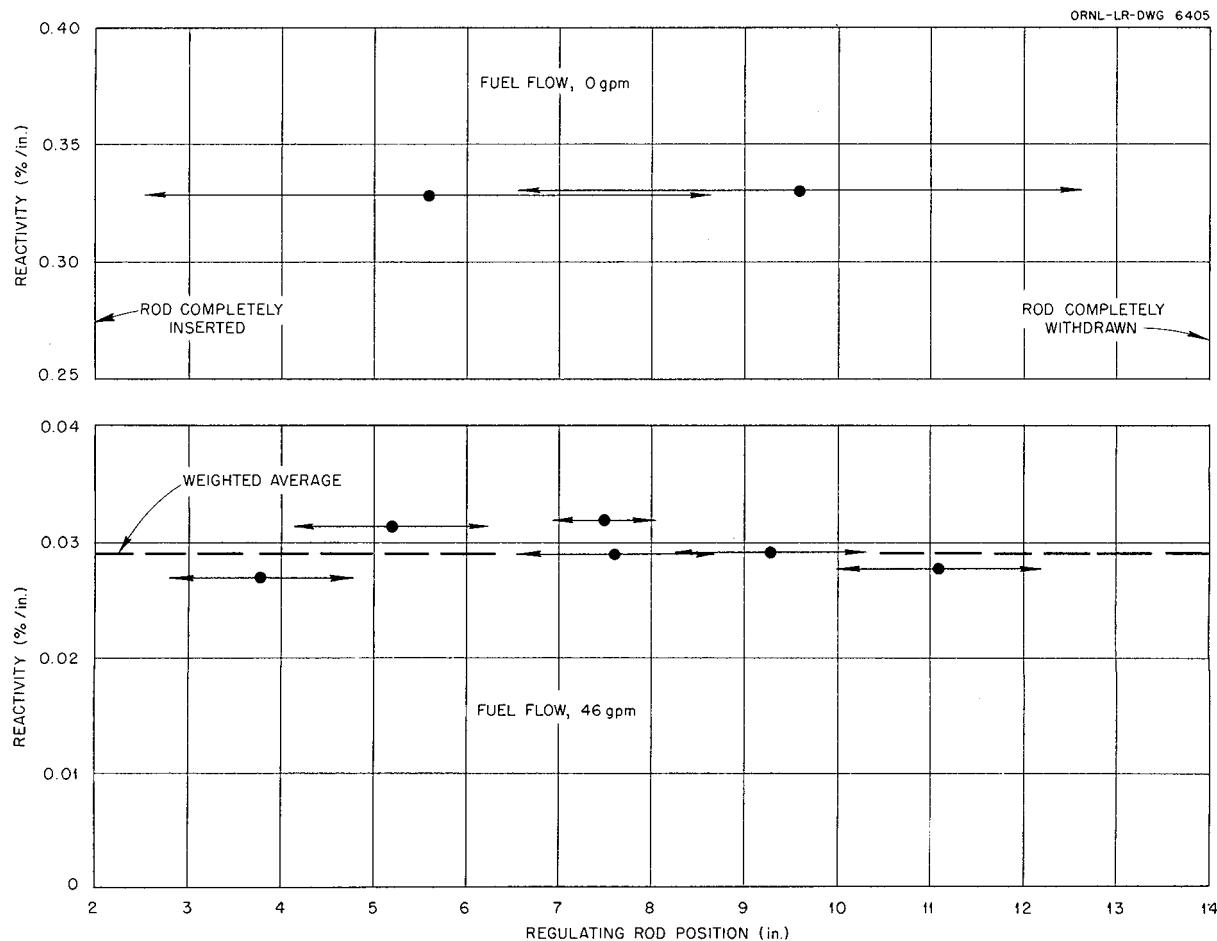


Fig. 5.7. Calibration of Regulating Rod from Reactor Period Measurements.

shim rod No. 3 was inserted until the servo action had withdrawn the regulating rod a compensating distance of about 10 in. The action was then stopped and the new rod positions were recorded. With shim rod No. 3 set, shim rods Nos. 1 and 2 were then adjusted to bring the regulating rod back to its original position, and again the rod positions were recorded. Again rod No. 3 was inserted until a 10-in. withdrawal of the regulating rod was attained. This process was repeated until rod No. 3 had been inserted about 14 in., and each new position had been recorded. This calibration agreed well with the calibration against fuel addition. Details of the results are given in Appendix J.

FUEL SYSTEM CHARACTERISTICS

The fuel system characteristics with the fuel concentrate in the system were determined for the

first (and only) time the day after the reactor first became critical (exp. L-3). The final amounts of concentrate (i.e., the excess to provide for burnup and poisoning during the subsequent power runs) had not yet been added to the system. Consequently, the fuel density at the time the data were taken was 3.32 g/cm^3 as compared with 3.36 g/cm^3 for the final fuel composition, and 3.08 g/cm^3 for the carrier; all densities were determined at 1300°F .

The measured and calculated flow data as a function of pump speed are shown in Fig. 5.8. The flow was calculated for two pump speeds by using the time between pips on the fission chamber as concentrate was first added to the system. The straight line joining the two calculated points is considered to be a good approximation because of the regime in which the pump was operated.

**TABLE 5.6. REGULATING ROD REACTIVITY CALIBRATION FROM REACTOR PERIOD MEASUREMENTS
(Exp. L-5)**

Run No.	Fuel Flow (gpm)	Average Period (sec)	$\Delta k/k$ from Inhour Equation	Average Regulating Rod Position (in.)	Movement of Regulating Rod (in.)	Reactivity, $(\Delta k/k)/\text{in.}$ (%/in.)
1	48	48	0.00036	7.5	1.1	0.0318
2	48	22.2	0.00060	7.6	2.08	0.0289
3	0	21	0.00206	9.6	6.05	0.0330
4	48	26	0.00054	3.8	2.0	0.0270
5	48	22	0.00061	11.1	2.2	0.0278
6	0	21.6	0.0020	5.6	6.1	0.0328
7	48	20.1	0.00065	5.2	2.08	0.0313
8	48	22.2	0.00060	9.3	2.06	0.0291
Average for 0-gpm flow						0.0329
Average for 48-gpm flow						0.029

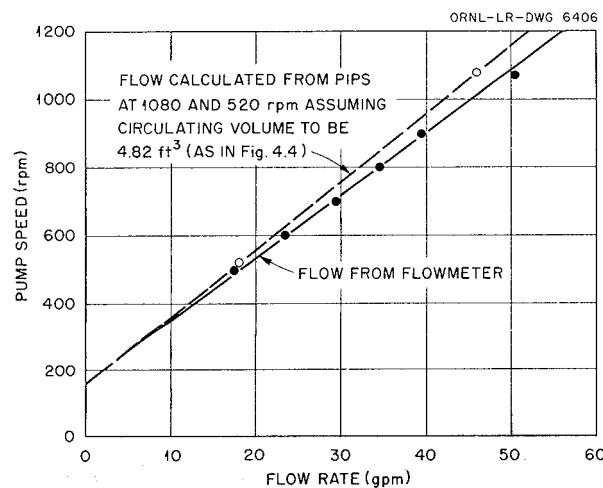


Fig. 5.8. Fuel Flow Rate as a Function of Pump Speed.

The flow data as a function of the system head loss from the reactor inlet to the pump tank are given in Fig. 5.9. The flow data are plotted directly vs head (by using the flow rates determined from pump speed as given by the upper curve in Fig. 5.8) and then as corrected for a "live" zero

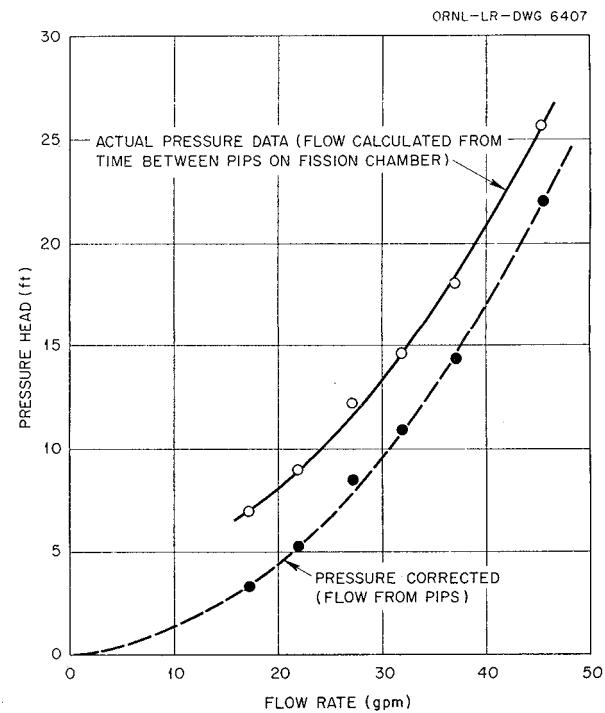


Fig. 5.9. Fuel Flow Rate vs the Pressure Head from the Pump Suction to the Reactor Inlet.

on the pressure transmitter from which the head values were obtained. The latter data fit the theoretical curve very well. Furthermore, these system data fit the pump performance data, if it is assumed that there is a 7-psi drop from the pump discharge to the reactor inlet at design flow (i.e., 46 gpm); there is no experimental measurement of this pressure drop. The pump performance characteristics determined in a test stand run with fuel at 1300°F are given in Fig. 5.10.

EFFECT OF FUEL FLOW ON REACTIVITY

An experiment was performed in which the effect of fuel flow on reactivity was observed (exp. L-7). For this experiment the reactor was brought to a nominal power of 1 watt and given over to the flux servo mechanism after full fuel flow of 46 gpm had been established. After recording the positions of the regulating and shim rods the flow rate was reduced step-wise until zero-flow was reached. Each reduction of the flow was accompanied by a change of position of the regulating rod. Reducing

the flow had the effect of allowing more delayed neutrons to contribute to the flux level in the reactor, and therefore the servo mechanism inserted the regulating rod to compensate for the excess reactivity created by the delayed neutrons. Each rate of fuel flow and the corresponding regulating rod position were recorded. The results of the experiment are shown in Fig. 5.11, where $\Delta k/k$ is plotted as a function of flow rate. It is observed that 12 in. of rod movement, or 0.4% $\Delta k/k$, was needed to compensate for the reactivity introduced when the flow rate was reduced from full to zero flow. This curve is comparable to that shown in Fig. D.2 of Appendix D. The data for this experiment are tabulated in Table 5.7.

Although not a part of experiment L-7, additional insight into fuel activity may be obtained from examination of Fig. 5.12, which shows activity as recorded by fission chamber No. 2. Before the data shown in the figure were recorded the reactor had been operating at a power of about 1 w with the fuel pump stopped. As shown, the reactor was

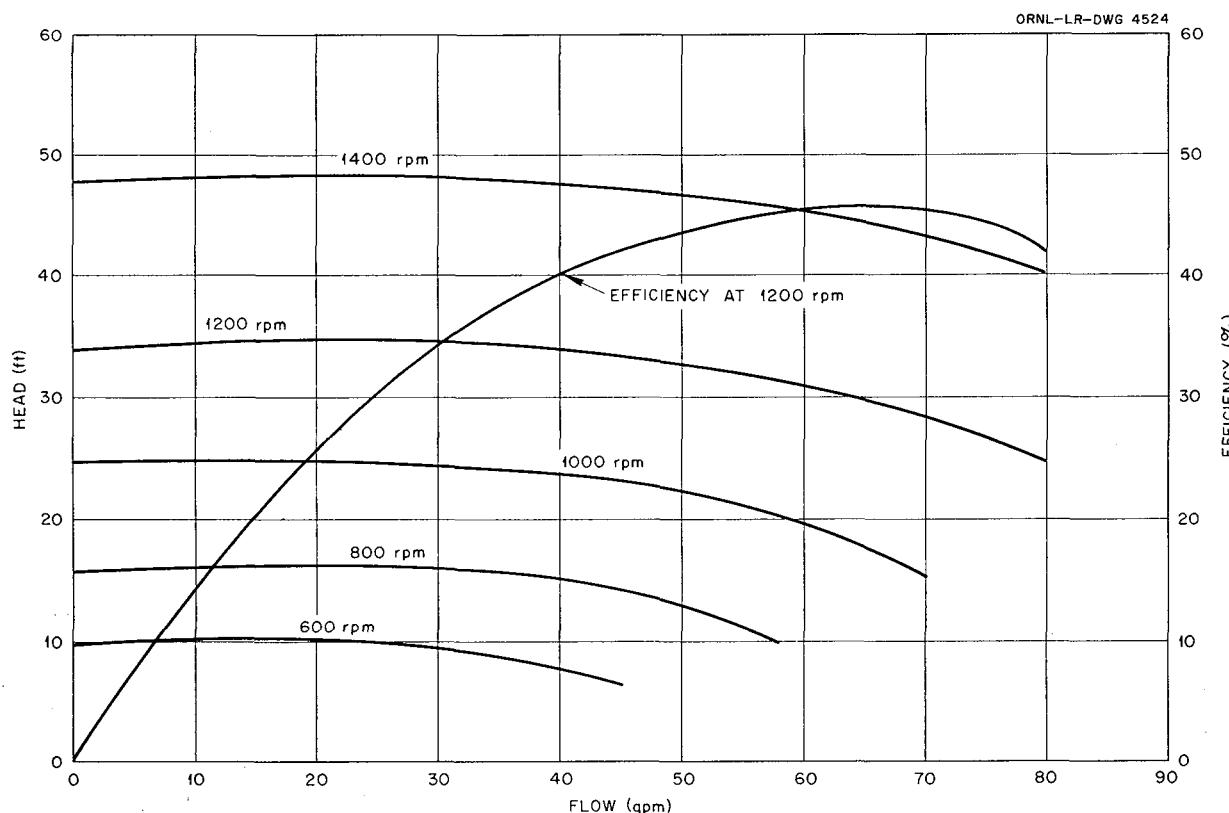


Fig. 5.10. Fuel Pump Performance Curves.

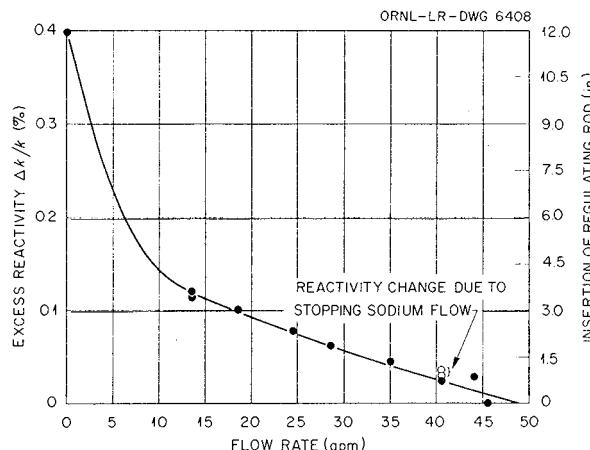


Fig. 5.11. Effect of Fuel Flow Rate on Reactivity.

**TABLE 5.7. EFFECT OF FUEL FLOW RATE ON REACTIVITY
(Exp. L-7)**

Run No.	Fuel Flow (gpm)	Sodium Flow (gpm)	Movement of Regulating Rod (in.)	Change in Reactivity, $\Delta k/k$ (%)
1	45.5	149	0	0
2	41	149	0.7	0.0231
3	35	149	1.4	0.0462
4	28.5	149	1.9	0.0627
5	23.8	149	2.4	0.0792
6	18	149	3.0	0.099
7	13.5	149	3.45	0.114
8	0	149	12.05	0.398
9	13.5	149	3.45	0.114
10	0	149	12.05	0.398
11	13.5	149	3.65	0.120
12	13.5	149	3.65	0.120
13	43.5	149	0.9	0.0297
14	41	149	0.96	0.0317
15	41	0	1.12	0.0370
16	41	149	0.96	0.0317

then scrammed¹ and the fuel pump started. The fuel which had been in the reactor before the scram was more active than the remainder of the fuel and

¹Scram, as used in this report, refers to an intentional shut down of the chain reaction by suddenly dropping the control rods into the core.

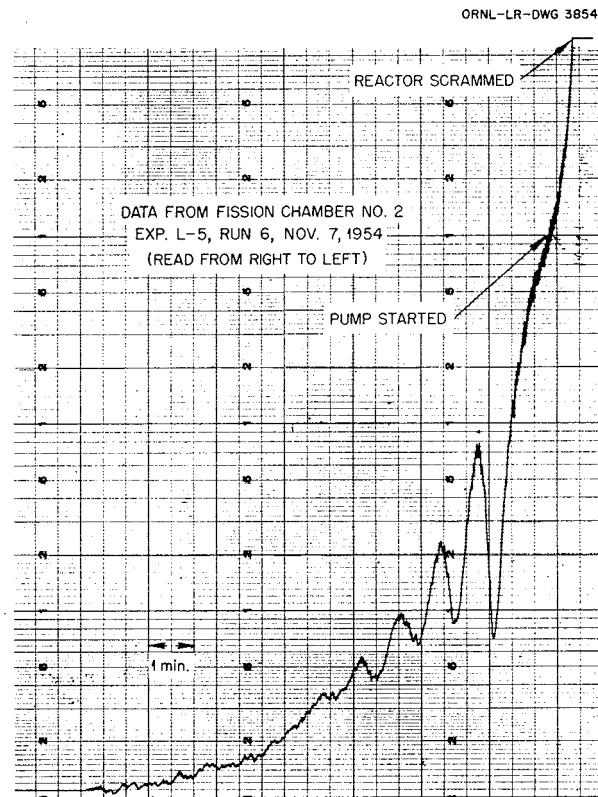


Fig. 5.12. Circulating Fuel Slugs after Starting Pump Following a Reactor Scram.

it was this excess activity which showed up as the fuel was circulated after the reactor was scrammed.

LOW-POWER MEASUREMENT OF THE TEMPERATURE COEFFICIENT

A measurement of the temperature coefficient of reactivity (exp. L-8) was made next. With the reactor isothermal at 1312°F and controlled by the flux servo mechanism, the heat barrier doors were raised and the helium blower turned on to 200 rpm to cool the fuel in the heat exchanger. As the temperature of the reactor decreased, the servo began to drive the regulating rod in to compensate for the increased reactivity. The recording of the regulating rod position vs time is shown in Fig. 5.13. Beginning at 0218, the rod was inserted by the servo quite rapidly, and by 0221 the rod was approaching its lower limit. With the regulating rod on servo, one of the shim rods was inserted as rapidly as possible. This shim rod insertion overcompensated for the increase in reactivity due to the temperature drop, and the

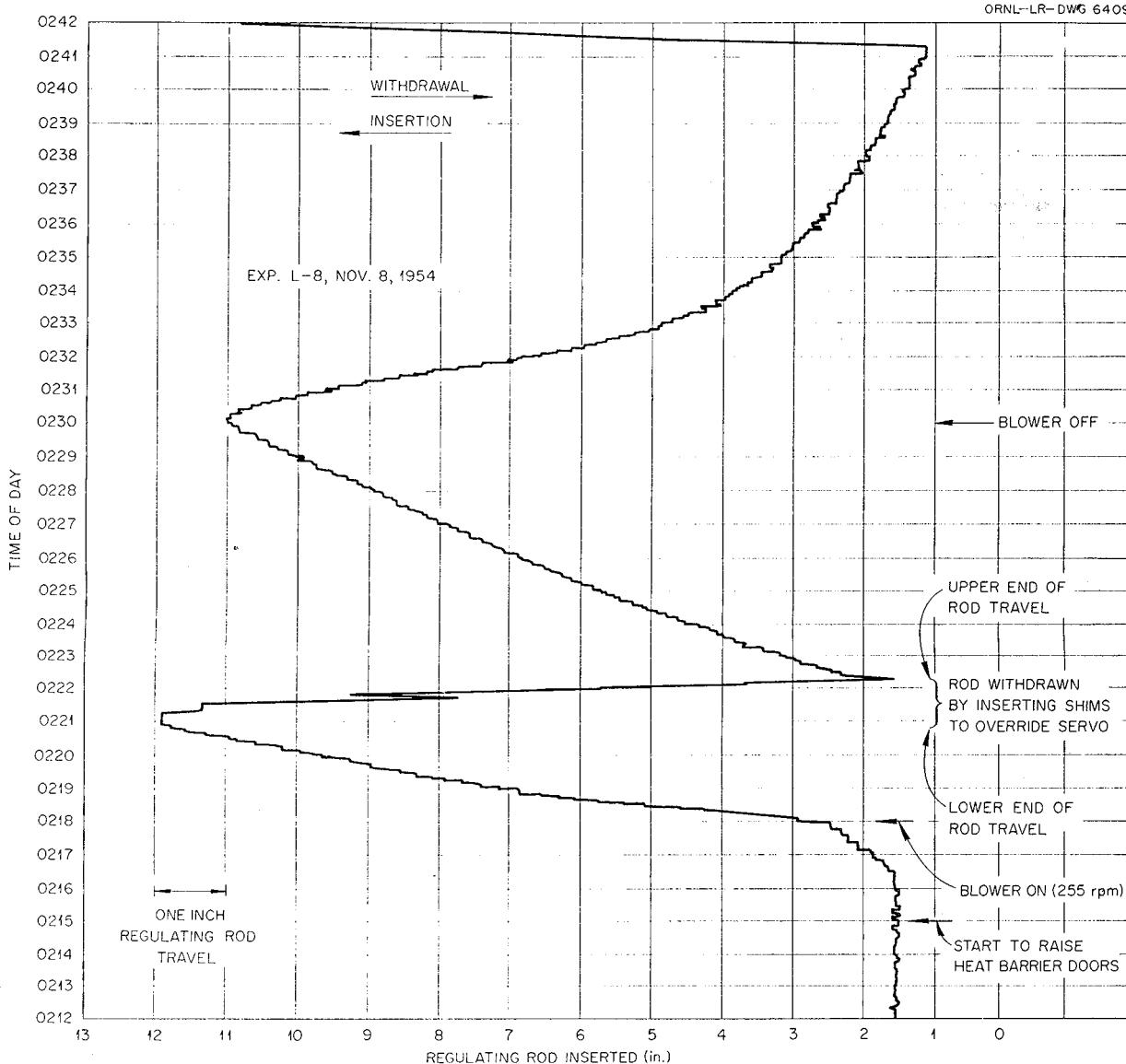


Fig. 5.13. Regulating Rod Position During Low-Power Measurement of the Reactor Temperature Coefficient.

servo quickly withdrew the regulating rod. Insertion of the shim rod was stopped when the regulating rod had been withdrawn to near its upper limit, and the regulating rod was again inserted by the servo to compensate for the reactivity introduced by the cooling of the fuel. By 0230, the outlet temperature in the heat exchanger was approaching its lower limit, 1150°F, so the helium blower was stopped and the run was ended.

A trace from the chart for recording the mean fuel temperature is shown in Fig. 5.14, and superimposed on it is a plot of the displacement of the

regulating rod as obtained from the previous figure. A measure of the temperature coefficient may be obtained by comparing the slopes of the two curves. At 0228 the rod was moving at exactly 1 in./min, corresponding to an increase in reactivity of $3.3 \times 10^{-4} (\Delta k/k)/\text{min}$. At the same time, the mean temperature was dropping at the rate of $5.1^\circ\text{F}/\text{min}$. The resulting reactor temperature coefficient, as obtained from these data, would appear to be $-6.48 \times 10^{-5} (\Delta k/k)/^\circ\text{F}$. By comparing the slopes of the curves obtained earlier during the run, a considerably higher coefficient

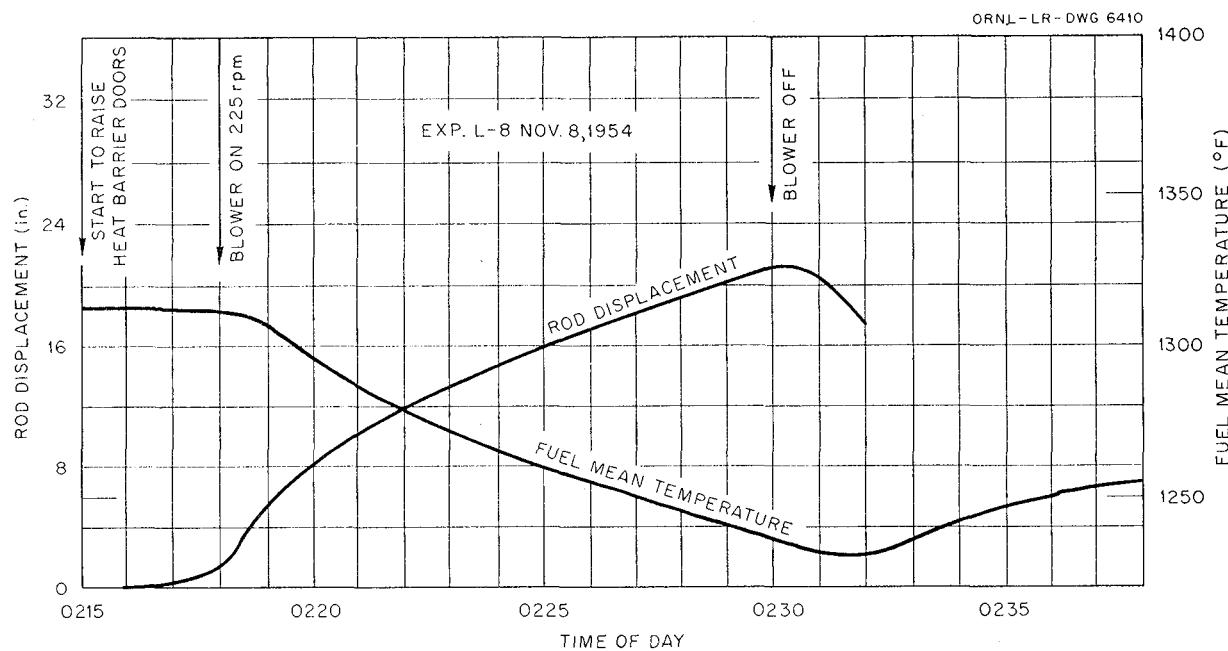


Fig. 5.14. Regulating Rod Position Superimposed on Fuel Mean Temperature Chart.

can be obtained that might approximate that for the fuel. In any case, the recorded mean temperature is believed to be in error (as explained in Appendix K) in such a manner that the actual rate of temperature change is about 40% higher than that given in Fig. 5.14. The measured value of the temperature coefficient was corrected accordingly to give a value of $-4.6(\Delta k/k)/^{\circ}\text{F}$ for the low power. This value is comparable to that subsequently obtained during high-power operation and, as noted in the subsequent discussion, the data from experiment H-8 yielded the best values for both the fuel and the reactor temperature coefficients.

The apparent time lag between the reactivity and the minimum mean temperature, as first noted during the subcritical measurement of the temperature coefficient, was still in evidence here. Possible explanations of the time lag, as well as other details of the various temperature coefficient measurements, are given in Appendix O.

ADJUSTMENT OF CHAMBER POSITION

During the critical experiment and the low-power operation, it was desirable to have the nuclear instruments positioned to read at as low a power as possible. The chambers were therefore as

close to the reactor as possible. Before increasing the power, it was necessary to adjust the positions of the nuclear chambers so that they would read at higher power levels. This was accomplished by adjusting the power level of the reactor to about 100 w and then moving the compensated log N chamber away from the reactor so that its reading was changed from 0.032 to 0.001, or its upper limit was extended by a factor of about 30. With the reactor power at about 1 kw, the micromicroammeter chamber was moved away from the reactor so that its reading was changed from 41.4 on the 5×10^{-7} amp range to 54 on the 1×10^{-8} amp range. This extended the upper limit of the meter by a factor of about 40. While one chamber was adjusted the reactor power was held constant by the other chambers so that the correlation between instrument readings was not lost. The nuclear power for the experiment was determined on this basis.

In the final analysis, the correlation between chamber readings and reactor power can be based on the 25-hr xenon run during which a good value for the extracted power was obtained. The micro-micromicroammeter read 52.5 on the 2×10^{-5} scale when the log N read 22.5, and both corresponded to an extracted power of 2.12 Mw.

6. HIGH-POWER EXPERIMENTS

The low-power tests were concluded by noon on November 8. During the last few days of the low-power tests all last minute details in preparing the system for high-power operation had been under way. These preparations included lubricating all rotating equipment, refilling oil reservoirs, changing filters, replacing motor brushes, checking all instrumentation, etc. By 1445 on November 8 the pits had been sealed, i.e., covered with three layers of $2\frac{1}{2}$ -ft-thick concrete blocks and caulked, and the experiment was ready for the high-power phase of the operation, the chronology of which is given in Fig. 6.1.

Prior to the start of the high-power experiment the final addition of fuel concentrate, which was to provide the reactor with sufficient excess reactivity to overcome burnup and fission-product poisoning, was made. This last addition consisted of 15.419 lb of concentrate diluted with 32.379 lb of partially enriched fuel (part of that removed from the system earlier when the pump level was trimmed) and was injected into the system through the sample line on the morning of November 7. The sample line was used for this final enrichment operation because the transfer line through which the concentrate had hitherto been injected into the system had again developed a leak. It was necessary to lower the melting point of the concentrate (by dilution) because it was not certain that the sample line could otherwise safely maintain the high temperature required.

High power, which may be defined for the ARE as anything over 0.1 Mw, was approached in a series of successive steps of increasing power. The power regime was not attained at once, because leakage of fission activity from the system into the pits and subsequently from the pits into the occupied parts of the building required that provision be made to maintain the pits at a subatmospheric pressure. The experiment could then continue safely, and a power of greater than 2 Mw was first attained early during the evening of November 9.

The remaining time (70 hr) of the ARE operation was devoted to several experiments to determine the high-power behavior of the reactor; these experiments are described in detail in the following sections. Starting in the evening of November 9, the fuel temperature coefficient of reactivity (Exp. H-4) and the over-all reactor temperature coefficient (Exp. H-5 and Exp. H-9) were measured.

The early hours of November 10 were used to take the reactor to power from subcritical by making use of the negative temperature coefficient (Exp. H-6). Later in the day the sodium temperature coefficient was measured (Exp. H-7), some other reactor kinetics were studied (Exp. H-8), and the moderator temperature coefficient was measured (Exp. H-10). During this time the operating crews had opportunity to familiarize themselves with the handling of the reactor at power.

At 1835 on November 10, a 25-hr full-power xenon run was started. For this run the reactor was held in steady-state operation at 2.12 Mw by the negative temperature coefficient and at a mean temperature of 1311°F . Since equilibrium temperature conditions prevailed during this run, a very good measurement of extracted power could be made. The run ended at 1935 on November 11. Later that night, the effect on the power of stopping the sodium flow was observed (Exp. H-12), and at 2237 a $\frac{1}{10}$ -power run (Exp. H-13) was started to observe the effect of xenon buildup and continued for a period of 10 hr. During this run the reactor power was approximately 200 kw. At 0835 on November 12 no effect of xenon buildup had been observed, and therefore the experiment was terminated.

The morning of the last day, November 12, was devoted to some more reactor kinetics studies and a measurement of the maximum extracted power available (Exp. H-14), which turned out to be about 2.5 Mw. On the afternoon of November 12 the building was opened to visitors with proper clearance, and the behavior of the reactor was demonstrated to them. At 2004, an estimated total operating time of 100 Mw-hr having been accumulated, the reactor was scammed and the ARE experiment was terminated.

APPROACH TO POWER

The initial phase of high-power operation of the ARE began at 1445 on November 8. As shown in Fig. 6.1, the power was raised in a series of successive steps. At each power level, when steady-state conditions had been obtained, a complete set of control room data was taken. The first experiment, H-1, was a 20-kw run. During this run the safety chambers were withdrawn and reset to scram at about 260 kw. At 1619 the reactor was shut down because of the presence of

CHRONOLOGY OF THE HIGH-POWER EXPERIMENTS

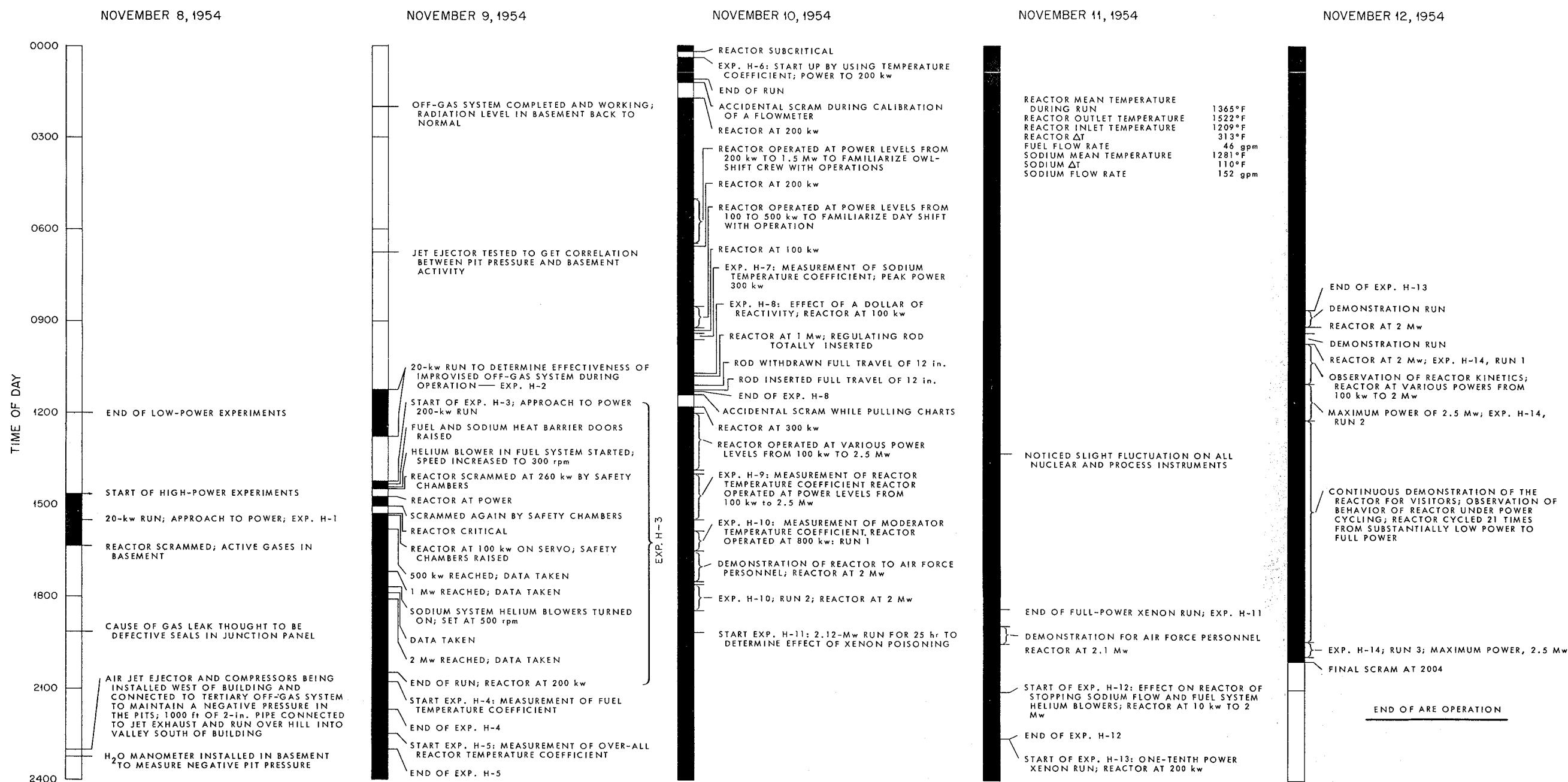
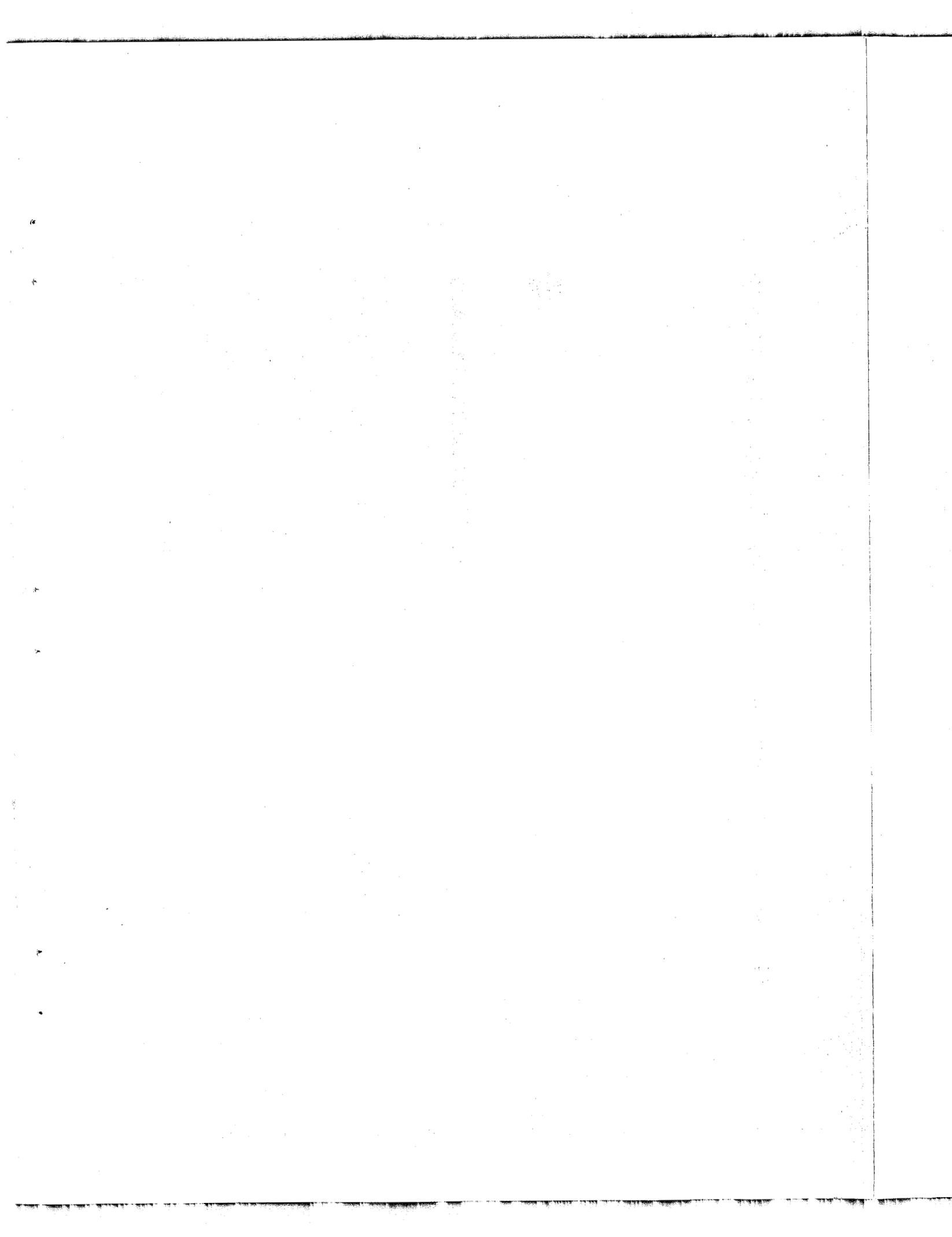


Fig. 6.1.



airborne radioactivity in the basement. Apparently the gas fittings to the main fuel pump were leaking and fission-product gases and vapors were leaking into the pits and from the pits into the basement through defective seals in some of the piping and electrical junction panels connecting the basement with the pits.

In order to prevent the leakage of activity into the basement it was decided to operate the pits at a slightly subatmospheric pressure. Accordingly, a 2-in. pipeline was run in a direction south of the ARE building for a distance of 1000 ft and terminated in an uninhabited valley. Then, by means of portable compressors and a jet, the pit pressure was lowered by about 6 in. H₂O, with the exhaust from the compressors being bled into the 2-in. pipeline. The pits were maintained at a negative pressure for the balance of the experiment.

At 1125 on November 9 the reactor was again brought to 20-kw power (Exp. H-2) for the purpose of testing the new off-gas system to determine whether or not the negative pressure of 6 in. H₂O in the pits was enough to keep the hot gases from diffusing into the basement. During this run the pit activity, as recorded on the pit monitrons, was watched, and its decay after shutdown of the reactor at 1246 was observed. From this run it was ascertained that the subatmospheric pit pressure would prevent pit activity from leaking into the building.

At 1520 on November 9 the approach to power was started again (Exp. H-3). At 1523 the reactor was brought to a nominal power of 200 kw on a 17-sec period and leveled out. Six minutes later the barrier doors were raised and the first attempt to extract power was made. At 1529 the fuel helium blower was turned on and the blower speed was increased to 300 rpm. The nuclear power again began to increase, but the safety chambers had not been withdrawn far enough and they scrammed the reactor when the power level had reached about 260 kw.

After another false start, the safety chambers were withdrawn again and set to scram at about 4 Mw. The reactor was then brought to 100 kw, leveled out, and placed on flux servo at 1625. At 1626 it was taken off servo and the blower speed was increased, this time to only 170 rpm. The reactor power slowly rose and at 1643 had leveled off on the reactor temperature coefficient at about 500 kw. After a set of data had been taken and the reactor mean temperature elevated, the blower

speed was increased to 400 rpm and the power level continued to rise. By 1715 the power level had leveled out at near 1 Mw.

The sodium blowers were turned on (at 1740) and brought to a speed of about 500 rpm. Half an hour later the fuel blower speed was increased to 1590 rpm, and in 10 min a steady-state power level of about 2 Mw was reached. At this time the nuclear and process instruments read as follows:

Log N power, ¹ Mw	1.32
Micromicroammeter power, ¹ Mw	1.38
Reactor inlet fuel temperature, ² °F	1203
Reactor outlet fuel temperature, ² °F	1440
Reactor mean fuel temperature, ² °F	1321
Fuel temperature difference across reactor, ² °F	237
Fuel flow, gpm	46
Reactor sodium mean temperature, °F	1281
Sodium temperature difference across reactor, °F	10
Sodium flow, gpm	152

From these data the extracted power was calculated as follows:

Power extracted from fuel, Mw	1.16
Power extracted from sodium, Mw	0.05
Power extracted from rod cooling, Mw	0.02
Total extracted power, ² Mw	1.23

However, it was subsequently discovered that the temperatures upon which this extracted power was calculated were in error and, as discussed in Appendix K, the actual temperature gradient at this time was about 40% higher. Therefore, the extracted power was correspondingly higher than that listed. A general discussion of the extracted power appears in a following section.

The above-described power operation was maintained for about 1 hr, during which time no further trouble was occasioned by the fission gases. Power was reduced at 1900 and the reactor scrammed at 1915, and thus the initial phase of the high-power operation was concluded.

TEMPERATURE COEFFICIENT MEASUREMENTS

Several experiments were performed in an attempt to measure the effect on reactivity of temperature changes of the various components of the

¹Set on the basis of the power calibration from fuel activation.

²The temperatures and consequently the extracted power values are in error as noted in the discussion following the data.

reactor. In addition to the over-all reactor coefficient, experiments were run to obtain data on the instantaneous fuel temperature coefficient and the coefficients attributable to the sodium and the beryllium oxide moderator. There were several anomalies that developed in the course of these experiments, the two most significant being (1) the interpretation of the lag in the response between the rod movement and the change in reactor temperatures as power was abstracted from the reactor and (2) the discrepancy between the thermocouple indications at the reactor (fuel and sodium inlet and outlet temperatures) and those along the lines to and from the reactor. These anomalies are discussed in detail in Appendixes O and K, respectively. It was concluded that the time lag was not real (i.e., the fuel temperature should show changes as soon as the reactivity does) and that the line temperature most accurately reflects the actual stream temperatures.

In the determination of a temperature coefficient by varying the power extracted from the reactor, the recorded temperatures are subject to correction, as described in Appendix K. However, when the temperature coefficient was determined, as in Exp. H-5, by withdrawing the shim rods so that the reactor slowly heated itself while the extracted power remained constant, no correction needed to be made for the temperature. Furthermore, this technique minimized the temperature lag anomaly, and the fuel and reactor temperature coefficients derived from Exp. H-5 are therefore believed to be the best experimental values for these coefficients.

Fuel and Reactor Temperature Coefficients

The fuel and reactor temperature coefficients were both obtained from the same experiment, the fuel being the instantaneous coefficient, the reactor the "equilibrium" coefficient. The initial attempts (Exp. H-4) to measure these coefficients were not satisfactory because of the difficulty in interpreting the results, and therefore the measurement was repeated (Exp. H-5) in a somewhat different manner.

In the first experiment, H-4, the procedure was similar to that described previously under "Low-Power Measurement of the Temperature Coefficient," and the data are presented in Figs. 6.2 and 6.3. The first of these figures is the recording of the position of the regulating rod as it was inserted by the servo as the fuel was cooled by the helium flow in the heat exchanger. Figure 6.3 is a recording of

the mean fuel temperature with the rod displacement as determined from Fig. 6.2 superimposed. Depending upon the time at which the slopes of the two curves are compared, the temperature coefficient appears to decrease from a value of $\sim -1.6 \times 10^{-4}$ $(\Delta k/k)/^{\circ}\text{F}$ to -4.43×10^{-5} $(\Delta k/k)/^{\circ}\text{F}$ toward the end of the run. These values represent the recorded data and are of course subject to the correction for temperature, as discussed in Appendix K, even as the data are subject to various interpretations because of the lag in the temperature data (see Appendix O). Furthermore, the changes were made quite rapidly, the entire run lasting only 5 min.

In an attempt to minimize the effect of the temperature anomalies, the temperature coefficients were then determined from an experiment (Exp. H-5) in which the extracted power was held constant and the shim rods were withdrawn. Starting with the reactor at a mean temperature of 1260°F , the withdrawal of the shim rods allowed the reactor to gradually heat the whole system to 1315°F . Since the reactor was a slave to the heat extraction system, which was not changed, the extracted power remained virtually constant during this time. This process took about 35 min during which the nuclear power was held constant at a nominal power of 200 kw by the flux servo. The regulating rod gradually withdrew to compensate for the decrease in reactivity as the reactor temperature increased. The data are tabulated in Table 6.1, and a plot of rod withdrawal vs mean reactor temperature is presented in Fig. 6.4. Inspection of Table 6.1 shows that the rate of change of the inlet and outlet fuel temperatures followed the change in mean fuel temperature very closely, and thus gave assurance that the fuel throughout the reactor was changing temperature at a uniform rate.

The most reliable values for the temperature coefficients of the ARE were obtained from this experiment. For the first 6 min the plot of rod withdrawal vs reactor mean temperature shows a slope of $0.296 \text{ in.}/^{\circ}\text{F}$. Since 1 in. of rod movement is equivalent to $3.3 \times 10^{-4} \Delta k/k$, the initial temperature coefficient was $-9.8 \times 10^{-5} (\Delta k/k)/^{\circ}\text{F}$. After the first 6 min and up until conclusion of the run, the curve in Fig. 6.4 demonstrates a constant value of the temperature coefficient of $-6.0 \times 10^{-5} (\Delta k/k)/^{\circ}\text{F}$. These are the best values for these coefficients that were obtained. It should be noted that the value for the over-all temperature coefficient agrees to within 25% with the value previously obtained from the low-power experiments. However,

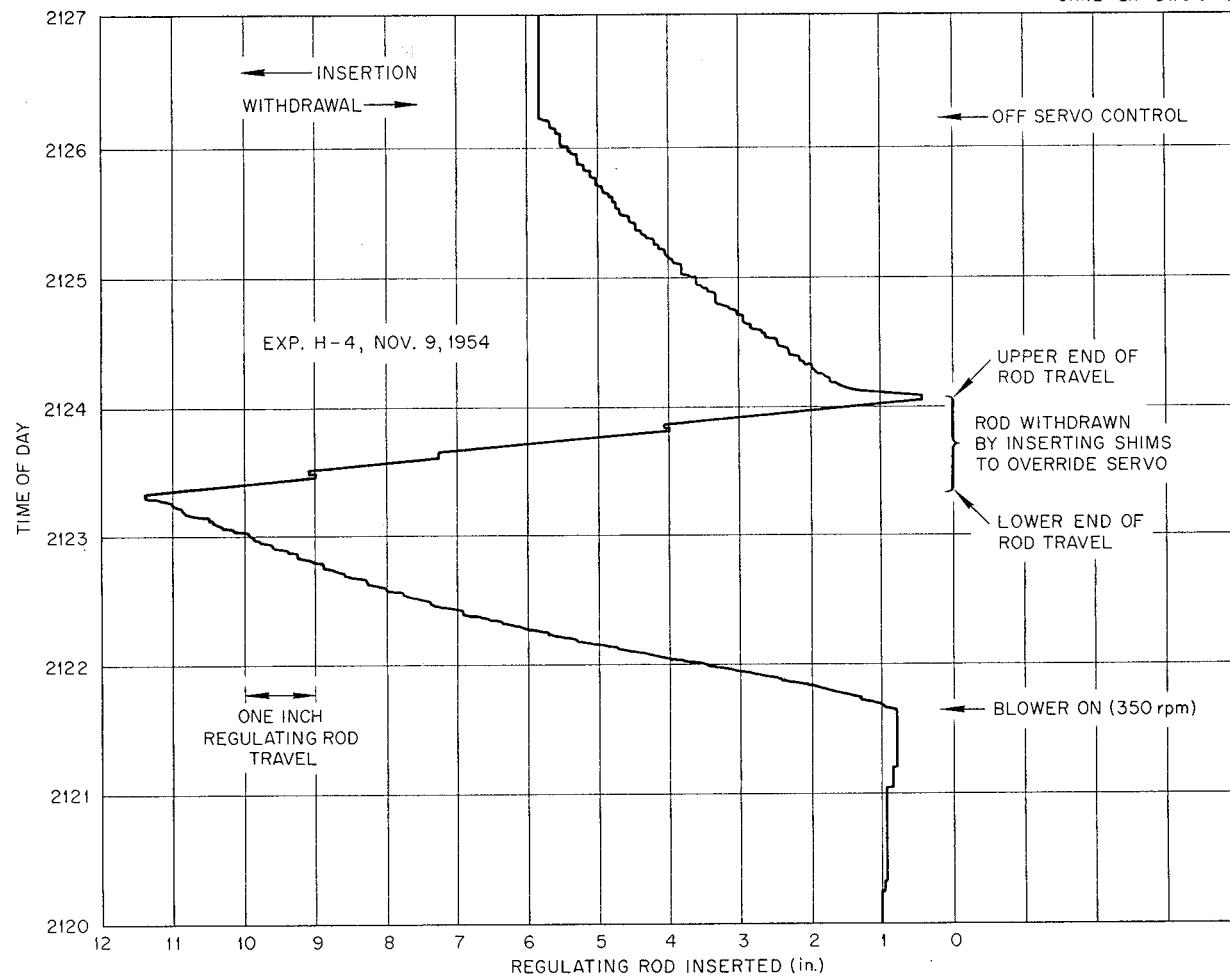


Fig. 6.2. Regulating Rod Position During Measurement of Reactor Temperature Coefficient. Experiment H-4.

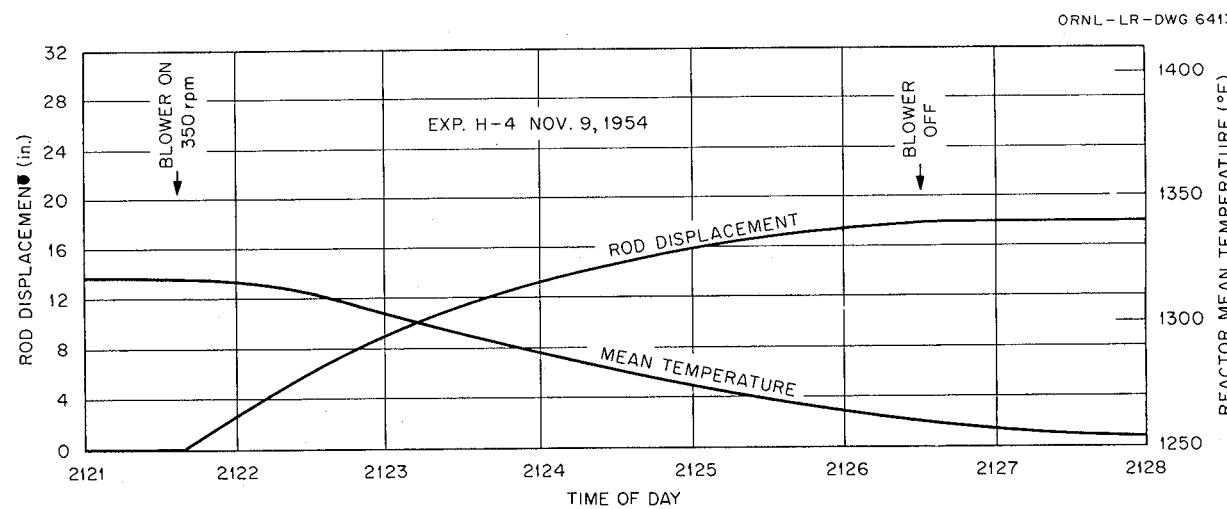


Fig. 6.3. Regulating Rod Position Superimposed on Fuel Mean Temperature Chart. Experiment H-4.

**TABLE 6.1. REACTOR TEMPERATURES AND ROD POSITIONS DURING
100-kw MEASUREMENT OF TEMPERATURE COEFFICIENTS (EXP. H-5)**

Time	Regulating Rod Position (in.)	Rod Withdrawal (in.)	Reactor Mean Temperature (°F)	Reactor Inlet Temperature (°F)	Reactor Outlet Temperature (°F)
2223	3.72	0	1263.5	1262.5	1283
24	3.84	0.12	1265	1263.5	1285
25	4.15	0.43	1266	1264	1286
26	4.43	0.71	1267	1265.5	1287
27	4.69	0.97	1268	1266	1288
28	4.96	1.24	1269	1267.5	1290
29	5.23	1.51	1270.3	1269	1291
30	5.50	1.78	1271.5	1271	1292
31	5.77	2.05	1273	1272	1293
32	6.02	2.30	1274	1273	1294
33	6.28	2.56	1275	1274.5	1296
34	6.49	2.77	1276.5	1275.5	1297
35	6.68	2.96	1277.5	1277	1298
36	6.90	3.18	1278.5	1278	1300
37	7.10	3.38	1279.5	1279	1301
38	7.35	3.65	1281	1280.5	1302
39	7.50	3.78	1282	1281.5	1303
40	7.69	3.97	1283	1282.5	1304
41	7.92	4.20	1283.5	1283.5	1305
42	8.14	4.42	1285	1284.5	1307
43	8.32	4.60	1286.3	1285.5	1308
44	8.55	4.83	1287.5	1286.5	1309
45	8.75	5.03	1288.5	1287.5	1310
46	8.94	5.22	1289.5	1289	1311
47	9.11	5.39	1291	1290	1312
48	9.31	5.59	1292.5	1291	1313
49	9.50	5.78	1293.5	1292	1314
50	9.68	5.96	1294.3	1293	1315
51	9.85	6.13	1295	1294	1316
52	10.05	6.33	1296.5	1295	1317
53	10.23	6.51	1297.5	1296	1318
54	10.45	6.73	1298.8	1297	1319
55	10.60	6.88	1299.5	1298	1320
56	10.78	7.06	1300.5	1299	1321
57	10.99	7.27	1301.3	1300	1322
58	11.17	7.45	1302.5	1301	1323
59	11.41	7.69	1303.5	1302.3	1324
2300	11.54	7.82	1305	1303	1325
01	11.80	8.08	1306.3	1304	1326
02	11.95	8.23	1307	1305	1327
03	12.20	8.48	1308	1306	1328
04	12.38	8.66	1308.8	1307	1329
05	12.57	8.85	1309.8	1308	1330
06	12.75	9.03	1310.5	1309	1331
07	12.90	9.18	1311.5	1310	1332.5
08	13.19	9.47	1312.5	1311	1333
09	13.25	9.53	1313.5		
10					

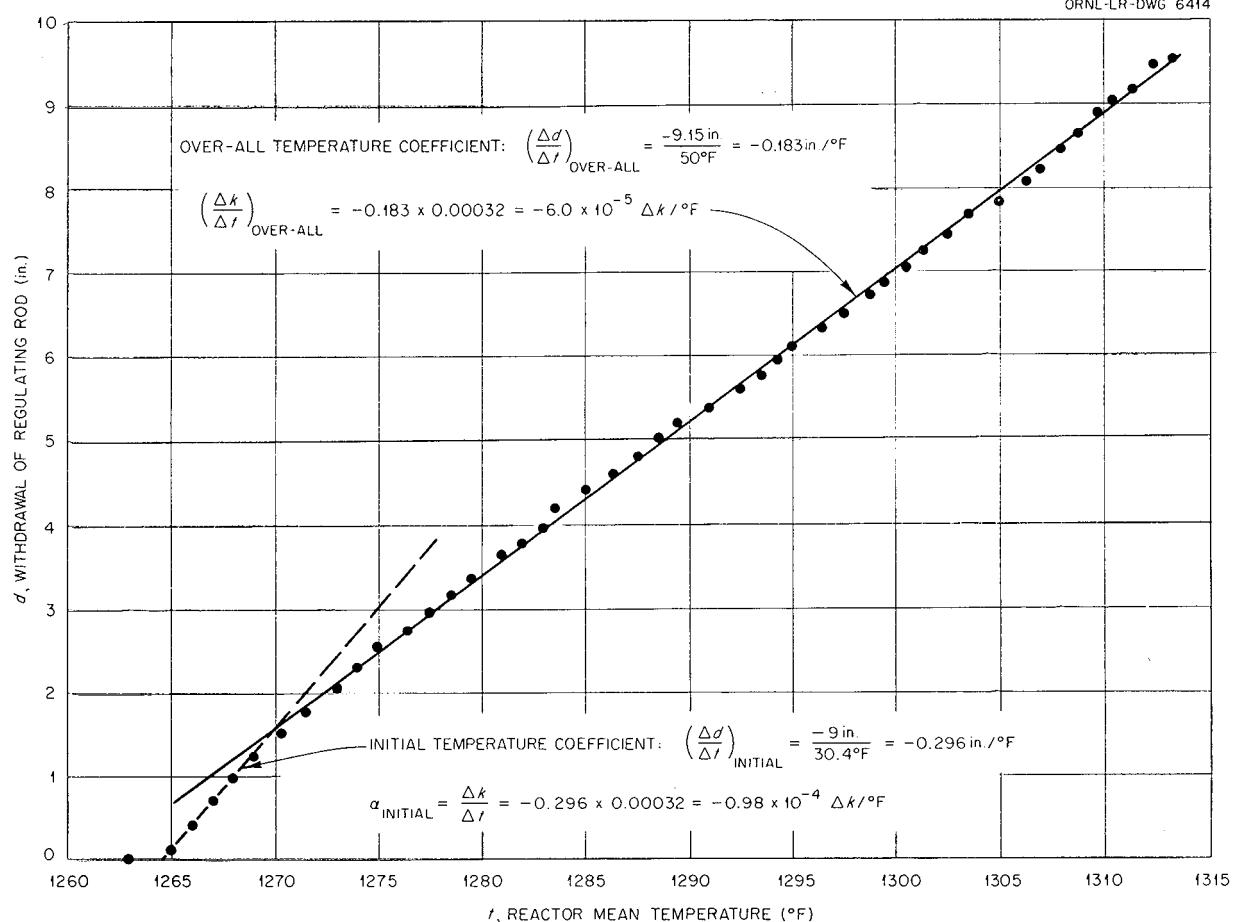


Fig. 6.4. Regulating Rod Movement as a Function of Reactor Mean Temperature. Experiment H-5.

the instantaneous value of $-9.8 \times 10^{-5} (\Delta k/k)/^\circ\text{F}$ is much more important from the reactor control standpoint, and it was this large fuel temperature coefficient which made the ARE demonstrate the excellent stability described below under the subtitle "Reactor Kinetics."

The value for the reactor temperature coefficient was subsequently confirmed in a later experiment (Exp. H-9) in which the system temperature was changed by gradually cooling the sodium, which in turn, cooled the fuel and the reactor. While the curve obtained from this experiment was very similar to that given in Fig. 6.4, the initial slope could not be that due to the fuel temperature coefficients, because the fuel is one of the last constituents in the reactor to feel the temperature change. The "equilibrium" slope, however, should be that determined by the reactor temperature coefficient, and a value of $-6.3 \times 10^{-5} (\Delta k/k)/^\circ\text{F}$

was obtained. No temperature correction was required because the extracted power in the fuel system did not change (although that in the sodium system did). This value agrees very well with that obtained in the preceding experiment.

Sodium Temperature Coefficient

In order to measure the sodium temperature coefficient an experiment (Exp. H-7) was performed in which the sodium was cooled and the corresponding changes in sodium temperature and reactivity were measured. In this experiment it was mandatory that the sodium be cooled rapidly and the data recorded before the moderator had time to cool. Otherwise, since the sodium bathes the moderator, the moderator temperature would follow the sodium temperature and introduce an extraneous effect due to its (i.e., moderator) temperature coefficient. Accordingly, with the reactor at about

33 kw and no power being extracted from either the fuel or the sodium, the sodium blower speeds (2 blowers) were quickly raised from 0 to 2000 rpm. The reactor period immediately started to change and went from infinity to 50 sec in 1.5 min, which, as shown in Fig. 5.4, corresponds to a reactivity change of $3.5 \times 10^{-4} (\Delta k/k)$. The consequent rate of reactivity change was $2.33 \times 10^{-4} (\Delta k/k)/\text{min}$. In this experiment the regulating rod, as well as the shim rods, was held in a fixed position. During the 1.5-min interval, the fuel temperature was changing at a rate of about $-1^\circ\text{F}/\text{min}$ and the sodium temperature was changing at a rate of $-2.3^\circ\text{F}/\text{min}$. (The rate of change of fuel mean temperature was corrected for the discrepancy in the recorded mean temperature, as described in App. K, but no comparable correction was necessary in the rate of change of the sodium temperature.) By applying the previously mentioned value of $-9.8 \times 10^{-5} (\Delta k/k)^\circ\text{F}$ for the instantaneous fuel temperature coefficient to give a rate of reactivity change for the fuel of $0.98 \times 10^{-4} (\Delta k/k)/\text{min}$ and subtracting from the rate of reactivity change observed upon cooling the sodium, it is found that the reactivity change caused by the decrease in the sodium temperature is

$$\begin{aligned} & 2.33 \times 10^{-4} (\Delta k/k)/\text{min} \text{ (observed)} \\ & - 0.98 \times 10^{-4} (\Delta k/k)/\text{min} \text{ (fuel)} \\ & = 1.35 \times 10^{-4} (\Delta k/k)/\text{min} . \end{aligned}$$

Then, by applying the observed rate of change of the sodium temperature, the sodium temperature coefficient is found to be

$$\begin{aligned} & \underline{1.35 \times 10^{-4} (\Delta k/k)/\text{min}} \\ & -2.3^\circ\text{F}/\text{min} \\ & = -5.88 \times 10^{-5} (\Delta k/k)^\circ\text{F} . \end{aligned}$$

This value is valid if it is assumed that the transient took place rapidly enough that there was no appreciable change in the moderator temperature. The measurements were, however, subject to considerable error because the temperature changes involved were so small as to be quite difficult to detect and a correction was necessary in the fuel temperature because of thermal lags.

Moderator Temperature Coefficient

An experiment (H-10) was conducted in order to determine the temperature coefficient of the moder-

ator. During this experiment the fuel temperature was held constant and the speed of the blowers for cooling the sodium was increased to change the temperature of the moderator coolant. Since this was done very slowly, the moderator did cool down, in contrast to the earlier experiment (H-7) in which the sodium temperature was changed so rapidly that the moderator temperature was unable to follow the sodium temperature. The earlier experiment gave information as to the temperature coefficient of the sodium alone, whereas experiment H-7 gave the combined effect of sodium and moderator changes. The reactivity was indicated by the position to which the regulating rod was adjusted by the flux servo.

The changes in the sodium and the moderator temperatures slightly increased the heat loss of the fuel, and the power had to be increased slightly to keep the fuel mean temperature constant. In fact, in the middle of the run the reactor mean temperature was lower than at the beginning, but before the final reading was taken, the reactor mean temperature was brought back to its original value. Table 6.2 gives the pertinent data. The sodium inlet temperature was taken from a recording of the temperature of the reflector coolant inlet 4 in. from the bottom of the reactor and the sodium outlet temperature was taken from a recording of the temperature of the reflector coolant outlet 3 in. from the top of the reactor. The time recorded in column one is the time when a reading was taken. The change of the blower speed preceded this time by a few minutes to allow the temperature equilibrium to be established. As an indication of the establishment of the equilibrium, use was made of the leveling off of the trace on the sodium temperature differential recorder.

As can be seen from the table, the decrease of the average sodium temperature from 1273 to 1246°F corresponds to a withdrawal of the regulating rod from the 8-in. position to the 8.9-in. position. At the lower temperature the reactor was less reactive and showed that the temperature coefficient was positive. The magnitude of this temperature coefficient was small, $(0.9 \text{ in.}/27^\circ\text{F}) \times 3.33 \times 10^{-4} (\Delta k/k)/\text{in.} = +1.1 \times 10^{-5} (\Delta k/k)^\circ\text{F}$. This coefficient is, however, the sum of the sodium temperature coefficient and the moderator temperature coefficient. Since the sodium temperature coefficient was -5.9×10^{-5} , the moderator temperature coefficient must be $+6.9 \times 10^{-5} (\Delta k/k)^\circ\text{F}$. This value is, of course, subject to all the inherent

TABLE 6.2. MODERATOR TEMPERATURE COEFFICIENT DATA

Time	Fuel Mean Temperature (°F)	Fuel Temperature Gradient (°F)	Blower Speed (rpm)		Sodium Temperature (°F)			Regulating Rod Position (in.)	Nuclear Power (Mw)
			No. 1	No. 2	Inlet	Outlet	Average		
1735	1313	206	960	1050	1265	1282	1273	8.0	1.98
1745	1314	206	1160	1050	1255	1280	1267	8.0	1.98
1752	1313	203	1170	1260	1248	1278	1263	7.6	1.98
1802	1308	200	1340	1250	1238	1272	1255	6.6	1.98
1809			Increased servo demand signal so as to withdraw rod						
1812	1311	204	1480	1240	1230	1268	1249	8.4	2.12
1825	1313	205	1470	1480	1225	1268	1246	8.9	2.12

errors of the measurement of the sodium temperature coefficient, as well as the additional errors in the temperatures recorded for this particular experiment.

MEASUREMENT OF THE XENON POISONING

At 1825 on November 10 a 25-hr run at a power of 2.12 Mw was started for the purpose of measuring the amount of xenon built up in the fuel (Exp. H-11). As discussed in Appendix P, the reactor should have been poisoned by about $2 \times 10^{-3} \Delta k/k$ after 25 hr, if it is assumed that no xenon escaped from the molten fuel. Not only did the 25-hr run demonstrate that very little of the fission-product gas

remained in the fuel but, also, that the reactor possessed phenomenal stability. Except for a minute withdrawal of the regulating rod to compensate for a barely detectable drop in the mean reactor temperature, all readings on both reactor and process instrumentation held constant within experimental error for the 25 hr. It was assumed that the rod withdrawal was due to xenon buildup in the fuel. However, it could have been due to any of a number of minor perturbations, and therefore the experiment demonstrated an absolute upper limit on the xenon poisoning.

An abstract of the log book and data sheets during the experiment follows:

November 10, 1954

1825 Run started; reactor power, 2.12 Mw; rod position, 9.00 in.; reactor mean temperature, 1311°F

November 11, 1954

0635 Reactor mean temperature had decreased to 1309°F; rod withdrawn to 9.05 in.
 0750 Reactor mean temperature up to 1310°F; rod withdrawn to 9.15 in.
 1020 Reactor mean temperature 1310.5°F; rod withdrawn to 9.25 in.
 1120 Reactor mean temperature 1311°F
 1435 Reactor mean temperature down to 1310°F; rod withdrawn to 9.30 in.
 1559 Reactor mean temperature up to 1311°F
 1932 Reactor mean temperature up to 1312°F; rod still at 9.30 in.; end of run

It is to be noted that the temperature recorded was actually one degree higher at the end of the experiment than at the start; this indicates that the withdrawal of the regulating rod by 0.3 in. may, indeed, have been too much. The withdrawal was unquestionably an upper limit on the compensation needed for xenon poisoning and corresponded to a $\Delta k/k$ of 1×10^{-4} . This was $\frac{1}{20}$ or 5% of the value to be expected if the xenon had not left the fuel (see Appendix P). Removal of the xenon probably occurred by means of the swirling action of the fuel as it went through the pump. As mentioned previously, fission-product gases that probably came from a leak in the gas fittings were detected in the pits early in the experiment.

At the conclusion of Exp. H-11 at 1935, the reactor was operated at various power levels for 2 hr in an experiment (Exp. H-12) for determining the effect of the sodium flow rate on the extracted power. At 2237 the reactor was set at 200 kw (one-tenth full power) and held there by the flux servo for 10 hr (Exp. H-13). If any appreciable amount of xenon had been built up in the fuel from decay of iodine formed during Exp. H-11, the poisoning effect should have been observed by a compensating rod withdrawal during this 10-hr period. No appreciable rod withdrawal was observed, and therefore it was concluded that if there was xenon poisoning from Exp. H-11, it was negligible.

POWER DETERMINATION FROM HEAT EXTRACTION

The most reliable method for determination of actual reactor power was that based on the energy removed from the reactor in the form of heat. The inlet, outlet, and mean temperatures, the temperature difference of the fuel across the reactor, and the temperature difference of the reflector coolant were continually recorded. The rates of flow of both the fuel and the sodium were recorded and could also be determined from the speeds of the pumps. Since the heat capacities of both the fuel and the sodium were known, the power level of the reactor could be determined by the sum of the values obtained from the following relations:

$$P_F = 0.11 q_F \Delta T_F$$

$$P_{Na} = 0.0343 q_{Na} \Delta T_{Na}$$

where

P_F = power from fuel heat extraction (Mw),

P_{Na} = power from sodium heat extraction (Mw),

q = volume flow rate (gpm),

ΔT = temperature gradient across reactor of the fuel or the sodium ($^{\circ}$ F).

Since both the fuel and the sodium were cooled by helium passing across a liquid-to-helium heat exchanger and the helium was cooled by passing it over a helium-to-water heat exchanger, the reactor power could also be determined from the water flow and temperature differences across the helium-to-water heat exchangers. Since the fuel-to-helium and sodium-to-helium heat exchangers are close to their respective helium-to-water heat exchangers, little heat was lost by the helium and therefore practically all of the heat removed from the fuel and sodium was transferred to the water. The heat balance thus obtained was known as the secondary heat balance, while that obtained directly from the fuel and sodium systems was known as the primary heat balance.

Initial comparisons of the primary and secondary heat balances revealed discrepancies of the order of 50%. Subsequent investigation revealed that the temperature drops of the primary heat balance were in error. The temperatures were obtained from a few thermocouples located on fuel and sodium lines within the reactor thermal shield that read considerably lower than several thermocouples located external to the thermal shield on the fuel and sodium lines to and from the reactor. This anomaly is discussed further in Appendix K. All reactor inlet and exit temperatures were subsequently based on the external thermocouple readings.

A detailed analysis of the extracted power was made (App. L) for the 25-hr xenon experiment primarily because of the certainty that equilibrium conditions had been established; also, this high-power run at more than 2 Mw contributed almost two-thirds of the megawatt-hours logged during the entire reactor operation. For this run the primary heat balance showed an extracted power of 2.12 Mw, and the secondary heat balance gave an extracted power of 2.28 Mw. The difference between the two determinations was 7%. Furthermore, for this run about 75% of the power was removed by the fuel, about 24% by the sodium, and about 1% by the rod cooling system.

Heat balances and, hence, power determinations were made for a number of other experiments during the high-power operation; these are tabulated in Appendix L. One such heat balance that was of particular interest was obtained during the maxi-

mum power run (Exp. H-14). For this run the mean temperature was raised to 1340°F (to avoid a low-temperature reverse), and the fuel and sodium system blower speeds were increased to their respective maximums. At equilibrium the power levels indicated by the primary and secondary heat balances were 2.45 and 2.53 Mw, respectively. The line temperatures throughout the fuel and sodium systems during this experiment are shown in Figs. 6.5 and 6.6, respectively. The temperatures indicated along the lines are the actual thermocouple readings of each point at equilibrium. It may be noted that the outlet fuel line temperature averaged about 1580°F. The temperature measured at the reactor was considerably lower, as shown in Fig. 6.7, which shows a portion of the instrument panel during this experiment.

REACTOR KINETICS

A distinctive control characteristic of any circulating-fuel reactor is that the reactor power is determined solely by that part of the system which is external to the reactor, i.e., the heat extraction equipment. In the power regime, control rods do not appreciably influence the steady-state power production, but the power extracted from the reactor does influence the reactivity of the reactor and hence renders the reactor controllable.

In order that such a system be acceptable as a power reactor, it is requisite that the reactor have a negative temperature coefficient of reactivity. One of the most gratifying results of the ARE operation was the successful demonstration of its large negative temperature coefficient. This temperature coefficient made it possible for the reactor to maintain a balance between the power extracted from the circulating fuel and coolant and the power generated within the reactor. The temperature cycling of the fuel was the mechanism by which equilibrium was maintained.

A thorough understanding of control processes in a circulating-fuel reactor with a negative temperature coefficient is necessary for an appreciation of the kinetic behavior of such a power reactor in the power regime. An important purpose of the ARE was the observation of the kinetic behavior of the reactor under power coupling to its load when perturbations in the reactivity were introduced. Transient conditions could be induced both by control rod motion and by variation of the external power load. Information on the kinetic behavior was obtained from a number of experiments

that were conducted during the period of power operation. These are described in the following sections. Preceding the discussion of these experiments is a detailed qualitative description of the temperature cycling of the circulating fuel which is inherent to all kinetic phenomena.

Reactor Control by Temperature Coefficient

The control of a circulating-fuel reactor with a negative temperature coefficient can best be understood by following the course of a "slug" of fuel as it traverses the ARE system. For a description of the course of a slug, it is assumed that at time zero the system is in equilibrium, with isothermal temperatures throughout; in this condition no power is being extracted. At time t the fuel system helium blower is turned on. It is also assumed that at this time the slug of fuel under observation is just entering the heat exchanger. In passing through the heat exchanger the slug is cooled by the helium blowing through the heat exchanger. About 20 sec later the cooled slug enters the reactor and is registered as a decrease on the inlet temperature indicator. Because it is cooler than the fuel it is displacing, its density is greater and therefore the number of uranium atoms per unit volume is greater. This results in a greater fission rate and, hence, a greater reactivity which, in turn, increases the power generated. The temperature of the slug rises as it passes through the reactor because of increased power generation. The rise in temperature of the slug results in its expansion and decrease in reactivity. This, in turn, lowers the rate of power generation. Eight seconds after the slug enters the reactor it passes out into the outlet line and is registered as an increase in temperature on the outlet fuel temperature indicator. In 47 sec from the start of its journey it is back at the heat exchanger to be cooled again.

The masses of fuel behind the initial slug follow the same pattern so that, since the fuel is a continuous medium, the power generated in the reactor³ will rise until the increased reactivity due to the incoming fuel and decreased reactivity due to the outgoing fuel attain a balance. At this point equilibrium is reached between power extracted by the helium and the power generated in

³With a power reactor it is appropriate to speak of two types of power: the nuclear power, i.e., the total power generated within the reactor; and the extracted or useful power, i.e., the power removed from the fuel and coolant by cooling.

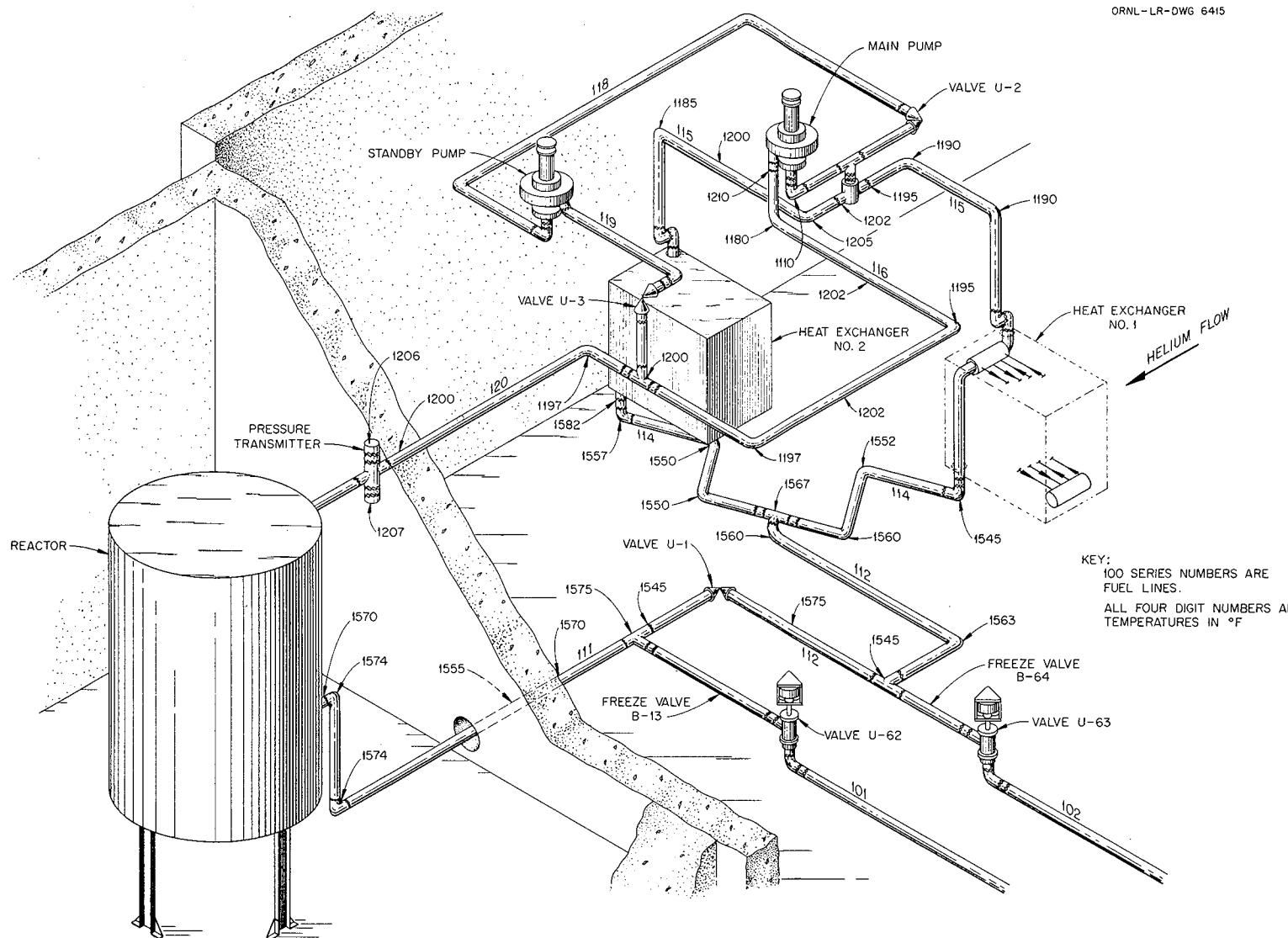


Fig. 6.5. Fuel System Temperatures During Maximum Power Run. Experiment H-14.

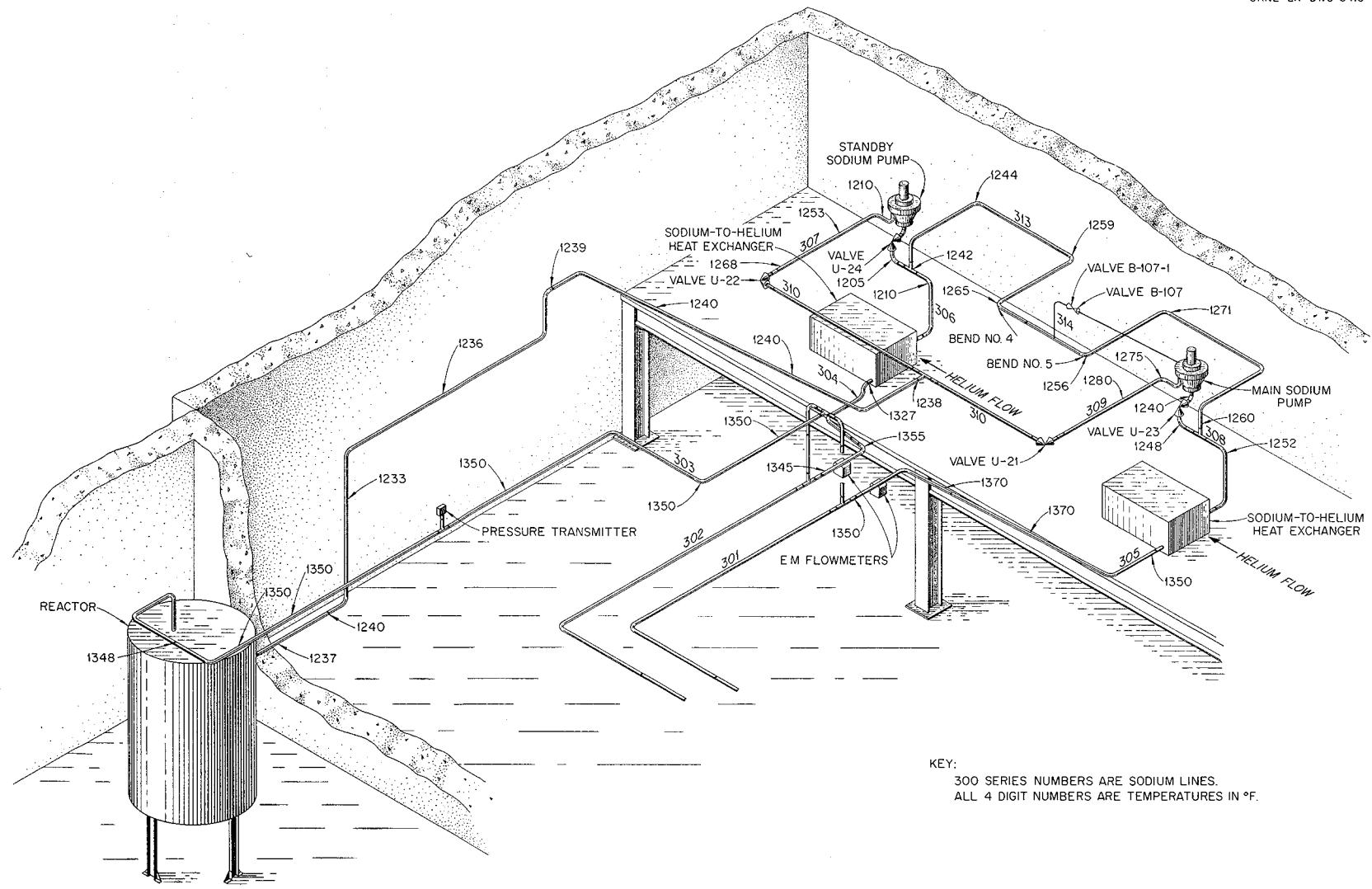


Fig. 6.6. Sodium System Temperatures During Maximum Power Run. Experiment H-14.

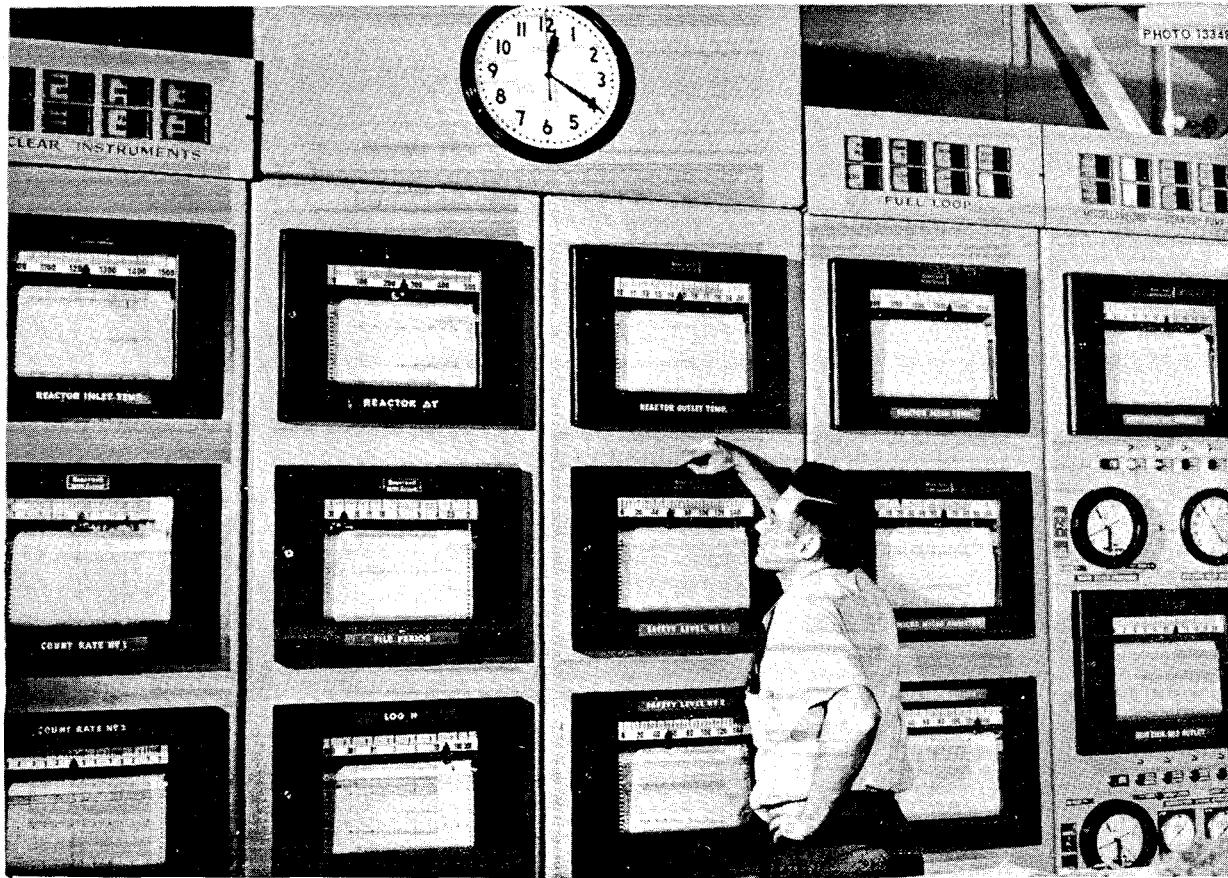


Fig. 6.7. Portion of Instrument Panel During Maximum Power Run. Experiment H-14.

the reactor. The reactor power can thus be varied at will merely by changing the rate of cooling, that is, the demand for power. This type of reactor is said to be a slave to the demand.

The nuclear power is proportional to the neutron flux for any given critical concentration. The neutron flux is conventionally measured by a neutron detector, such as a Log *N* chamber system, which consists essentially of a neutron detector coupled to an electronic system which has a logarithmic-type of output signal. This signal is proportional to the neutron flux (and, hence, the power) level, and is indicated and recorded on a logarithmic scale.

The extracted power, on the other hand, is proportional to the product of either the fuel flow and the temperature difference between the inlet and outlet sides of the heat exchanger (or reactor) or the secondary (or tertiary) coolant flow and its temperature difference. In the ARE the fuel was cooled by helium flowing across it in the fuel-to-

helium heat exchangers. The heat picked up by the helium was then removed by water in a helium-to-water heat exchanger. It was possible to measure the extracted power in both the fuel loop and the water loop, as explained in a preceding section.

When no power is being extracted from a power reactor, the nuclear power is determined by the control rod and shim rod settings, and the reactor is controlled by some type of servo mechanism which keeps the power at some desired level. When the reactor is taken off the servo and allowed to respond to the demand of the cooling produced in the heat exchanger, it will seek a power level determined by the rate of heat removal. Once an equilibrium between nuclear and extracted power has been established, changing the shim rod or regulating rod settings merely changes the nuclear power level but does not alter the amount of power being extracted. This change in nuclear power results in a raising or lowering of the reactor mean temperature, and, once the temperature change has

been effected and equilibrium re-established, the nuclear power and the extracted power will again be equal.⁴

The control of the ARE by extracted power demand is illustrated in Fig. 6.8, which shows the tracings made by several of the control room instrument recorders during power operation between 1258 and 1329 on November 10, 1954. The reactor behavior is demonstrated by reading the tracings right to left, proceeding as follows: At 1258 the reactor was in an equilibrium condition at about a 50-kw power level. At 1259 the fuel system helium blower was turned on and its speed was increased to 500 rpm. The reactor power, as noted on the Log N chart, rose on a 10-sec period to slightly over 1 Mw, "overshot" its mark, fluctuated somewhat in the manner of a damped oscillator, and, finally, some 4 min later, came to an equilibrium power of around 900 kw. Soon,⁵ but not immediately, after the blower was turned on, the reactor fuel inlet temperature began to drop and the fuel outlet temperature began to rise, while the reactor mean temperature began to drop slightly. Each of these temperatures showed the oscillatory phenomenon noted with the Log N recorder. The reason for the drop in the mean temperature was that both the decrease and rate of decrease of the inlet temperature were greater than the corresponding increase and rate of increase of the outlet temperature. The inlet temperature dropped from 1335 to 1256°F⁶ at a rate of 1.54°F/sec and the outlet temperature rose from 1405 to 1475°F at a rate of 1.36°F/sec; as a result the mean temperature fell from 1370 to 1365°F at a rate of about 0.1°F/sec. The fact that the mean temperature dropped (and this was a characteristic phenomenon noted throughout the power operation) rather than remaining constant can be explained, at least in part, by the distortion of the flux patterns within the reactor. The highest fluxes were toward the inlet fuel passages, and the lowest fluxes were toward the outlet fuel passages (cf., App. O).

At 1310 the blower speed was increased from 500

⁴On several occasions the nuclear power, as indicated on the Log N recorder, rose temporarily above 2.5 Mw, but the extracted power, limited by the system capacity for removing heat, never exceeded 2.5 Mw.

⁵Errors in marking the charts could conceivably account for as much as 1/2 min of the time differences noted. This phenomenon of time lag is discussed later in this section.

⁶The temperature readings given here and elsewhere in this section have been corrected by the method given in Appendix K.

to 1000 rpm, and the power rose from 1 to 1.8 Mw on a period of 7.5 sec, with corresponding changes of the inlet, outlet, and mean temperatures. Although the power increase in this case was comparable to the first power increase, the rates of rise of both the power and temperatures were much less, being on the order of one-half as much for the temperatures.

The effect of withdrawing the regulating rod 3 in. is demonstrated with the next rise at 1312 in Fig. 6.8. Up to this time the trace of the regulating rod position was constant, since it was not on servo. With the withdrawal of the rod the rise of the nuclear power was immediate. After some delay, all of the temperatures showed a rise. Interestingly enough, the outlet temperature rose 16°F, the mean 12°F, and the inlet 9°F. This pattern, with the outlet temperature showing the greatest change, was characteristic of the temperature changes incurred by shim rod and regulating rod movement during power operation. After the rod movement the temperatures leveled out at the higher values, but the nuclear power level slowly drifted back to the equilibrium position.

At 1321 the blower was shut off and the charts show the result of the shift toward isothermal (no power) conditions. Two minutes later, when the nuclear power had decreased to about 600 kw, the blower was again started and its speed was increased to 1500 rpm. The nuclear power level rose initially to 2.6 Mw, and it again went through an oscillatory cycle before settling down to 2.2 Mw. The corresponding temperature oscillations were again noted. These oscillations were of sufficient strength to determine an oscillation period of about 2.25 min. An interesting observation at this point was that the time lag of temperature response for a higher initial power (600 kw compared with 50 kw) was only about one-half the lag during the first rise to power at 1259. This phenomenon had been noted previously in connection with the various temperature coefficient experiments (cf., App. O).

Table 6.3 shows the data obtained from the nuclear and process instruments during the typical operation period shown in Fig. 6.8.

Startup on Demand for Power (Exp. H-6)

To illustrate how completely the reactor was a slave to the load, an experiment was performed in which the reactor was brought to subcritical and then taken to critical on temperature coefficient (i.e., by the power demand and without use of

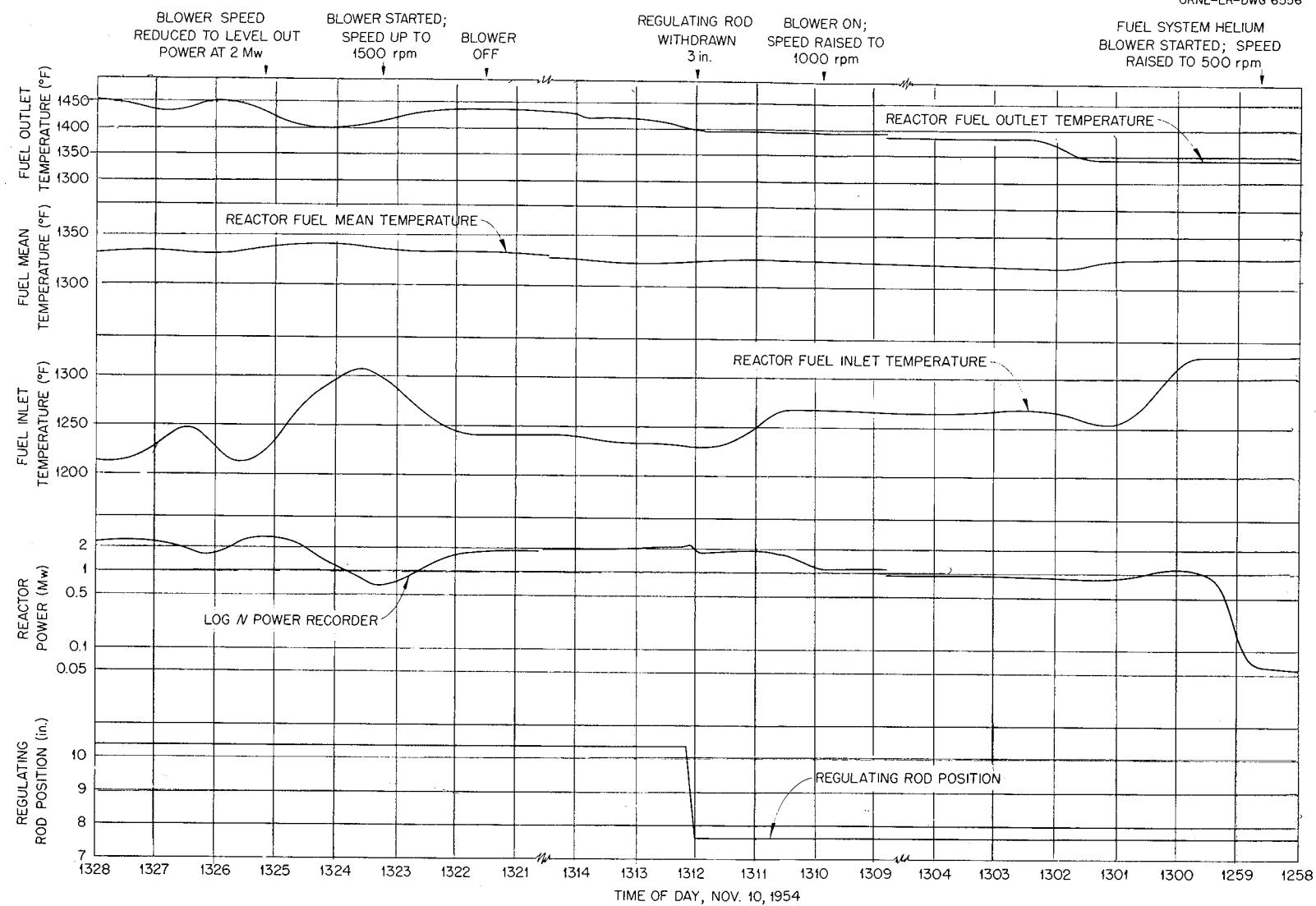


Fig. 6.8. Typical Reactor Behavior During Power Operation.

**TABLE 6.3. NUCLEAR AND PROCESS DATA OBTAINED DURING
A TYPICAL OPERATION PERIOD (NOV. 10)**

Type of Measurement	Type of Data Obtained*	Operation Performed				
		Fuel System Blower Speed Increasing	Fuel System Blower Speed Increasing	Regulating Rod Withdrawn	Fuel System Blower Speed Decreasing	Fuel System Blower Speed Increasing
Time		1300	1310	1312	1321	1323
Log N power	P_1 , Mw	0.0566	0.99	1.58	1.56	0.57
	P_2 , Mw	1.07	1.70	1.94	0.57	2.17
	δP , Mw	1.013	0.71	0.36	0.99	1.60
	δt , sec	28	41	9	60	81
	$\delta P/\delta t$, Mw/sec	0.0363	0.0173	0.04	0.016	0.198
	T_r , sec	10	75	33	63	54
Fuel outlet temperature	$T_{o,1}$, °F	1405	1485	1527	1546	1491
	$T_{o,2}$, °F	1474	1527	1543	1491	1566
	δT_o , °F	69	42	16	-55	75
	δt , sec	45	56	24	75	58
	$\delta T_o/\delta t$, °F/sec	1.54	0.75	0.67	-0.73	1.29
Fuel inlet temperature	$T_{i,1}$, °F	1335	1269	1231	1239	1314
	$T_{i,2}$, °F	1256	1227	1240	1314	1208
	δT_i , °F	-79	-42	9	75	-106
	δt , sec	58	53	42	75	88
	$\delta T_i/\delta t$, °F/sec	-1.36	-0.79	0.21	1.00	-1.20
Fuel mean temperature	$T_{m,1}$, °F	1370	1377	1379	1388	1402
	$T_{m,2}$, °F	1365	1377	1391	1402	1387
	δT_m , °F	-5	0	12	14	-15
	δt , sec	52		33	75	73
	$\delta T_m/\delta t$, °F/sec	-0.096	0	0.36	0.19	-0.20
Reactor fuel ΔT	ΔT_1 , °F	70	216	296	287	177
	ΔT_2 , °F	218	300	303	177	358
	$\delta(\Delta T)$, °F	148	84	7	-110	181
	δt , sec	52	54.5	33	75	73
	$\delta(\Delta T)/\delta t$, °F/sec	2.87	1.54	0.21	-1.47	2.49
Regulating rod movement	d_1 , in.			7.60		
	d_2 , in.			10.37		

TABLE 6.3 (continued)

Type of Measurement	Type of Data Obtained*	Operation Performed				
		Fuel System Blower Speed Increasing	Fuel System Blower Speed Increasing	Regulating Rod Withdrawn	Fuel System Blower Speed Decreasing	Fuel System Blower Speed Increasing
Regulating rod movement	δd_1 , in.			2.77		
	δt , sec			9		
	$\delta d/\Delta t$, in./sec			0.32		
	$\Delta k/k$, %			0.0914		
	$(\Delta k/k)/\delta t$, %/sec			0.011		
Fuel system helium blower speed	s_1 , rpm	0	500		1000	0
	s_o , rpm	500	1000		0	1500
	δs , rpm	500	500		-1000	1500
	δt , sec	14	14		60	42
	$\delta s/\delta t$, rpm/sec	36	36		-17	36

*The following symbols are used:

Quantity	Subscript
P power	1 initial condition
t time	2 final condition
T period	o outlet condition
T temperature	i inlet condition
d position	m mean
k multiplication factor	
s speed	
δ change in quantity	
Δ difference between two quantities	

The δt 's are the times required to go from the initial condition to the final condition at the greatest observed rate of change. The temperatures quoted have all been corrected by the method described in Appendix K.

rods). The experiment consisted of two runs. In the first run the reactor was taken directly from 100 kw to slightly over 2 Mw. In the second run the reactor was taken to power from a subcritical condition.

The progress of these experiments, as recorded by the thermocouple recorders on the inlet and outlet sides of the six individual fuel tubes, is shown in Fig. 6.9. Reading from right to left, the reactor was at 200 kw power at 2300 on November 9 at the beginning of the experiment. The fuel system helium blower speed was increased to 1700 rpm slowly, starting at 2307. Ten minutes later the sodium system coolant blowers were turned on. As the power rose to about 2.5 Mw, a temperature difference of some 320°F appeared across the reactor tubes. This is shown in Fig. 6.9 by the parting of the inlet and outlet temperature indications of the reactor fuel tubes. This temperature

difference remained constant until the blower speed was reduced at 2340. At 2345 the inlet and outlet tube temperatures were nearly the same again at 200 kw power. A sharp drop in the tube temperatures at this point corresponded to the insertion of the shim rods.

The sharp increase in the temperature differential across the tubes at 2353 was the result of a steep rise in power when the blower speed was increased from 0 to 1700 rpm. At 0005 on November 10, the regulating rod was first entirely inserted (from 7 in. withdrawn) and then fully withdrawn. This motion was followed by a drop and then a sharp rise in the fuel tube temperatures. This action marked the end of Run 1.

During Run 2 the reactor was brought subcritical by turning off the fuel system helium blower and inserting the regulating rod, starting at 0016. The sodium system helium blowers had been operating

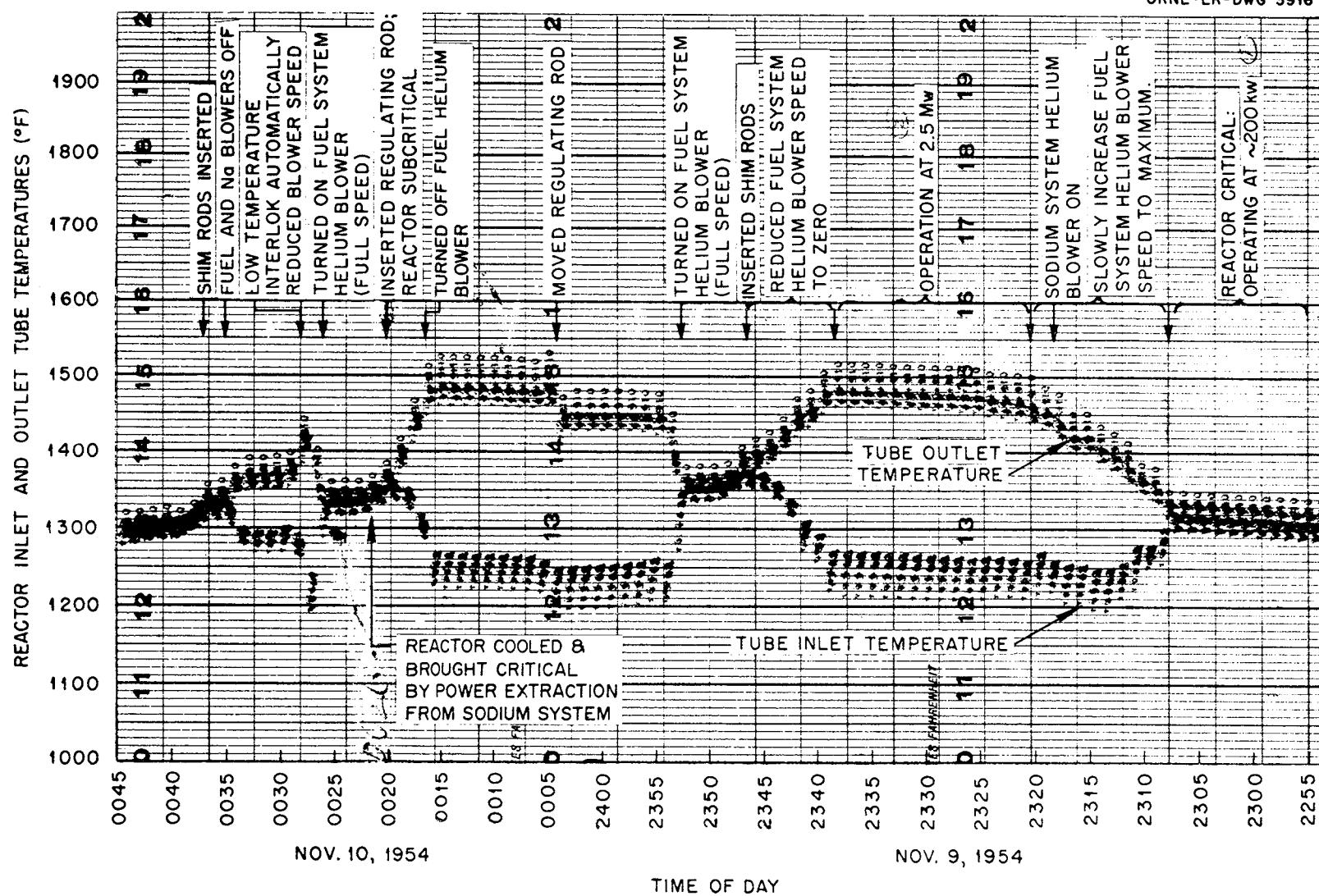


Fig. 6.9. Behavior of Reactor Fuel Tube Inlet and Outlet Temperature During Experiment on Control by Temperature Coefficient.

some of the time during Run 1 to extract power from the sodium. As soon as the reactor became sub-critical the operation of the sodium system blowers, which were then removing about 400 kw of power from the sodium, made the reactor go critical again and stabilize at the 400 kw level within 5 min. It is interesting to note that because the mean sodium temperature was some 65°F lower than the mean fuel temperature, the fuel temperatures dropped 65°F during this time from a mean temperature of 1395 to 1330°F, even though the nuclear power was increasing. At 0026 the fuel system blower was turned on again and the nuclear power temporarily rose to 3 Mw.⁴ Two minutes after the fuel system blower was turned on, the fuel heat exchanger outlet temperature went below 1150°F and the automatic heat-exchanger-temperature interlock reduced the blower speed until the heat exchanger outlet (reactor inlet) temperature had risen above 1150°F. At 0030 the reactor power had leveled out at 1 Mw. It had thus been successfully demonstrated that the power demand would bring the reactor critical; therefore, at 0033, the fuel and sodium system blowers were turned off and the experiment brought to an end.

Effect of One Dollar of Reactivity (Exp. H-8)

One of the objectives of the ARE was the observation of effects of introducing excess Δk into the reactor during high-power operation. The introduction of the excess Δk could be most easily accomplished by movement of the regulating rod, which was worth 0.4% excess k (one dollar of reactivity). One experiment consisted merely of withdrawing the regulating rod from an entirely inserted position, and recording or noting the effects and, then, after equilibrium had been established, inserting the rod to its original position. Since the regulating rod had a travel rate of 0.32 in./sec, reactivity could be introduced at the rate of 0.011% $\Delta k/k \cdot \text{sec}$. Fig. 6.10 shows the history of the experiment.

At 1110 on November 10, with the reactor at an initial power of 2.2 Mw, the regulating rod was withdrawn its full 12 in. of travel. The reactor went on an observed 42-sec period⁷ until the nuclear power was 3.9 Mw 35-sec later. The re-

actor fuel temperatures rose an average of 45°F in 49 sec. Once the rod withdrawal had been completed, the fuel inlet and outlet temperatures leveled off at new values. The extracted power rose a few per cent when the rod was withdrawn, mainly because, with the higher fuel mean temperature, the rate of cooling and, hence, the rate of heat removal in the heat exchanger was greater. Since the extracted power rose only slightly during this time, the nuclear power slowly drifted downward from its peak of 3.9 Mw to 2.9 Mw, as can be seen in Fig. 6.10. Note that the mean temperature continued its upward trend. Three minutes later the rod was completely inserted. The nuclear power decreased from 2.9 to 1.4 Mw on a 47-sec⁷ period and then slowly drifted back to 2.2 Mw, the starting power. The fuel temperatures then returned to values slightly higher than their original values. A characteristic behavior of the outlet temperature was again noted during this experiment, namely, that movement of a rod affected the outlet temperature most and the inlet temperature the least. Additional data on this experiment are given in Table 6.4.

Again, with this experiment, a time lag was noted; the inlet temperature lagged behind the outlet temperature by about the fuel transit time of 47 sec. A reasonable explanation for this lag is that the time required for the fuel in the reactor at the start of the experiment to affect the inlet line thermocouple is the transit time through the system.

Because of this difference in response of the thermocouples on the inlet and outlet fuel lines when the rod was withdrawn, the temperature differential across the reactor rose from 341°F to a peak value of 395°F in about 1 min and then dropped to a more or less constant value of 355°F, which was 14°F higher than at the start. This means that the extracted power rose slightly, about 8%. Examination of the tracings of the fuel and sodium heat exchanger cooling water recorders for this time indicated that the fuel power extraction went up 6% and the sodium power extraction roughly 2%. The rise in power extraction was due mainly to the higher mean temperatures and thus the higher cooling rates attained. The extracted power rose to about 2.4 Mw at the new equilibrium. The difference (500 kw) between this value and 2.9 Mw, as shown by the Log N recorder, went to heating the reactor. This was evidenced not only by the continuing increase in reactor mean fuel temperature but also by the rising travel in inlet and outlet

⁷This period was measured from the Log N recorder trace. The period recorded on the period meter was partially a time rate of change of period since $\Delta k/k$ was not constant but was increasing during this time. A discussion of this is given in Appendix S.

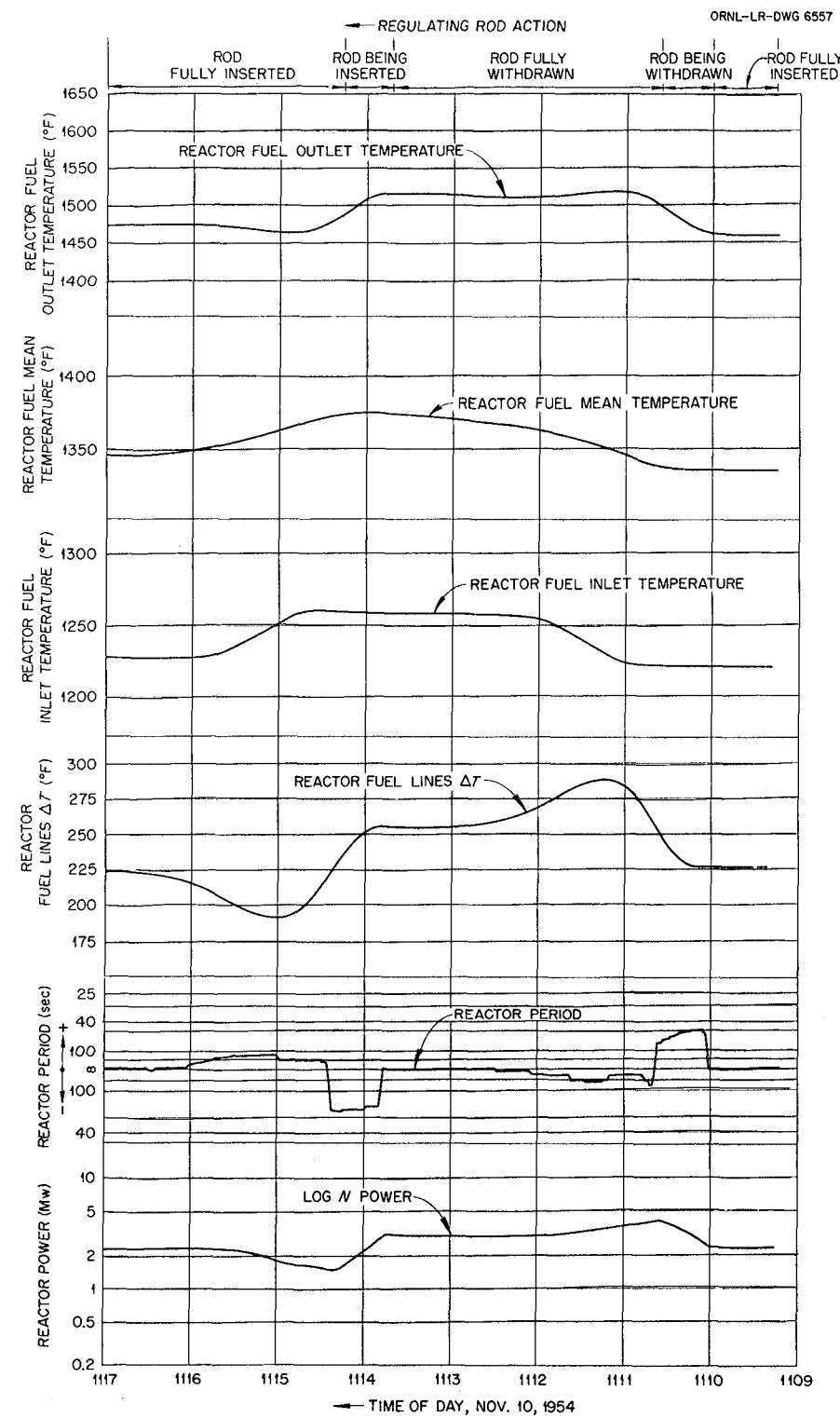


Fig. 6.10. Kinetic Behavior of Reactor Upon Introduction of a Dollar of Reactivity.

TABLE 6.4. NUCLEAR AND PROCESS DATA OBTAINED DURING EXPERIMENT H-8 FOR DETERMINING THE EFFECT OF ONE DOLLAR OF REACTIVITY (NOV. 10)

Type of Measurement	Type of Data Obtained*	Operation Performed	
		Regulating Rod Withdrawn	Regulating Rod Inserted
Time		1110	1114
Log N power	P_1 , Mw	2.34	2.92
	P_2 , Mw	3.94	1.41
	δP , Mw	1.60	1.51
	δt , sec	35	35
	$\delta P/\delta t$, Mw/sec	0.046	0.043
	T , sec	42	47
Fuel outlet temperature	$T_{o,1}$, °F	1573	1620
	$T_{o,2}$, °F	1623	1572
	δT_o , °F	50	-48
	δt , sec	41	41
	$\delta T_o/\delta t$, °F/sec	1.22	-1.17
Fuel inlet temperature	$T_{i,1}$, °F	1217	1258
	$T_{i,2}$, °F	1257	1221
	δT_i , °F	40	-37
	δt , sec	57	56
	$\delta T_i/\delta t$, °F/sec	0.70	-0.66
Fuel mean temperature	$T_{m,1}$, °F	1395	1439
	$T_{m,2}$, °F	1440	1396
	δT_m , °F	45	-43
	δt , sec	49	49
	$\delta T_m/\delta t$, °F/sec	0.92	-0.88
Reactor fuel ΔT	ΔT_1 , °F	356	362
	ΔT_2 , °F	366	351
	$\delta(\Delta T)$, °F	10	-11
	δt , sec	49	49
	$\delta(\Delta T)/\delta t$, °F/sec	0.20	-0.21
Regulating rod movement	d_1 , in.	2.0	14.0
	d_2 , in.	14.0	2.0
	δd , in.	12.0	-12.0

*See footnote to Table 6.3.

TABLE 6.4 (continued)

Type of Measurement	Type of Data Obtained*	Operation Performed	
		Regulating Rod Withdrawn	Regulating Rod Inserted
Regulating rod movement	δ_t , sec	37	37
	$\delta d/\delta t$, in./sec	0.32	-0.32
	$\Delta k/k$, %	0.4	0.4
	$(\Delta k/k)/\delta_t$, %/sec	0.011	-0.11
Fuel system helium blower speed	s_1 , rpm	1750	1750
	s_2 , rpm	1750	1750
	δs , rpm	0	0
	δt , sec	-	-
	$\delta s/\delta t$, rpm/sec	0	0

*See footnote to Table 6.3.

fuel temperatures just before the rod was inserted at 1114.

Power Cycling of Reactor

The last day of operation of the ARE, November 12, was devoted to maximum power runs and to demonstrations of the reactor operation to visitors. The complete history of the reactor operation during that time is shown in Fig. 6.11. Chart A shows the trace of the sodium temperature differential across the reactor and chart B shows the trace of the outlet temperature of the water from the fuel heat exchangers. Clearly seen in chart A are the three maximum power runs at 10:00 AM, 12:30 and 7:45 PM. Both charts show the cycling of the extracted power that the system underwent, but the cycles are especially well defined in chart B, which shows the heat exchanger water temperatures varying from a low of 65°F to a high of 140°F, corresponding to total extracted powers of from around 100 kw to over 2 Mw. In the 12 hr between 8:00 AM and 8:00 PM, 24 complete cycles were recorded. In the afternoon hours between 1:00 and 4:00 PM, when the most visitors were present, the reactor was cycled an average of 3 times per hour. Of interest to the visitors were the tracings of the reactor fuel tube ΔT recorders. The photograph reproduced as Fig. 6.12, which was taken during one of the cycles, shows each of the six fuel tube ΔT recorders simultaneously tracing out the same power cycle pattern. The picture was taken about

12:30 PM during one of the maximum power runs. The recorders show ΔT 's of around 250°F. The actual fuel tube differences at this time were more nearly 355°F.

Additional information on the power cycling may be obtained from Fig. 6.13 which shows the three temperature cycles recorded in the hour between 1:10 and 2:10 PM on the last day. Shown in this figure are traces from the six fuel tube ΔT recorders, a time condensation⁸ of the micromicroammeter recorder (which traced the power), one of the heat exchanger outlet temperature recorders, and the individual fuel tube temperature recorder.

Referring to the micromicroammeter trace and reading from right to left starting at 1317, the events are elaborated for the first cycle. The other two cycles are similar.

At 1317 the fuel system helium blower was turned off, and the reactor power was allowed to decrease from a level of 1.8 Mw. Eight minutes later the power had fallen to about 130 kw, and the blower was turned on to 1700 rpm. The power rose quickly to 2.3 Mw, at which point a low-heat-exchanger-temperature blower reverse occurred; that is, when the helium cooling lowered the heat exchanger outlet fuel temperature to 1150°F (as noted above), a relay was automatically actuated that decreased the helium blower speed until such time as the

⁸This condensation was necessary because the original chart ran at a speed of 80 in./hr, while charts used subsequently ran at a speed of only 4 or 5 in./hr.

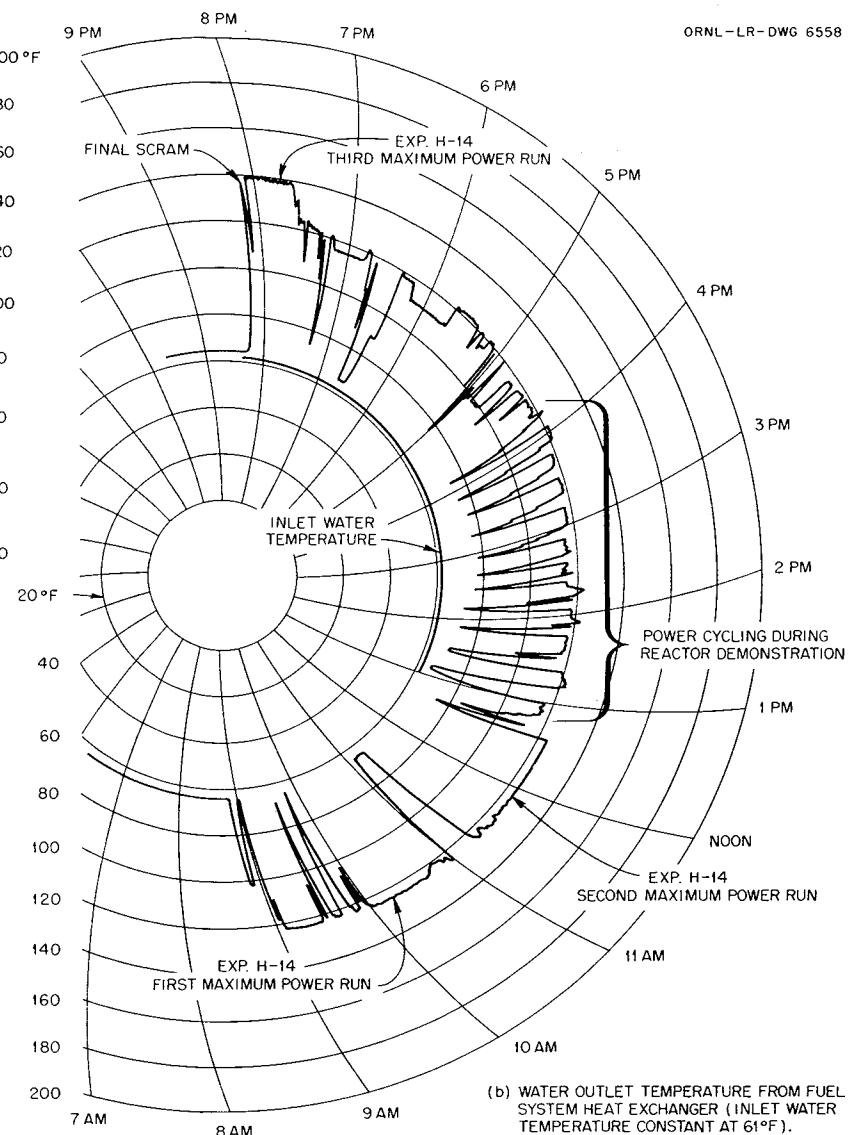
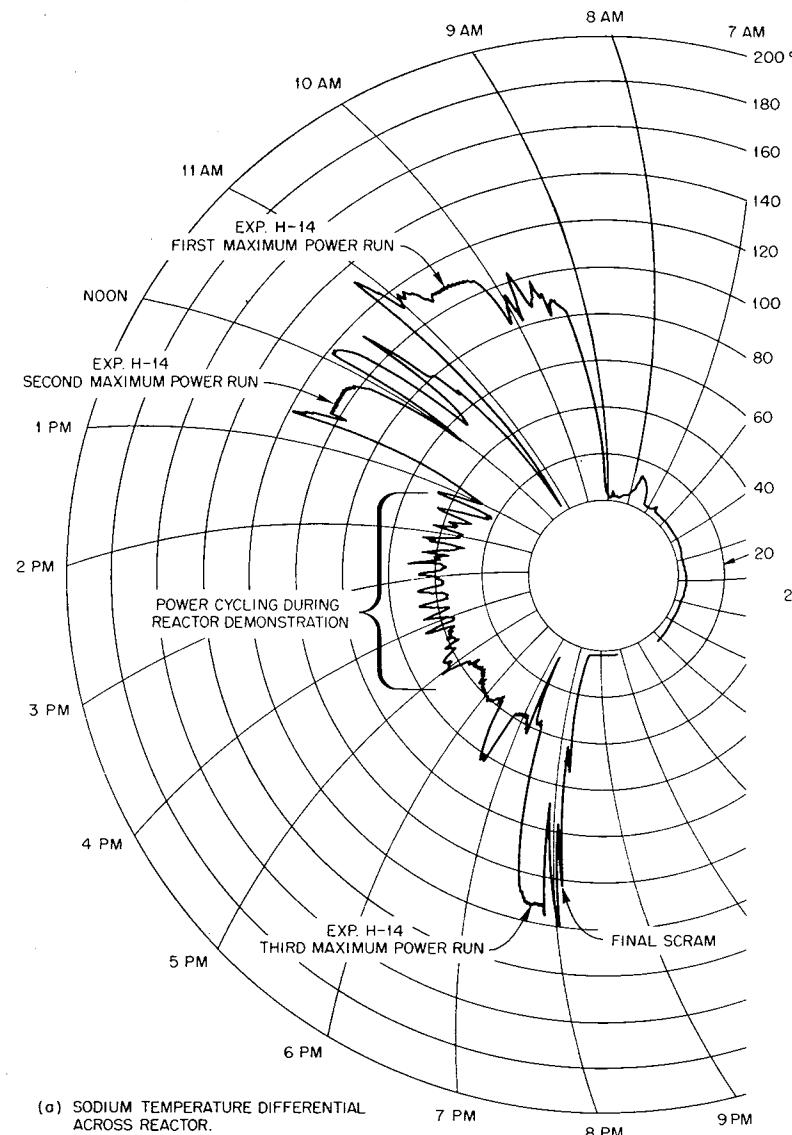


Fig. 6.11. Temperature Cycles in Fuel and Sodium Systems During Last Day of Operation.

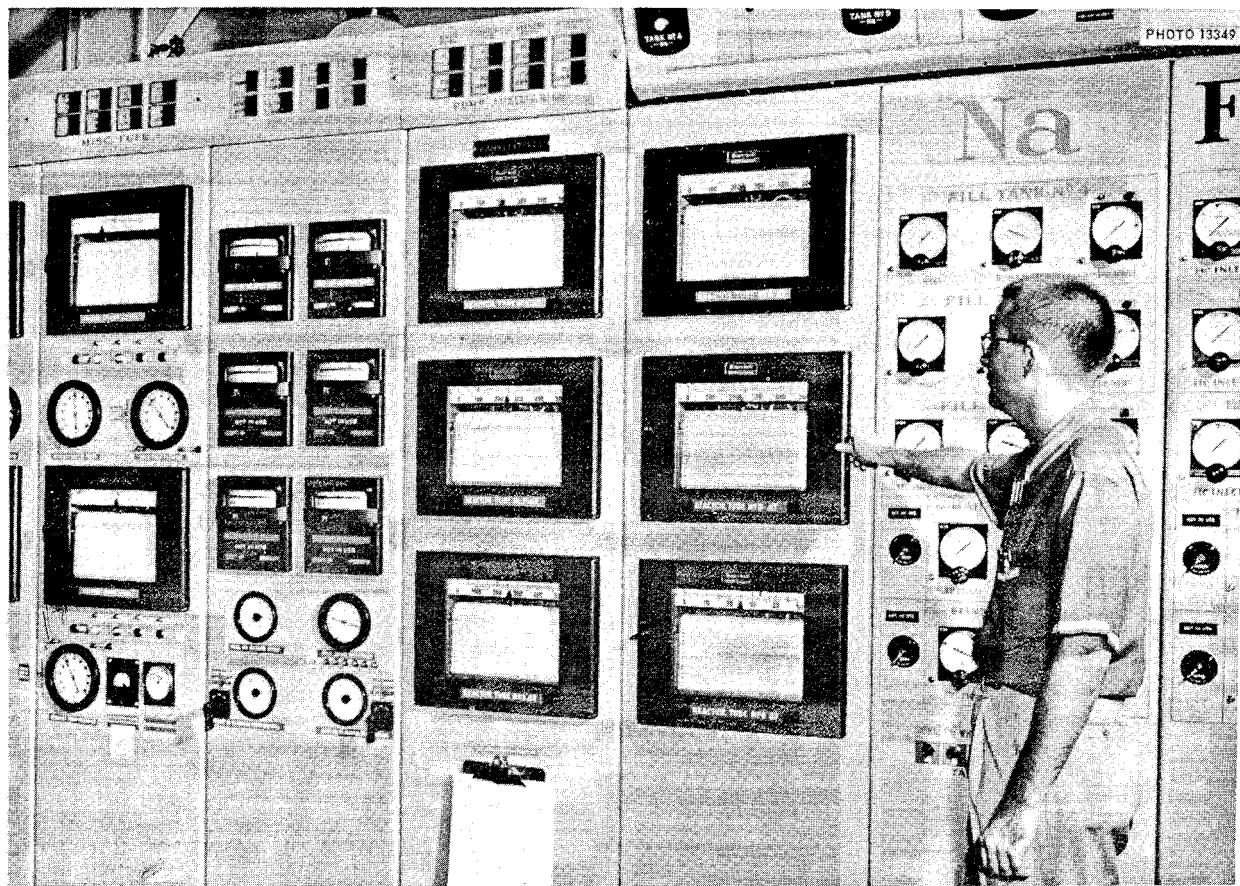


Fig. 6.12. Reactor Fuel Tube ΔT 's During High-Power Operation.

outlet temperature rose to above 1150°F . During this time the power fell to 1.1 Mw. At 1328 a "permit" signal was given and the power was again increased. When 2 Mw was reached the reactor was leveled off on extracted power and for 10 min the effect of regulating rod movement was demonstrated to visitors.

The maximum nuclear power attained during the first cycle was 2.8 Mw^4 at 1340°F . During the third cycle at 1410 a nuclear power of 3.4 Mw was reached.

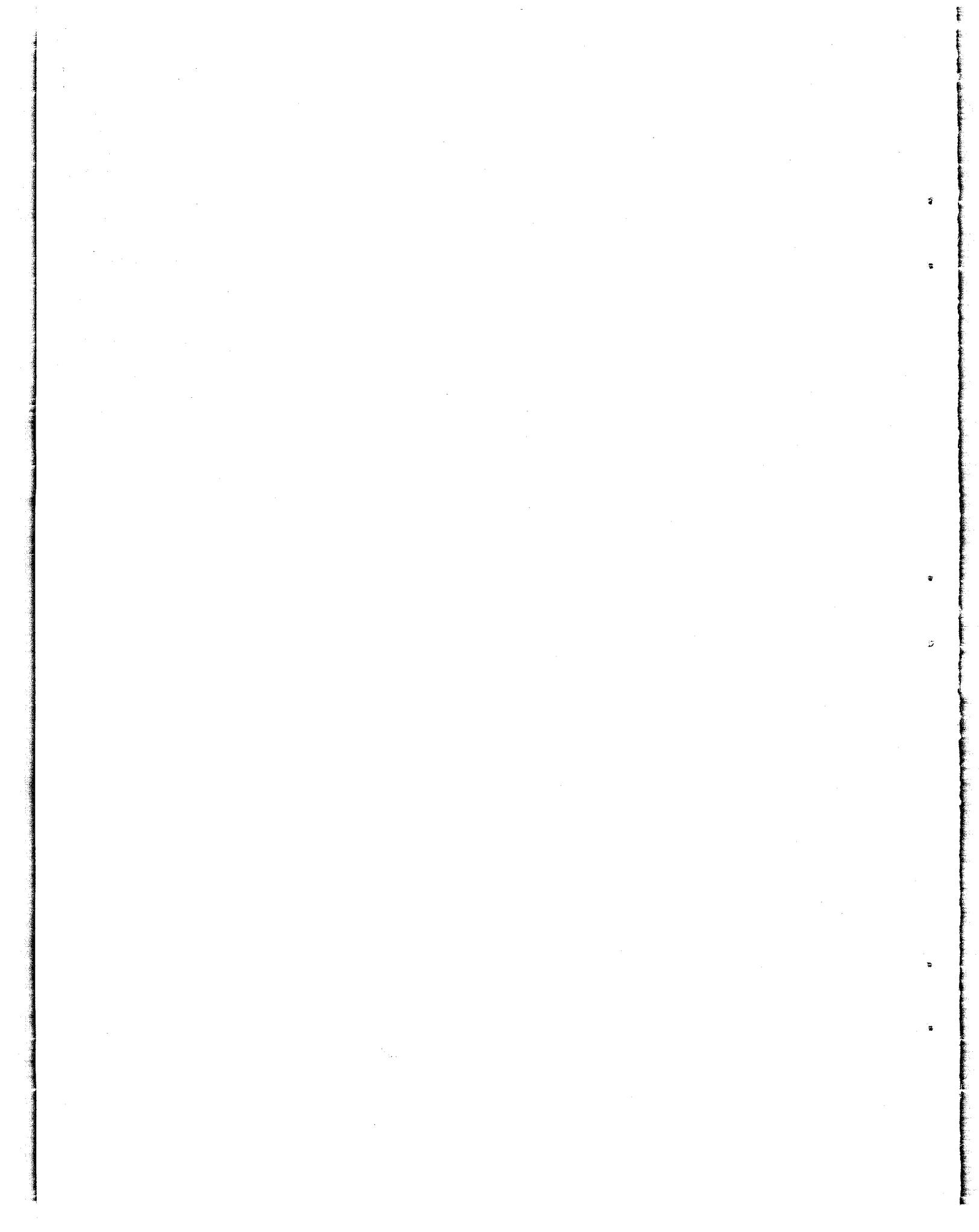
The six fuel tube ΔT recorders (Fig. 6.12) followed exactly the same pattern as the micromicroammeter recorder. It should be noted, however, that the actual ΔT 's were of the order of 100 degrees higher than those shown on the charts. At the high power peaks of the third cycle the fuel outlet line temperatures, as read in the basement, were indicated to be about 1625°F . The inlet temperatures ranged from an actual (vs observed)

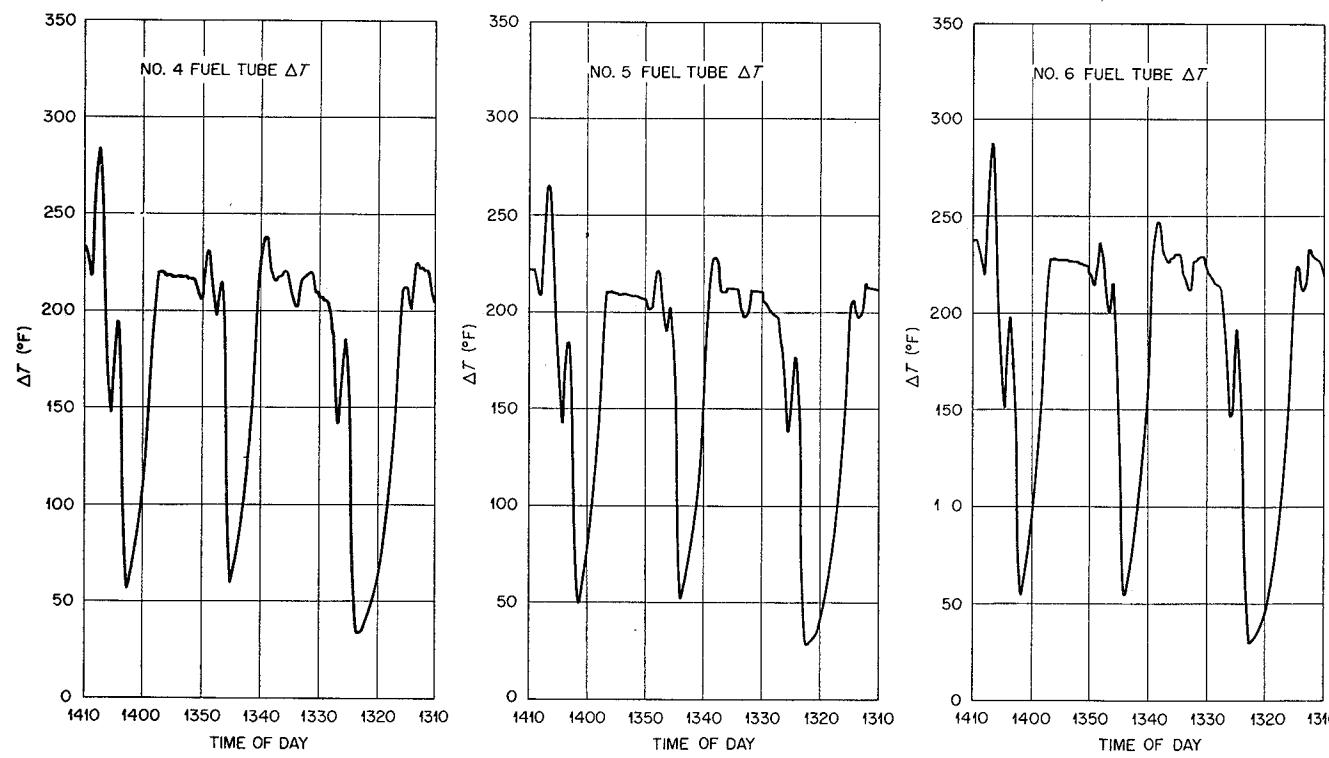
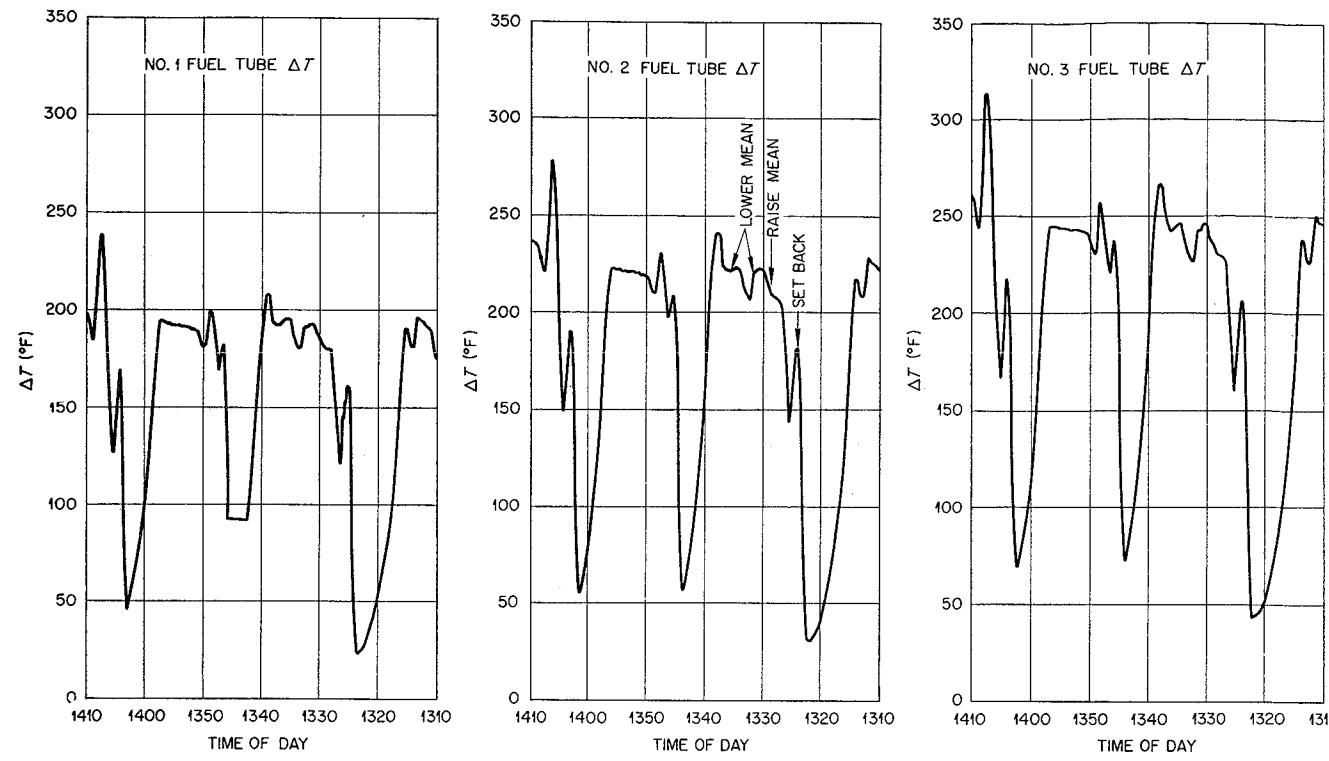
high of 1340°F to a low of 1150°F during the low-heat-exchanger-temperature blower reverse.

The change in tube ΔT 's as a result of rod movement was due partly to the phenomenon of the time lag between the inlet and outlet thermocouples. Had there been no lag the effect of rod motion on these couples would have been small.

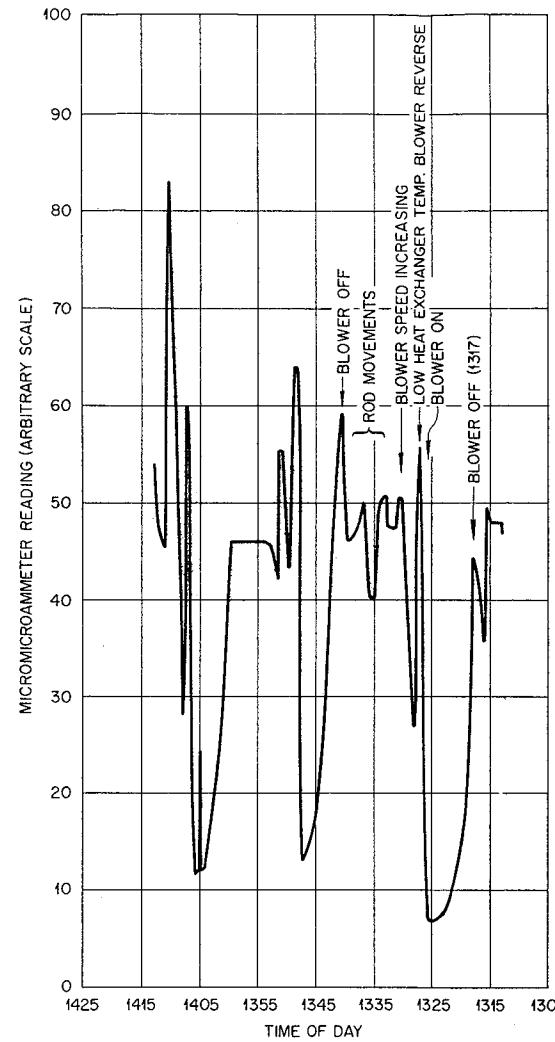
The fuel heat exchanger outlet temperatures showed the temperature cycles in reverse. The first high peak corresponds to the condition at 1300°F with the blower off. As the blower was turned on the temperature decreased to 1150°F , at which point, as noted, the blower reverse occurred with the resultant decrease in blower speed. The heat exchanger outlet temperature then rose to 1250°F before the blower speed was allowed to increase again.

The data from these and other recorder charts during this time, together with calculated rates of change, are given in Table 6.5.

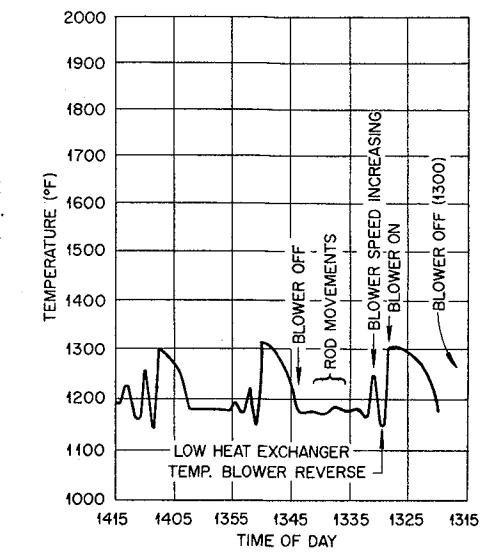




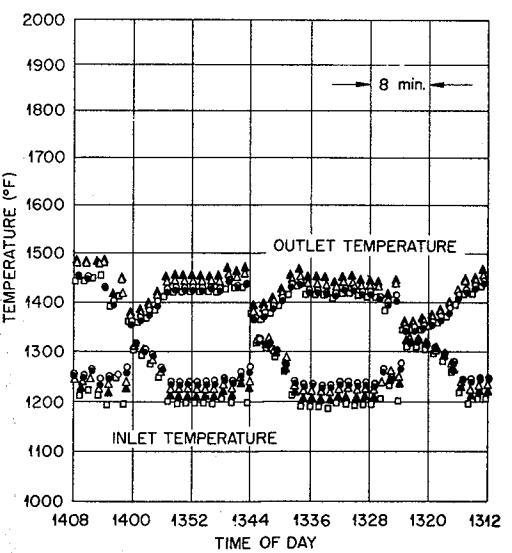
ORNL-LR-DWG 6559



CONDENSATION OF MICROMICROAMMETER
READINGS FROM 80 in./hr TO 4 in./hr



FUEL HEAT EXCHANGER OUTLET TEMPERATURE



INDIVIDUAL FUEL TUBES INLET AND OUTLET TEMPERATURE

Fig. 6.13. Reactor Characteristics During Power Cycling.

TABLE 6.5. CHARACTERISTIC NUCLEAR AND PROCESS DATA DURING POWER CYCLING OF REACTOR (NOV. 12)

Type of Measurement	Type of Data Obtained ^a	Power Cycle No. 1				Power Cycle No. 2				Power Cycle No. 3			
		Blower ^b Speed Increasing	Blower ^c Speed Decreasing	Blower ^b Speed Increasing	Blower ^c Speed Decreasing	Blower ^b Speed Increasing	Blower ^c Speed Decreasing	Blower ^b Speed Increasing	Blower ^c Speed Decreasing	Blower ^b Speed Increasing	Blower ^c Speed Decreasing	Blower ^b Speed Increasing	Rod Withdrawn ^d
Time		1324	1326	1327	1340	1346	1348	1349	1405	1406	1407	1408	
Log N power	P_1 , Mw	0.283	2.26	1.04	2.01	0.462	2.42	1.62	0.387	2.06	0.962	2.01	
	P_2 , Mw	2.26	1.04	2.03	0.48	2.42	1.62	2.09	2.06	0.962	2.01	3.21	
	δP , Mw	1.98	-1.22	0.99	-1.53	1.96	-0.80	0.47	1.67	-1.10	1.05	1.20	
	δt , sec	35	69	37	275	38	37	42	35	70	40	23	
	$\delta P/\delta t$, Mw/sec	0.057	-0.18	0.027	-0.0056	0.052	-0.022	0.011	0.045	-0.016	0.026	0.052	
	τ , sec	18	-89	54		24	59	110	19	60	52	46	
Fuel outlet temperature	$T_{o,1}$, °F	1402	1526	1457	1551	1446	1559	1540	1426	1538	1485	1532	
	$T_{o,2}$, °F	1526	1452	1529	1446	1559	1540	1558	1538	1485	1532	1595	
	δT_o , °F	124	-74	72	-105	113	-19	18	112	-53	47	63	
	δt , sec	48	76	50	321	49	37	46	44	55	41	39	
	$\delta T_o/\delta t$, °F/sec	2.58	-0.97	1.44	-0.33	2.31	-0.51	0.39	2.55	-0.96	1.15	1.62	
Fuel inlet temperature	$T_{i,1}$, °F	1340	1208	1271	1212	1347	1209	1247	1333	1207	1262	1207	
	$T_{i,2}$, °F	1208	1271	1210	1346	1209	1247	1218	1207	1267	1207	1254	
	δT_i , °F	-132	63	-61	134	-138	38	-29	-126	55	-55	47	
	δt , sec	65	56	49	356	53	35	46	49	52	49	62	
	$\delta T_i/\delta t$, °F/sec	-2.03	1.13	-1.24	0.38	-2.60	1.09	-0.63	-2.58	1.06	1.12	0.76	
Fuel mean temperature	$T_{m,1}$, °F	1371	1367	1364	1381	1397	1384	1394	1380	1373	1374	1370	
	$T_{m,2}$, °F	1367	1362	1369	1396	1384	1393	1388	1372	1373	1370	1424	
	δT_m , °F	-4	-5	5	15	-13	9	-6	-8	0	-4	54	
	δt , sec	56	66	50	338	51	36	46	47		45	50	
	$\delta T_m/\delta t$, °F/sec	-0.04	-0.076	0.10	0.04	-0.25	0.25	-0.13	-0.17	0	-0.09	1.08	
Reactor fuel ΔT	ΔT_1 , °F	62	318	186	339	99	350	293	93	331	223	325	
	ΔT_2 , °F	318	181	319	100	350	293	340	331	223	325	341	
	$\delta(\Delta T)$, °F	256	-137	133	-239	251	-57	47	238	-108	102	16	
	δt , sec	57	66	50	338	51	36	46	46.5	54	51	55	
	$\delta(\Delta T)/\delta t$, °F/sec	4.49	-2.08	2.66	-0.71	4.92	-1.58	1.02	5.11	-2.00	2.00	0.29	

^aSee footnote to Table 6.3.^bDuring power cycling no data available on blower speeds.^cLow-heat-exchanger-temperature blower reverse caused blower speed to decrease. No data available on blower speeds.^dNo data recorded on which rod was moved. Estimated $\Delta k/k$ introduced was 0.33%. This would correspond to a group movement of all three shim rods for a 10-sec period.

Reactor Transients

One of the characteristics of the reactor that was most important from the operator's point of view was the behavior under transient conditions, because it is only through transient effects that the operator acquires a "feel" for the way the reactor responds to his control under varying conditions. The various ways in which transients may be introduced into the reactor are the following:

1. operation of fuel system helium blower,
2. operation of sodium system helium blowers,
3. operation of rod cooling system helium blowers,
4. changing the fuel flow rate,
5. changing the sodium flow rate,
6. movement of shim rods,
7. movement of regulating rods.

A discussion of the effects on the ARE of some of these operations is given in succeeding paragraphs. Effects 3 and 5 were very small although observable. Effect 4 was not observed at high power because of the danger of freezing fuel in the pump, although it can be calculated from the inhour curves (Fig. 5.11) and the known rate of change of fuel pump speed. Table 6.6 lists calculated rates of interjection of $\Delta k/k$ into the reactor by the various means listed above.

It has already been pointed out that the ARE reactor and system were very sluggish in responding to demands at high power. Furthermore, it was observed that the response at low power (less than 100 kw) was much different from its response at higher powers (at 1 Mw or greater). One way to examine the behavior of the reactor is to plot sys-

tem characteristics against the initial power, since this represents the behavior from a given initial condition of the reactor.

One of the properties investigated in the above manner was the reactor period. Some of the observed reactor periods are plotted as a function of the initial power in Fig. 6.14. Since the reactor could be put on any period from infinite to a given minimum, the points in Fig. 6.14 are scattered. Most of the longer periods represent periods observed during such times as the initial rise to power, which was approached with caution. As the operators became more familiar with the operation at power, deliberate attempts were made to see how fast a period the reactor would attain due to blower operation or rod movement. As a result, definite lower limits were established beyond which reactor periods could not be induced by the controls available to the operator. The solid line in Fig. 6.14 represents the lower limit for periods during blower operation and the dashed line is that corresponding to shim and regulating rod movement.⁹ The smallest period observed during high-power operation was the 10-sec period represented by the rise in the Log N chamber at 1259, Fig. 6.8. A few smaller periods were observed in the very low-power regime just above critical. The two lines shown in the figure indicate that the lower the power the greater the transient that can

⁹If the reactor had been taken to power with the shim rods inserted to greater depths, smaller periods would have been observed for shim rod motion than are represented by the dashed line, since the reactivity value of the rods would have been greater for those insertions.

TABLE 6.6. CALCULATED RATES OF INCREASE OF $\Delta k/k$ IN ARE FROM VARIOUS OPERATIONS

Operation	Range	$(\% \Delta k/k)/\text{sec}$
Fuel system helium blower speed increase	0 to 1500 rpm	0.0035
	1000 to 1500 rpm	0.0011
Regulating rod movement	Whole rod insertion or withdrawal	0.011
Shim rod movement, single rod	At 4 in. insertion	0.0039
	At 8 in. insertion	0.0067
Shim rod movement, group operation	At 4 in. insertion	0.012
	At 8 in. insertion	0.019
Fuel flow rate	0 to 46 gpm	0.013
Sodium flow rate	0 to 150 gpm	1×10^{-6}

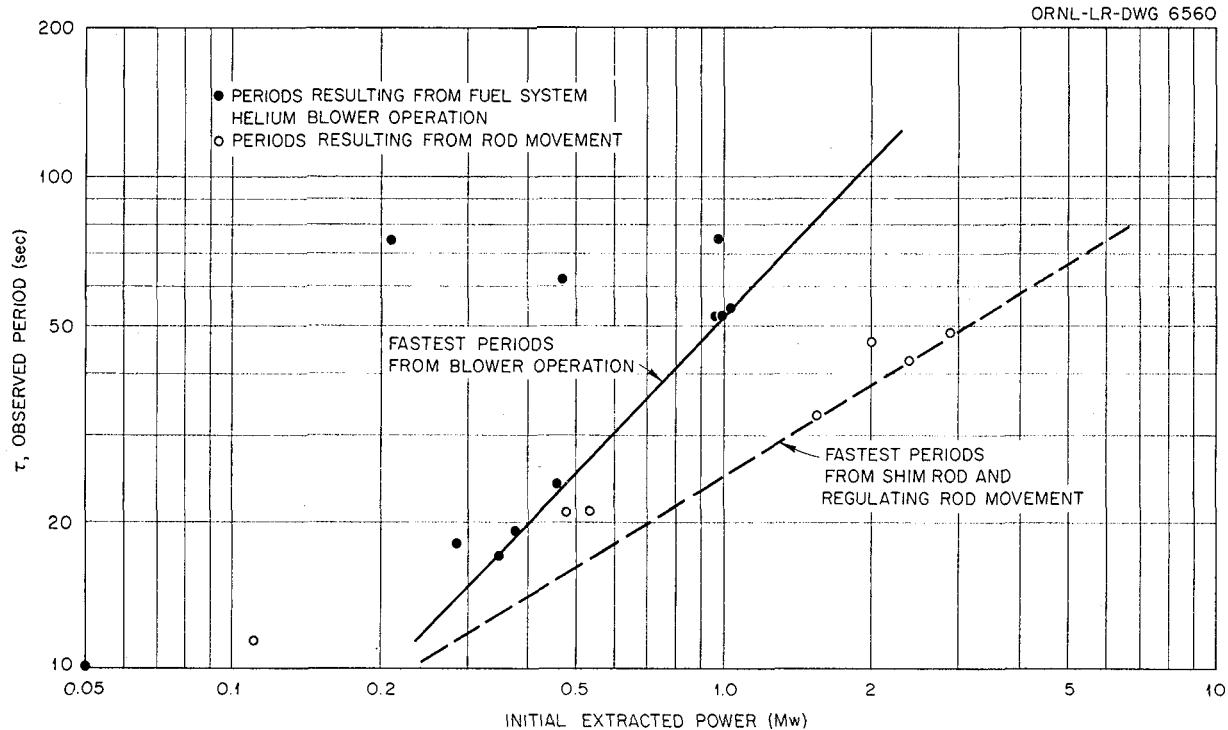


Fig. 6.14. Induced Reactor Periods as a Function of Initial Extracted Power.

be introduced into the reactor, i.e., the higher the power the harder it becomes to introduce a transient condition. Extrapolation of the solid line to a power of 1 kw indicates that at this power reactor periods of 1 sec or less could have been introduced by blower operation.

It should be pointed out that periods could be observed which were not true periods but were a combination of the observed period and its time derivative. Whenever a sudden reactivity change occurred, such as when a rod was moved slightly, the period meter would register a transient peak period that was very small compared with the true period. The beginning peak in the period curves of Fig. 5.4 are of this nature. Whenever a continuing change of $\Delta k/k$ was taking place, the observed period was not a true period but, again, a combination of the true period and its time derivative. In Fig. 6.10 the period meter did not register a constant period when the regulating rod was moved but, rather, a continually changing period. Also, it is to be noted that the Log N power recorder did not register straight slopes during the power changes but, instead, constantly changing

ones, which again indicated that the period was changing (cf., App. S).

The time behavior of the fuel temperatures as a result of blower operation was obtained by plotting inlet and outlet fuel temperature time rates of change against the initial power. These plots are shown in Fig. 6.15. Larger rates of change of fuel temperatures were observed at lower powers, and they corresponded to the smaller periods observed. The greatest rates of change of the fuel temperatures were observed at an initial power of 280 kw, at which time the inlet temperature changed at a rate of $-2.75^{\circ}\text{F/sec}$ and the outlet temperature at a rate of $+2.6^{\circ}\text{F/sec}$. The only reason higher rates of change were not observed at powers lower than this was that in the low-power regime the kinetic behavior was not well known and therefore a conservative approach to transient conditions was used.

The rates of decrease of temperatures when the blower was turned off and the reactor was allowed to come to a lower power are also plotted in Fig. 6.15. The trend of rates of change of the temperatures seems to be reversed.

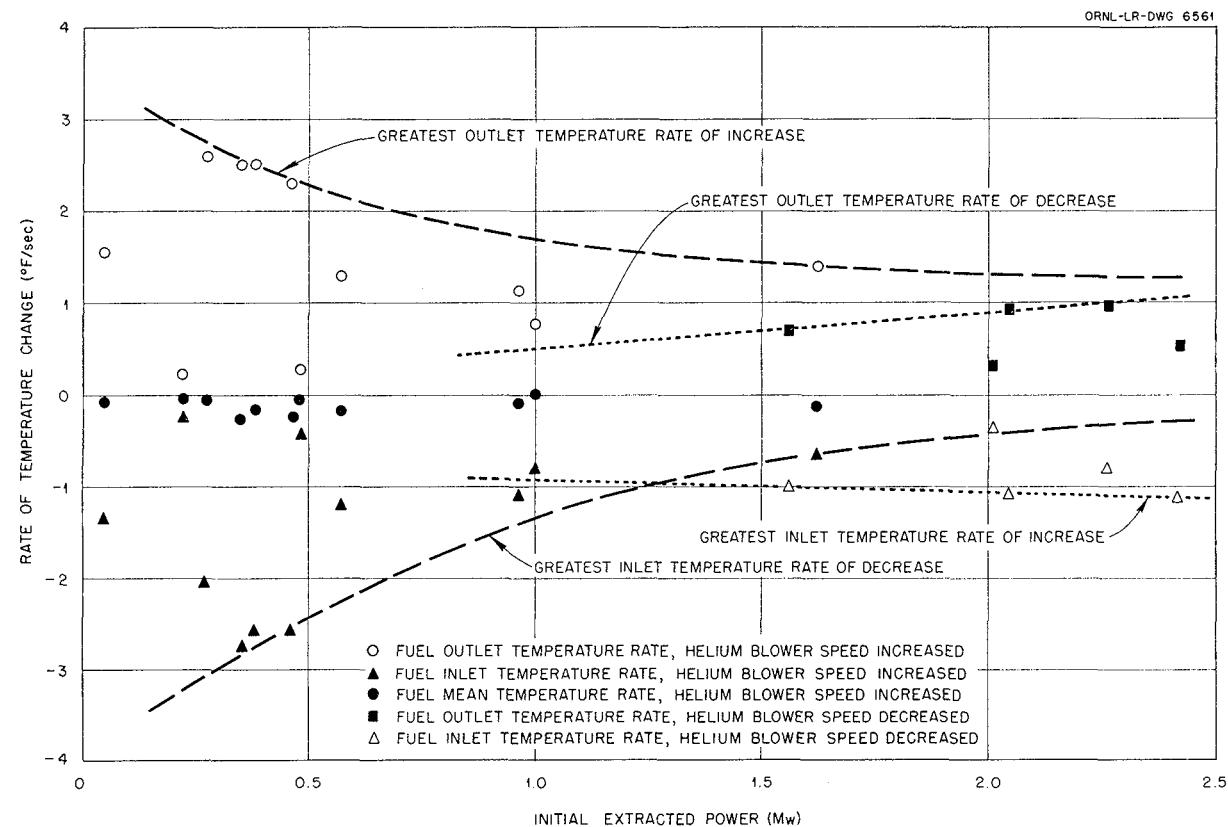


Fig. 6.15. Time Behavior of Reactor Fuel Temperatures as a Function of Initial Extracted Power.

Some very general observations on the transient behavior of the ARE reactor are summarized below.

Reactor Periods. In general, the lower the initial power the faster was the transient introduced by any type of operation that resulted in upsetting the equilibrium between nuclear and extracted power. The smaller periods were associated with lower initial powers.

Oscillation of Reactor Power. The characteristic behavior of the nuclear power during an established transient was to "over-shoot" and then oscillate around a mean value before settling down to that power. The period of the oscillation appeared to be of the order of 2 min and lasted for about 2 cycles.

Movement of Rods. The reactor was always more prompt to respond to rod motion than it was to blower operation. Also the reactor periods observed at a given power were smaller due to rod movement than those due to blower operation.

Nuclear Power. Whenever blower speed was changed the nuclear power rose (with oscillations

as noted above) to a higher power level than the corresponding extracted power demand. When a rod movement occurred, the nuclear power changed considerably, which resulted in higher or lower reactor over-all temperatures, and then leveled out to a new balance with the extracted power at about the original power level.

Extracted Power. Extracted power was essentially a function only of the demand and changed due to a change in operation of one of the various heat exchanger blowers. During rod movement at a given demand power, the extracted power remained essentially constant. The unbalance between extracted and nuclear power resulted in a change of the mean reactor temperature.

Reactor Outlet Fuel Temperature. The outlet fuel temperature always rose and fell in the same direction as the nuclear power level. For blower operation the rise in the outlet temperature was always less than the fall of the inlet temperature. The opposite was true for regulating rod movement.

Reactor Inlet Fuel Temperature. The inlet fuel

temperature rose and fell in the opposite direction to the change in nuclear power during blower operation and in the same direction as the nuclear power during rod movements. The inlet temperature change was greater than the outlet temperature change for blower operation. The opposite was true for shim rod operation.

Reactor Mean Temperature. The reactor mean temperature followed the trend of the reactor inlet temperatures in all cases, except that the changes and rates of change were much smaller.

Time Lags. The system was very sluggish because of the long transit time (47 sec) of the fuel. In addition to the sluggishness of the system, there appeared to be time lags between the responses of various temperature indicating instruments for the same action. These lags were of the order of 2 min for low-power operation (less than 100 kw) and of the order of 1 min for full-power operation in the megawatt range. The topic of time lags is discussed in greater detail in a following section.

Calculated Power Change Resulting from a Regulating Rod Movement

A formula was developed which would estimate a power change in the reactor from a given change in the reactor outlet temperature and a regulating rod movement. This was possible primarily because of the relationships existing between P , ΔT , and $\Delta k/k$. The development of the relationship is described below.

$$\begin{aligned} \Delta P &= 2(0.11)(46) \left[\Delta T_o - \frac{1}{0.72 \times 9.8 \times 10^{-5}} (0.00033) \Delta d \right] \times 10^{-3} \text{ Mw} \\ &= (10.12 \Delta T_o + 47.75 \Delta d) \times 10^{-3} \text{ Mw} . \end{aligned}$$

When equilibrium exists between extracted power and nuclear power, the power level is given by

$$P = kq \Delta T = kq (T_o - T_i) ,$$

where

k = a constant (specific heat of the fuel),

q = fuel flow (gpm),

ΔT = the difference between inlet and outlet fuel temperatures,

T_o = outlet fuel temperature,

T_i = inlet fuel temperature.

Also the mean reactor fuel temperature is given by

$$T_m = \frac{1}{2} (T_o + T_i) ,$$

and

$$\Delta T = T_o - T_i .$$

From this it is seen that

$$\Delta T = 2T_o - 2T_m ,$$

and

$$P = 2kq (T_o - T_m) .$$

Now consider a change ΔP in the power:

$$\Delta P = 2kq (\Delta T_o - \Delta T_m) ,$$

but the temperature coefficient reactivity α is

$$\alpha = \frac{\Delta k/k}{\Delta T_m}$$

so that

$$\Delta P = 2kq \left[\Delta T_o - \frac{1}{\alpha} (\Delta k/k) \right] .$$

Since

$$\Delta k/k = [(\Delta k/k)/\text{in.}]_{RR} \times \Delta d_{RR} ,$$

where

Δd_{RR} = regulating rod movement,

$[(\Delta k/k)/\text{in.}]_{RR} = 0.033\% \text{ in. for the regulating rod,}$

by putting in the experimental values,¹⁰ it is seen that

$$\left[\frac{1}{0.72 \times 9.8 \times 10^{-5}} (0.00033) \Delta d \right] \times 10^{-3} \text{ Mw}$$

The change in power, as calculated from this formula, checked closely the observed power change for several different cases which were examined. The calculated data are given in Table 6.7.

Reactor Temperature Differential as a Function of Helium Blower Speed

A relationship between the fuel system helium blower speed and the resulting fuel ΔT was obtained from the data taken during ARE operation.

¹⁰The factor 0.72 is used to correct the temperatures in the manner described in Appendix K.

TABLE 6.7. SOME CALCULATED AND OBSERVED POWER CHANGES FROM REGULATING ROD MOTION

Date	Time	Observed Outlet Temperature Change ΔT_o ($^{\circ}$ F)	Regulating Rod Movement (in.)	Calculated Power Change (Mw)	Observed Power Change (Mw)
Nov. 10	1110*	55	12	1.59	1.60
	1114*	53	12	1.55	1.51
	1321	13	2.8	0.37	0.36

*Data recorded during Exp. H-8.

Some of the experimental fuel ΔT 's are plotted in Fig. 6.16 as a function of their corresponding blower speeds. These points could be represented by a parabola of the form

$$\Delta T^2 = Ks ,$$

where

K = a constant of proportionality,

s = the blower speed.

The curve that fit the experimental points best was found to be

$$\Delta T = (0.75s)^{1/2} ,$$

where ΔT is expressed in hundreds of degrees F and s is given in hundreds of rpm.

The extracted power can now be expressed in terms of blower speed:

$$\begin{aligned} P &= kq \Delta T = kq (0.75s)^{1/2} \\ &= [0.11 \times 46 \times (0.75s)^{1/2}] \times 10^2 \times 10^{-3} \\ &= 0.506 (0.75s)^{1/2} \text{ Mw} . \end{aligned}$$

The factor 10^2 is used because ΔT is expressed in the empirical formula in hundreds of degrees. The 10^{-3} factor expresses power in megawatts. The results obtained with the formula checked with the observed values of power in numerous cases. As an example, during experiment H-3, for a blower speed of 1590 rpm, an extracted power of 1.75 Mw was observed. The formula gives

$$P = 0.506 [0.75 (15.9)]^{1/2} = 1.75 \text{ Mw} .$$

The Phenomenon of the Time Lag

One of the most noteworthy phenomena encountered during the experiment was the time lag that seemed to be an intrinsic part of the system behavior. It was remarkably demonstrated in Fig. 6.8 when the blower was turned on. It was 0.75 min

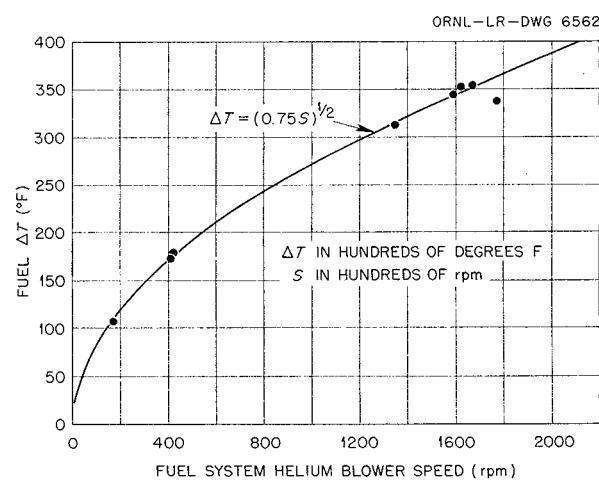


Fig. 6.16. Reactor ΔT as a Function of Fuel Helium Blower Speed.

later that the inlet temperature records showed a response, about 1.5 min before the mean temperature began dropping, and almost 2 min before the outlet temperature showed a corresponding rise. The reasons for the lags are obscure, but in an attempt to analyze the phenomenon several things must be considered: the extensiveness of the system, the reactor geometry, i.e., location of inlet and outlet fuel passages with respect to reactor core, heat transfer properties and possible phenomena within reactor, location, design, and attachment of the thermocouples within the reactor, and other unknown factors. There is a good possibility that the time lag phenomenon was connected with the temperature discrepancies noted in Appendix K.

Errors in marking the charts could possibly account for as much as 0.5 min, but certainly this cannot wholly account for the lag which was noted

consistently throughout the progress of the experiment. There is no doubt the system was very sluggish and slow to respond. This sluggishness was undoubtedly due, in large part, to the length of the fuel system. The transit time in the system was about 47 sec at full pump speed, as observed during the critical experiments. There does not seem to be any convenient mechanism for explaining longer time lags. A partial explanation is advanced in Appendix O, where geometrical considerations show that the instantaneous temperature change of the fuel was greater near the center of the reactor than at the points of the thermocouple locations. Thus the nuclear power was observed to change before the inlet and outlet thermocouples indicated changes.

An attempt was also made to analyze the heat transfer conditions within the reactor. Since the fuel and sodium flows were in opposite directions within the reactor, the fuel inlet line thermocouples were located near sodium outlet lines and the fuel outlet line thermocouples were located near sodium inlet lines. The temperature differences existing between the sodium (and moderator) and the fuel near the inlet and outlet thermocouples were of the order of 100°F or more and could possibly have influenced the readings of the thermocouples. This phenomena was investigated,¹¹ and no delay approaching 2 min could be ascribed to the heat transfer characteristics of the system. The greatest time lag which could be found in the heat transfer mechanism was of the order of a few seconds. The time lags of the reactor ΔT and mean temperature thermocouples were also investigated because these thermocouples had been insulated from the metal of the system. The time lags found were of the order of 15 sec or less, and thus they were about the same as those for uninsulated thermocouples. An experimental check showed that helium from the rod-cooling system had no appreciable effect on the readings of fuel temperatures when the blower speed was changed. Therefore, the phenomena of lag and low temperature readings could not be attributed to this cause.

It may well be that what may be described as "thermal inertia" played a part in the time lag. Since the reactor as a whole did not respond to a temperature change very fast, even though the fuel did, the thermocouple readings could have been affected to the extent that they received heat

not only from the fuel tubes but from other parts of the reactor. Better design and location of the thermocouples might have prevented such time lags.

Reactivity Effects of Transients in the Sodium System

The introduction of transient conditions into the sodium system was expected to have only small effects on reactor behavior. This proved to be the case in the few instances for which data are available. The two operations of the sodium system which were observed to have effects on reactivity were changing the rate of sodium flow and changing the rate of sodium cooling.

The first effect was observed as a part of one of the low-power experiments (Exp. L-7), in which, with the reactor on servo at 1-w power, the fuel flow rate was varied and the change in the regulating rod position was noted. The concluding portion of the experiment consisted in stopping the sodium coolant flow and observing the change in regulating rod position with the fuel flow at its normal value of 46 gpm. During this time the regulating rod changed from 7.85 to 7.69 in., a movement of 0.16 in., which corresponded to a $\Delta k/k$ of only 5.3×10^{-5} . This experiment was not repeated at high power, and therefore no data are available on reactor power and temperature changes as a function of sodium flow.

The second effect, the effect on the reactor system of changing the sodium cooling rate, was observed in Exp. H-12 during high-power operation. In this experiment the sodium system helium blowers were turned off and the following power and temperature changes were observed. At 2110 on November 11 the reactor was at 2.1-Mw extracted power; of this amount, approximately 1.6 Mw was being extracted from the fuel and 0.5 Mw from the sodium. At 2113 the sodium system helium blowers were turned off, and the power dropped, in the next 90 sec, to 1.96 Mw at a rate of 1.5 kw/sec, and, in the next $9\frac{1}{2}$ min, it dropped at a much slower rate of 280 w/sec and leveled off at 1.80 Mw. The total decrease in power was 300 kw. It is to be noted that since the extracted power from the sodium at the beginning of the experiment was 500 kw, about 200 kw of heat was still being lost by radiation and other means through the barrier door openings and other parts of the circuit, even with the helium circulation stopped. When the helium blower was turned on again at 2124 the reactor responded with an initial rise of 120 kw to

¹¹H. F. Poppendiek, Reactor Experimental Engineering,

1.92 Mw at the rate of 1.33 kw/sec and then a very slow rise over a period of nearly 18 min to 2.06 Mw at a rate only 0.1 as great.

Any over-all reactor temperature effect from sodium transients would have been reflected in a change in the mean fuel temperature, and therefore the mean fuel temperature was observed. When the sodium blower was turned off at 2113 the reactor mean fuel temperature dropped from 1313 to 1310°F in 3 min, corresponding to the initial power decrease noted. There was no drop in temperature which matched the very slow rate of decrease in power after the initial decrease. Upon starting the sodium blowers again at 2124 the mean temperature rose 13°F in 5 min to a new value of 1323°F, 10°F higher than at the start of the experiment. The increase over the initial temperature was partly attributable to the thermal inertia of the reactor. The reactor did not lose heat rapidly, but, when the blowers were again turned on, the nuclear power production increased by 300 kw and raised the temperature level to above that at the initial condition.

It may be concluded from these results that neither stopping the sodium flow or the sodium cooling had much effect on the reactor behavior. It is interesting to observe that the mean reactor fuel temperature went down with the decrease in nuclear power, which resulted from stopping the sodium blowers. It might be suspected that the reactor mean temperature would have risen because of lack of cooling in the moderator.

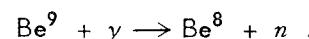
Reactivity Following a Scram

The behavior of a reactor after a scram is determined primarily by delayed neutrons and photoneutrons,¹² which in the ARE were produced in the beryllium oxide moderator. These processes keep the flux of the reactor from decaying immediately.

It was observed that after every scram the reactor decay took place in a series of descending oscillations, the time between oscillations being equal to the fuel transit time of 47 sec. Figure 6.17 shows a trace of one of the fission chambers after the scram at the conclusion of Run 7 of Exp. L-5, one of the low-power runs. The scram took place at the extreme right-hand edge of the trace. Six prominent pips and many lesser ones can be seen as the decay progressed.

¹²S. Glasstone and M. C. Edlund, *Elements of Nuclear Reactor Theory*, Van Nostrand, p 88-89 (1952).

This behavior can be explained on the basis that the slug of fuel passing through the reactor at the instant before the scram carried the last group of delayed neutron emitters produced at power. This phenomenon was particularly pronounced at the time the photograph of Fig. 6.17 was taken because it was at that time that an experiment¹³ was under way in which the reactor was allowed to rise from 1-w power to a predetermined power level of from 50 to 100 w on a constant period before it was scrammed. At the instant of scram the power of the reactor was 100 w, whereas one transit time previously (47 sec) the power was only about 14 w. As a result, immediately after the scram the delayed neutrons were particularly intense in the slug of fuel which was in the reactor at the time of the scram. The transit time of 47 sec is comparable to the 56-sec group of delayed neutrons.¹⁴ As this slug traversed the system and went back through the reactor, the delayed neutron emitters gave rise to neutron multiplication within the reactor and, at the same time, the associated gamma rays fell on the beryllium of the moderator and gave rise to more neutrons by the reaction



The total effect of both types of reactions was to give a strong multiplication every 47 sec. During the first pip shown in Fig. 6.17, the flux rose by a factor of 2; with succeeding pips, the multiplication became less. The average mean decay time of the first four pips was 72 sec. For the two longest lived groups of delayed neutrons the mean lives are 32 and 80 sec.¹⁴ Therefore, the attenuation of the pips closely followed the theoretical delayed neutron decay. A remarkable feature of Fig. 6.17 is that the pips could be distinguished for about 12 min. Since after the first 3 or 4 min the delayed neutron emitters were gone, the remaining effect was due solely to photoneutrons.

The scram behavior at high power was very similar, as observed with the use of the safety chambers. The fission chambers could not be used at high power, and therefore the first few seconds after a scram could not be observed with them.

¹³In experiment L-5 the regulating rod was calibrated by the periods induced by rod motion (cf., chap. 4).

¹⁴Glasstone and Edlund, *op. cit.*, p 65.

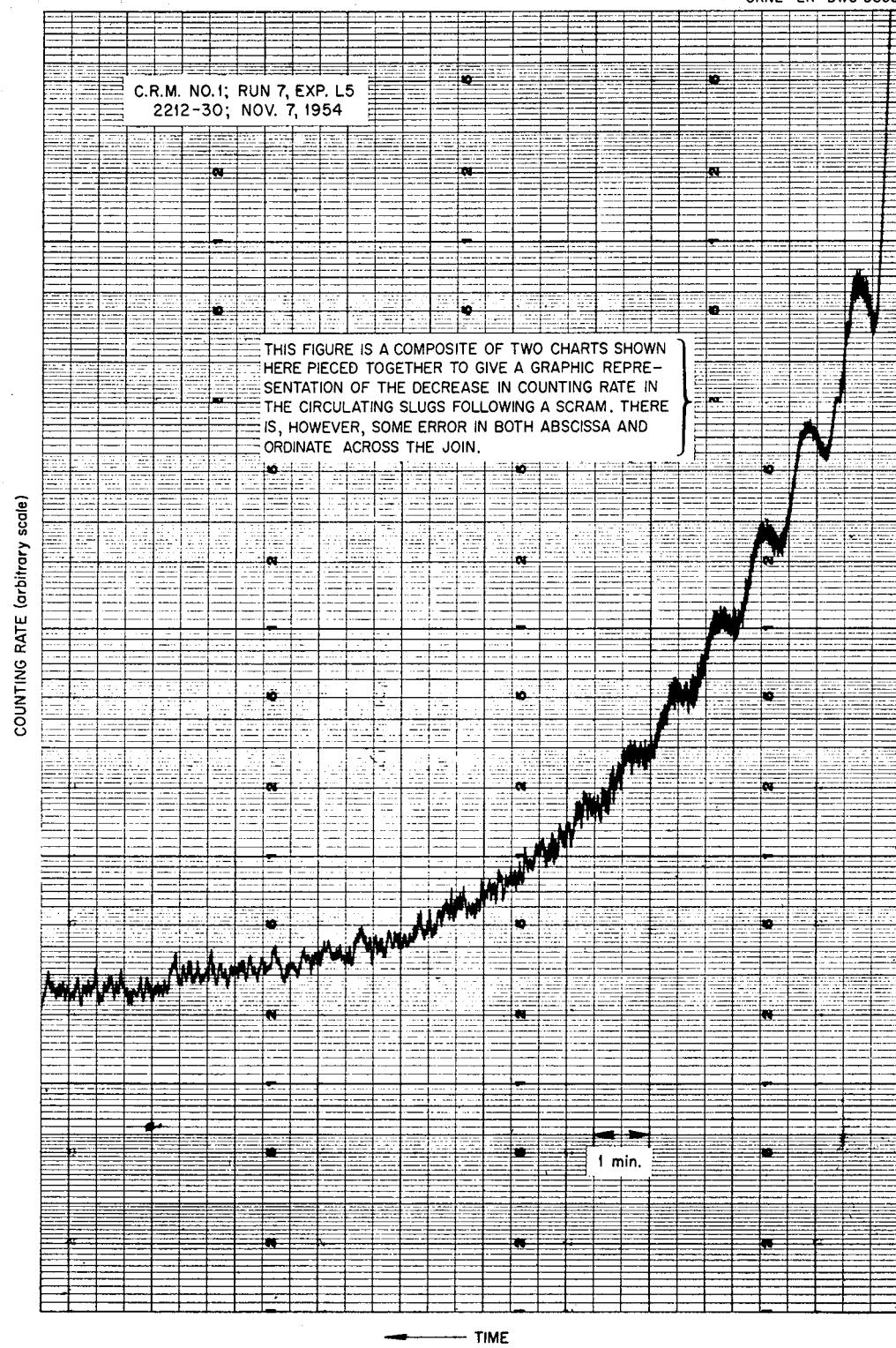


Fig. 6.17. Circulating Slugs After a Scram.

FINAL OPERATION AND SHUTDOWN

The last scheduled experiment conducted on the reactor was the measurement of the xenon buildup following the 25-hr run at 2.12 Mw. The 10-hr period of operation at one-tenth full power was concluded at 0835 on November 12. During the following 11½-hr period from 0835 to 2004, when the reactor was shut down the final time, the operation of the reactor was demonstrated for Air Force and ANP personnel who were gathered for the quarterly ORNL-ANP Information Meeting. The demonstrations included repeated cycling of the load by turning the blowers on and off, and group movement of the three shim rods to change the reactor mean temperature. The information obtained during this time on the dynamic behavior of the reactor is described above under the subtitle "Reactor Kinetics."

Also during the final 11½-hr period of operation, two complete surveys of system temperatures were taken with the reactor at maximum power. It was during one of these runs that the equilibrium fuel outlet temperature of 1580°F and the total reactor power of 2.45 Mw was attained (cf., App. L).

Since all operational objectives of the experiment had been attained and it was estimated on the basis of time and the assumed reactor power that the desired integrated power of 100 Mwhr would be attained by 2000 on Friday, November 12, it was decided to terminate the experiment at that time. Colonel Clyde D. Gasser, Chief, Nuclear Powered Aircraft Branch of WADC, who was then visiting the Laboratory, was invited to officiate at the

termination of the experiment. At 8:04 PM on November 12, with Colonel Gasser at the controls, the reactor was scrammed for the last time and the operation of the Aircraft Reactor Experiment was brought to a close. A photograph taken in the control room at that time is shown as Fig. 6.18.

At the time the experiment was terminated it was believed that the total integrated power was more than the 100 Mwhr which had been prescribed as a nominal experimental objective, but subsequent graphical integration of the Log N charts, Appendix R, revealed that the actual total integrated power was about 96 Mwhr. At the time the reactor was scrammed the sodium system had been in operation (circulating sodium) for 635.2 hr and the fluoride system for 462.2 hr. Of this total fluoride circulating time 220.7 hr were obtained with the reactor critical and 73.8 hr after the reactor was first brought to power.

Although the nuclear operation was concluded on Friday evening, the fuel and sodium were permitted to circulate until the following morning, at which time they were dumped into their respective dump tanks. The final phase of the experiment, including the dumping operation, subsequent analysis and recovery of the fuel, and examination of the systems and components for corrosion, wear, radiation damage, etc., are to be discussed in a subsequent report. Since much of the data cannot conveniently be obtained until the radioactivity has decayed, the last report will not be forthcoming immediately.



Fig. 6.18. Termination of the Aircraft Reactor Experiment: The Final Scram.

7. RECOMMENDATIONS

No comprehensive report is complete without conclusions, discussion, and recommendations. In this report the conclusions are presented in the summary at the beginning, and the discussion is incorporated in the text and, especially, in the Appendixes. Furthermore, certain alterations and modifications that would have been desirable in the conduct of the experiment are implicit in the discussions throughout the report. However, the changes, if effected for any similar future experiments, could lead to substantial improvements in design, instrumentation, operation, and interpretation. Accordingly, a list of recommendations based on the ARE experience is presented; no significance is inferred by the order of listing.

1. The operating crew should maintain the same shift schedule as the craft labor - electricians, instrument mechanics, pipe fitters, etc. - assigned to the operating crew, and all members of one crew should have their off-day at the same time. In particular, there should be four operating crews that maintain the same rotating schedule as the rest of the plant.

2. The cause of the obvious discrepancy between the temperatures read by the line thermocouples close to the reactor and those further removed from the reactor should be ascertained. No physical phenomena, with the possible exception of radiation, have been proposed, to date, which could account for the observed difference.

3. In order to measure the extracted reactor power from the secondary or tertiary heat transfer mediums, these systems should be adequately instrumented for flow rates and temperatures. Such instrumentation might also make possible a thermodynamic analysis of the performance of the various heat exchangers.

4. Thermocouples on the outer surface of fuel and sodium tubes in the heat exchangers should be installed so that they read wall temperatures rather than an intermediate gas temperature.

5. Of the two thermocouples which were required to measure the reactor mean temperature and the two required to measure the temperature gradient, one was electrically insulated from the pipe wall. The insulation effected a time lag between the wall and thermocouple temperatures of about 15 sec. Thermocouple installations for obtaining time-dependent data should be made so that the wall temperature can be read without a time lag.

6. To heat small (up to $\frac{3}{8}$ in. OD) lines and associated valves, tanks, etc. to uniform high temperatures ($\sim 1400^{\circ}\text{F}$) requires a surprising degree of precision in the installation of both heaters and insulation. Furthermore, where calrod heaters are employed, they should be installed on opposite sides of a line, and the heaters and line should be jointly wrapped with heat shielding before insulation is applied.

7. To control accurately the temperature of any system, thermocouples should be installed at any discontinuity of either the heaters (i.e., between adjacent heaters) or the system (i.e., at the junction of two lines, etc.), and, with the exception of obviously identical installations, each heater should have its own control.

8. Where gas lines are subject to plugging due to the condensation of vapor from the liquid in the system to which the lines are connected, it is necessary either to heat the lines to above the freezing point of the vapor or to employ a vapor trap. While a vapor trap proved satisfactory in preventing the fuel off-gas line from plugging, it was not possible to heat the sodium off-gas line sufficiently (because of temperature limitation of the valves) to prevent the gradual formation of a restriction. Gas valves that can be operated at higher temperatures and are compatible with sodium are needed.

9. The double-walled piping added a degree of complexity to the system that was far out of proportion to the benefits derived from the helium annulus. Parts of the annulus were at subatmospheric pressure, and no leak tests were made on the fuel system once it was filled with the fluoride mixture. The helium flow was not needed for distributing heat in the sodium system, and it was of uncertain value in the fuel system. Consequently, future systems should not include such an annulus.

10. The use of any type of connection other than an inert-arc-welded joint in any but the most temporary fuel or sodium line should be avoided.

11. All joints, connections, and fittings in the off-gas system should be welded, and, in general, they should be assembled with the same meticulous care that characterized the fabrication of the fuel and sodium systems in order to minimize the possibility of the unintentional release of fission gases.

12. As a secondary defense in the event of the release of activity in the reactor cell (i.e., pit), the cell should be leaktight. The leak-tightness of the numerous bulkheads out of such a cell should be carefully checked.

13. The air intake to the control room was located on the roof of the building, and thus adverse meteorological conditions readily introduced off-gas activity into the control room. With an airtight control room equipped with its own air supply (or a remotely located filtered intake), the control room operations could continue without concern for the inhalation of gaseous activity.

14. The off-gas monitrons should be shielded from direct radiation. Furthermore, although these monitrons were not needed during the experiment, they are known to build up background activity which would eventually mask that of the gas they are to measure. The development of monitrons in which activity will not accumulate is recommended.

15. The radiation level and the airborne activity throughout the building were measured by monitrons and constant air monitors, respectively. The data from both instruments should be continuously recorded. Furthermore, the output of the air monitors should be modified by the addition of a differentiating circuit so that the recorded data would give better measures of the airborne activity.

16. The helium ducts leaked to the extent that it was possible to attain only a fraction of the desired helium concentration therein. They were of the conventional bolted-flange design and should have been modified to permit seal welding of all joints; they should be subjected to stringent leak tests.

17. The helium consumption for the last three and one-half months of the ARE experiment was $\frac{2}{3}$ million standard cubic feet (over 3000 standard cylinders). The average consumption rate during the last two weeks of the experiment was about 8.5 cfm, and peak consumption rates of 25 cfm were recorded. This extraordinarily high helium consumption could be reduced by the use of dry air or nitrogen for much of the pneumatic instrumentation in which helium was used.

18. Various valves in both the gas and liquid systems leaked across the valve seats. The valve development program should be emphasized until valves are obtained that can be depended upon as reliable components of high-temperature ($\sim 1200^{\circ}\text{F}$) sodium, fluoride, or gas systems. Furthermore, either limit switches that would operate at higher

temperatures to indicate valve open or closed should be developed, or the existing limit switches should be located in cooler regions.

19. The use of frangible disks to isolate the standby fuel pump did not enhance the feasibility of continuing the experiment in the event of the failure of the main fuel pump during high-power operation. The frangible disks are objected to in that they require a nonreversible operation. In general, leak-tight valves should be developed that may be used rather than the frangible disks.

20. Although the ARE, as designed, was to incorporate numerous "freeze sections," only two were included in the system as finally constructed, and the operability of these two was so questionable that their use was not contemplated during the course of the experiment. Such sections should either be eliminated from consideration in future systems, or a reliable freeze section should be developed.

21. Much useful information would be obtained if provisions could be made for sampling each liquid system throughout the operation. This was possible on the ARE only prior to the high-power experiments.

22. The variable inductance-type flow and level indicators should be converted to the null-balance type of instruments in order to eliminate the temperature dependence of the pickup coil signal. Furthermore, these coils should be located in a region at much less than 1000°F in order to increase coil life.

23. Although numerous spark plug probes were satisfactorily employed to measure levels in the various tanks, the intermittent shorts that were experienced with several sodium probes might have been avoided if clearances between the probe wire and the stand pipe in which the probes were located had been greater.

24. The use of mercury alarm switches on vibratory equipment where there is little leeway between the operating and alarm condition will give frequent false alarms and should therefore be avoided.

25. Weight instruments are of questionable accuracy in a system in which the tank being weighed is connected through numerous pipes to a fixed system, especially when these pipes are covered with heaters and insulation and are subject to thermal expansion.

26. The flame photometer is an extremely sensitive instrument for the detection of sodium and

NaK. However, in employing this instrument to detect the presence of sodium (or NaK) in gas, the sampling line should be heated to about 300°F.

27. The magnet faces in the shim rods should be designed so that dirt particles cannot become trapped thereon and thus require higher holding currents.

28. The two control points, i.e., the upstairs control room and the basement heater and instrument panels, should have been more convenient to one another in order to effect the greatest efficiency of operation.

29. The communications system in the building was inadequate. Except for the auxiliary FM system, which was frequently inoperative, there was only one phone in the control room, which was on the main station of the PA system. However, the PA system was not capable of audibly supporting two conversations at the same time. Accordingly, the capacity of the PA system should be increased so that as many as 4 or 5 conversations may be simultaneously effected. Also, more outlets should be provided both in the control room and at other work areas in the building.

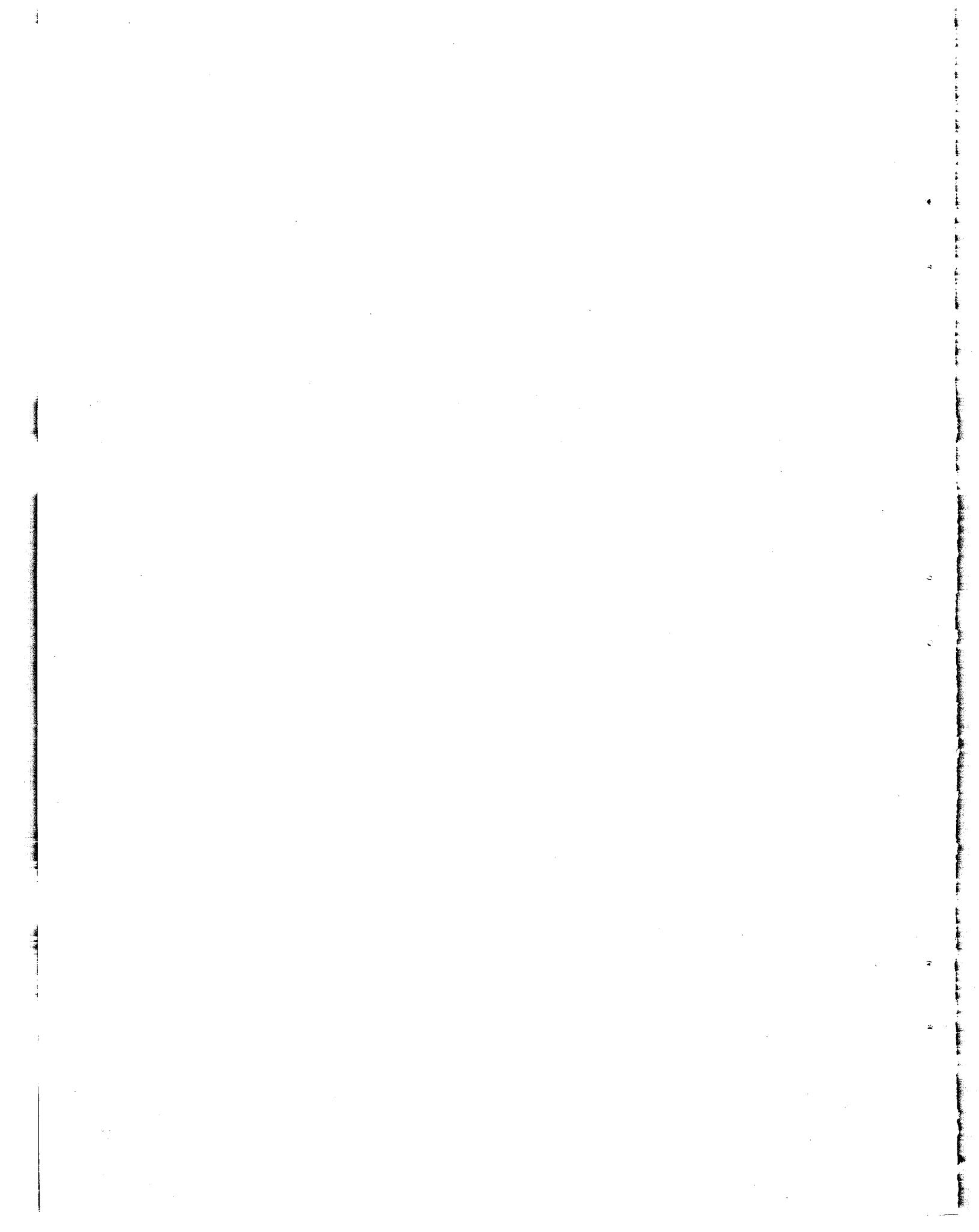
30. A megawatt-hour meter should be installed (possibly on the log N or the ΔT recorder) in order to provide a continuous measure of the integrated power as the experiment progresses.

31. In order to analyze various related time-

dependent data (as required, for example, in the determination of the various temperature coefficients), it is necessary that the recorder charts be marked at the start of the experiment. While the charts can be marked by hand, this was a source of error which became very important in the analysis of data from fast transients. Accordingly, all such charts should be periodically and simultaneously marked by an automatic stamper. Furthermore, each chart should be stamped with a distinctive mark that would positively identify it.

32. To analyze the kinetic behavior of a reactor system it is necessary to have a recorder chart of the time behavior of all equipment which can introduce transients in the reactor, as well as charts of the process data and conventional nuclear data. Therefore the helium blower speeds and shim rod positions should have been recorded continually.

33. The recorded data and the data sheets comprise a fairly comprehensive picture of the experiment. However, even if all the data are recorded they are of value only to the extent that meaningful interpretations can be made. While automatically marking the data charts will be helpful, it will still be necessary to rely on log book information which should be recorded in great detail, possibly to the extent of making this the only responsibility of a shift "historian."



Appendix B SUMMARY OF DESIGN AND OPERATIONAL DATA

This appendix tabulates both the design and operational data pertinent to the aircraft reactor experiment. Most of the design data were extracted from two design memoranda,^{1,2} although some values had to be revised because of subsequent modifications in the design. In addition to the design data, the experimental values of the various system parameters are included. All values obtained experimentally are shown in italics and, for comparative purposes, are tabulated together with the corresponding design values. There are, of course, numerous design numbers for which it was not possible to obtain experimental numbers. The flow diagram of the experiment is presented in Fig. B.1. The values of temperature, pressure, and flow given on this drawing are design values — not experimental values.

¹W. B. Cottrell, *ARE Design Data*, ORNL CF-53-12-9 (Dec. 1, 1953).

²W. B. Cottrell, *ARE Design Data Supplement*, ORNL CF-54-3-65 (March 2, 1954).

DESCRIPTION

1. The Reactor Experiment

Type of reactor	Circulating fuel, solid moderator
Neutron energy	Thermal and epithermal
Power (maximum)	2.5 Mw
Purpose	Experimental
Design lifetime	1000 hr
Fuel	$\text{NaF-ZrF}_4\text{-UF}_4$ (53.09-40.73-6.18 mole %)
Moderator	BeO
Reflector	BeO
Primary coolant	The circulating fuel
Reflector coolant	Sodium
Structural material	Inconel
Test stand	Concrete pits in Building 7503
Shield	$7\frac{1}{2}$ ft of concrete
Heat flow	Fuel to helium to water

2. Physical Dimensions of Reactor (in.)

	Cold (70°F)	Hot (1300°F)
Core height	35.60	35.80
Core diameter	32.94	33.30
Side reflector height	35.60	35.80
Side reflector inside diameter	32.94	33.30
Side reflector outside diameter	47.50	48.03
Top reflector thickness	4.00	4.25
Top reflector diameter	32.94	33.30
Bottom reflector thickness	4.93	4.98
Bottom reflector diameter	32.94	33.30
Pressure shell inside diameter	48.00	48.55
Pressure shell wall thickness	2.00	2.02
Pressure shell inside height	44.50	45.00
Pressure shell head thickness	4.00	4.04
Fuel elements	66 parallel Inconel tubes containing the circulating fuel. The tubes were connected in six parallel circuits each having 11 tubes in series. Each tube was 1.235 in. O.D., with a 60-mil wall.	

3. Volumes of Reactor Constituents (Cold)

a. Inside Pressure Shell

	Volume (ft ³)					
	BeO	Fuel	Na	Inconel	Rods ^a	Total
Core	14.55	1.33	0.80	0.37 ^b	0.50	17.55
Side reflector	17.68	0	0.91	0.10 ^c	0.26 ^d	18.95
Annulus outside reflector	0	0	0.58	0.19	0	0.77
Top reflector	0	0.21	1.62	0.08 ^b	0.06	1.97
Bottom reflector	0	0.24	1.67	0.44 ^b	0.07	2.42
Space above reflector and annulus	0	0	2.14	0.04 ^c	0.03 ^d	2.21
Space below reflector and annulus	0	0	2.17	0.52 ^c	0.04 ^d	2.73
Total	32.23	1.78	9.89	1.74	0.96	46.60

^aTotal volume inside inner rod sleeve.

^bIncludes the Inconel-clad stainless steel rod sleeves.

^cIncludes all three sleeves around fission chambers

^dIncludes volume of insulating material around inner fission chamber sleeve.

b. Operating Fuel System

	Volume (ft ³)	
	Cold	Hot
Core	1.33	1.37
External system (to minimum pump level)	3.48	3.60
Pump (available above minimum level)	~1.65	~1.70
Total	6.46	6.67

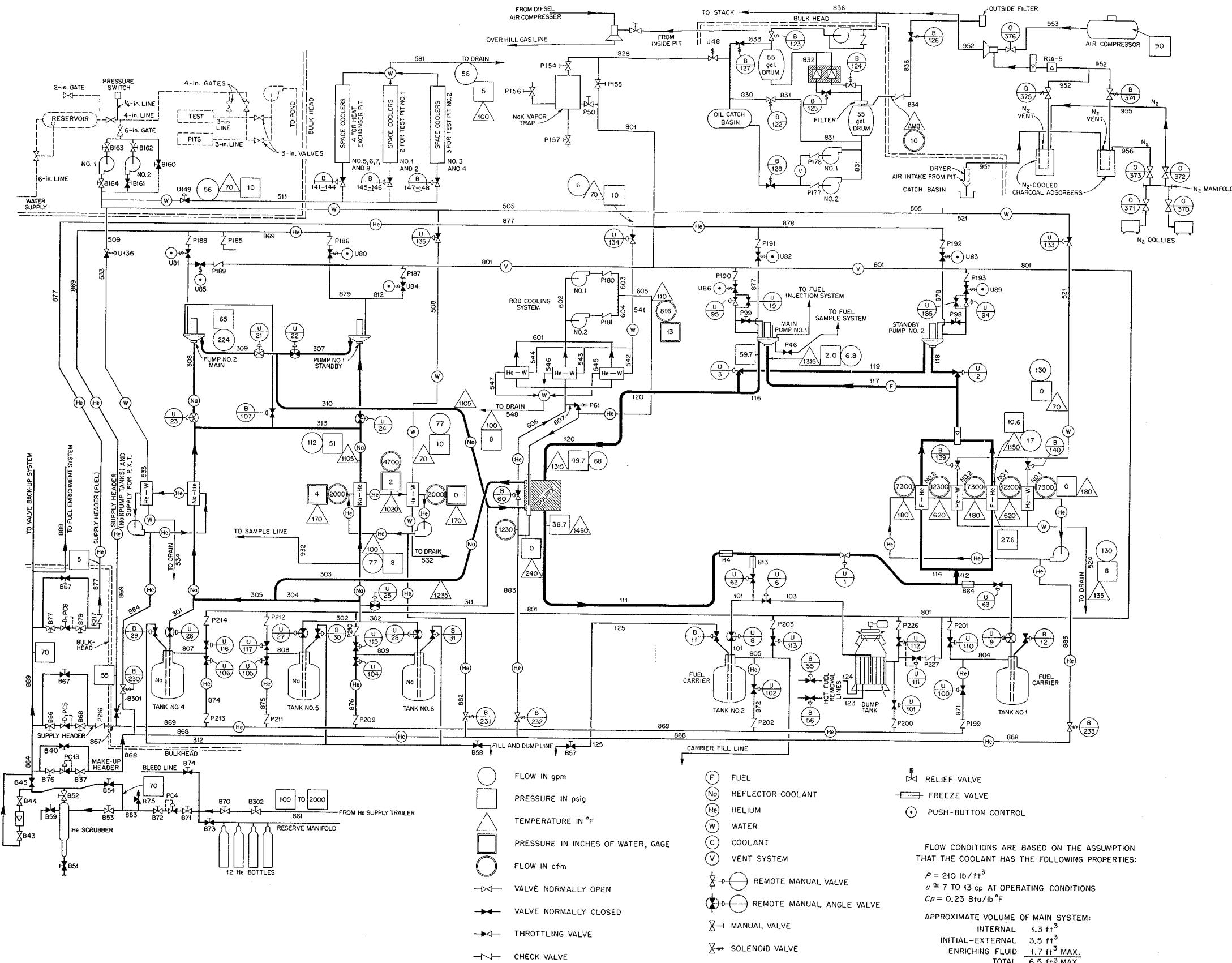
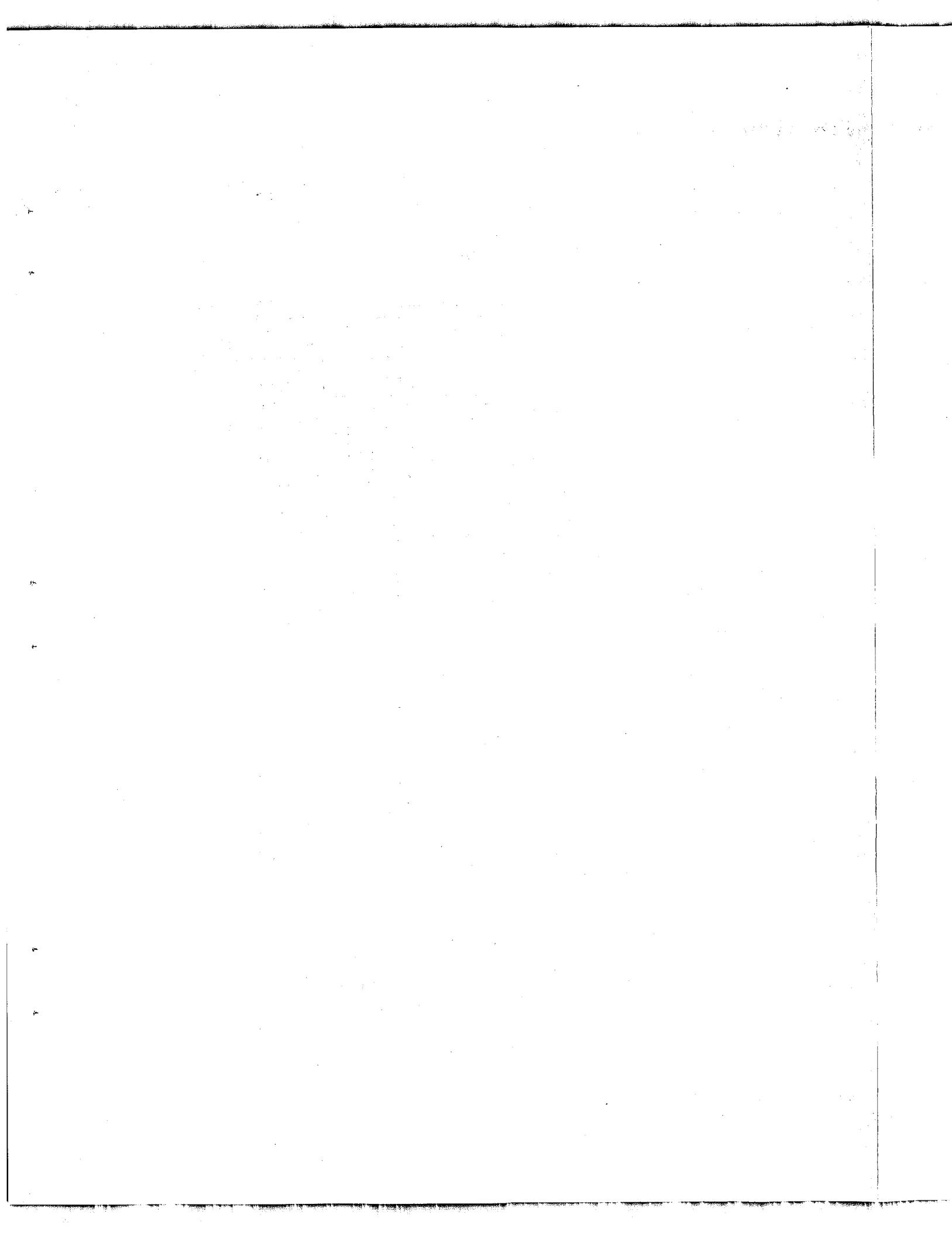


Fig. B.1. ARE Flow Diagram.



c. Miscellaneous Fuel System

	Volume (ft ³)
Maximum capacity fill and flush tanks	14.5
Bottom (waste) in fill and flush tanks	0.3
Dump line to fill and flush tank No. 2	0.8
Dump line to fill and flush tank No. 1	0.75
By-pass leg	0.4
Heat exchanger leg from pump to fill line to Tank No. 2	1.6
Reactor leg from fill line to pump (minimum operating level)	3.0
Pump capacity, minimum to maximum level	1.7
Carrier available	15.5
Concentrate available	1.3

d. Sodium System

	Volume (ft ³)
Inside pressure shell	10
Outside pressure shell	~ 10
Total	<u>20</u>

MATERIALS

1. Amounts of Critical Materials

BeO blocks (assuming $\rho = 2.75 \text{ g/cm}^3$)	5490 lb
BeO slabs (assuming $\rho = 2.75 \text{ g/cm}^3$)	48 lb
Amount of uranium requested	253 lb of U ²³⁵
Uranium enrichment	93.4% U ²³⁵
Uranium in core	30 to 40 lb
Uranium inventory in experiment	126 to 177 lb

2. Composition of Reactor Constituents

a. Fluoride Fuel Mixture

	Fuel ^a	Fuel Carrier	Fuel Concentrate
NaF			
mole	53.09	50	66.7
wt %	22.34	20.1	21.3
ZrF ₄			
mole %	40.73	50	0
wt %	62.12	79.9	0
UF ₄			
mole %	6.18	0	33.3
wt %	17.54	0	78.7
Impurities (ppm)			
Ni	<5 ^b	25 ^c	47 ^d
Fe	5 ^b	35 ^c	84 ^d
Cr	445 ^b	10 ^c	~20 ^d

^aFuel composition for high-power operation.

^bFinal analysis before high-power operation.

^cAverage of all 14 batches of carrier.

^dEstimate based on a few preliminary analyses.

b. Inconel^a

Constituent	Amount (wt %)	Constituent	Amount (wt %)	Constituent	Amount (wt %)
Ni	78.5	Co ^b	0.2	Zr ^b	0.1
Cr	14.0	Al ^b	0.2	C	0.08
Fe	6.5	Ti ^b	0.2	Mo	Trace
Mn	0.25	Ta ^b	0.5	Ag, B, Ba	Trace
Si	0.25	W ^b	0.5	Be, Ca, Cd	Trace
Cu	0.2	Zn ^b	0.2	V, Sn, Mg	Trace

^aB. B. Betty and W. A. Mudge, *Mechanical Engineering*, February 1945.

^bAccuracy, $\pm 100\%$. Y-12 Isotope Analysis Methods Laboratory (spectrographic analysis). Y-12 Area Report Y-F20-14.

c. Beryllium Oxide*

Impurities	Amount (ppm)	Impurities	Amount (ppm)	Impurities	Amount (ppm)
Si	1050	Ca	780	Na	330
Al	213	Fe	114	Mg	50
Pb	45	Zn	<30	K	<25
Ni	<20	Cr	10	Li	<5
Mn	<5	B	2.8	Ag	<1
Co	<1				

*W. K. Ergen, *Activation of Impurities in BeO*, Y-12 Area Report Y-F20-14 (May 1, 1951).

d. Helium

Oxygen contamination < 10 ppm

e. Sodium

Oxygen contamination < 0.025 wt %

3. Physical Properties of Reactor Materials

	Melting Point (°C)	Thermal Conductivity (Btu/hr.ft.°F)	Viscosity (cp)	Heat Capacity (Btu/lb.°F)	Density (g/cm³)
Fuel Carrier:^a					
NaF-ZrF ₄ (NaZrF ₅) 50-50 mole %	510	2.5 ± ^b 5	8.0 at 600°C 5.3 at 700°C 3.7 at 800°C	0.30 ^b	$\rho = 3.79 - 0.00093T$ $600 < T < 800^{\circ}\text{C}$
Fuel Concentrate:^a					
NaF-UF ₄ (Na ₂ UF ₆) 66.7-33.3 mole %	635	0.5 (estimated)	10.25 at 700°C 7.0 at 800°C 5.1 at 900°C	0.21 ^b	$\rho = 5.598 - 0.00119T$ $600 < T < 800^{\circ}\text{C}$
Fuel:^a					
NaF-ZrF ₄ -UF ₄ 53.09-40.73-6.18 mole %	530	1.3 (estimated)	8.5 at 600°C 5.7 at 700°C 4.2 at 800°C	0.24 ^b	$\rho = 3.98 - 0.00093T$ $600 < T < 800^{\circ}\text{C}$
BeO ^c	2570	16.7 at 1500°F 19.1 at 1300°F 22.5 at 1100°F		0.46 at 1100°F 0.48 at 1300°F 0.50 at 1500°F	from 2.27 ^d to 2.83 at 20°C
Inconel ^e	1395	8.7 from 20 to 100°C 10.8 at 400°C 13.1 at 800°C		0.101 77 < T < 212°F	8.51 at 20°C
Sodium ^f	98	43.8 at 300°C 38.6 at 500°C 0.18 at 700°C	0.38 at 250°C 0.27 at 400°C	0.30	0.85 at 400°C 0.82 at 500°C 0.78 at 700°C
Helium ^g	<-272.2	0.100 at 200°F 0.119 at 400°F 0.136 at 600°F	0.0267 at 200°C 0.0323 at 400°C 0.0382 at 600°C	1.248 0 < T < 300°C	1.79×10^{-4} at 0°C 1.30×10^{-4} at 100°C 1.03×10^{-4} at 200°C
Insulation					
Superex (SiO ₂)	0.18				0.38
Sponge felt (MgSiO ₃)	0.13				0.48

^aData from ANP Physical Properties Group.^bPreliminary values for the liquid 600 to 800°C.^cData from *The Properties of Beryllium Oxide*, BMIT-18 (Dec. 15, 1949).^dPorosity of BeO, from ANP Ceramics Group, 23% at $\rho = 2.27$, 0% at $\rho = 2.83$.^eData from *Metals Handbook*, 1948 Ed., The American Society for Metals.^fData from *Liquid Metals Handbook*, NAVEXOS P-733 (June 1952).^gB. O. Newman, *Physical Properties of Heat Transfer Fluids*, GI-401 (Nov. 10, 1947).

REACTOR PHYSICS

1. General

Neutron energy	Thermal and epithermal
Thermal fissions, %	60
Neutron flux, n/cm ² .sec	$\sim 10^{14}$
Gamma flux, $\gamma/cm^2.sec$	$\sim 10^{11}$

2. Power

Maximum power, Mw	1.5	(2.5)
Design power, Mw	1.0	
Power density (core av at max power) w/cm ³	3	(5)
Maximum specific power (av kw/kg. of U ²³⁵ at 1.5 Mw)	94	(153)
Power ratio (max/av)		
Axially	1.5 : 1	
Radially in core	1.2 : 1	
Radially in fuel tube	1.7 : 1	
Maximum power density in fuel, w/cm ³	110	(180)
Maximum power density in moderator, w/cm ³	1.3	(2.2)

3. Neutron Flux in Core (n/cm².sec)

Thermal (max)	1.5×10^{13}
Thermal (av)	0.7×10^{13}
Fast (max)	3.5×10^{13}
Fast (av)	1.5×10^{13}
Intermediate	2.0×10^{13}

4. Leakage Flux (per fission)

Reflector	
Fast	0.0011
Intermediate	0.066
Thermal	0.191
Ends	
Fast	0.013
Intermediate	0.102
Thermal	0.0002

5. Fuel

Enrichment, % U ²³⁵	93.4
Critical mass, lb of U ²³⁵ in clean core	(32.75)
U ²³⁵ in core (i.e., critical mass plus excess reactivity) lb	30 to 40 (36)
U ²³⁵ in system, lb	126 to 177 (138)
U ²³⁵ consumption at maximum power, g/day	1.5 (2.5)

6. Neutron Flux in Reflector

Maximum flux at fission chamber holes, nv/w	1.5×10^6
Counting rate of fission chambers, counts/sec.w	2×10^5

7. Reactivity Coefficients

Effect	Symbol	Value
Thermal base	$\Delta k/k$	-0.011 from 68 to 1283°F -0.009 from 1283 to 1672°F
Uranium mass (at $k = 1$)	$\frac{\Delta k/k}{(\Delta M/M)}$	0.25 (0.236)
Sodium density	$\frac{\Delta k/k}{(\Delta \rho/\rho)}$	-0.05 from 90 to 100% ρ
Moderator density	$\frac{\Delta k/k}{(\Delta \rho/\rho)}$	0.5 from 95 to 100% ρ
Inconel density	$\frac{\Delta k/k}{(\Delta \rho/\rho)}$	-0.17 from 100 to 140% ρ
Fuel temperature	$(\Delta k/k)/^{\circ}\text{F}$	(-9.8×10^{-5})
Reactor temperature	$(\Delta k/k)/^{\circ}\text{F}$	-5×10^{-5} (-6.1×10^{-5})
Sodium temperature	$(\Delta k/k)/^{\circ}\text{F}$	(-5.88×10^{-5})
Moderator temperature	$(\Delta k/k)/^{\circ}\text{F}$	(1.1×10^{-5})

SHIELDING

1. Material

	Thickness (in.) (from source outward)	Density (g/cm ³)
Barytes concrete block in the reactor pit only	12	3.3
Poured Portland concrete	18	2.3
Barytes concrete block	60	3.3

2. Composition

Cement	$\text{CaCO}_3 + \text{SiO}_2 + \text{Al}_2\text{O}_3$
Concrete	Cement and aggregate of gravel
Barytes	Cement and aggregate of BaSO_4

3. Relaxation Lengths (cm)

	Barytes Concrete	Portland Cement
1-Mev gamma rays	4.14	4.62
2.5-Mev gamma rays	6.72	6.86
7.0-Mev gamma rays	9.46	14.0
Fast neutrons (1 to 5 Mev)	8.2	11.0

4. Source Intensities

	No. per Fission	Energy (Mev)
Core gammas		
Prompt	2.0	2.5
Fission-product decay	2.0	2.5
Capture gammas	0.94	7.0
Gamma flux outside of reactor thermal insulation per watt		
2.0-Mev gammas		$3 \times 10^4 \gamma/\text{cm}^2 \cdot \text{sec}$
7.0-Mev gammas		$0.8 \times 10^4 \gamma/\text{cm}^2 \cdot \text{sec}$
Neutron flux outside of reactor thermal insulation per watt		
Thermal to 250 kev		$3 \times 10^5 \text{n}/\text{cm}^2 \cdot \text{sec}$
Fast to 250 kev		$1.5 \times 10^4 \text{n}/\text{cm}^2 \cdot \text{sec}$

5. Activity in External Fuel Circuit per Watt

Time Out of Reactor (sec)	0.52-Mev Gamma Activity (photons/cm ³ .sec)	1-Mev Delayed-Neutron Activity (n/cm ³ .sec)
0	8.1×10^6	8.5×10^3
5	6.6×10^6	2.3×10^3
10	5.9×10^6	1.4×10^3
20	5.1×10^6	0.74×10^3
30	4.7×10^6	0.50×10^3
40	4.5×10^6	0.35×10^3

REACTOR CONTROL

1. Control Elements

Source	1
Regulating rod	1
Shim rods	3
Temperature coefficient, $(\Delta k/k)/^\circ\text{F}$	$\sim -5 \times 10^{-5}$ (-6.1×10^{-5})

2. Source

Location	Core axis
Type	Po-Be
Strength, curies	15 (7)
Neutron intensity, n/sec	3.5×10^7 (1.6×10^7)

3. Regulating Rod

Location	Core axis
Diameter, in.	2
Travel, in.	12
Cooling	Helium
Total $\Delta k/k$, %	0.40 (0.40)
Maximum $(\Delta k/k)/\text{sec}$ (slowspeed), %	0.010 (0.011)
Speed, in./sec	0.3 or 3 (0.32) (fast speed not used)

Backlash, in.	0.007
Servo motor	Diehl 1A, 115 v, 60 cycle, 3400 rpm, reversible
Actuation	Manual
	Temperature error-signal (not used)
Regulation	Flux signal, $\leq \pm 2\% N_F$; $\leq 1.3^\circ F$ mean T

There were seven regulating rods made up which gave a calculated $\Delta k/k$ from 0.13 to 1.35%. The rod used in the experiment was the one which most nearly gave a measured $\Delta k/k$ of 0.4%.

Rod number	1	2	3	4	5	6	7
Calculated $\Delta k/k$	0.13	0.18	0.27	0.39	0.56	0.90	1.35
Measured $\Delta k/k$				(~0.25)	(0.40)		
Weight per inch of rod, lb	0.042	0.061	0.091	0.132	0.21	0.32	0.50

4. Shim Rods (3)

Location	One at each 120 deg on 7.5-in.-radius circle
Diameter, in.	2
Travel, in.	36
Cooling	Helium
Material	B_4C
Magnet release time, sec	$<10^{-2}$
Maximum withdrawal speed, in./sec	0.036 (0.046)
Total $\Delta k/k$ per rod, %	5.0 (5.8)
Maximum (% $\Delta k/k$)/sec per rod	0.005, av over rod (0.0039 at 4-in. insertion)
Motor	Janette 1.2 amp, 115 v, 60 cycle, 1725 rpm, reversible

5. Nuclear Instrumentation

a. Fission Chambers (2)

Function	Counting-rate signal
Sensitivity	0.14 (counts/sec) per ($n/cm^2 \cdot sec$)
Range	10^{11} , i.e., 10^4 in instrument, 10^7 in position and shielding

b. Parallel-Circular-Plate Ionization Chambers (3)

Function (2 chambers) (2 chambers)	Safety level (scram signal) Regulating rod temperature servo
Sensitivity Range	$50 \mu A$ at $10^{10} n/cm^2 \cdot sec$ $\sim 10^3$, i.e., from 5×10^{-2} to $1.5 N_F$

c. Compensated Ionization Chambers (2)

Function (1 chamber) (1 chamber)	Micromicro ammeter Regulating rod flux servo
Sensitivity Range	$50 \mu A$ at $10^{10} n/cm^2 \cdot sec$ $\sim 10^6$, i.e., from 10^{-6} to $3 N_F$

6. Scrams and Annunciators

a. Automatic Rod Insertion and Annunciation

Cause	Set Point	Nuclear Scram	Process Scram	Reverse ^a	Annunciator No.
Neutron level	1.2 and 1.5 N_F ^b	x			30
Period	1 sec	x			30
Period	5 sec			x	32
Reactor exit fuel temperature	>1550°F		x		25
Heat exchanger exit fuel temperature	<1100°F		x		25
Fuel flow	<10 gpm		x		25
Power	Off		x		30
Scram switch	Scram position		x		30

^aShim rods automatically driven in.

^bNeutron level set so that the fast scram annuator, No. 30, would annunciate at 1.2 N_F (normal flux) although the safety rods would not be dropped until the neutron level reached 1.5 N_F . There was not another neutron level annuator at 1.5 N_F .

b. Nuclear Annunciators

	Set Point	Annunciator No.
Safety circuit	Electronic trouble	28
Count rate meter	Off-scale	26
Servo	Off-scale	31
Rod-cooling helium	Off	29
Neutron level	1.2 N_F	27

c. Fuel System Annunciators

	Set Point	Announcer No.
Pump power (main pump)	>50 amp	33
Low heat exchanger fuel flow	<20 gpm	34
High heat exchanger water temperature	>160°F	35
Low heat exchanger fuel temperature	<1150°F	36
High fuel level (main pump)	Maximum pumping level	37
Low fuel level (main pump)	Minimum pumping level	38
High pump pressure (main pump)	>5 psi	39
High fuel reactor pressure	>50 psi (>41 psig)	41
High fuel level (standby pump)	Maximum pumping level	45
Low fuel level (standby pump)	Minimum pumping level	46
High pump pressure (standby pump)	>5 psi	47
Pump power (standby pump)	>50 amps	48
High temperature differential across reactor tubes	>235°F (>400°F)	49
High fuel temperature	>1500°F	51
Low heat exchanger fuel temperature	<1100°F	52
High heat exchanger tube temperature	>1500°F	53
Low heat exchanger tube temperature ^a	<1150°F	54
Pump lubricant (main pump)	<4 gpm (<2 gpm)	65
Pump coolant (main pump)	<2 gpm (<2 gpm)	66
Pump lubricant (standby pump)	<4 gpm (<2 gpm)	69
Pump coolant (standby pump)	<2 gpm (<2 gpm)	70

^aThe helium blower was interlocked so that when the fuel temperature decreased below this temperature the blower speed was reduced to zero until the fuel temperature exceeded 1150°F.

d. Sodium System Annunciators

	Set Point	Announcer No.
Pump power (main pump)	>50 amp	9
Low sodium flow (back loop)	<100 gpm	10
High heat exchanger water temperature	>160°F	11
Low heat exchanger sodium temperature	<1100°F	12
High sodium level (main pump)	Maximum pumping level	13
Low sodium level (main pump)	Minimum pumping level	14
High pump pressure (main pump)	>65 psi	15
Pump power (standby pump)	>50 amp	17
Low sodium flow (front loop)	<100 gpm	18
High heat exchanger water temperature	>160°F	19
Low heat exchanger sodium temperature	<1100°F	20
High sodium level (standby pump)	Maximum pumping level	21
Low sodium level (standby pump)	Minimum pumping level	22
High pump pressure (standby pump)	>65 psi	23
High sodium temperature differential across reactor	>60°F	24
Low sodium reactor pressure	<60 psig (>48 psig)	42
Pump lubricant (main pump)	<4 gpm (<2 gpm)	67
Pump coolant (main pump)	<2 gpm (<2 gpm)	68
Pump lubricant (standby pump)	<4 gpm (<2 gpm)	71
Pump coolant (standby pump)	<2 gpm (<2 gpm)	72

e. Miscellaneous Annunciators

	Set Point	Announcer No.
Sodium system helium blower	Sodium system blower on before fuel system blower	1
Pit oxygen	<90% He (Disconnected)	2
Pit humidity	>10% relative humidity	3
Helium supply low	<500 psi	4
Space cooler water temperature	>160°F	5
Low water flow (any of 5 systems)	>10% below design	6
Rod cooling water temperature	>160°F	7
Low reservoir level	<16 psi	8
Stack closed	<5 mph wind velocity or high ion chamber reading	55
Pit activity	0.8 μ c/cm ³	56
Monitrons	>12 mr/hr (>7.5 mr/hr)	57
Vent gas monitor	0.8 μ c/cm ³	58
Vent header vacuum	>29 in. Hg vacuum	59
Low nitrogen supply	<300 psi	60
Low air supply	<40 psi	61
DC-to-AC motor-generator set	Off	63
AC-to-DC motor-generator set	Off	64

SYSTEM OPERATING CONDITIONS³

1. Reactor

Fuel inlet temperature, °F	1315 (1209)
Fuel outlet temperature, °F	1480 (1522)
Mean fuel temperature, °F	1400 (1365)
Sodium inlet temperature, °F	1105 (1226)
Sodium outlet temperature, °F	1235 (1335)
Fuel flow through reactor (total), gpm	68 (46)
Fuel flow rate in fuel tubes (11.3 gpm), fps	4 (3)
Sodium flow through reactor, gpm	224 (150)
Heat removed from fuel, kw	1270 (1520)
Heat removed from sodium, kw	650 (577)
Fuel dwell time in reactor, sec	8.3
Fuel cycle time	
For 50% of fuel, sec	33.6 (47)
For rest of fuel, sec	46.4 (47)
Maximum fuel tube temperature, °F	1493
Maximum moderator temperature, °F	1530
Sodium circulating time, hr	1000 (635)
Fuel circulating time,* hr	1000 (462)

*After 462 hr of circulating time, the last 221 hr were attained after the reactor first became critical, and 74 of these after the reactor first operated above 1 Mw.

³The design values were taken from drawing A-3-0, "Primary Heat Disposal System," Flow Sheet, in which the physical properties of the fuel were assumed to be $\rho = 3.27 \text{ g/cm}^3$, $\mu = 7 \text{ to } 13 \text{ cp}$, and $c_p = 0.23 \text{ Btu/lb} \cdot ^\circ\text{F}$. The operating values were taken from the 25-hr Xenon run (Exp. H-8).

2. Fuel System

a. Fuel Loop

	Temperature (°F)	Pressure (psig)	Flow (gpm)
Reactor outlet	1450 (1522)	46	40
Heat exchanger inlet	1450 (1522)	34	20 ^a
Heat exchanger outlet	1150 (1209)	12	20
Pump inlet	1150 (1209)	2 (0.3)	40 (46)
Pump outlet	1150 (1209)	54	40
Reactor inlet	1150 (1209)	50 (39)	40

^aThere were two fuel-to-helium heat exchangers in parallel.

b. Helium Loop

	Temperature ^a (°F)	Pressure (in. H ₂ O)	Flow (cfm)
Fuel-to-helium heat exchanger No. 1 inlet	180	2.2	7,300
Fuel-to-helium heat exchanger No. 1 outlet	620	1.5	12,300
Helium-to-water heat exchanger No. 1 inlet	620	1.5	12,300
Helium-to-water heat exchanger No. 1 outlet	180	1.2	7,300
Fuel-to-helium heat exchanger No. 2 inlet	180	1.1	7,300
Fuel-to-helium heat exchanger No. 2 outlet	620	0.4	12,300
Helium-to-water heat exchanger No. 2 inlet	620	0.4	12,300
Helium-to-water heat exchanger No. 2 outlet	180	0.1	7,300
Blower outlet	180	2.3	7,300

^aThe helium passed through two temperature cycles in each loop.

c. Water Loop

	Temperature ^a (°F)	Pressure (psig)	Flow ^b (gpm)
Helium-to-water heat exchanger inlet	70 (61)	10	65 (103)
Helium-to-water heat exchanger outlet	135 (124)	8	65

^aThe water entered each heat exchanger at ambient temperature and was then dumped.

^bThere were two helium-to-water heat exchangers in parallel; total flow, 130 gpm.

3. Sodium System

a. Sodium Loop

	Temperature (°F)	Pressure (psig)	Flow (gpm)
Reactor outlet	1235 (1335)	58	224 (152)
Sodium-to-helium heat exchanger inlet	1235 (1335)	52	112
Sodium-to-helium heat exchanger outlet	1105 (1226)	51	112
Pump inlet	1105 (1226)	48 (36)	224
Pump outlet	1105 (1226)	65	224
Reactor inlet	1105 (1226)	60 (49)	224

b. Helium Loop

	Temperature (°F)	Pressure (in. H ₂ O)	Flow (cfm)
Sodium-to-helium heat exchanger inlet	170	4	2000
Sodium-to-helium heat exchanger outlet	1020	2	4700
Helium-to-water heat exchanger inlet	1020	2	4700
Helium-to-water heat exchanger outlet	170	0	2000
Blower outlet	170	4	2000

c. Water Loop

	Temperature (°F)	Pressure (psig)	Flow (gpm)
Helium-to-water heat exchanger inlet	70 (61)	10	77 (38.3)
Helium-to-water heat exchanger outlet	100 (114)	8	77

4. Rod Cooling System

a. Helium Loop

	Temperature (°F)	Pressure (in. H ₂ O)	Flow (cfm)
Rod assembly outlet	240		1270
Helium-to-water heat exchanger inlet	240		423 ^a
Helium-to-water heat exchanger outlet	110	0	333
Blower	110	13	1000 ^b
Rod assembly inlet	110		1000

^aThere were three heat exchangers in parallel.

^bCapacity of each of the two parallel blowers; however, the second blower was in standby condition.

b. Water Loop

	Temperature ^a (°F)	Pressure (psig)	Flow ^b (gpm)
Water-to-helium heat exchanger inlet	70 (61)	10	18 (17.6)
Water-to-helium heat exchanger outlet	100 (63)	8	18

^aThe water entered each heat exchanger at ambient temperature and was then dumped.

^bTotal flow for three parallel heat exchangers.

5. Water System

Equipment	Flow per Unit (gpm)	No. of Units	Flow (gpm)
Space coolers	7	8	56 (56)
Reflector coolant system	77	2	154 (77.6)
Rod cooling system	6	3	18 (17.6)
Fuel coolant system	65	2	130 (206)
Pump cooling systems	3	4	12 (13)
Total			370 (370.2)

MISCELLANEOUS

1. Welding Specifications^a

Process	Inert-gas, shielded-arc, d-c weld
Base metal	Inconel
Position	Horizontal rolled, fixed vertical, or horizontal
Filler metal	$\frac{1}{16}$ to $\frac{3}{32}$ in. Inconel rod (Inco No. 62 satisfactory)
Preparation of base metal	Machined, cleaned, and unstressed
Cleaning fluid	Trichloroethylene
Clearance in butt joints	$\frac{3}{32}$ to $\frac{1}{8}$ in. with 100 deg bevel
Clearance in lap joints	Flush at weld
Welding current	d-c, electrode negative, 38 to 80 amp
Electrode	$\frac{1}{16}$ to $\frac{3}{32}$ in. tungsten, 90 deg point
Shielding gas blanket	Argon, 99.8% pure; 35 cfh
Gas blanket beneath weld	Helium, 99.5% pure; 4 to 12 cfh
Welding passes	1 to 5
Welders qualifications	Welded or passed QB No. 1 ^b within 45 days

^aFor details, see *Procedure Specifications*, PS-1, ORNL Metallurgy Division, September 1952.

^b*Operation Qualification Test Specifications*, QTS-1, ORNL Metallurgy Division, September 1952.

2. Stress Analysis

a. Moments and Stress in the Pressure Shell Ends

Maximum radial stress (per psi pressure)	85 psi
Minimum radial stress (per psi pressure)	-80 psi
Maximum radial moment (per psi pressure)	80 in.-lb
Minimum radial moment (per psi pressure)	-55 in.-lb
Maximum tangential stress (per psi pressure)	70 psi
Minimum tangential stress (per psi pressure)	-18 psi
Maximum tangential moment (per psi pressure)	180 in.-lb
Minimum tangential moment (per psi pressure)	-10 in.-lb

b. Stress in the Pressure Shell Vessel

Maximum circumferential stress (per psi pressure)	14 psi
Minimum circumferential stress (per psi pressure)	-23 psi
Maximum longitudinal stress (per psi pressure)	13 psi
Minimum longitudinal stress (per psi pressure)	-75 psi

c. Summary of Pipe Stresses^a

Line No.	Pipe Size (in.)	Maximum Cold Prestress (lb)	Maximum Hot Prestress (lb)	Temperature ^b (°F)	Pressure (psig)
Fuel Piping					
111	2	3,850	2,170	1500	39
112	1½	11,230	6,450	1500	34
113	1½	24,300	13,900	1400	34
114	1	15,400	8,850	1500	34
115	1	38,000	19,600	1375	11
116	1½	28,200	14,500	1325	60
117 ^c	2				11
118	2	28,000	12,800	1500	11
119	1½	22,000	11,300	1325	60
120	2	15,350	7,900	1325	60
Sodium Piping					
303	2½	5,260	3,690	1050	58
304	1½ and 2	4,280	3,000	1050	58
305	1½ and 2	4,300	3,020	1050	58
306	1½, 2, 3	13,250	9,310	1050	51
307	2	4,170	2,935	1050	65
308	1½, 2, 3	13,250	9,310	1050	51
309	2	2,210	1,550	1050	65
310	2½	4,430	3,110	1050	65
313	2	28,600	16,400	1325	51

^aAll piping ASI Schedule 40.

^bNot all temperatures and pressures given were reactor design point values.

^cThis line consisted primarily of pipe connections and was not stress analyzed.

3. Fluoride Pretreatment

Treatment	Purpose	Time (hr)	Temperature (°C)
Hydrofluorination	Remove water	2	RT to 700
Hydrogenation	Reduce oxides and sulfates	2	700 to 800
Hydrofluorination	Fluorinate oxides and sulfates	4	800
Hydrogenation	Remove HF, NiF ₂ and FeF ₂	24 to 30	

Appendix C

CONTROL SYSTEM DESCRIPTION AND OPERATION¹

F. P. Green, Instrumentation and Controls Division

CONTROL SYSTEM DESIGN

The control system designed for the ARE had to be able to maintain the reactor at any given power and, when necessary, had to also be able to overcome quickly the excess reactivity provided for handling fuel depletion, fission-product poisons, and power level increases. The motor speeds and gear ratios were set so that safety-rod withdrawal could not add $\Delta k/k$ at a rate greater than 0.015%/sec. The rods were designed to contain 15% $\Delta k/k$, and the control system was designed to limit the fast rate of regulating rod withdrawal to be used for high-power operation to an equivalent $\Delta k/k$ of 0.1%/sec, with a maximum $\Delta k/k$ of 0.40%, which is one dollar, for steady-state fuel circulation. For the critical experiment and low-power operation, the regulating rod withdrawal rate was limited to an equivalent $\Delta k/k$ of 0.01%/sec.

A fundamental distinction was made between insertion and withdrawal of the shim rods. Either the operator or an automatic signal could insert any number of rods at any time, whereas withdrawal was always subject to both operator and interlock permission. Withdrawal was limited, moreover, to what was needed or safe under given circumstances.

Quantitative, rather than qualitative, indication of control parameters was used where possible. Where feasible, only one procedure of manual control was mechanically permitted to minimize time-consuming arbitrary decisions on the operator's part.

The control philosophy of paramount importance in the general operating dynamics was the use of only absorber rods to control the nuclear process and the use of only helium coolant to control the power generation.

Most of the control and safety features of the ARE were similar to those of other reactors. Considerable care was exercised in the design of instrument components, control rods, and control circuits to make them as nearly fail-safe as was practical. An instrumentation block diagram of the reactor control system is shown in Fig. C.1,

in which the reactor is shown to be subject to effects of the control rods and to certain auxiliary facilities. The reactor, in turn, affected certain instruments which produced information that was transmitted to the operator and to the control system. The operator and the control system also received information from indicators of rod position and motion. By means of the operator's actions and instrument signals, the control system transmitted appropriate signals to the motors and clutches. The actuators located over the reactor pit in the actuator housing, in turn, affected the reactor by corresponding rod motions which closed the control loop. In addition to the above indications that were at the operator's disposal on the console, there were many annunciators physically located along the top of the vertical board in the control room. The group of eight annunciators labeled "Nuclear Instruments" were provided to indicate that conditions were improper for raising the operating power level or that improper operating procedures had caused safe limits to be exceeded.

INSTRUMENTS DESCRIPTION

The reactor instruments discussed in the following have been arbitrarily limited to those directly concerned with the measurement of neutron level and with fluid temperatures and flows associated with the reactor. The parallel-circular-plate and compensated ion chambers, the fission chambers, and BF₃ counter were of ORNL design, and, except for the latter two, were identical to those used in the MTR and LITR.² Since the fission chambers were located in a high-temperature region within the reactor reflector, a special chamber had to be developed that could be helium cooled. The compensated ion chambers and the log N and period meters had a useful range of approximately 10⁶, and thus they indicated fluxes of 10¹⁰ n/cm².sec (maximum) and 10⁴ n/cm².sec (minimum). The BF₃ counter had a maximum counting rate of about 10⁵ n/sec and the fission chambers and count rate meters were capable of covering

¹This appendix was originally issued as ORNL CF-53-5-238, ARE Control System Design Criteria, F. P. Green (May 18, 1953), and was revised for this report on March 7, 1955.

²S. H. Hanauer, E. R. Mann, and J. J. Stone, *An Off-On Servo for the ARE*, ORNL CF-52-11-228 (Nov. 25, 1952).

a range of 10^{11} if they were withdrawn from the reflector as the flux increased. Since the count rate meter has a long integrating time and the resultant time delays would make it an unsatisfactory instrument for automatic control, it was used as an adjunct to manual control.

The instantaneous positions of the four control rods were reported to the operator by selsyns. In addition, the positions of the rods with respect to certain fixed mechanical limits were detected by means of lever-operated microswitches. The limit-switch signals tied in with the control system and with signal lights on the control console. The upper limit switches on the three shim rods operated when the rods were withdrawn to about 36 in. from the fully inserted position. Their exact location was adjusted to provide optimum sensitivity of shim rod action. The lower limit switches served to cut the rod drive circuits when the magnet heads reached the magnet keepers.

The seat switches operated indicating lights on the console, which served only to indicate the proximity of the pneumatic shock absorber piston to the lower spring shock absorber. The lights told the operator the immediate effectiveness of a "scrammed" or dropped rod and, hence, that the rod had not jammed on its fall into the reactor core.

The regulating rod was equipped with two travel limit switches whose actions tied in intimately with the manual and automatic regimes of the servo-control system, which is described in a following section.

Thermocouples were located at many points on the reactor and the heat exchangers to monitor the fuel temperatures, since temperature extremes or low flow rates could have resulted in serious damage to the reactor. The temperatures were recorded, and electrical contacts in the recorders interlocked with the scram circuit to provide shutdown if the reactor inlet temperature dropped below 1100°F or the outlet temperature exceeded 1550°F. The operator was also warned by an annunciator alarm of low helium pressure in the rod-cooling system because loss of cooling would have increased the danger of a rod jamming due to mechanical deformation.

CONTROLS DESCRIPTION

Motion of the shim rods or the regulating rod was obtained from two energy sources, gravitational and electromechanical. Rod motion by safety

action was obtained by gravitational force upon release of the shim rods from their holders as a result of de-energizing the electromagnetic clutches.

The three shim rods, each with its magnet, were subject to a number of different possible sources of safety signal. The necessary interconnecting circuitry was centered about an "auction" or "sigma" bus. Instrument signals were fed to this bus by sigma amplifiers. The sigma bus may be said to go along with the "highest bidder" among the grid potentials of the sigma amplifiers. This important auction effect allowed all rods to be dropped by any one safety signal. If all three amplifiers and the three magnets had been identical in adjustment and operation, all three rods would have dropped simultaneously as the sigma bus potential rose or fell past some critical value. Usually, only one of the rods dropped initially, and the others were released by interlocked relay action.

Two kinds of scrams were possible: "fast" scrams caused by amplifier action and "slow" scrams caused by interruption of magnet power as the result of the action of relays. In a fast scram the shim rods were dropped when the reactor level reached or exceeded a specified flux level, as determined by the safety chambers. The signal from the safety chambers was amplified by the sigma amplifiers and subsequently caused the magnet current to become low enough to drop the rods. The slow scram was the actual interruption of power to the magnet amplifiers by relay action. This relay action could be caused by temperatures in excess of safe limits or stoppage of fuel flow.

The shim rod drives were 3-wire, 115-v, instantaneously reversible, capacitor-run motors rated at 1800 rpm. The shim-rod head, or actuator assembly, was a worm gear driven through a gear reducer at slightly less than $2\frac{3}{4}$ in./min. The sequence of shim rod scram, rod pick-up, and withdrawal required a minimum of 25 min.

Both individual and group activation of shim rods were selected in preference to group control alone to permit increased (vernier) flexibility in approaching criticality. Group shim rod action would have made difficult the control of flux shading throughout the reactor, particularly on rod insertion, since, upon cutting the motor power, the friction characteristics of the three drives would have caused the rods to coast to different levels.

The regulating rod drive consisted of two Diehl Manufacturing Company, 200-w, instantly reversible,

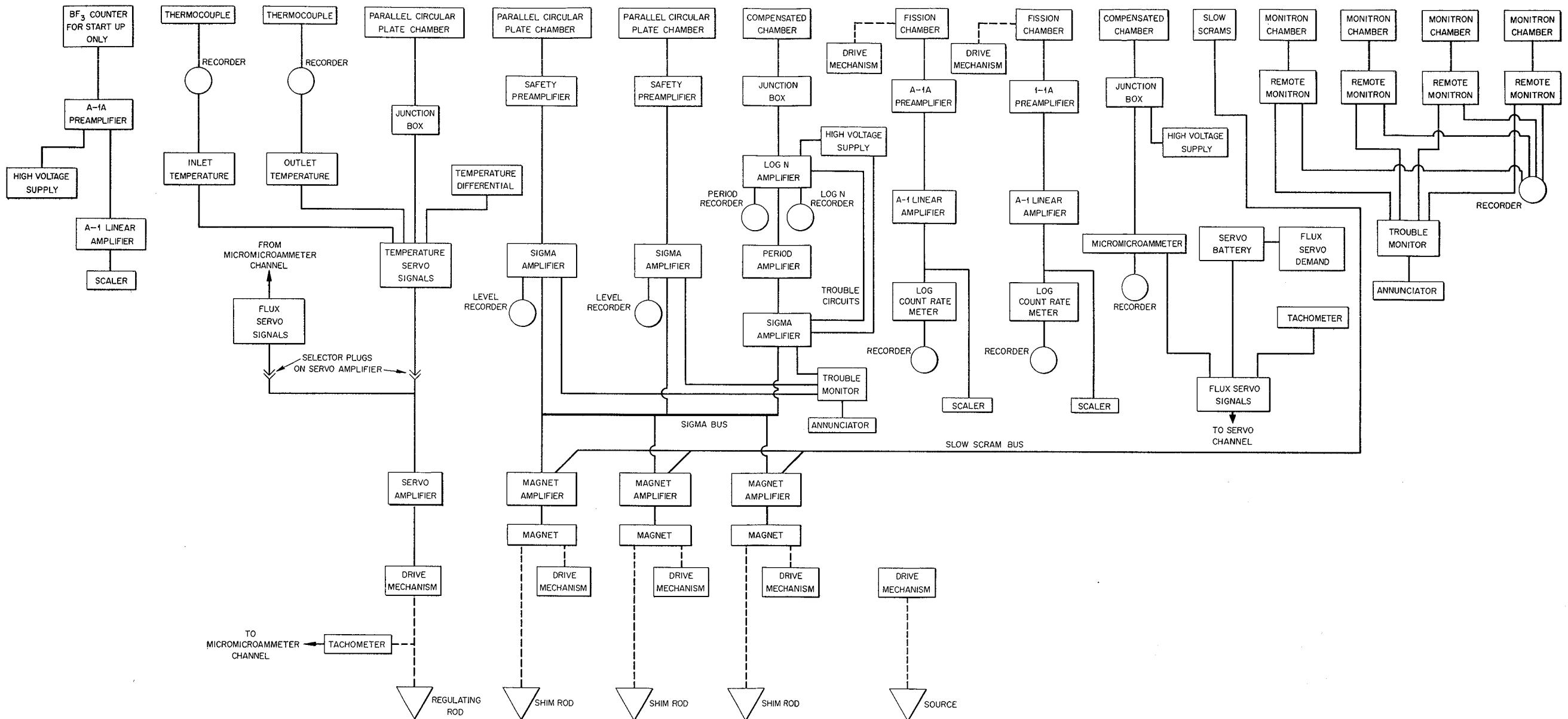
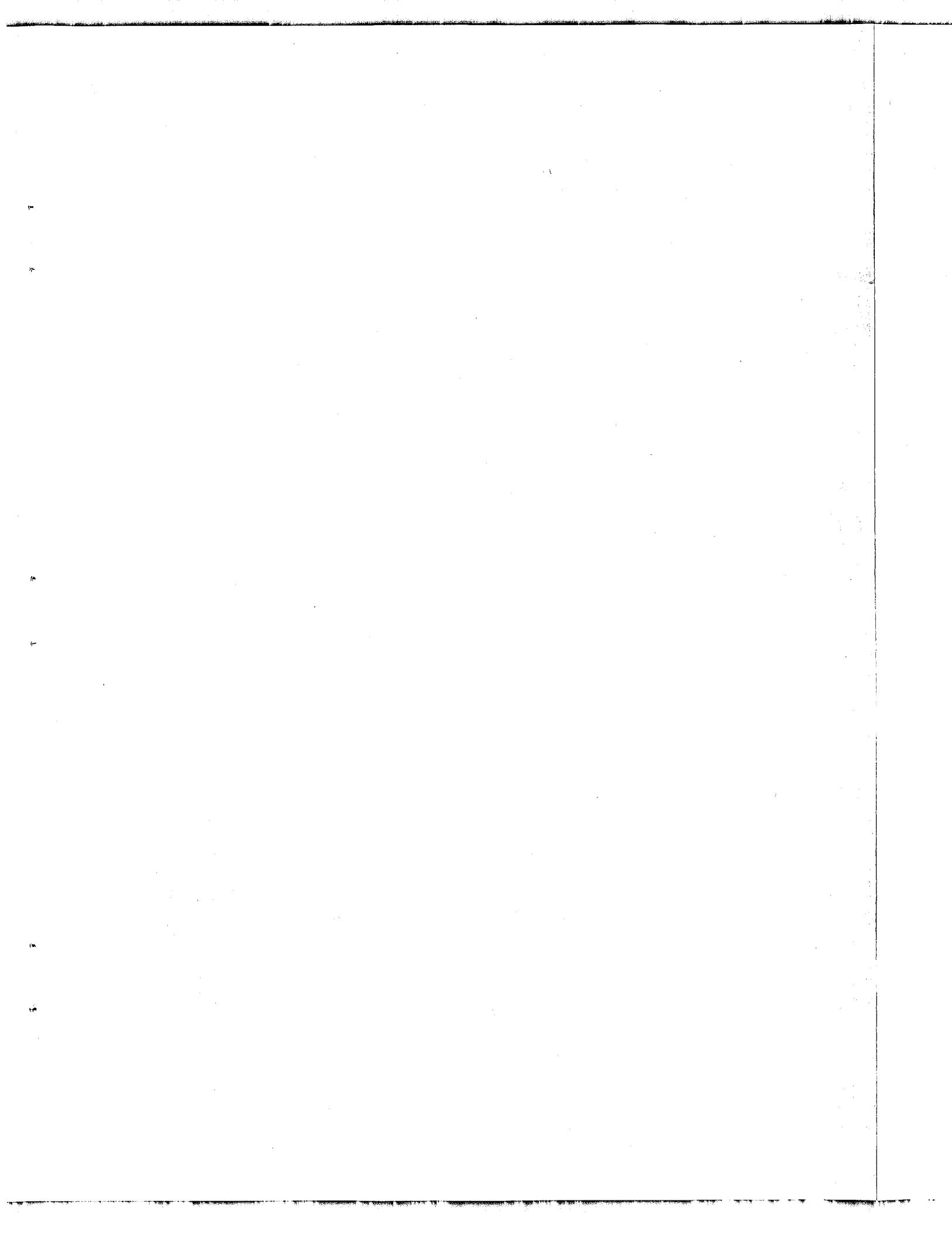


Fig. C.1. Control System Block Diagram.



two-phase servomotors that operated from reversing contactors which received their actuation from a mixer-pilot relay located in the servo amplifier. Only one of the motors operated at a time, depending on whether the temperature or flux servo was coupled into the control loop. For the flux servo operation, an additional speed reducer was used so that the speed of the rod was one tenth that available for temperature servo operation.

Initiation of the flux servo "auto" regime was contingent on reactor power great enough to give a micromicroammeter reading of more than 20 and a servo-amplifier error signal small enough so that no control rod correction was called for. With the servo on auto the regulating rod upper or lower limit switches actuated an annunciator. Although not used in the experiment, initiation of the temperature servo auto regime was contingent on reactor power greater than a minimum controllable power ($> 2\% N_F$) and a servo-amplifier error signal small enough that the servo would not call for rod motion.

The rod-cooling system consisted of a closed loop for circulating helium through the annuli around the shim rods, the regulating rod, and the fission chambers and then through three parallel helium-to-water heat exchangers. The helium was circulated by two 15-hp a-c motor-driven positive-displacement blowers. The motors were controlled from the reactor operating console.

The fuel and reflector coolant temperatures were also controlled from the console. The helium coolant removed heat from fuel and sodium system heat exchangers and passed it to an open-cycle helium-to-water heat exchanger, from which the water was dumped. The helium in the fuel system was circulated by an electric-motor-driven fan that was controlled from the console. The helium in the sodium system was circulated by two hydraulic-motor-driven blowers for which only the on and off controls were located on the console.

In order that the reactor operation would be as free as possible from the effects of transient disturbances or outages on the purchased-power lines, a separate electrical power supply was available for the control system. The supply consisted of a 250-v, 225-amp, storage-battery bank of 2-hr capacity. The bank was charged during normal power source operation by a 125-kw motor-generator set. This emergency d-c supply fed emergency lights and a 25-kw motor-generator set to supply instrumentation power (120/208 v, single

phase alternating current) during purchased-power outages. An auto-transfer switch provided an automatic switchover transient of several cycles upon loss of the purchased-power source. The auto-transfer switch automatically returned the system to normal power 5 min after resumption of purchased-power supply. The system could be returned to normal power manually at any time after resumption of the purchased-power supply.

CONSOLE AND CONTROL BOARD DESCRIPTION

The control console was made up of two large panels, one to the right and one to the left of the operator's chair, and eight subpanels directly in front of the operator, Fig. C.2. Over the top of the console, the operator also had a full view of the vertical board of instruments which indicated and recorded nuclear parameters and pertinent process temperatures. The rotary General Electric Company type SB-1 switches used were of the center-idle, two- and three-position variety. They were wired so that clockwise rotation produced an "increase" in the controlled parameter; such operation has been described as potentially dangerous. However, the scram switch, an exception, produced a scram in either direction of rotation.

The top row of the left-hand panel of the console contained the source-drive control (Fig. C.2). In the second row the first two switches were the controls for the two-speed rod-cooling helium blowers, and the third switch was the on-off control for the electric motors which were the prime movers for the hydraulic-motor-driven blowers. In the bottom row were the group control for the three shim rods and the annunciator acknowledge and reset pushbuttons.

The center eight subpanels were identical in size and shape and contained the six selsyns which indicated the rod and fission chamber positions and the two servo control assemblies. The temperature calibrated potentiometer located near the panel center was used to set the fuel mean temperature for automatic, servo-controlled operation. The subpanel on the extreme left contained the flux vernier (not shown) used to set flux demand into the flux servo system for controlled operation. The dial was calibrated to correspond to a setting of from 20 to 100 on the micromicroammeter Brown recorder. Associated with all controls were the necessary limits-of-travel indicating lights, along with the on-off and speed-range indicators.

The right-hand panel contained the switches most

closely associated with the fuel system and the energy removal controls. In the upper row were the switch for the fuel-loop helium-blower prime mover, which was a 50-hp electric motor, the scram switch, and the by-pass switch (not shown on Fig. C.2). The by-pass switch was provided to permit the fuel-loop prime mover to be run, even though the reactor power was low, to remove the afterheat that was expected to be present after a shutdown. The bottom row on the right-hand panel contained the fuel-system-helium blower speed control, the selector switch for barrier-door control, and the barrier-door drive control.

The four panels in the center of the vertical board contained the 12 recorders which pertained to the reactor. They were, left to right, top row: reactor inlet temperature, reactor ΔT , reactor outlet temperature, reactor mean temperature; center row: count rate No. 1, pile period, safety level No. 1, and micromicroammeter. In the bottom row there were: count rate No. 2, log N , safety level No. 2, and control rod position.

The range of flux through which the reactor passed from the insertion of the source to full-power operation was so great, more than 10^{13} , that

several classes of instruments were used. The normal flux (N_F) was arbitrarily designated as 1, and then the first, and lowest, range encountered was the source range, from somewhat less than 10^{-13} to 10^{-11} ; the second was the counter range, from 10^{-11} to 10^{-6} ; the third was the period range, from 10^{-6} to 3.3 times 10^{-3} , and the last was the power range, from 3.3×10^{-3} to 1. At greater than 10^{-5} , in the period range, the servo system could be put into auto operation if desired.

CONTROL OPERATIONS

In the operation of the ARE, operator initiative was overridden by two categories of rod-inserting action: scram, the dropping of safety rods; and reverse, the simultaneous continuous insertion of all three shim rods, which was operative only during startup. The fast scram was in a class by itself, being the ultimate safety protection of the reactor, and could never be vetoed by the operator. The various occasions for automatic rod insertion and annunciation for nuclear trouble are listed in Table C.1.

There were five interlocks between nuclear reactor control, fuel and moderator coolant pumping,

TABLE C.1. CAUSES OF AUTOMATIC ROD INSERTION AND ANNUNCIATION

	Fast Scram	Slow Scram	Reverse	Annunciation
Neutron level ($1.5 N_F$)	x			x
Neutron level ($1.2 N_F$)				x
1-sec period	x			x
5-sec period		x	x	x
Fuel temperature ($>1550^{\circ}\text{F}$)	x			x
Loss of fuel flow (power $>10 \text{ kw}$)	x			x
Loss of control bus voltage	x			x
Loss of purchased power	x			x
Manual scram	x			x
Reactor power ($\Delta T > 400^{\circ}\text{F}$)				x
Fuel temperature ($<1100^{\circ}\text{F}$)	x			x
Fuel helium blowers on without reflector helium blowers on				x
Servo off range				x
Rod coolant helium off				x
Count rate meter off scale				x
Safety circuit trouble				x

PHOTO 45056

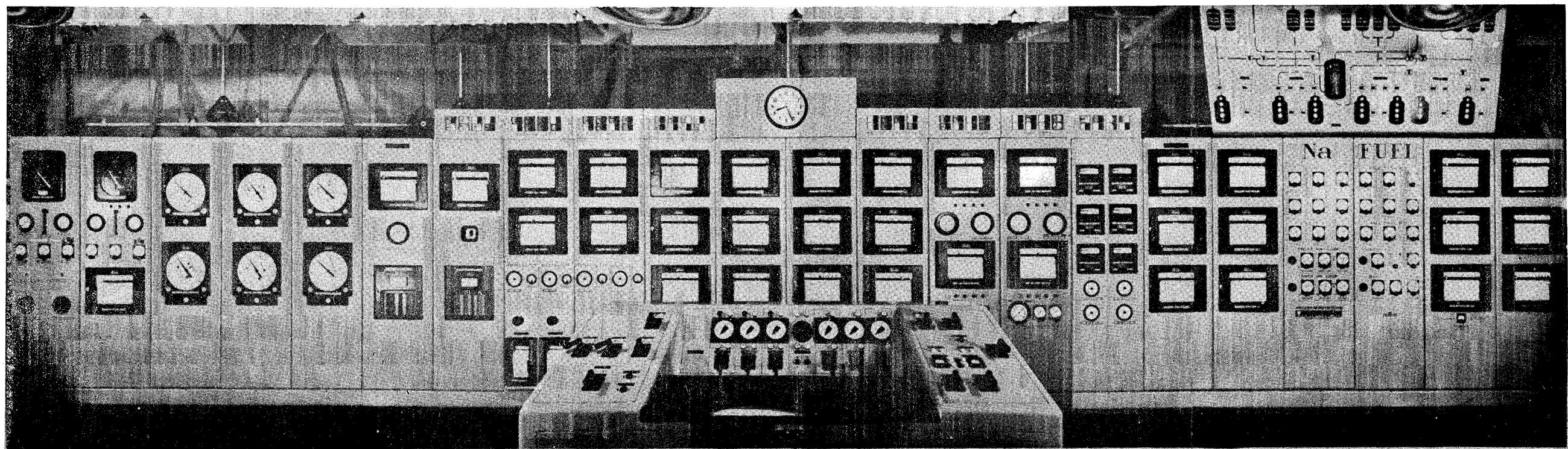
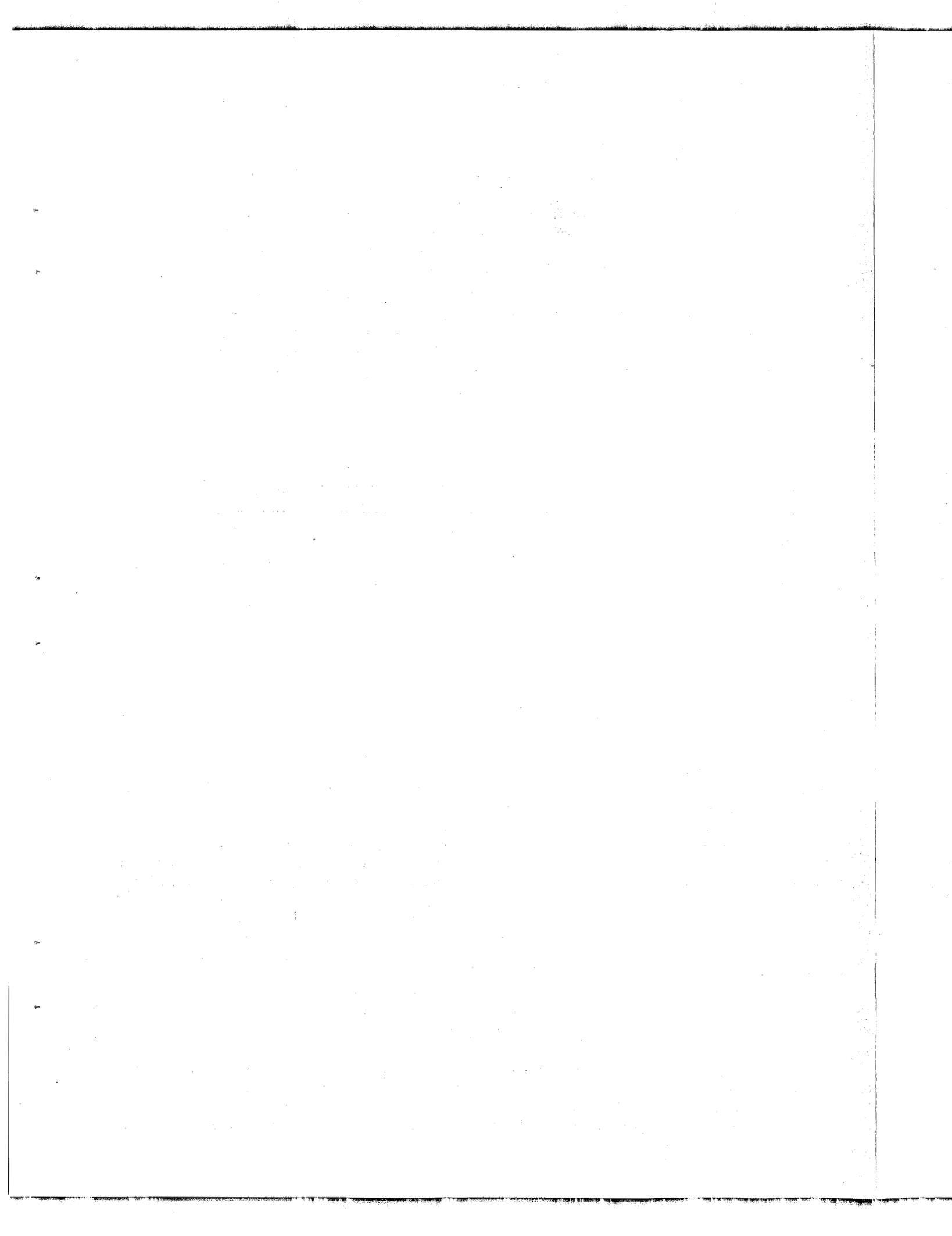


Fig. C.2. Control Console and Vertical Board.



and helium-cooling operation. (1) When operating at power (above 10 kw), loss of fuel flow would have initiated a slow scram. (2) Loss of fuel flow would have, likewise, removed a permissive on operation of the fuel-loop helium-blower prime mover. (3) Excessive deviation of fuel temperature from set point would have produced a scram for either too high or too low a temperature. Low fuel temperature would also cause the helium pilot motor to run the magnetic clutch control for the helium blowers to the zero position and thereby stop the blowers and thus stop fuel cooling. (4) Moderator coolant flow was interlocked with the moderator coolant helium blowers to prevent helium circulation when the sodium flow was low or stopped. A slug of cold sodium would have entered the reactor when circulation was restarted if this precaution had not been taken. (5) Permissives on increasing helium flow were fuel temperature in

range, prime movers operating, reactor in power range, and power greater than 10 kw. The operator was notified by the "permit" light when these conditions were satisfied. A pilot decrease was not interruptible by the operator until the cause of the automatic action was alleviated.

The elementary control diagram is shown in Fig. C.3. The various relay and limit switches referred to in Fig. C.3 are described in Tables C.2 and C.3, respectively. These tables and Fig. C.3 show the procedural features of the control system as it applied to operator initiative. This system was divided into channels, each consisting of one or more relays actuated by the operator subsequent to properly setting up interlock permissives. The interlocks often depended upon the aspects of relays in other channels. Primarily, the channels corresponded to a mechanical unit involving a rod control, a process loop control, or an instrument system control. The channels were:

1. Two fission chamber drives
 - a. Manually actuated.
 - b. Travel limit switches, panel-light indicated.
 2. Servo control system
 - a. Auto initiated manually by permission of power greater than $2\% N_F$, for temperature servo, and power great enough to give a reading of more than 20 on the micromicroammeter recorder for any scale range, for flux servo, and a demand error close to zero (neither light burning) for either servo system.
 - b. Auto regime sealed-in light indicated if initiated with proper conditions and power remained greater than that specified in 2a above.
 - c. Manual regime regained by manually dropping out seal or by manipulation of control rod switch.
 - d. Reverse interrupted rod withdrawal by any means and caused rod insertion.
 - e. Manual control rod overrode automatic regime and dropped out seal.
 - f. Permits on manual rod control required that either the reactor to be at a power level greater than $10^{-5} N_F$ or one count rate meter be "on scale."
 3. Slow scram
 - a. A series-parallel relay system was used to initiate a scram. This system was used because a large number of series contacts would have been inducive to false drop-outs and hence false scrams. The three most urgent criteria calling for scram had to be fail-safe and were therefore placed in the series-connected section.
 - b. R-16 was inactive in the operating regime; R-17 and R-18 were normally actuated and were responsive to manual scram, scram reset, fuel temperature extremes, and R-16.
 4. Reverse, R-23 and R-24, plus an indicator light
 - a. Operated all three rods if the by-pass switch was in "normal" and
 - (1) the group insert switch was closed, or
 - (2) a slow scram occurred (equivalent to a scram follower), or
 - (3) the servo system was in the manual regime; the reactor power was less than 10 kw; and a period of less than 5 seconds occurred.
- On initial startup, No. a(3) initiated the reverse at any power level (due to jumper-shorted

- contact) until a negative temperature coefficient of reactivity was proved.
- b. The by-pass switch prevented reverse (but not slow scram) when in "by-pass" position.
5. Shim rod withdrawal
- a. Permissives were:
- (1) no reverse in progress,
 - (2) reading on-scale on at least one count rate meter or neutron level greater than $10^{-5} N_F$
 - (3) no manual insertion in progress,
 - (4) rod heads not resting on upper travel limits.
6. Shim rod insert
- a. Permitted if heads not on lower travel limits.
 - b. Actuated individually and manually.
 - c. Actuated together by any action operating reverse.
7. Fuel-system helium-blower prime movers
- a. The prime movers could be started by S-13 if
 - (1) clutch relays were actuated (rods "hung"), or if by-pass switch S-5 was on by-pass,
 - (2) helium blower speed lower limits were closed, and
 - (3) fuel flow was not below 20 gpm.
 - b. The prime movers were automatically turned off if a shim rod was dropped or fuel flow dropped below 20 gpm.
 - c. Relay R-38 started the prime movers by activating the starter relay RF-1 located in the basement.
8. Helium pilot controls (power-loading system)
- a. Permit indicators on power increase were lit if
 - (1) the reactor level was greater than 10 kw or the by-pass switch was set on by-pass,
 - (2) the prime movers were running, and
 - (3) the fuel temperature was above 1100°F.
 - b. Power increase from the coolant system could be demanded if
 - (1) the permit lights were on and
 - (2) pilot switch, S-14, was thrown to "increase."
 - c. If the power decreased and the controls were not already on shut-off limits, the helium circulation would be shut off.
 - (1) manually by using switch S-14, or
 - (2) automatically by whichever system suffered from low fuel temperature, from prime mover cut-out, or from low power (<10 kw), since by-pass switch contact S5-3 was closed during normal critical and power operation. Low fuel temperature interlocks automatically decreased the corresponding helium pilot controls if the fuel dropped below the critical temperature at either of the two heat exchangers.
9. The by-pass switch function was somewhat obscure since it occurred in the prime movers, pilot controls, and reverse circuits. Its inclusion resulted from the possibility of requiring additional fuel cooling following a shutdown and after an extensive running period at power level. A large gamma heat source, primarily in the moderator (because of its very large heat capacity), called the afterheat, remained in the reactor immediately following power operation.
- By using both hands, the operator could throw and hold S5 on by-pass while he restarted the prime movers and subsequently increased the helium pilot controls to such a point that the temperature leveled off.
- The by-pass circuits permitted testing of cooling system control circuits and presetting of cooling system control limits while the reactor was shut down and also permitted the vital subcritical test for fuel temperature coefficient of reactivity.³

³Wm. B. Cottrell and J. H. Buck, ARE Hazards Summary Report, ORNL-1407 (Nov. 20, 1952).

The use of the manual reverse cut-out, S5-6, operated by throwing the by-pass switch, was divorced from the above considerations and devoted only to test operation of the shim rod motors at shutdown, at low power, or with the magnet amplifiers turned off.

10. Source drive

- a. Manually actuated.
- b. Travel limit switches, panel-light indicated.

REACTOR OPERATION

The preliminary operating plan for the ARE was described in ORNL-1844.⁴ In the check operations, considerable time was spent in loading the inert fuel carrier and in the subsequent shakedown run. Critical loading, subcritical measurement of fuel temperature coefficient, regulating rod calibration, zero-power operation at 1200 to 1300°F, and power operation are described in Appendix D.

In the starting of a freshly loaded reactor the operator is most concerned about a reliable neutron signal. Attention must therefore be given to assuring that the fission chambers are in their most sensitive positions, and that they are giving a readable signal on the scalers or count rate meters. It is imperative that the source be inserted for the earliest indication of subcritical multiplication to be seen during the first startup. Use of the source in subsequent experiments becomes less important as the history of the reactor operation builds up.

For a normal, intentional shutdown the operator had the choice of a variety of procedures. For every scram, however, the interlocks of the system were such that the helium flow in the fuel-to-helium heat exchangers was cut off by opening the electrical circuits of the motors. This action was necessary to prevent the fuel from freezing in the heat exchangers. The various slow scrams included the following: (1) maximum reactor outlet temperature, (2) minimum reactor inlet temperature, (3) a 1-sec period, (4) N_F greater than 3.0 Mw, (5) fuel flow below 20 gpm. A 5-sec period inserted the shim rods, which decreased $\Delta k/k$ at a rate of 0.015%/sec, and operated only during low-level startup.

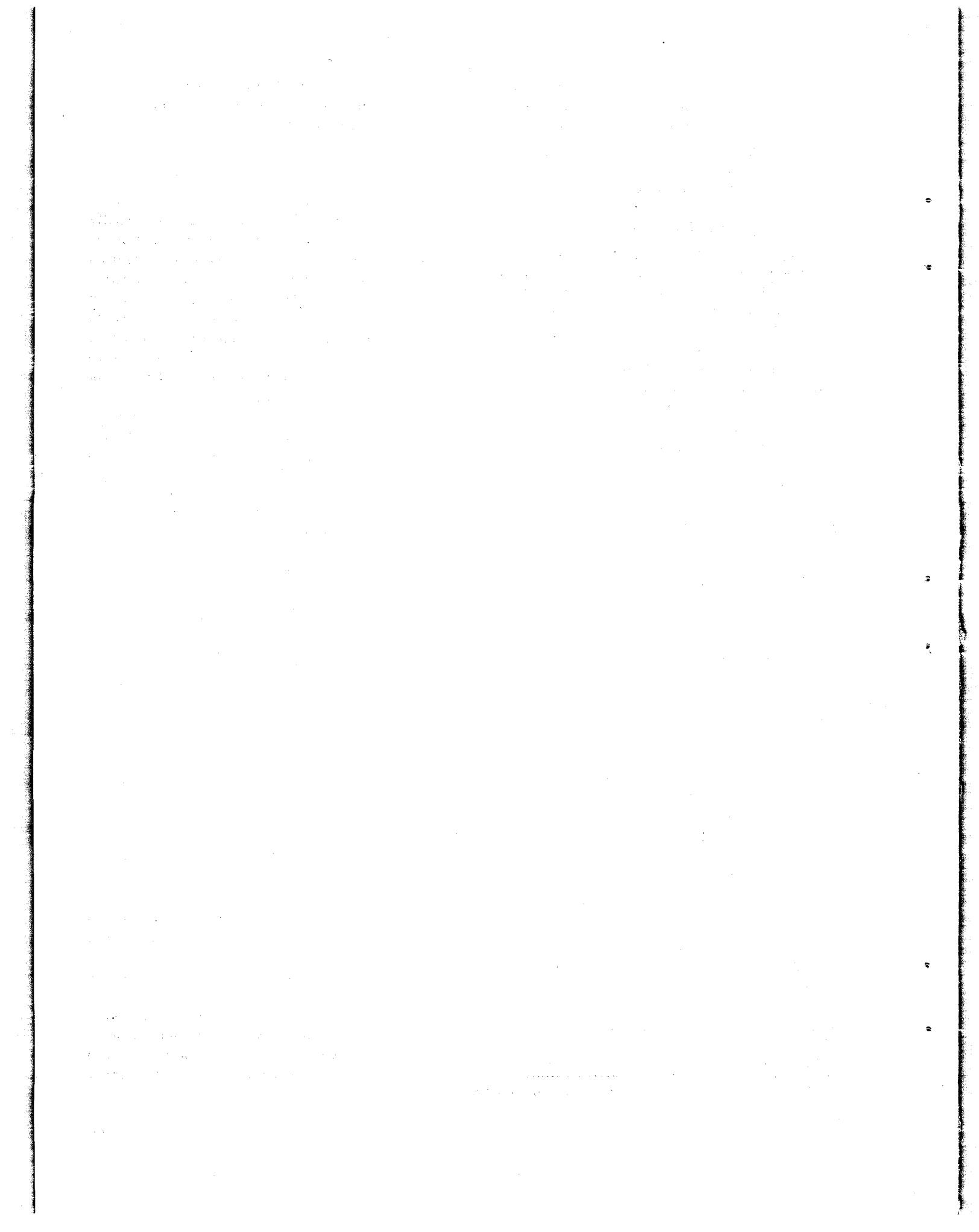
In addition to the process signals which initiated slow scrams, there were several other potential process malfunctions for which it might have been desirable to scram the reactor. However, the action to be taken in these situations was left up to the decision of the operator. There were two reasons for not putting these process malfunctions

on automatic scram. First, sensory signals usually lag the event to such an extent that a fast scram cannot provide better protection than a delayed scram. Second, reaction to the signals requires limited judgment. An annunciator alarm signal was provided to draw the operator's attention to the possible difficulty for each case that would have required limited judgment. The cases were the following: (1) pronounced changes in differential temperatures between reactor outlet tubes, (2) lowering level in any surge tank, (3) rising level in any surge tank, (4) alarm from a pit radiation monitor or monitron, (5) high oxygen concentration or humidity in the pits.

The operation of placing the "position"-type regulating rod servo system on automatic control in any part of the power range above 2% N_F , for temperature servo, and a micromicroammeter recorder reading of greater than 20 on any scale, for flux servo, was arranged to require that the reactor to be on a stable, infinite period. In the normal course of events, the rod should have been manually set at mid-range. Six d-c voltage signals were fed into the servo amplifier, three from the servo ion chamber, inlet temperature recorder, and outlet temperature recorder, one from the voltage supply adjusted by the "temperature demand" potentiometer, and two from the flux demand and micromicroammeter recorders. The operator therefore had a unique temperature setting for each level of power operation that produced "zero error" in the amplifier output, and hence no "error"-light indications and no demand for rod movement. It was at this setting that the servo "auto" regime could be initiated. A small change in reactor mean temperature or flux level could be effected in the auto regime by resetting the temperature demand or flux demand potentiometers, but the power level could not be changed.

No clear line could be drawn between normal operation and operation under difficulty. A few of the situations in which the operator would have expected to feel more than average need for attention to instrument signals and control actions were loss or interruption of power, automatic shutdown

⁴Design and Installation of the Aircraft Reactor Experiment, ORNL-1844 (to be published).



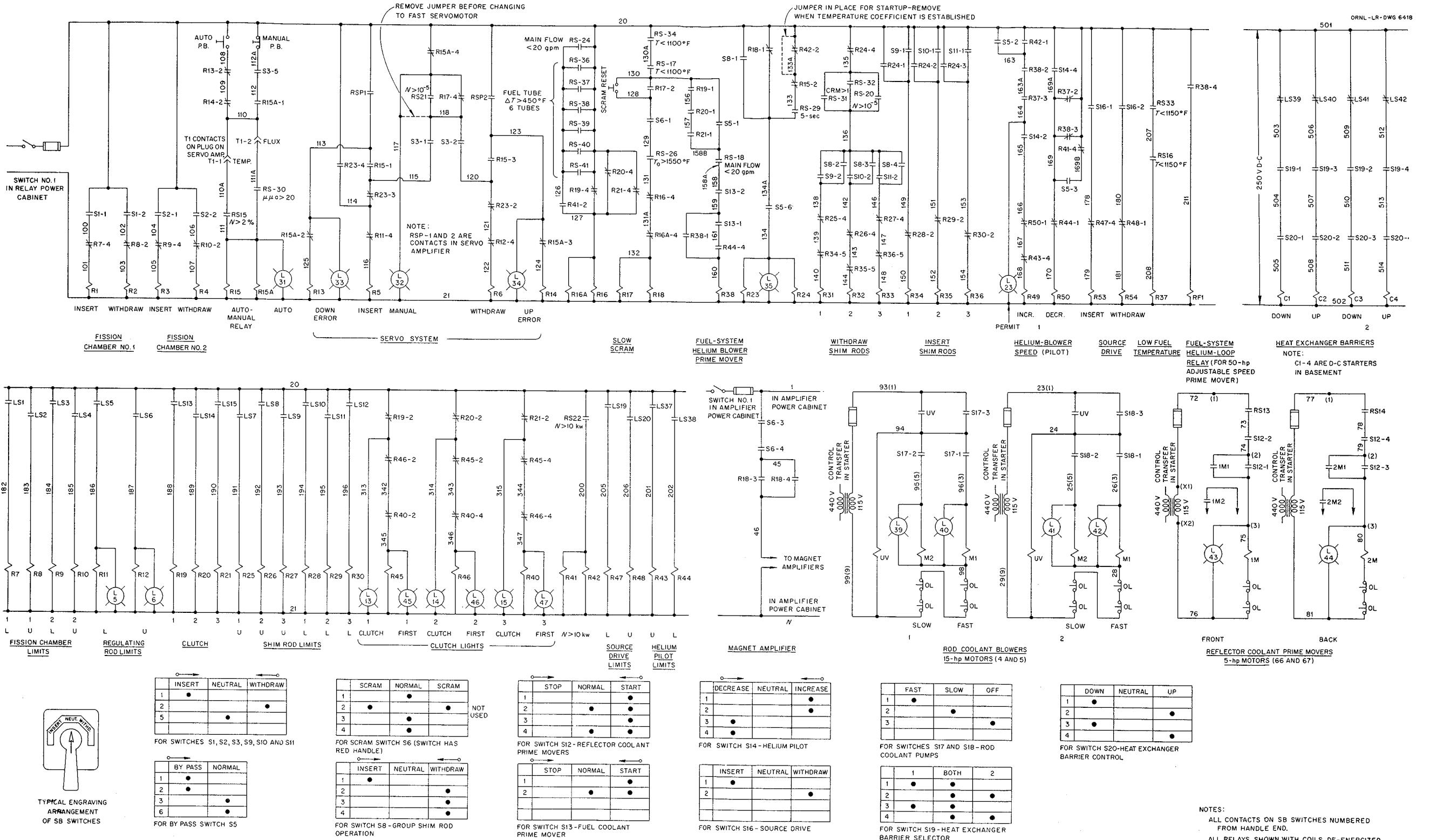


Fig. C.3. Elementary Control Diagram.

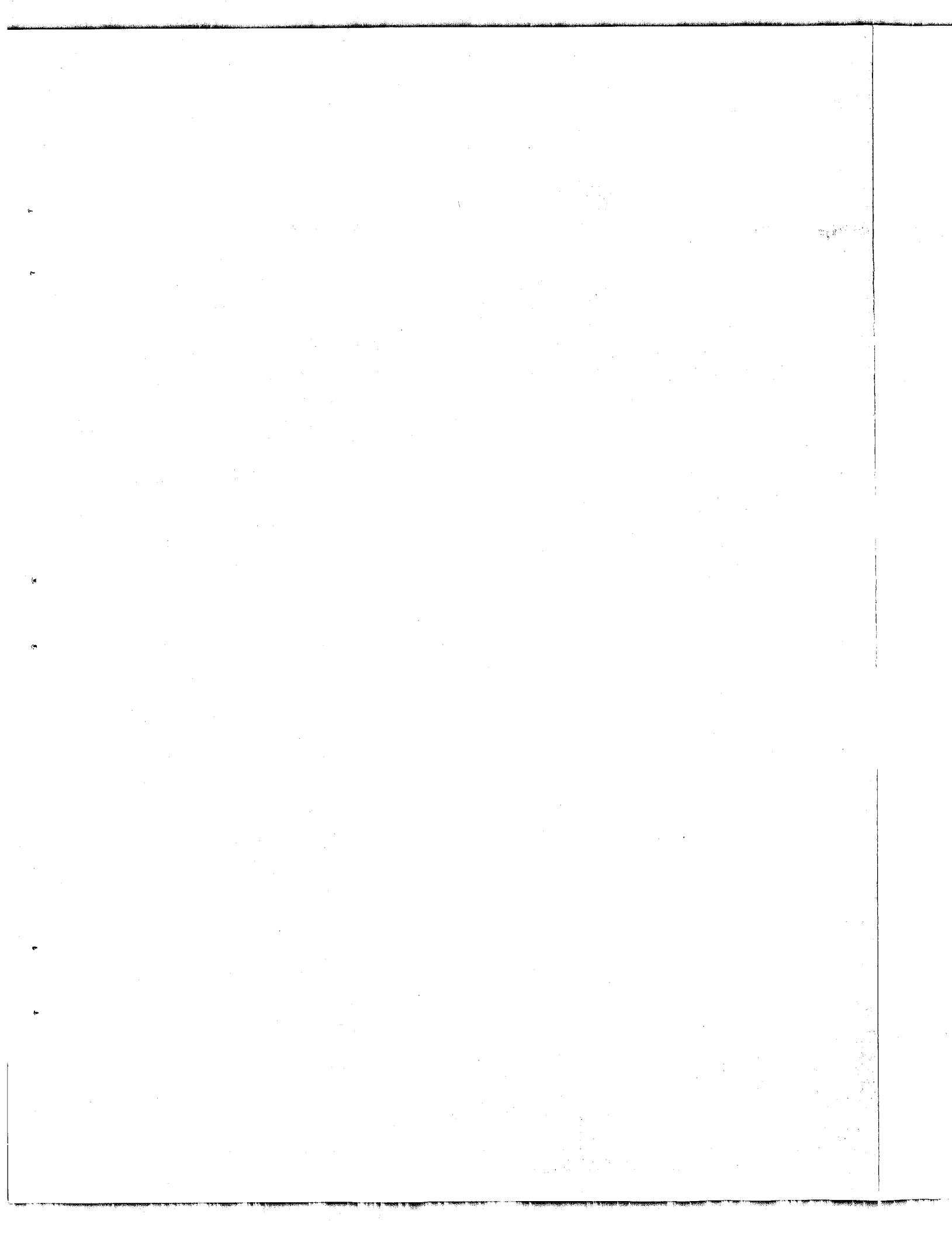


TABLE C.2. LIST OF RELAY SWITCHES

Contact	Instrument	Set Point
RS-9	Count rate recorder No. 1	Closed above 1 count/sec
RS-10	Count rate recorder No. 1	Opened off scale
RS-11	Count rate recorder No. 2	Closed above 1 count/sec
RS-12	Count rate recorder No. 2	Opened off scale
RS-13	Front sodium flow	Closed above 60 gpm
RS-14	Back sodium flow	Closed above 60 gpm
RS-15	Log N	Closed when $N > 2\% N_F$
RS-16	Fuel heat exchanger No. 2 outlet	Closed above 1150°F
RS-17	Fuel heat exchanger No. 2 outlet	Closed above 1100°F
RS-18	Fuel flow	Closed above 20 gpm
RS-19	Not used	
RS-20	Log N	Closed when $N > 10^{-5} N_F$
RS-21	Log N	Closed when $N > 10^{-5} N_F$
RS-22	Log N	Closed when $N > 6.67 \times 10^{-3} N_F$
RS-23a	Safety level No. 1	Opened above 120
RS-23b	Safety level No. 2	Opened above 120
RS-24	Fuel flow	Opened above 20 gpm
RS-25	Not used	
RS-26	Reactor outlet temperature (mixed manifold)	Opened above 1550°F
RS-27	Not used	
RS-28	Not used	
RS-29	Pile period	Closed at less than 5 sec
RS-30	Micromicroammeter	Closed above 20 μA
RS-31	Count rate recorder No. 1	Closed above 1 count/sec
RS-32	Count rate recorder No. 2	Closed above 1 count/sec
RS-33	Fuel heat exchanger No. 1 outlet	Closed above 1150°F
RS-34	Fuel heat exchanger No. 1 outlet	Closed above 1100°F
RS-35	Pile period	Opened at less than 5 sec
RS-36	ΔT across reactor tube No. 1	Closed above 450°F
RS-37	ΔT across reactor tube No. 2	Closed above 450°F
RS-38	ΔT across reactor tube No. 3	Closed above 450°F
RS-39	ΔT across reactor tube No. 4	Closed above 450°F
RS-40	ΔT across reactor tube No. 5	Closed above 450°F
RS-41	ΔT across reactor tube No. 6	Closed above 450°F
RS-42	Not used	
RS-43	Not used	

TABLE C.2 (continued)

Contact	Instrument	Set Point
RS-44	Not used	
RS-45	AC-to-DC M-G set	Closed when set was charging batteries
RS-46	Not used	
RS-47	Not used	
RS-48	Not used	
RS-49	Not used	
RS-50	Fuel flow	Closed above 20 gpm
RS-51	Fuel flow	Closed above 20 gpm
RS-52	Reactor outlet temperature (mixed manifold)	Opened above 1500°F
RS-53	Wind velocity recorder	Wind above 5 miles/hr or vent gas monitors
RS-54	Fuel heat exchanger No. 1 outlet	Closed above 1150°F
RS-55	Fuel heat exchanger No. 1 outlet	Closed above 1100°F
RS-56	Fuel heat exchanger No. 2 outlet	Closed above 1150°F
RS-57	Fuel heat exchanger No. 2 outlet	Closed above 1100°F
RS-58	Main fuel pump low-water-flow alarm	Closed above 4 gpm
RS-59	Fuel heat exchanger No. 2 outlet	Closed above 1100°F
RS-60	Secondary fuel pump low-water-flow alarm	Closed above 4 gpm
RS-61	Back sodium heat exchanger outlet	Closed above 1100°F
RS-62	Front sodium flow	Closed above 100 gpm
RS-63	Back sodium flow	Closed above 100 gpm
RS-64	Helium concentration recorder	Closed at less than 90% He
RS-65	Pit humidity indicator	Opened at >10% relative humidity
RS-66	Helium supply header pressure	Opened at <500 psig
RS-67	Water reservoir level	Opened at <16 psig (<18,000 gal)
RS-68	Main sodium pump tank level	Opened at low level
RS-69	Main sodium pump tank level	Opened at high level
RS-70	Standby sodium pump tank level	Opened at low level
RS-71	Standby sodium pump tank level	Opened at high level
RS-72	Main fuel pump tank level	Opened at low level
RS-73	Main fuel pump tank level	Opened at high level
RS-74	Standby fuel pump tank level	Opened at low level
RS-75	Standby fuel pump tank level	Opened at high level
RS-76	Water controller for front sodium heat exchanger	Opened above 160°F
RS-77	Water controller for back sodium heat exchanger	Opened above 160°F
RS-78	Water controller for fuel heat exchanger	Opened above 160°F
RS-79	Standby sodium pump motor ammeter	Opened above 50 amp

TABLE C.2 (continued)

Contract	Instrument	Set Point
RS-80	Water controller for space coolers	Opened above 160°F
RS-81	Water controller for rod-cooling heat exchanger	Opened above 160°F
RS-82	Individual heat exchanger tube temperature	Opened above 1500°F
RS-83	Individual heat exchanger tube temperature	Closed above 1150°F
RS-84	Main sodium pump motor ammeter	Opened above 50 amp
RS-85	ΔT across reactor tube No. 1	Opened above 400°F
RS-86	Main fuel pump motor ammeter	Opened above 50 amp
RS-87	ΔT across reactor tube No. 2	Opened above 400°F
RS-88	Standby fuel pump motor ammeter	Opened above 50 amp
RS-89	ΔT across reactor tube No. 3	Opened above 400°F
RS-90	Standby sodium pump low-water-flow alarm	Closed above 4 gpm
RS-91	ΔT across reactor tube No. 4	Opened above 400°F
RS-92	Main sodium pump low-water-flow alarm	Closed above 4 gpm
RS-93	ΔT across reactor tube No. 5	Opened above 400°F
RS-94	Main fuel pump low-oil-flow alarm	Closed above 2 gpm
RS-95	ΔT across reactor tube No. 6	Opened above 400°F
RS-96	Standby fuel pump low-oil-flow alarm	Closed above 2 gpm
RS-97	Standby sodium pump low-oil-flow alarm	Closed above 2 gpm
RS-98	Main sodium pump low-oil-flow alarm	Closed above 2 gpm
RS-99	Sodium outlet pressure at reactor	Closed above 48 psig
RS-100	Fuel inlet pressure at reactor	Opened above 48 psig
RS-101	Main sodium pump tank pressure	Opened above 47 psig
RS-102	Standby sodium pump tank pressure	Opened above 47 psig
RS-103	Standby fuel pump tank pressure	Opened above 5 psig
RS-104	Main fuel pump tank pressure	Opened above 5 psig
RS-105	Rod cooling helium pressure	Closed above 13 psig
RS-106	Fuel loop water flow	Closed above 110 gpm
RS-107	Water flow to fuel and sodium pumps	Closed above 10 gpm
RS-108	Rod cooling water flow	Closed above 15 gpm
RS-109	Front sodium loop water flow	Closed above 65 gpm
RS-110	Back sodium loop water flow	Closed above 65 gpm
RS-111	Space cooler water flow	Closed above 45 gpm
RS-112	Vent header vacuum	Opened below 29 in. Hg
RS-113	Reserve nitrogen header supply pressure	Opened at <300 psig
RS-114	Rod cooling helium	Opened at <40 psig
RS-115	DC-to-AC M-G set	Closed when set was running

TABLE C.2 (continued)

Contact	Instrument	Set Point
RS-116	AC-to-DC M-G set	Closed when set was running
RS-117	Heat exchanger pit radiation monitor	Opened at high level
RS-118	Heat exchanger pit radiation monitor	Opened at high level
RS-119	Vent gas monitor	Opened at high level
RS-120	Vent gas monitor	Opened at high level
RS-121	Sodium ΔT at reactor	Opened at $<60^{\circ}\text{F}$

TABLE C.3. LIST OF LIMIT SWITCHES

Contact	Device	Set Point
LS-1	Fission chamber No. 1 lower limit	Closed on limit
LS-2	Fission chamber No. 1 upper limit	Closed on limit
LS-3	Fission chamber No. 2 lower limit	Closed on limit
LS-4	Fission chamber No. 2 upper limit	Closed on limit
LS-5	Regulating rod lower limit	Closed on limit
LS-6	Regulating rod upper limit	Closed on limit
LS-7	Shim rod No. 1 upper limit	Closed on limit
LS-8	Shim rod No. 2 upper limit	Closed on limit
LS-9	Shim rod No. 3 upper limit	Closed on limit
LS-10	Shim rod No. 1 lower limit	Closed on limit
LS-11	Shim rod No. 2 lower limit	Closed on limit
LS-12	Shim rod No. 3 lower limit	Closed on limit
LS-13	Shim rod No. 1 clutch	Closed when rod was attached
LS-14	Shim rod No. 2 clutch	Closed when rod was attached
LS-15	Shim rod No. 3 clutch	Closed when rod was attached
LS-16	Shim rod No. 1 seat	Closed on seat
LS-17	Shim rod No. 2 seat	Closed on seat
LS-18	Shim rod No. 3 seat	Closed on seat

action, and buildup of xenon poison after a shutdown.

As far as loss of power is concerned, the operator would have been left figuratively, and nearly literally, in the dark were the instrument bus and control bus to go dead simultaneously. In this very unlikely occurrence, all the instrument lights and all relay-indicating lights would have been out, leaving the operator without visual knowledge of whether the scram (automatic on loss of power)

was effective. If he had reasonable faith in the law of gravity, he would probably have remained at his post until power was restored. There would have been no normal scram indication if the relay cabinet main fuse were to have opened. However, since the amplifier power cabinet would have operated from emergency power, there was a check on release of the shim rods in the fact that the magnet currents would have been interrupted.

Whenever the reactor was subject to automatic

shutdown action, the operator's concern was divided between the causative effects and the chances of returning the reactor to normal operation. The circuits prevented the operator from interfering with shutdown actions as long as the causative conditions remained. Hence the operator's reaction to anything less drastic than a scram was to clear the responsible condition.

When the reactor was scrammed, the chances of getting back into normal operation were of course dependent upon the time history of previous operation as well as upon the need for remedying the trouble. However, any length of complete shutdown could have been tolerated after prolonged operation at normal flux, since xenon poison buildup was low.

Appendix D

NUCLEAR OPERATING PROCEDURES¹

The importance and critical nature of the program, as well as the short time scheduled for the operation of the reactor and system, necessitated a tight experimental program and precise operating procedures. The nuclear operating procedures were, of course, prescribed in advance of the experiment. It is of considerable interest to note that the actual experimental program followed the anticipated program very closely throughout. The only significant deviations were the inclusion of some additional experiments as time permitted. The following appendix is a verbatim copy of the procedures by which the reactor was operated. Some minor discrepancies in operating conditions (i.e., 34-gpm fuel flow vs 46-gpm actual flow) and procedures (i.e., use of the original enrichment system, which was replaced) will be noted.

It is anticipated that the reactor and its associated circuits will be operated for about 250 hr with fused salts in the system prior to the introduction of fuel. All process instrumentation and components (non-nuclear) will be checked out during this period. The mechanical operation of the nuclear equipment will be checked out at temperature. The safety rods will be raised and dropped approximately 50 times during this period.

Several tests preliminary to the fuel loading will have been run. The rated flow of the fuel carrier will be 34 gpm at a mean temperature of 1300°F.

1. The fuel loading system will be operated with carrier. The fuel storage tank will be installed and carrier forced into the transfer tank and then into the reactor system. The strain gage weighing devices will be checked.

2. The helium blowers will be operated and the resultant drop in mean temperature observed. The operating crew will practice in handling the helium flow so as to drop the mean temperature at a rate of 10°F/min and at a rate of 25°F/min. Care will be exercised not to drop the temperature of the fuel carrier to below 1150°F as it leaves the heat exchangers. As the latter temperature approaches that value, the helium flow will be reduced and the system brought back to its mean operating temperature of 1300°F.

3. With the helium blowers off and starting with fuel carrier at rated flow of 34 gpm and mean temperature of 1300°F, the flow rate will be decreased in steps to about one-third rated value. All temperatures will be observed to note any spurious changes caused by the decreased flow.

¹This appendix was originally issued as ORNL CF-54-7-144, ARE Operating Procedures, Part II, Nuclear Operation, J. L. Meem (July 27, 1954).

ADDITION OF FUEL CONCENTRATE²

The fuel concentrate will be added in batches to an "eversafe" container which will contain 115 kg of U²³⁵. The density of the fuel concentrate may be represented by the equation:

$$\rho \text{ (g/cm}^3\text{)} = 5.51 - 0.0013 T \text{ (}^{\circ}\text{C)}$$

At a temperature of 1300°F, the density is 4.59 g/cm³, or 287 lb/ft³. In each pound of the fuel concentrate there is 0.556 lb of U²³⁵.

One quart of the concentrate weighing 9.59 lb and containing 5.33 lb of U²³⁵ will be forced into the transfer tank and weighed. With the safety rods completely withdrawn and the neutron source and fission chambers inserted, the fuel concentrate will be forced into the fuel circuit. At this time the carrier flow will be 34 gpm and the concentrate and carrier temperatures will be 1300°F. The scram level on the safety chambers will have been set at about 10 kw and the period scram at 1 sec. A BF₃ counter will have been installed temporarily in place of the neutron ion chamber for the temperature servo control, and the regulating rod will be on slow-speed drive.

The system volume up to the minimum operating level in the fuel pump is calculated to be 4.64 ft³. Assuming a critical mass of 30 lb in the 1.3 ft³ of reactor core, there will be approximately 124 lb of U²³⁵ in the fuel circuit when the reactor first goes critical with the shim rods completely withdrawn. Accordingly, it is anticipated that approximately 0.78 ft³ or 23.4 quarts of fuel concentrate must be added for initial criticality. Twelve quarts will be added in succession with the shim rods completely withdrawn and the fission chambers fully

²As previously noted, the original enrichment system was not employed, although the principles and techniques of enrichment outlined here were followed.

inserted. After each quart of concentrate is added, counts will be taken on both fission chambers and the BF_3 counter. The reciprocal counting rate will be plotted vs. the fuel concentration to observe the approach to criticality.

After 50% of the fuel concentrate (12 quarts) has been added to the system, a sample of the mixed fuel and carrier will be withdrawn for chemical analysis.

SUBCRITICAL EXPERIMENTS

During the addition of the first 12 quarts of fuel concentrate, the safety rods have been completely withdrawn from the reactor. From here on, the shim rods will be inserted approximately 25% while a quart of fuel concentrate is being added. The shim rods will then be withdrawn and a count taken on the fission chambers as before. The shim rods

will be inserted and withdrawn in this fashion for each succeeding fuel addition. The reciprocal of the counting rate vs. fuel concentration will still be plotted to indicate the increase in criticality.

When approximately 90% of the critical mass has been added, the fuel addition will be stopped and several subcritical experiments performed. For these experiments it is desired that the k of the reactor be about 0.97 to 0.98. In Fig. D.1 is shown the relationship between $\Delta k/k$ and $\Delta M/M$ as a function of the critical mass M . Using this curve, an estimate of the point at which fuel addition must be stopped can be made.

For the first experiment, the fuel temperature will be decreased at a rate of $10^\circ\text{F}/\text{min}$ by starting the helium flow. Assuming a temperature coefficient of $-5 \times 10^{-5} (\Delta k/k)/^\circ\text{F}$, the resultant $\Delta k/k$ should be about 0.25% after 5 min. If $\Delta M/M$ is

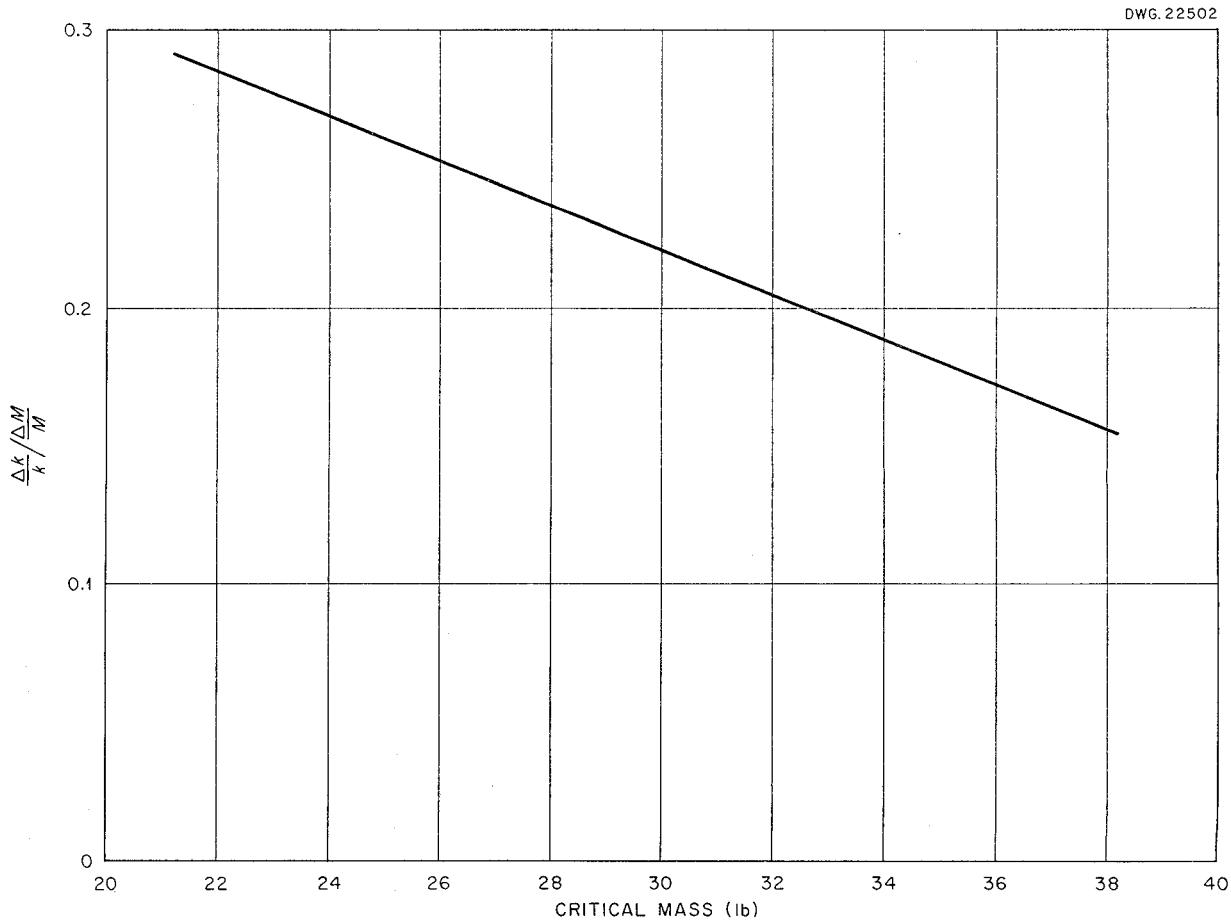


Fig. D.1. Reactivity-Mass Ratio as a Function of Critical Mass.

approximately $4 \Delta k/k$ (Fig. D.1), the count rate should increase by an amount corresponding to the addition of 1.0% more fuel. If the change in count rate is too small to be definite, the experiment will be repeated at a rate of decrease of $25^{\circ}\text{F}/\text{min}$ until a definite increase in count rate is observed, or until the temperature has been decreased 100°F . If, after this decrease in temperature, no increase in count rate is observed, it will be assumed that the temperature coefficient is negligibly small and the experiment will proceed. As has always been

the philosophy on the ARE, if the temperature coefficient is observed to be positive, the experiment will be concluded and the fuel circuit drained.

For the second experiment, the reactor temperature will be returned to its original value of 1300°F , and with the reactor containing 90% of the critical mass, the fuel flow rate will be gradually decreased. If the available delayed neutron fraction is $0.47\% \Delta k$ at full flow and $0.75\% \Delta k$ when the flow is stopped (Fig. D.2), a Δk of 0.28% should appear. The count rate should in-

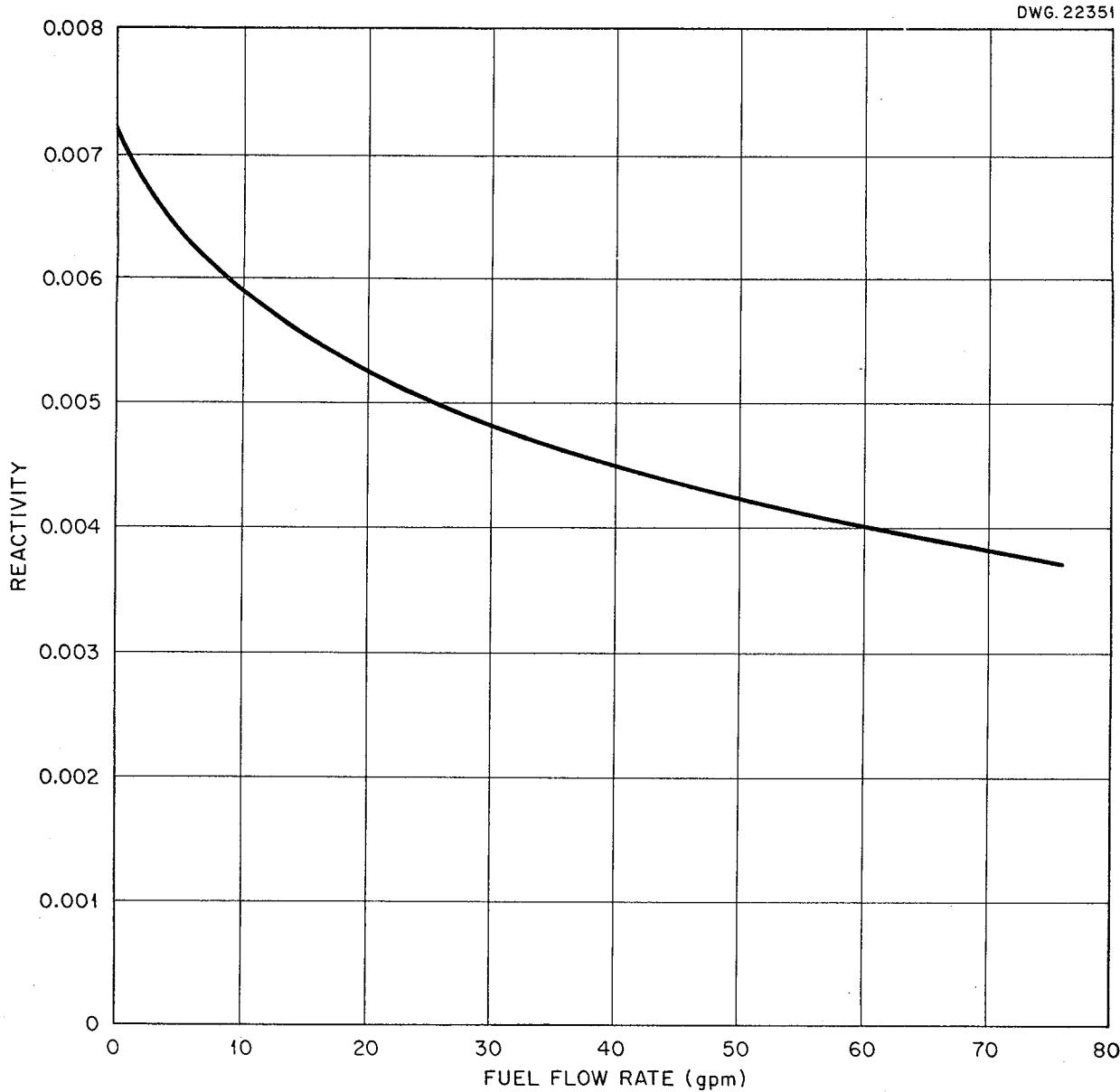


Fig. D.2. Reactivity from Delayed Neutrons as a Function of Fuel Flow.

crease by an amount equivalent to the ΔM corresponding to additional Δk in the delayed neutrons. A rough experimental check on the calculated value of the delayed neutron fraction will thus be available.

During the period of subcritical operation, the count rate will be carefully observed for sudden changes that could be caused by fuel segregation. No such difficulty is anticipated, but if such an effect is observed, the reactor will be shut down until the reason for such behavior is ascertained.

INITIAL CRITICALITY

Upon completion of the subcritical experiments, the fuel flow and reactor temperature will be returned to the initial conditions of 34 gpm³ and 1300°F. Counts will be taken on the fission chambers with the shim rods 25% inserted and completely withdrawn. The shim rods will then be 50% inserted and a quart of fuel concentrate added. The rods will be withdrawn to 25% and a count taken and then completely withdrawn and a count taken. From here on, two curves of reciprocal counting rate vs. fuel concentration will be plotted, one at 25% rod insertion and the original curve with the rods completely withdrawn. If the reactor contained 90% of the critical mass during the subcritical experiments, about two 1-quart additions of fuel concentrate will bring the reactor critical with the rods completely withdrawn. The last fuel additions will be made very slowly. When criticality has been definitely reached, the reactor will be shut down and a fuel sample taken for chemical analysis.

After the sample has been taken, the reactor will again be brought barely critical (a few hundredths of a watt) and held at constant power by watching the count rate meters. The gamma-ray dosage will be measured with a "Cutie-pie" at all pertinent points throughout the pits and recorded for future reference on radiation damage and shielding.

ROD CALIBRATION vs FUEL ADDITION

The reactor will be brought critical at a very low power and the shim rods adjusted so that the regulating rod is 5 in. above center. The regulating rod is estimated to be worth about 0.04% Δk /in. One quart of fuel is approximately 4% ΔM or 1% Δk (Fig. D.1). Therefore, $\frac{1}{25}$ of a quart should be worth about 1 in. of regulating rod.

Figures D.3 and D.4 show a calibration of a regulating rod taken on a mockup of the ARE at the Critical Experiment Facility. While it would be fortuitous if the regulating rod in the actual ARE gave the same calibration, it is expected that the general shape of the curves will be the same.

With the shim rods in a fixed position, the regulating rod will be fully inserted and approximately $\frac{1}{25}$ of a quart of fuel concentrate will be added slowly to the system. The reactor will be brought critical on the regulating rod and its new position noted. This procedure will be repeated until the regulating rod has been calibrated from 5 in. above to 5 in. below its mid-position.

The above experiment will have been run with the shim rods almost completely withdrawn. The shims will now be inserted about 25% and $\frac{1}{2}$ quart of fuel added (approximately 0.5% Δk). The shim rods will be withdrawn until the reactor goes critical. This procedure will be continued to give a rough calibration of shim rod position vs fuel addition over one-fourth of the rod. When the reactor is critical with the shims approximately 15% inserted, the shims will be adjusted so that the regulating rod is 5 in. above center, and a second calibration of the regulating rod vs fuel addition will be run as above.

Calibration of the shim rods vs fuel addition will then be continued until the reactor is critical with the rods about 25% inserted. At this time, a third and final calibration of the regulating rod vs fuel addition will be run. The reactor will then be shut down and a fuel sample taken.

LOW-POWER EXPERIMENTS

The nominal power of the reactor is obtained as follows: It is estimated that in the reflector at the mid-plane of the reactor the fission producing flux is 2×10^6 nv/w, and the average flux over the length of the fission chamber when fully inserted is 1.5×10^6 nv/w. Preliminary tests on the fission chambers show a counting efficiency of approximately 0.14 counts/sec·nv. The relationship between counting rate and power is therefore approximately 2×10^5 counts/sec = 1 w. The nominal power of the reactor will be based on this relationship during the preceding experiments.

Until this time the reactor has been operated on the fission chambers alone at a nominal power

³Actual, 46 gpm.

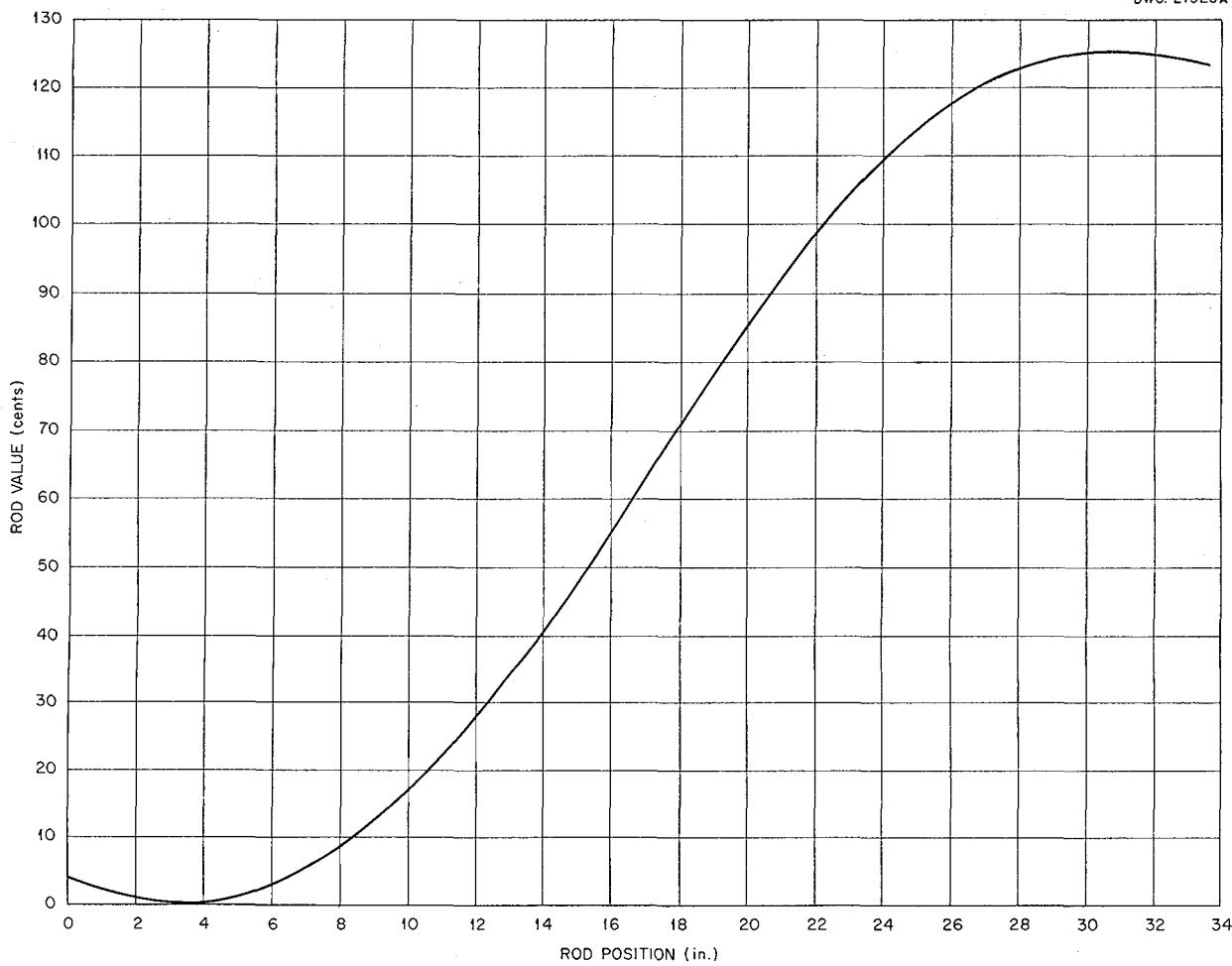


Fig. D.3. Regulating Rod Calibration (Rod B).

of about 0.01 w (about 2000 counts/sec). The reactor power will now be increased to about 1 to 10 w, at which time the neutron ionization chambers should begin to give readings on the log N recorder, the micromicroammeter, and the period recorder. The reactor will be leveled out and the flux servo turned on. One of the fission chambers will be completely withdrawn, which should reduce its counting rate by several orders of magnitude. A careful comparison of the new count rate vs the old count rate will be made.

The reactor will be held at constant power for exactly 1 hr and then scrammed. A fuel sample will be drawn off and sent to the Bulk Shielding Facility for determining its activity. This activity will be compared with that of a previous sample (Fig. D.5), which was exposed in a known neutron

flux in the Bulk Shielding Reactor. From the comparison, the fission rate or absolute power of the ARE will be determined for this run (cf., app. H). All neutron level instruments will be calibrated accordingly.

Rod Calibration vs Period. A family of curves of reactivity vs reactor period (in hour curves) with the rate of flow of the fuel as a parameter is shown in Fig. D.6.

With the fuel flow rate at 34 gpm, the servo will be turned off and the reactor placed on infinite period manually with the regulating rod at mid-position. From the rod calibration vs fuel plot and the theoretical inhour curve, the regulating rod withdrawal for a 30-sec period will be estimated (present estimate is about 1 in.). The rod will be withdrawn accordingly and the neutron

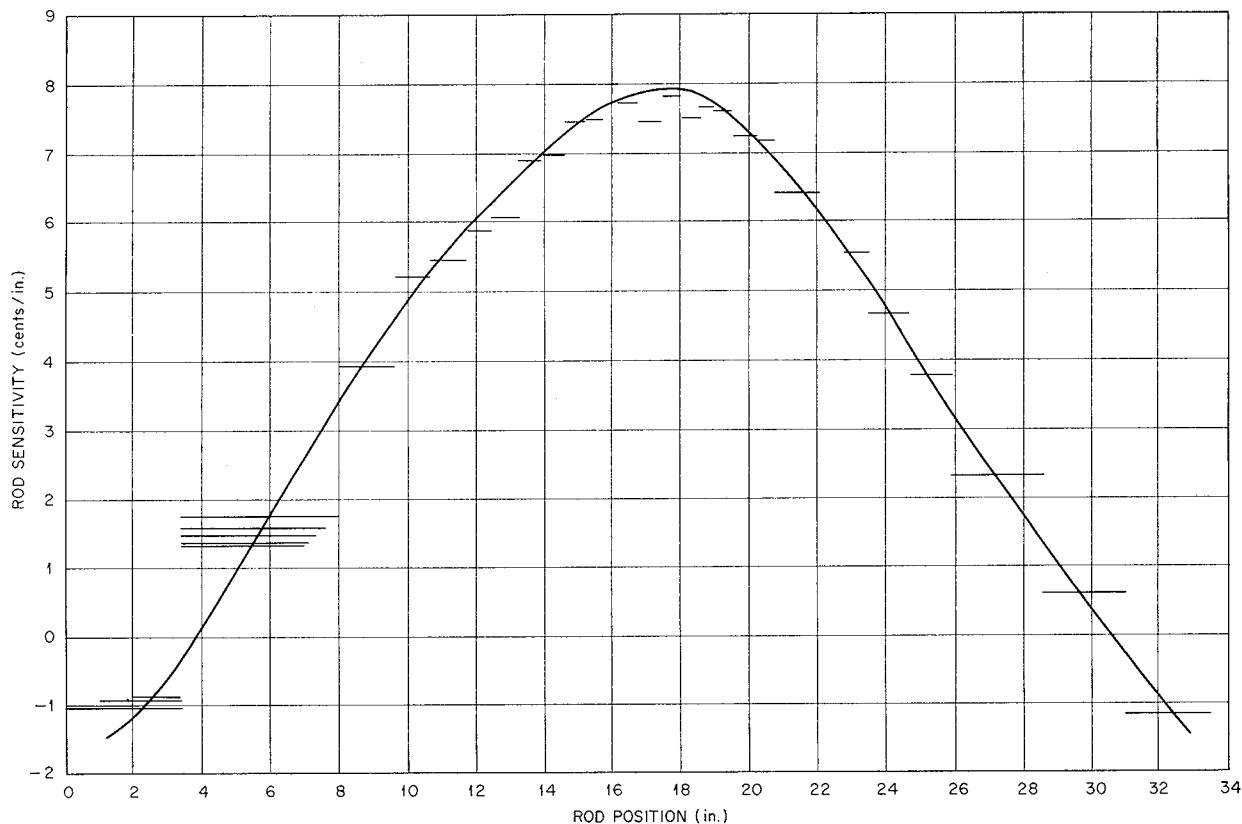


Fig. D.4. Regulating Rod Sensitivity (Rod B).

level allowed to rise about two orders of magnitude, whereupon the regulating rod will be fully inserted and the induced gamma rays allowed to decay for about 20 min. The reactor will then be brought back to its original power, as determined by the fission chambers. If the position of the regulating rod does not return to its original value because of photoneutrons, the reactor power will again be reduced by insertion of the regulating rod until the photoneutron effect becomes negligible. The above procedures will be repeated for 20-sec and 10-sec periods. The 10-sec period should correspond roughly to a 2-in. withdrawal of the regulating rod. Runs will then be made at correspondingly longer periods until the period for a $\frac{1}{2}$ -in. withdrawal of the rod is obtained (approximately 100 sec). At this time a repeat run on the 30-sec period will be made to ascertain whether photoneutron buildup is causing appreciable error in the measurements.

The shims will then be adjusted so that the

regulating rod is 1 in. below center at infinite period. The rod will be withdrawn 1 in. and the period recorded. This procedure will be repeated at successive starting positions of the regulating rod 1 in. apart from 5 in. below center to 5 in. above. A check on the initial 30-sec run with the rod withdrawn from the mid-position will be made periodically to ensure that photoneutron buildup is not interfering with the measurements. From the standpoints of safety and experimental convenience, the regulating rod should be worth between 0.3% and 0.5% Δk for its full 12-in. travel. If these experiments show that the value of the rod is not in this range, a new rod will be installed at this time and the period calibration repeated. If convenient, a fuel sample will be taken at this time.

Measurement of the Delayed Neutron Fraction. The delayed neutron fraction for a stationary fuel reactor is about 0.73%. For the ARE at a design flow of 34 gpm, the fraction is calculated to be

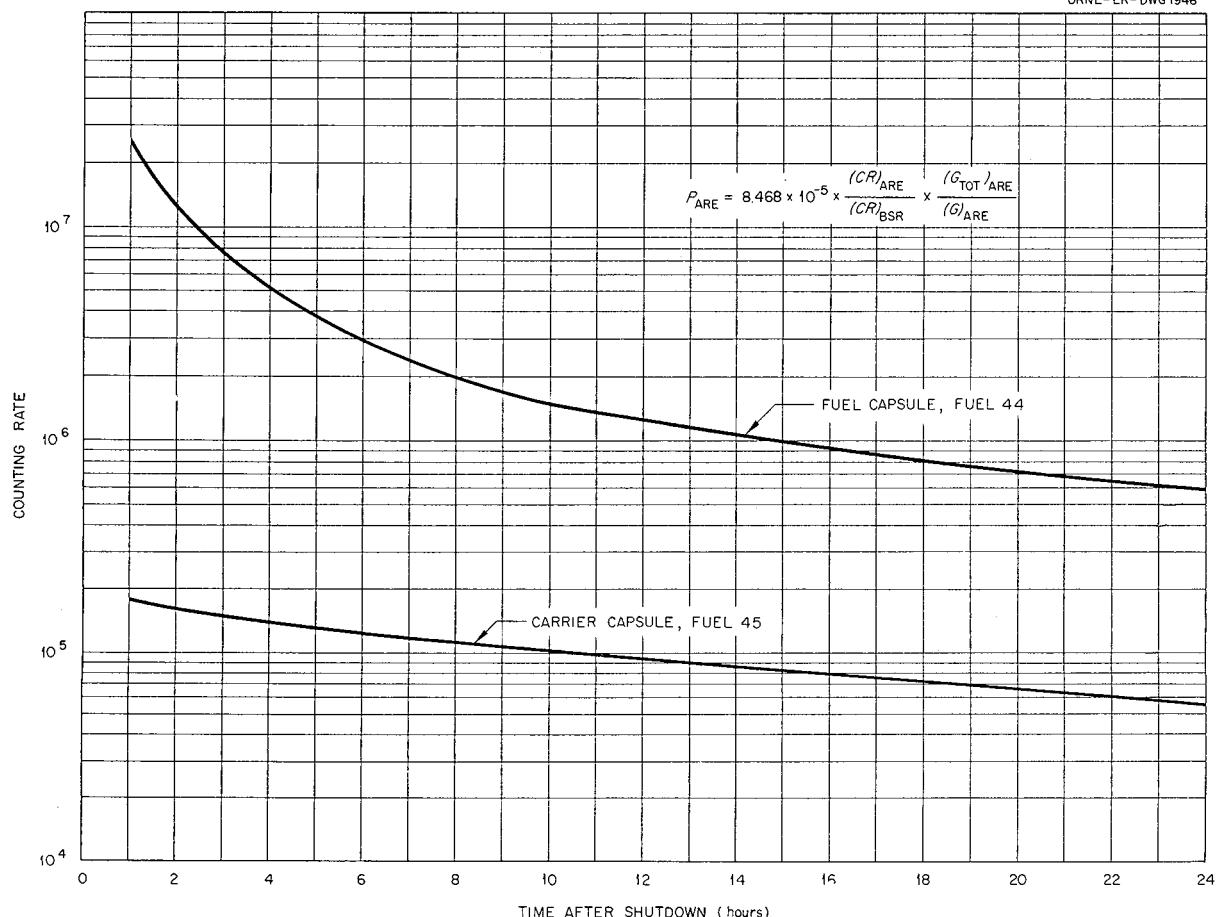


Fig. D.5. Decay Curves for Fluoride Activated in the Bulk Shielding Reactor.

0.47%, and for smaller flow rates, the corresponding reactivity may be found from Fig. D.2.

Starting with the reactor stabilized at 34 gpm and the flux servo on, the flow rate will gradually be reduced. The calibrated regulating rod should be inserted so as to indicate the same reactivity as shown in Fig. D.2. This will give experimental verification of the previously calculated inhour curves, Fig. D.6.

Preliminary Measurements of Temperature Coefficient. With the reactor held at 10 w by the flux servo, the helium flow will be turned on so as to drop the fuel temperature at a rate of 10°F/min. As the mean reactor temperature drops, the servo will insert the regulating rod so as to maintain constant flux, and from the rod calibration, the corresponding Δk can be obtained. Before the rod has reached the limit of its travel, the helium

flow will be shut and the fuel allowed to return to its original temperature. From the recordings of rod position and mean temperature, a plot of Δk vs mean temperature can be obtained. The initial slope of this curve will correspond to the fuel temperature coefficient. Because of the weak signal received by the flux servo, this measurement will be only approximate and is to be repeated at higher power.

Depending upon how the reactor responds, the procedure can be repeated by dropping the fuel temperature at rates of up to 25°F/min. Care will be taken not to drop the fuel temperature so low as to set off the low-temperature scram.

APPROACH TO POWER

At the conclusion of the above experiments and before the fuel storage tank is removed from the

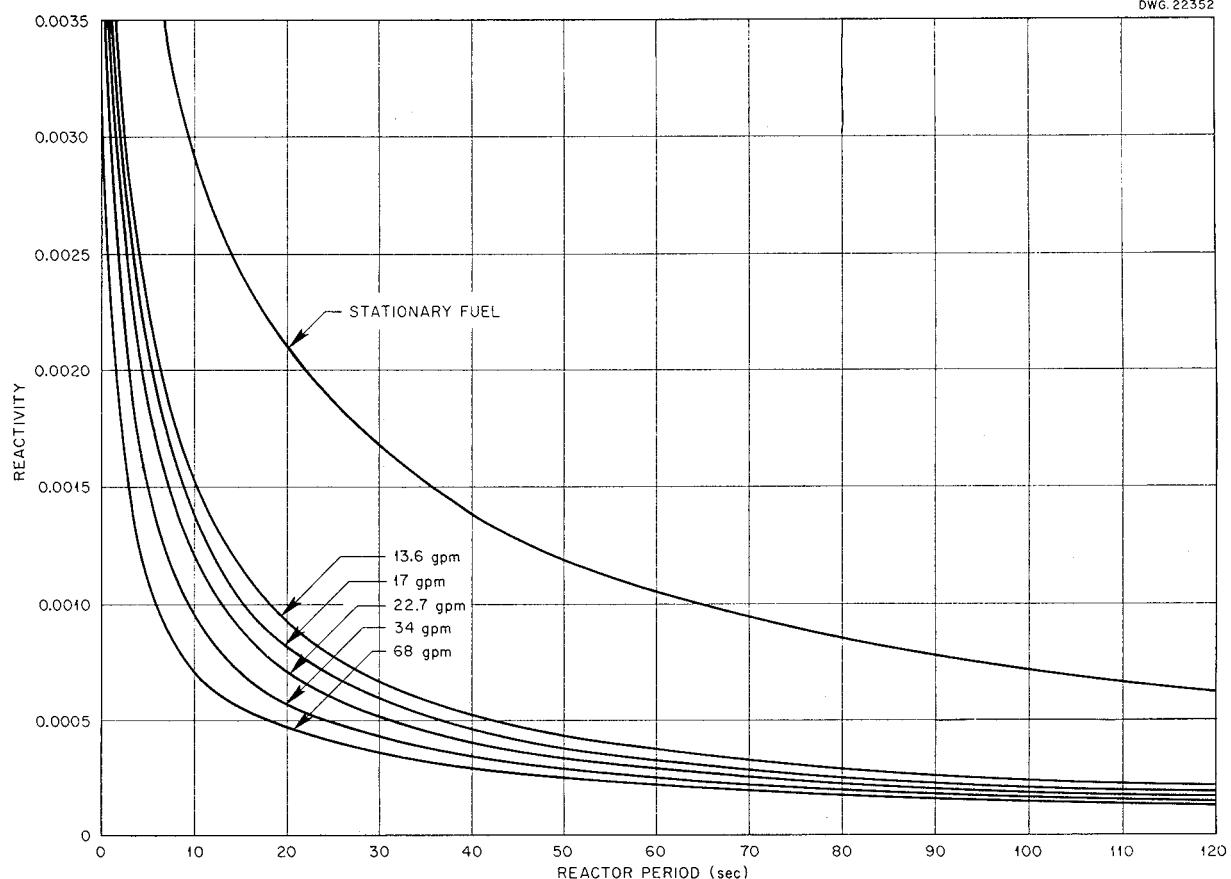


Fig. D.6. Reactivity as a Function of Reactor Period for Several Fuel Flow Rates.

pits, sufficient fuel concentrate will be added to the system so that 4% excess reactivity is available. This excess reactivity will be absorbed with the shim rods. The shim rods will have a rough calibration by this time, and it is expected that they will be worth about 12% in excess reactivity. Therefore, they will need to be inserted about one-third of their length. After addition of the final amount of fuel concentrate the liquid level in the pump will be checked to ensure that at least 0.3 ft³ of volume remains for expansion of the fuel. This expansion volume will allow the fuel to expand isothermally from 1300 to 1600°F, which is well above the high-temperature scram level. The final sample of fuel will be taken for chemical analysis.

The reactor will now be shut down so that the concrete block shields can be put over the pits and the pits flooded with helium. The fuel storage tank will first be removed and a final check on

all process equipment made. The BF₃ counter will be removed and the temperature servo chamber installed. The regulating rod will be put on fast drive. A check list is being prepared of all items to be reviewed before the pits are sealed.

If the temperature coefficient is of sufficient magnitude to control the reactor, the flux servo will be left in. However, if the magnitude of the temperature coefficient is marginal, the flux servo will be removed at this time and the temperature servo connected.

After the pits have been sealed, the reactor will be brought to a power of 1 kw and allowed to stabilize. Up until this time all neutron ion chambers have been fully inserted. The ion chambers will be withdrawn slowly, one by one, while the power level is being constantly monitored with the fission chambers. The ion chambers will be set for a maximum reading of around 5 Mw.

The safety chambers will be set to scram at the same level.

The reactor is now ready for full power operation. The rod will be withdrawn and the reactor put on about a 50-sec period. Somewhere in the region from 10 to 100 kw a noticeable increase in reactor period and an increase in reactor temperatures should be observed. The helium flow will be started slowly and gradually increased until a nominal power of 100 to 200 kw is reached (ΔT from 25 to 50°F).

At this time, the reactor will be allowed to stabilize for about $\frac{1}{2}$ hr and all readings recorded. If the temperature coefficient is of insufficient magnitude to stabilize the reactor, as determined by previous measurements, the control of the reactor will be turned over to the temperature servo.

The power as determined from the heat extraction by the helium will now be measured. The heat capacity of the fuel is 0.23 Btu/lb. $^{\circ}$ F and the density of the fuel is represented by

$$\rho \text{ (g/cm}^3\text{)} = 4.04 - 0.0011 T \text{ (}^{\circ}\text{C}) .$$

At a mean temperature of 1300°F, the average density is 3.27 g/cm³. The power can be expressed as

$$\rho \text{ (kw)} = 0.11 \times \Delta T \text{ (}^{\circ}\text{F)} \times \text{flow (gpm)} .$$

Therefore at 34 gpm the power extracted by the fuel is 3.74 kw/ $^{\circ}$ F.

Having obtained a heat balance, the extraction of heat from the fuel in the heat exchanger will be increased until a power of about 500 kw ($\Delta T = 134^{\circ}$ F) is reached. Again the reactor will be allowed to stabilize and the extracted power measured. A third and final heat balance will be made at a power of about 1 Mw ($\Delta T = 268^{\circ}$ F). This is close to the maximum power obtainable without changing the initial conditions of 1300°F mean reactor temperature and 34-gpm fuel flow.

During the preceding discussion, no mention has been made of heat extraction other than in the fuel circuit. An appreciable quantity of heat will be removed by the sodium in the reflector coolant circuit. Before the reactor goes to high power, the sodium inlet and outlet temperatures will be near the isothermal temperature of 1300°F. Since there is some gamma heating in the reflector region, it will be necessary to lower the inlet temperature of the sodium by extracting heat with the reflector coolant heat exchangers. The sodium flow rate will be held at 224 gpm and the sodium

mean temperature at 1300°F. Since the heat capacity of the sodium is 0.30 Btu/lb. $^{\circ}$ F and its specific gravity is 0.78, the power extracted by the sodium will be 7.7 kw/ $^{\circ}$ F. No more than 10% of the power generated is expected to go into the sodium.

EXPERIMENTS AT POWER

Measurement of the Temperature Coefficients. After the reactor power has been calibrated, the power will be reduced to about 500 kw and allowed to stabilize. The flux servo will be turned on, and by means of the helium demand the mean temperature will be dropped at an initial rate of 10°F/min. (If the temperature servo is connected, it will have to be replaced for this experiment.) As discussed previously the initial slope of the plot of Δk vs mean temperature will represent the fuel temperature coefficient. Contrary to the procedure at low power, however, the helium flow will not be decreased after the temperature has dropped. The reactor will be allowed to stabilize, and, after about 30 min, the regulating rod will have leveled out at a new position, and the reactor will have assumed a new mean temperature. These readings will represent the over-all reactor temperature coefficient (fuel plus moderator). If, during the above experiment, the servo inserts the rod to its limit, it will be left at that position since the temperature should stabilize the reactor.

If the fuel temperature coefficient is quite small, the experiment can be repeated with an initial rate of temperature decrease of 25°F/min. Care will be taken that the reactor does not go on too fast a period and that the low-temperature scram limit is not exceeded.

Maximum Power Extraction. Except for specifically stated instances, the reactor has been operated continuously up to this time at a mean temperature of 1300°F and a fuel flow rate of 34 gpm. Under these conditions, the maximum obtainable power is 1.1 Mw. At this power, the reactor outlet temperature and the heat exchanger inlet temperature are both 1450°F. The heat exchanger outlet and the reactor inlet are both at 1150°F. It is to be noted that when the heat exchanger outlet temperature drops below 1150°F, an alarm is sounded.

The mean reactor temperature will be elevated from 1300 to 1325°F by a slight withdrawal of the shim rods. The mean temperature of both fuel and sodium will be held at this temperature. The helium blower speed will now be increased until

a ΔT of nearly 350°F appears across the reactor. With this ΔT , the reactor outlet and heat exchanger inlet are at the upper limit of 1500°F , and the heat exchanger outlet and reactor inlet are at the lower limit of 1150°F . The power from the fuel will be 1.3 Mw. At this time the pump speed can be increased from 34 gpm to about 40 gpm, caution being taken that the reactor inlet pressure does not exceed 50 psig. The maximum ΔT across the reactor will still be 350°F , and the power extracted in the fuel circuit will be 1.5 Mw. This is the maximum power at which the reactor can be operated.

Power Transients. With the reactor on manual control and the regulating rod at mid-position, the helium blower speed will be regulated until the power in the fuel system is 1 Mw, and the reactor will be allowed to stabilize. The helium flow will be suddenly increased to its maximum and the transient response of all temperature and nuclear recordings noted. The experiment can be repeated from successively decreasing initial powers of 500, 200, 100, 50, 20, and 10 kw. At some level below 100 kw, the power cannot be reduced further because the helium blowers will be completely shut off. When this lower limit of initial power has been reached, the series of experiments will be concluded. If at any time the reactor period gets too fast or the upper or lower temperature limits are approached, the experiments will be concluded.

Sudden Changes in Reactivity. The reactor will be brought to a power of 1 Mw and allowed to stabilize. From the previous calibration of the regulating rod, the rod will be placed at a position such that a complete withdrawal will give 10 cents of excess reactivity. The rod will suddenly be withdrawn and the transient response of the inlet pressure and all nuclear and temperature recorders noted. The experiment can be repeated with sudden changes of 25, 50, 75, and 100 cents of reactivity. If the fuel temperature coefficient has a value of approximately -5×10^{-5} , as expected, a sudden change in reactivity of 100 cents should be safe. However, if the experiments with smaller reactivity changes indicate that such a large step will be unsafe, this series of experiments will be concluded. Otherwise, the experiment will be repeated from initial powers of 100 kw, 10 kw, and successively lower power levels.

Reactor Startup Using the Temperature Coefficient. The reactor will be brought to 1 Mw of

power and the shims adjusted so that the regulating rod is completely withdrawn. The helium flow will be cut off and the reactor power allowed to drop to its normal power with no heat extraction (estimated to be between 10 and 100 kw). The regulating rod will now be inserted by 0.1% of reactivity and the reactor allowed to go subcritical for about 10 min. After this time, helium flow will gradually be increased. If the temperature coefficient is -5×10^{-5} , a drop in the mean temperature of the reactor of 20°F will bring the reactor critical again. As soon as a positive period is noted, the helium cooling flow will be held fixed and the reactor allowed to come up to power and level out of its own accord.

The experiment can be repeated by driving the reactor subcritical by 0.2, 0.3, and 0.4% with the regulating rod. Care will be exercised not to approach the upper or lower temperature limits.

Effect of Xenon Buildup. The change in reactivity calculated from xenon buildup in the ARE is shown in Fig. D.7. The reactivity as plotted is nominal because of uncertainties in the xenon cross sections and is probably a maximum. The shape of the curves represents the change in reactivity if no xenon is lost by off-gassing. The reactor will be operated for 5 hr at full power, and then reduced to 10% of full power. If no xenon is lost, the reactivity should change as shown in the lower curve of Fig. D.7. The reactor will then be operated for 25 hr at full power, and subsequently reduced to 10% power. Again if no xenon is lost, the reactivity change should be as shown in the upper curve of Fig. D.7. If some xenon does off-gas, the shape of the curves will be changed, and by proper analysis, an estimate of the amount of off-gassing can be obtained.

At full power, the reactivity change will be calculated from the change in reactor mean temperature and the temperature coefficient. At 10% power, the reactor will be put on flux servo and the movement of the regulating rod will measure the reactivity change. Since the moderator will contain considerable heat when the power is reduced, the mean reactor temperature will slowly decrease during about the first $\frac{1}{2}$ hr after the power is reduced to 10%. This will cause an insertion of the regulating rod by the flux servo. Since the xenon buildup will cause a withdrawal of the regulating rod, a correction must be applied for the effect of the drop in moderator temperature.

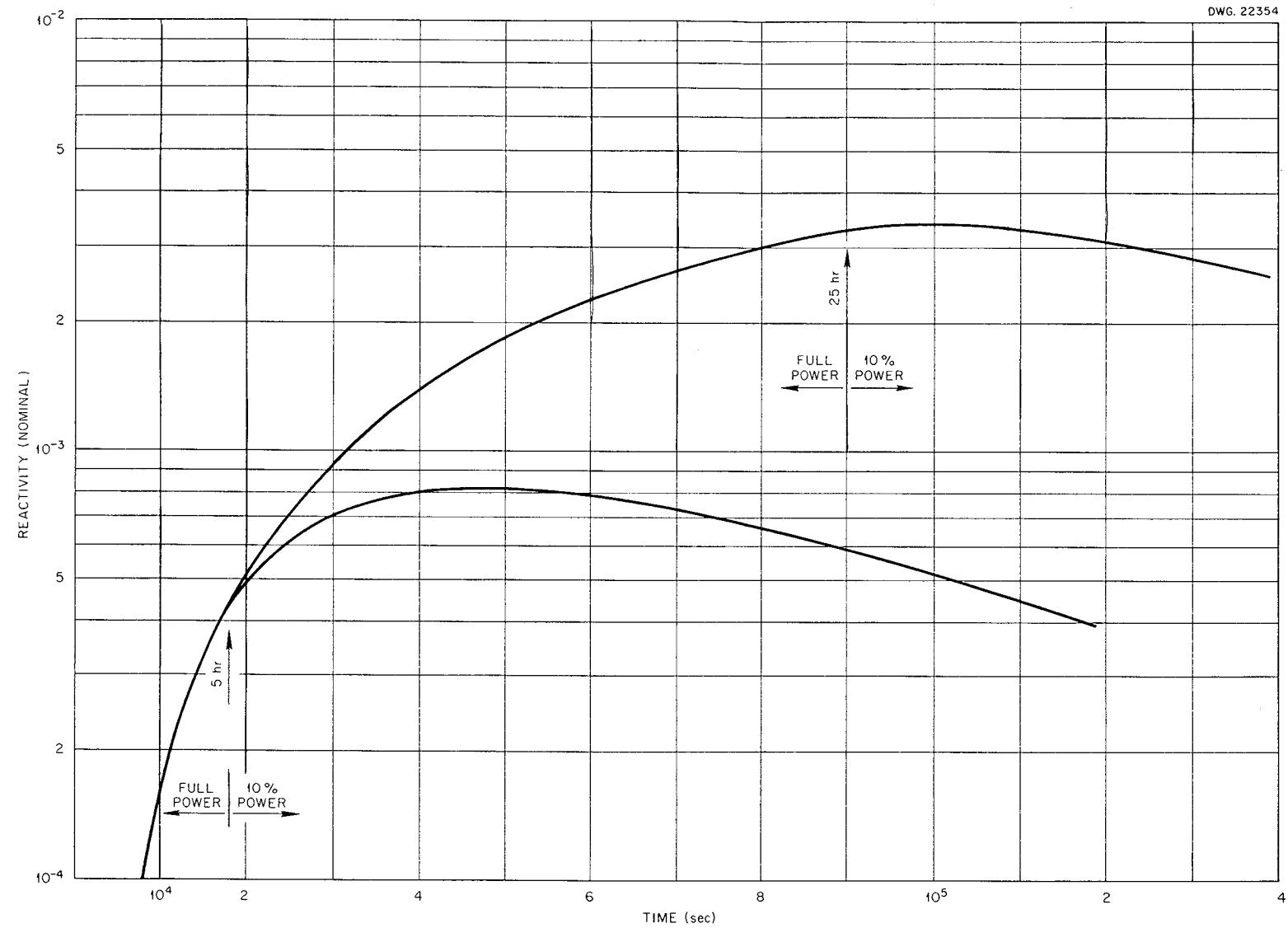


Fig. D.7. Effect of Xenon Buildup.

To obtain this correction experimentally, a control experiment will be performed. The reactor will be operated at full power for $\frac{1}{2}$ to 1 hr and the moderator allowed to come up to temperature. During this short time, no appreciable xenon will

be formed. The reactor will then be reduced to 10% power and the flux servo turned on. The reactivity change from the drop in moderator temperature will be observed and used as a correction for the xenon buildup experiments.

Appendix E

MATHEMATICAL ANALYSIS OF APPROACH TO CRITICALITY

W. E. Kinney

When the ARE was brought to critical by successive fuel additions, it was observed that the usual plot of $[1 - (1/\text{multiplication constant})]$ vs uranium concentration increased, at first, very rapidly, but, when the curve got close to 1, the rise was very slow. Qualitatively, such behavior is observed in many reactors, but the ARE exhibited the effect to an unusual degree. In order to explain this, the ORACLE three-group, three-region code was modified so that flux shapes at successive fuel additions could be calculated. Group constants were obtained by flux weighting with fluxes from an Eyewash calculation on the ARE.

Figure E.1 shows the space distribution of the thermal flux for no fuel and for runs 2 through 6.

The effect of the reflector as fission neutrons become more numerous can be seen. Figure E.2 compares experimental and calculated startup curves for the fission chambers which were located in the reflector as indicated in Fig. E.1. In the calculation,

$$CR \sim \sigma_{f_1} \phi_1 + \sigma_{f_2} \phi_2 + \sigma_{f_3} \phi_3 ,$$

where CR is the counting rate of the fission chamber, σ_{f_i} is the fission cross section for group i , and ϕ_i is the group i flux. For the ARE startup

$$m = \frac{CR_j}{CR_0} ,$$

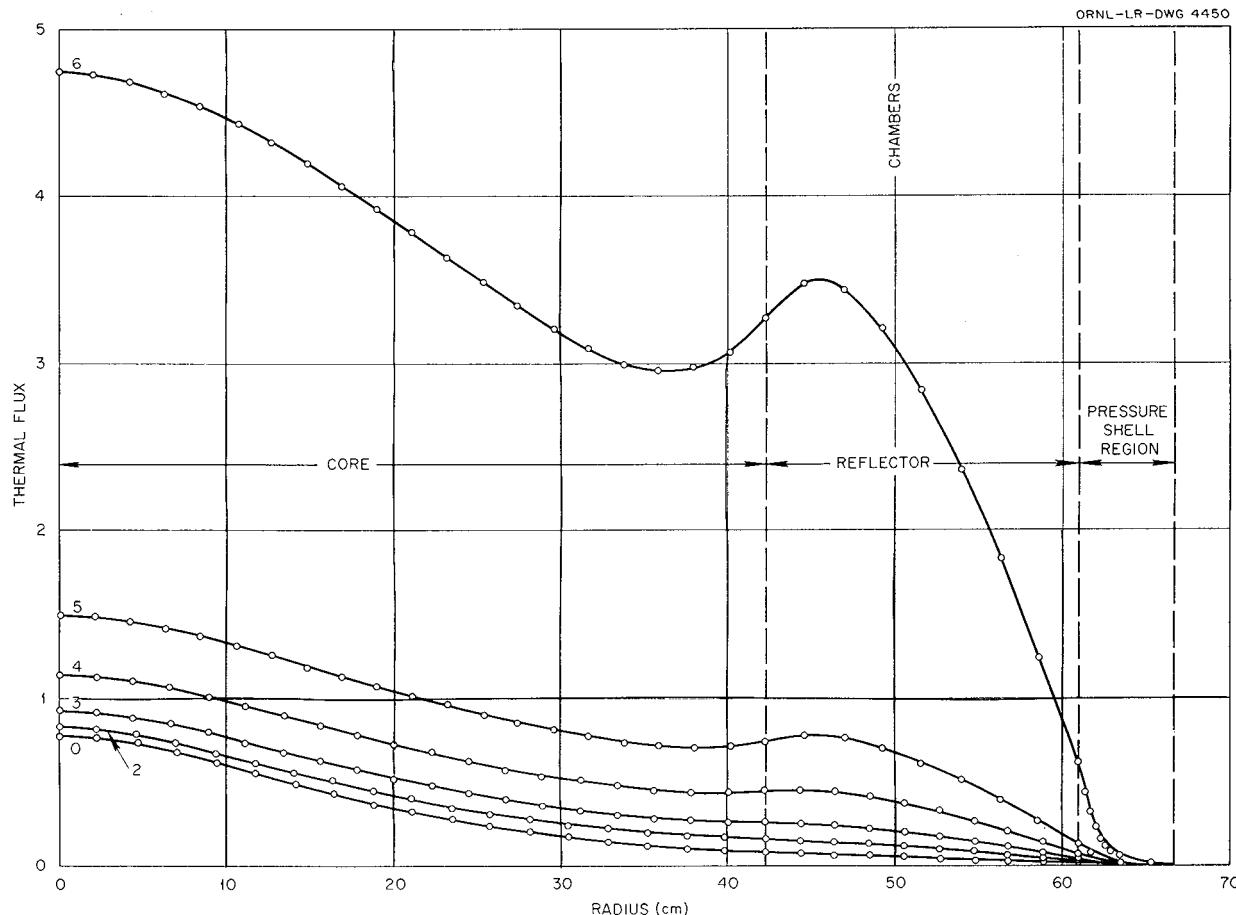


Fig. E.1. Thermal Flux vs Radius.

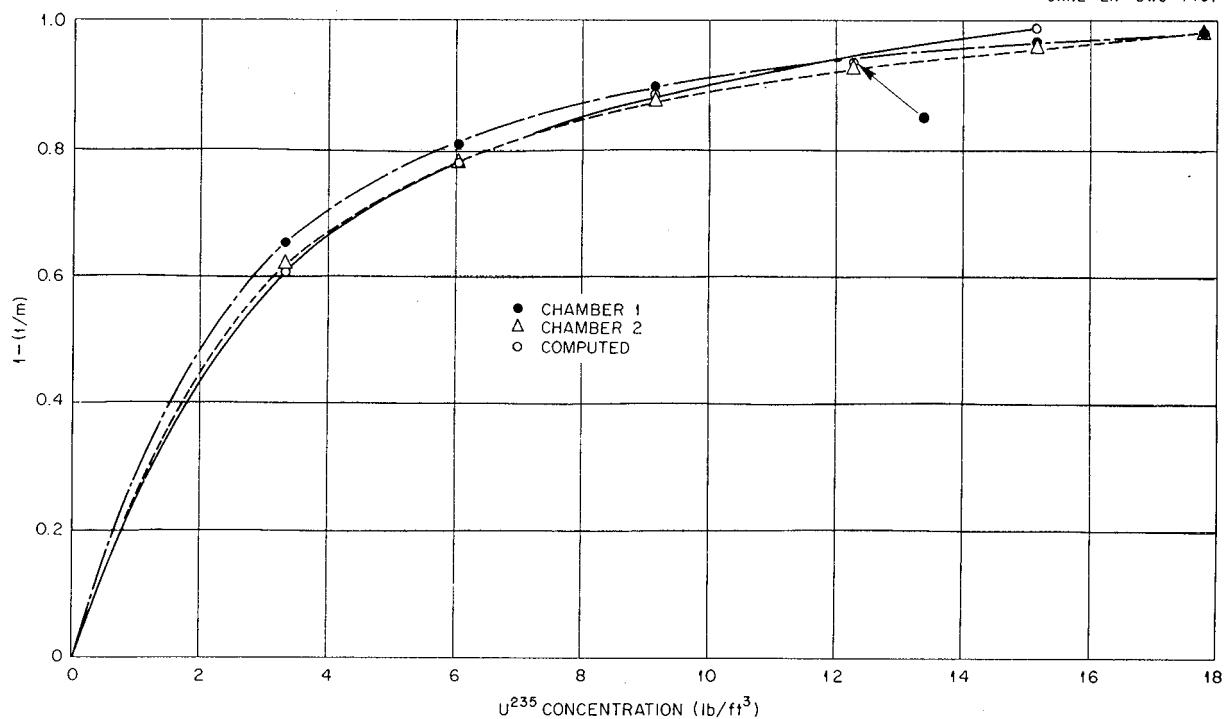


Fig. E.2. $1 - (1/m)$ vs U^{235} Concentration.

where m is the multiplication constant, CR_j is the counting rate on run j , and CR_0 is the counting rate with no fuel. It seems, then, that the unexpected, rapid initial rise in the counting rate of the fission chamber and the $[1 - (1/m)]$ curve is due not only to the general rise in flux level but

also to the formation of the thermal-flux maximum near the fission chambers. Once the shape of spatial distribution of the thermal-neutron flux is set up, the fission chambers register only the general increase in flux level and the count rate increases slowly.

Appendix F

COLD, CLEAN CRITICAL MASS

The value of the cold, clean critical mass is of interest in connection with any reactor, since it is the calculation of this elusive number that takes so much time during the design of the reactor and system. The cold, clean critical mass may be found by extrapolating the curve of uranium (lb of U²³⁵) in the core vs $\Delta k/k$ (%) in the rods to the point where there is no rod poisoning. On the other hand, if the mass equivalent of the rod poisoning is determined and deducted from that then in the core, another curve may be obtained. This curve gives corrected mass vs $\Delta k/k$ (%) in the rod and may also be extrapolated to 0% $\Delta k/k$ in the rods. Both these curves, as shown in Fig. F.1, extrapolate to the same mass value at 0% $\Delta k/k$ in the rods, which indicates that the rod calibration was quite accurate and the data were reliable. The value of the cold, clean critical mass extrapolated from Fig. F.1 was 32.75 lb of U²³⁵.

The data from which the curves in Fig. F.1 were plotted are tabulated in Table F.1. The data used to determine the cold, clean critical mass were those obtained during the rod calibration from fuel addition (Exp. L-2). This experiment and Exp. L-5, rod calibration from reactor period, then provided the information on the value of the regulating rod. The values of the shim rods were taken from Appendix J, "Calibration of the Shim Rods." The $\Delta k/k$ values in both regulating and shim rods were then converted to their mass equivalents by using the $(\Delta k/k)/(\Delta M/M)$ ratio of 0.236, as determined experimentally. Three points listed in the table and shown in the figure were derived by using the first regulating rod, which was subsequently replaced because it was too "light." The calibra-

tion for that rod was not accurate, and, hence, the three points were disregarded in extrapolating the curves.

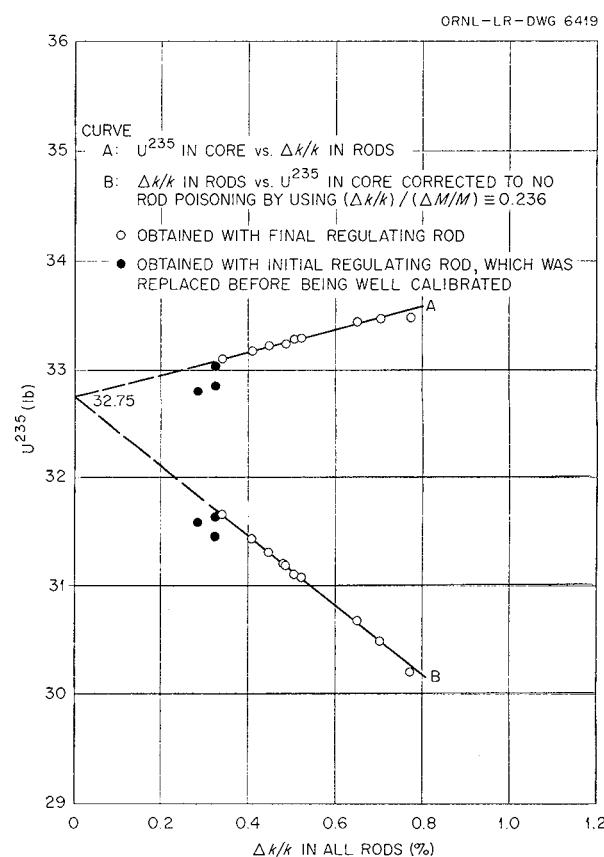


Fig. F.1. Extrapolation to Cold, Clean Critical Mass.

TABLE F.1. CRITICAL URANIUM CONCENTRATIONS FOR VARIOUS ROD INSERTIONS
(Exp. L-2)

Run No.	Regulating Rod Insertion (in.)	Shim Rod Insertion (in.)			$\Delta k/k$ of Regulating Rod (%)	$\Delta k/k$ of Shim Rods (%)			U^{235} Concentration (lb/ft ³)	U^{235} in Core (lb)	Total $\Delta k/k$ in Rods (%)	Total $\Delta M/M$ in Rods	U^{235} in Clean Core (lb)
		No. 1	No. 2	No. 3		No. 1	No. 2	No. 3					
0	0.92	3.3	1.7	0	0.016	0.19	0.08	0	23.94	32.80	0.286	1.212	31.59
1	3.35	3.3	1.7	0	0.058	0.19	0.08	0	23.98	32.85	0.328	1.390	31.46
2	0.93	3.3	2.5	0	0.016	0.19	0.13	0	24.12	33.04	0.326	1.381	31.66
3	4.25	0	0	3.5	0.140	0	0	0.20	24.17	33.11	0.340	1.441	31.67
4	6.35	0	0	3.5	0.210	0	0	0.20	24.22	33.18	0.410	1.737	31.44
5	7.5	0	0	3.5	0.248	0	0	0.20	24.25	33.22	0.448	1.898	31.32
6	8.5	0	0	3.5	0.281	0	0	0.20	24.27	33.25	0.481	2.038	31.21
Level Trimmed	7.4	2.2	2.5	0	0.244	0.11	0.13	0	24.27	33.25	0.484	2.051	31.20
7	8.0	2.2	2.5	0	0.264	0.11	0.13	0	24.29	33.28	0.504	2.135	31.14
8	8.52	2.2	2.5	0	0.281	0.11	0.13	0	24.31	33.30	0.521	2.207	31.09
9	10.92	2.7	2.8	0	0.360	0.14	0.15	0	24.41	33.44	0.650	2.754	30.69
10	1.25	5	5	0	0.041	0.33	0.33	0	24.43	33.47	0.701	2.970	30.50
11	11.56	4	3	0	0.382	0.23	0.16	0	24.44	33.48	0.772	3.271	30.21

Appendix G

FLUX AND POWER DISTRIBUTIONS

A. D. Callihan

D. Scott

There were, of course, no measurements of the flux or power distribution in the reactor during the actual experiment. These distributions were measured, however, on a zero power, critical mock-up of the experimental reactor over a year earlier. A detailed description of the critical mockup, including the reactor parameters obtained therefrom, may be found in ORNL-1634.¹ The neutron flux distributions obtained from indium and cadmium-covered indium foil measurements, the fission neutron flux distributions obtained by the catcher-

foil method, and the power distributions obtained from aluminum catcher foils, which are of particular interest, are presented here.

NEUTRON FLUX DISTRIBUTIONS

The neutron flux distributions were measured with indium and cadmium-covered indium foils in a number of runs in which a remotely placed uranium disk and an aluminum catcher foil were used to normalize the power from run to run. The results of the bare indium and cadmium-covered indium traverses made at a point 12.06 in. from the center of the reactor are shown in Fig. G.1. The zero of the abscissa is the bottom of the beryllium oxide

¹A. D. Callihan and D. Scott, *Preliminary Critical Assembly for the Aircraft Reactor Experiment*, ORNL-1634 (Nov. 28, 1953).

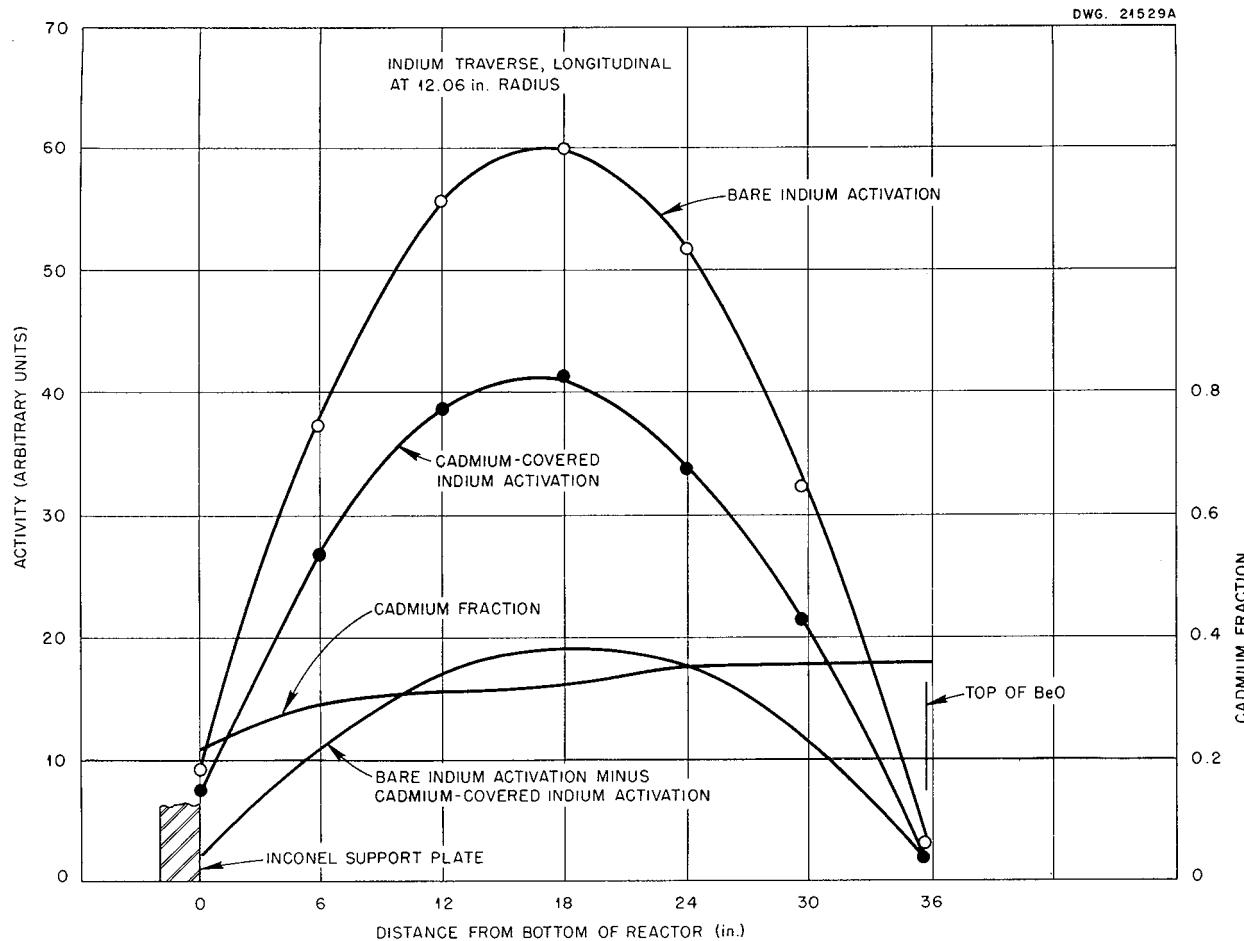


Fig. G.1. Longitudinal Neutron Flux Distribution.

column where it rests on the 1-in.-thick Inconel support plate. The scattering by the Inconel probably accounted for the reduction of the cadmium fraction at this point.

The radial flux traverse at the mid-plane of the reactor with the regulating rod inserted is given in Fig. G.2. The dashed lines on the figure are activities extrapolated from the data obtained in the fine-structure measurements made near the 11-in. position. The wide gap in this traverse was unexplored because of the importance which was attached to the study of a unit core cell in the time available. This emphasis has been at least partially contradicted by the fission flux traverse described in the following section. The strong effect of the center regulating rod assembly is indicated in these curves. The comparatively small flux and cadmium fraction depressions at

the center of the regulating rod accentuated the relative inefficiency of this type of rod and guide tube arrangement for reactor control. In another measurement of the radial flux, this time with the regulating rod withdrawn, the traverses were very similar to that shown in Fig. G.2, but the neutron flux was slightly greater (~8%).

FISSION-NEUTRON FLUX DISTRIBUTION

A measure of the distribution of neutrons that caused fissions was obtained by using the catcher-foil method in which the aluminum foil, together with some uranium, was both bare and cadmium covered. A radial traverse taken at the mid-plane of the reactor is shown in Fig. G.3. The flux of low-energy neutrons produced fission peaks near the reflector and was depressed by the Inconel tube (regulating rod sleeve) at the center. The

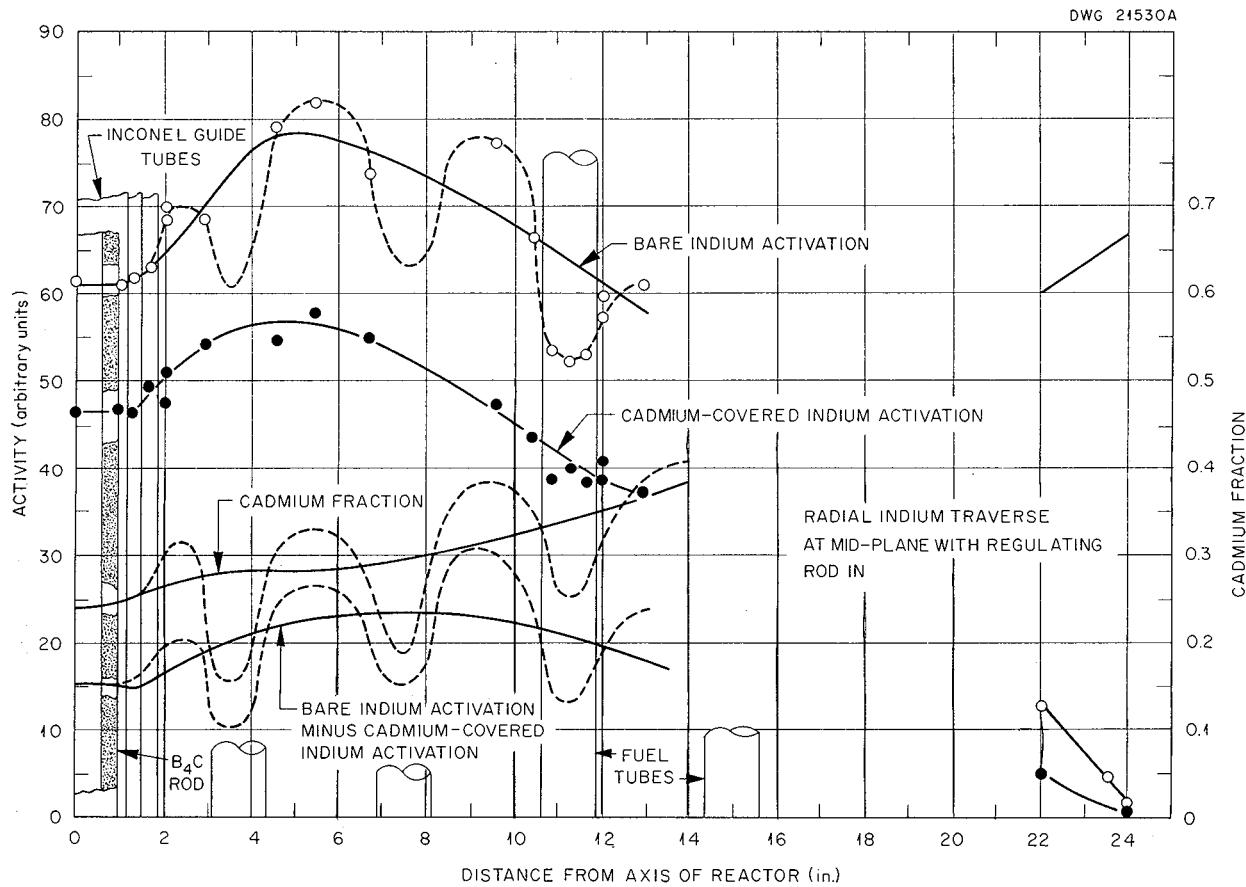


Fig. G.2. Radial Neutron Flux Distribution.

cadmium fraction followed roughly the same pattern. Similar half-length longitudinal traverses are shown in Fig. G.4 for a position 10.09 in. from the center.

POWER DISTRIBUTION

Three longitudinal power distributions in this reactor assembly were measured by using aluminum catcher foils placed against the end surfaces of the short, cast, fuel slugs contained in an Inconel tube. The size of these foils was such that the counting rate from each was higher than necessary for the desired statistics. In the arbitrary units reported, an activity of 50 represents approximately 10^5 counts. Had time permitted, it would have

been desirable to repeat the experiment with smaller foils to improve the resolution, particularly since the results were very sensitive to foil location because of fuel self-shielding. Each catcher foil was nominally located centrally on the axis of a fuel slug. One traverse extended from below the Inconel support plate to above the top of the beryllium oxide; the other two covered the upper half of the core. The data obtained in the fuel tubes at the indicated radii are shown in Fig. G.5. The data of Fig. G.5 are replotted in Fig. G.6 to show the radial power distribution at several elevations in the reactor, all normalized at the center. It is to be noted that the 37.86-in. elevation traverse is 2 in. above the top of the beryllium oxide column.

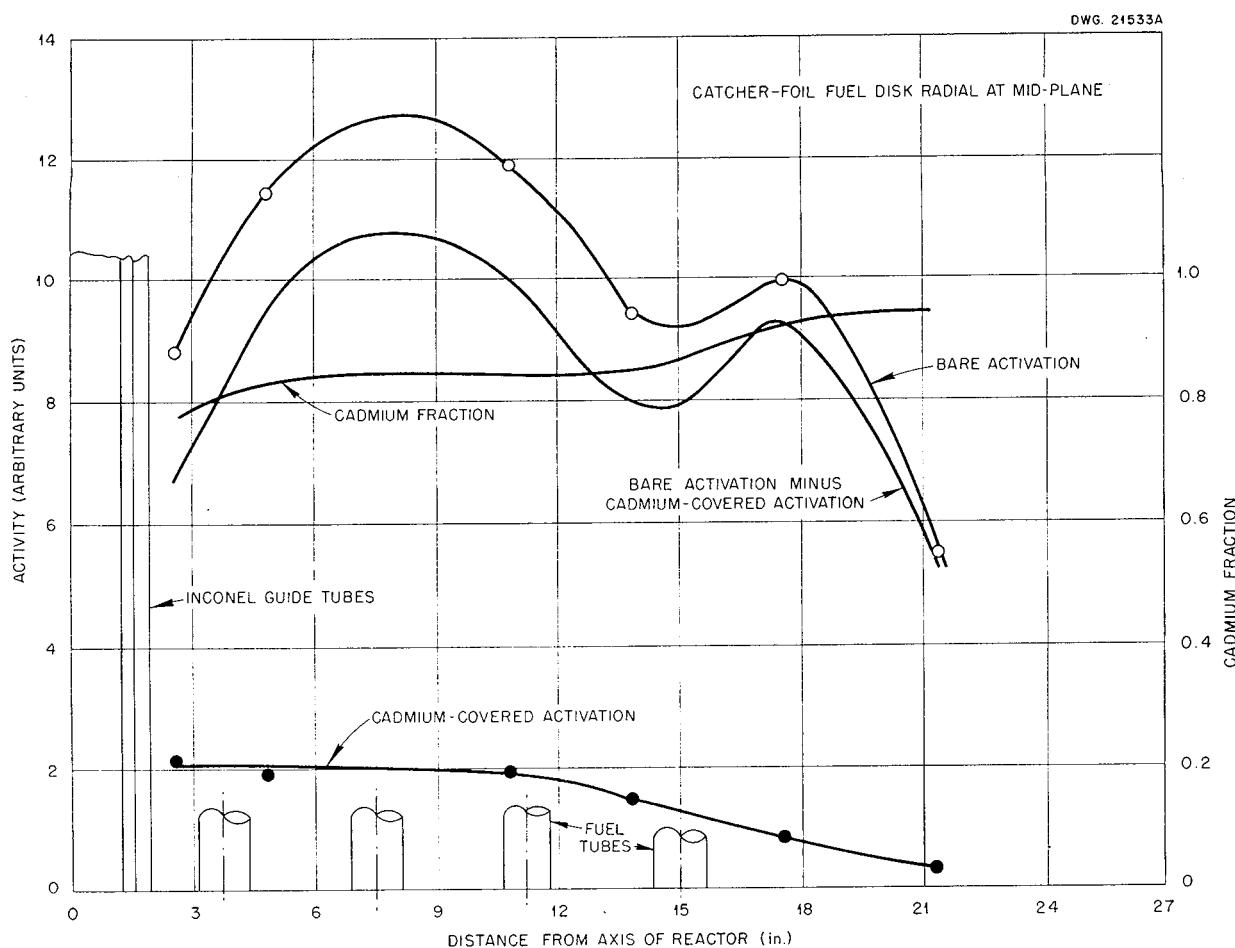


Fig. G.3. Radial Fission Neutron Flux Distribution.

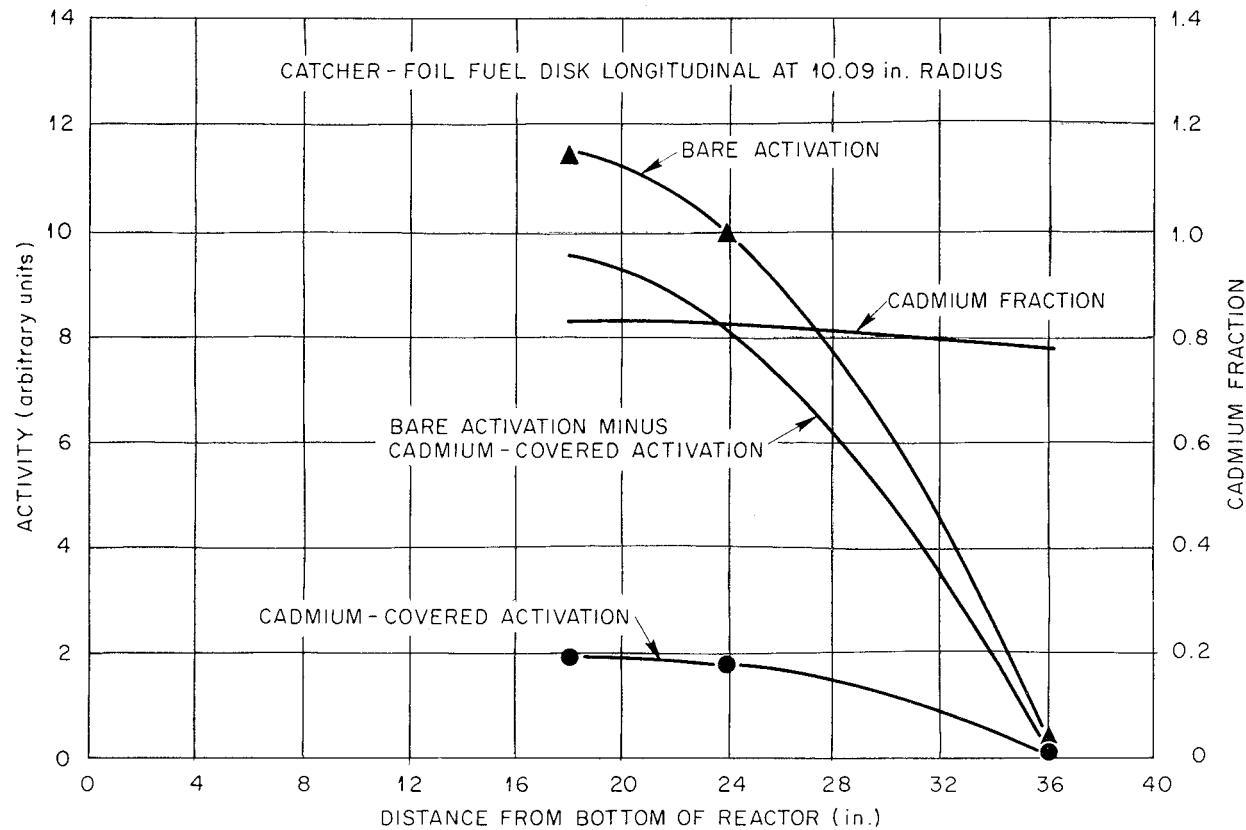


Fig. G.4. Longitudinal Fission Neutron Flux Distribution.

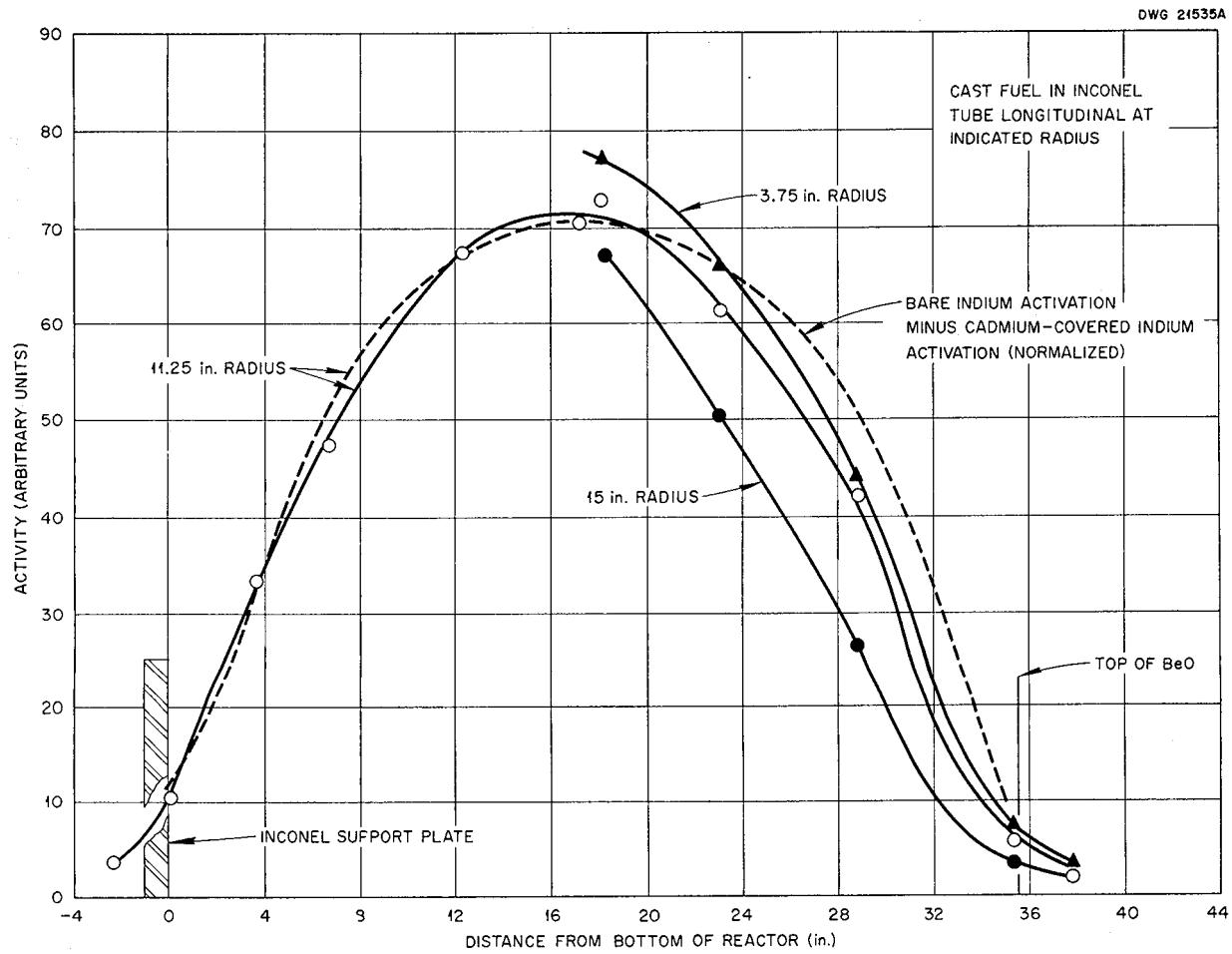


Fig. G.5. Longitudinal Power Traverses.

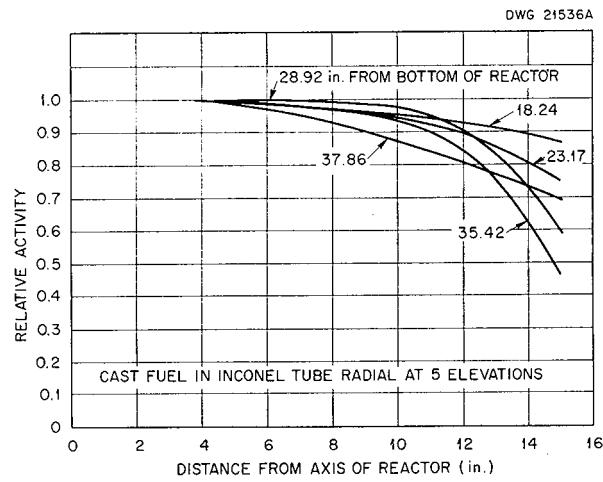


Fig. G.6. Radial Power Traverses.

Appendix H

POWER DETERMINATION FROM FUEL ACTIVATION¹

E. B. Johnson

Perhaps the most basic value obtained from the operation of the ARE was the power level at which it operated. This quantity was determined both from activation of the fuel and from a heat balance. The determination of reactor power from activation of the fuel was based on the measurement of the relative activity of samples of the fuel exposed in the ARE and that exposed in a known flux in the Bulk Shielding Reactor (BSR).

The activity of the aggregate of fission products is not easy to predict because of the large number of isotopes for which calculations would be required. For identical conditions of exposure and decay, that is, for identical flux, exposure time, and waiting period after exposure, the specific activity should be the same, however. Furthermore, at low fluxes the activity should be proportional to the flux.

The ARE was operated at a nominal power level of approximately 1 w for 1 hr, was then shut down, and a sample of the irradiated fuel was withdrawn for counting and analysis. Since the activity in this fuel sample was too low to measure accurately, the test was repeated at an estimated power of 10 w. The ARE experimental program then proceeded as scheduled. Decay curves were obtained from the fuel samples from the ARE and were then compared with the decay curve of a similar fuel sample irradiated in the BSR in a known neutron flux of about the same magnitude. From the relative activity of the samples, a determination of the power of the ARE was made.

THEORY

It has been shown² that the power (in watts) produced in an enriched-fuel thermal reactor is

$$P = 4.264 \times 10^{-11} \times nv_{th} \times G,$$

where G is the number of grams of U^{235} in the volume over which the average thermal-neutron flux is nv_{th} , and the constant, 4.264×10^{-11} , contains

¹This appendix was originally issued as ORNL CF-54-7-11, *Fuel Activation Method for Power Determination of the ARE*, E. B. Johnson (July 31, 1954), and was revised for this report on April 22, 1955.

²J. L. Meem, L. B. Holland, and G. M. McCommon, *Determination of the Power of the Bulk Shielding Reactor, Part III. Measurement of the Energy Released per Fission*, ORNL-1537 (Feb. 15, 1954).

the fission cross section, energy release per fission, and the necessary conversion factors. Obviously, if the thermal-neutron flux and the amount of fuel present are known, it is quite simple to obtain the power. The problem was to obtain the power without measuring the flux in the ARE.

The quantity P/G obtained from the measurement in the BSR will be called $(P/G)_{BSR}$. The decay curve for the two fuel samples irradiated in the BSR is shown in Fig. D.5 of Appendix D. The power production in a given sample is proportional to both the counting rate and the amount of fissionable material in the sample. Thus,

$$\frac{(P/G)_{ARE}}{(P/G)_{BSR}} = \frac{(CR/G)_{ARE}}{(CR/G)_{BSR}}$$

where

CR = counting rate at time t after shutdown,

G = weight of uranium in the sample.

This equation can be rewritten as

$$(P/G)_{ARE} = (P/G)_{BSR} \times \frac{CR_{ARE}}{CR_{BSR}} \times \frac{G_{BSR}}{G_{ARE}}.$$

The total power of the ARE is then the product of the power per gram (in the sample) and the total amount of uranium in the fuel circuit (G_{tot})_{ARE}, or

$$\begin{aligned} P_{ARE} &= (P/G)_{ARE} \times (G_{tot})_{ARE} \\ &= (P/G)_{BSR} \times \frac{CR_{ARE}}{CR_{BSR}} \\ &\quad \times \frac{G_{BSR}}{G_{ARE}} \times (G_{tot})_{ARE}. \end{aligned}$$

The unperturbed thermal-neutron flux in which the samples were exposed in the BSR was 1.895×10^7 neutrons/cm².sec. However, the self-depression³ of the flux by the uranium sample was 0.80. Therefore $(P/G)_{BSR}$ becomes

$$\begin{aligned} (P/G)_{BSR} &= 4.264 \times 10^{-11} \times 1.895 \times 10^7 \times 0.80 \\ &= 6.464 \times 10^{-4} \text{ w/g}. \end{aligned}$$

³W. K. Ergen, private communication.

Each of the fuel samples irradiated in the BSR contained 0.131 g of U²³⁵. Thus

$$P_{ARE} = 6.464 \times 10^{-4} \text{ w/g} \times \frac{CR_{ARE}}{CR_{BSR}}$$

$$\times \frac{0.131}{G_{ARE}} \times (G_{tot})_{ARE}$$

$$= 8.468 \times 10^{-5} \times \frac{CR_{ARE}}{CR_{BSR}}$$

$$\times \frac{(G_{tot})_{ARE}}{G_{ARE}}$$

This equation was then used to determine the power of the ARE as indicated by fuel activation during the previously mentioned operation of 1 hr

at 1- and 10-w nominal power. The instruments which recorded the neutron level (log N, etc.) were then calibrated in terms of reactor power.

EXPERIMENTAL PROCEDURE

The BSR is immersed in a pool of water which serves as moderator, coolant, reflector, and shield. Therefore, any material which is to be activated in the BSR must be placed in a watertight container before immersion in the pool. Capsules to contain the ARE fuel were made of 2S aluminum with screw-type caps and were sealed with a rubber gasket. Each capsule contained approximately 1 g of material; one of the capsules is shown in Fig. H.1.

Since it was desirable to irradiate the capsules in the reactor core, the reactor was loaded with a partial element, containing only half the usual number of plates, in the interior of the lattice, as

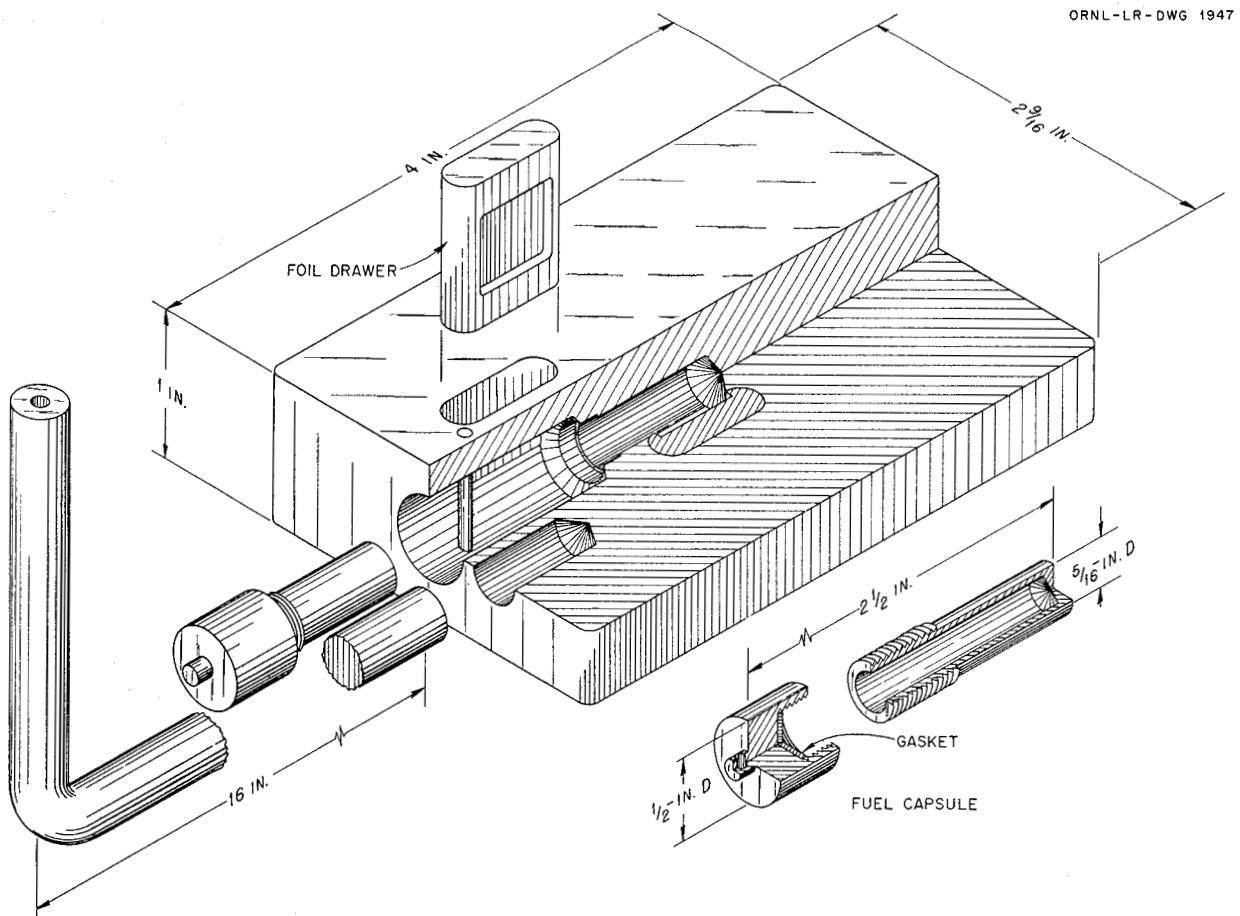


Fig. H.1. Apparatus for Fuel Exposure in the Bulk Shielding Reactor.

shown in Fig. H.2. A lucite holder was designed which would fit inside this partial element and support the capsule to be irradiated at approximately the vertical centerline of the element. Small gold foils for measuring the thermal-neutron flux were mounted in "drawers" adjacent to the capsule, as shown in Fig. H.1. A monitoring foil was placed on the bottom of the lucite block.

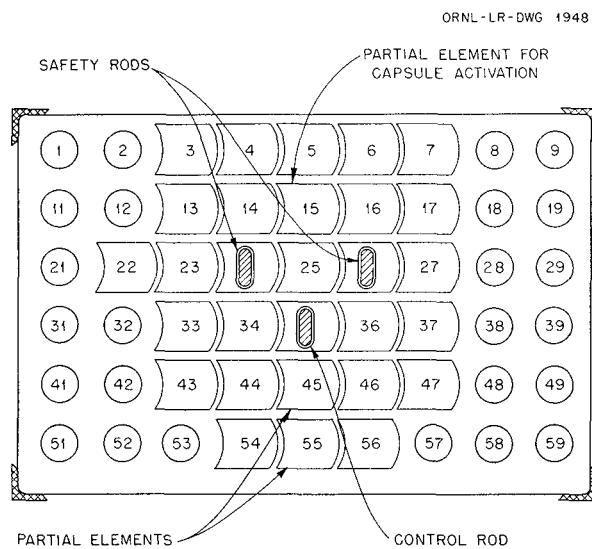


Fig. H.2. Bulk Shielding Reactor Loading (No. 27).

Two samples of each of two ARE-type fuels of different composition were irradiated. One (No. 44) contained 53.5-40.0-6.5 mole % of $\text{NaF-ZrF}_4-\text{UF}_4$ and was the anticipated fuel of the ARE. The other was No. 45, which was the carrier to which the uranium-containing fuel concentrate was added during the critical and low-power experiments; it contained 50-50 mole % of NaF-ZrF_4 .

It was necessary in the BSR to expose the samples in the aluminum capsules; at the ARE the fuel was, of course, first activated and then poured into the capsules. Therefore it was necessary to determine the contribution of the aluminum capsule

to the activity observed. Two empty capsules were exposed (in separate runs) for 1 hr at a nominal power level of 1 w. At the same time, gold foils were exposed in the positions adjacent to the capsule to determine the thermal flux. Similarly, two carrier-filled capsules and two fuel-filled capsules were irradiated, each separately but each for 1 hr at 1 w. The capsules each contained 1 g of material.

The decay curves taken on each capsule were made with two counters because of the difference in disintegration rates between the empty and the fluoride-filled capsules. A scintillation counter was used to obtain the curves for the empty capsules and for the carrier-filled capsules, and the high-pressure ion chamber was used to measure the activity in the fuel-filled capsules. The data for the carrier-filled capsules were converted, on the assumption that all the activity was attributable to sodium, to equivalent counting rates in the high-pressure ion chamber. The assumption that the activity was due to sodium was apparently valid, since the decay curve indicated a half-life of about 15 hr at approximately 6 hr after shutdown.

It was found from the decay curves that the aluminum activity was a factor of approximately 10 less than that of the carrier-filled capsules 3 hr after shutdown and a factor of 450 less than that of the fuel-filled capsules at the corresponding time, and was therefore negligible. The activity in the carrier-filled capsule was about 4% of that in the fuel-filled capsule 6 hr after shutdown. There was essentially no difference between the two different fuel-filled capsules and the two different carrier-filled capsules. For this reason, only one curve is shown for each in Fig. D.5.

The nuclear power of the Aircraft Reactor Experiment was then set on the basis of the activation in fuel samples irradiated for 1 hr at 10 w. This power calibration was the basis of all power levels indicated in the nuclear log up to the last day of the experiment, by which time it had become obvious from the various heat balances that the actual reactor power was considerably higher (app. L). A comparison of the two methods of power calibration is given in Appendix N.

Appendix I

INHOUR FORMULA FOR A CIRCULATING-FUEL REACTOR WITH SLUG FLOW¹

W. K. Ergen

As pointed out in a previous paper,² the circulating-fuel reactor differs in its dynamic behavior from a reactor with stationary fuel, because fuel circulation sweeps some of the delayed-neutron precursors out of the reacting zone, and some delayed neutrons are given off in locations where they do not contribute to the chain reactions. One of the consequences of these circumstances is the fact that the inhour formula usually derived for stationary-fuel reactors,³ requires some modification before it becomes applicable to the circulating-fuel reactor. The inhour formula gives the relation between an excess multiplication factor, introduced into the reactor, and the time constant T of the resulting rise in reactor power. If the inhour formula is known, then the easily measured time constant can be used to determine the excess multiplication factor, a procedure frequently used in the quantitative evaluation of the various arrangements causing excess reactivity. Furthermore, the proper design of control rods and their drive mechanisms depends on the inhour formula.

Frequently, the experiments evaluating small excess multiplication factors are carried out at low reactor power, and the reactor power will then not cause an increase in the reactor temperature. This case will be considered here. In this case, the time dependence of the reactor power P can be described by the following equation:⁴

$$(1) \quad dP/dt$$

$$= (1/\tau)[(k_{ex} - \beta)P + \beta \int_0^{\infty} D(s) P(t-s) ds] .$$

τ is the average lifetime of the prompt neutrons and k_{ex} the excess multiplication factor (or excess reactivity). The meaning of β and $D(s)$ for a

¹This appendix was issued earlier as ORNL CF-53-12-108, *The Inhour Formula for a Circulating-Fuel Nuclear Reactor with Slug Flow*, W. K. Ergen (Dec. 22, 1953).

²William Krasny Ergen, *J. Appl. Phys.*, Vol. 25, No. 6, 702-711 (1954).

³See, for instance, S. Glasstone and M. C. Edlund, *The Elements of Nuclear Reactor Theory*, D. Van Nostrand Co., Inc., 1952, p. 294 ff.

⁴Some authors, for instance Glasstone and Edlund, loc. cit., write the equations corresponding to (1) in a slightly different form. The difference consists in terms of the order $k_{ex}(\tau/T)$ or $k_{ex}\beta$, which are negligibly small.

circulating-fuel reactor has been discussed in some detail in ref. 2. We approximate in the following the actual arrangement by a reactor for which the power distribution and the importance of a neutron are constant and for which all fuel elements have the same transit time $\theta_1 - \theta$ through the outside loop. In this approximation, $\beta D(s)$ is simply the probability that a fission neutron, caused by a power burst at time zero, is a delayed neutron, given off inside the reactor at a time between s and $s+ds$. $D(s)$ is normalized so that

$$(2) \quad \int_0^{\infty} D(s) ds = 1 .$$

If the fuel is stationary, $\beta D(s)$ is the familiar curve obtained by the superposition of 5 exponentials:

$$(3) \quad \beta D(s) = \sum_{i=1}^5 \beta_i \lambda_i e^{-\lambda_i s} .$$

The λ_i are the decay constants of the 5 groups of delayed neutrons, and the β_i are the probabilities that a given fission neutron is a delayed neutron of the i th group.

For the circulating-fuel reactor we first consider the fuel which was present in the reactor at time zero. At any time s , only a fraction of this fuel will be found in the reactor. This fraction is denoted by $F(s)$, and by multiplying the right side of (3) by $F(s)$, we obtain the function $\beta D(s)$ for the circulating-fuel reactor.

Since θ_1 is the total time required by the fuel to pass through a complete cycle, consisting of the reactor and the outside loop, it is clear that at $s = n\theta_1$

$(n = 0, 1, 2 \dots)$, $F(s)$ is equal to 1;

at $s = n\theta_1 + \theta$

$(n = 0, 1, 2 \dots)$, $F(s)$ is equal to zero.

(We assume $\theta_1 \geq 20$ so that the fuel under consideration has not started to re-enter the reactor when the last of its elements leaves the reacting zone.) Between $s = n\theta_1$ and $s = n\theta_1 + \theta$, $F(s)$ decreases linearly, and hence has the value $(n\theta_1 + \theta - s)/\theta$. At $s = n\theta_1 - \theta$ ($n = 1, 2, 3 \dots$),

$F(s)$ is zero, but since the fuel under consideration re-enters the reactor between this moment and $s = n\theta_1$, $F(s)$ increases linearly: $F(s) = (s - n\theta_1 + \theta)/\theta$. For $\beta D(s)$ we thus obtain:

$$(4) \quad \begin{aligned} \beta D(s) &= \frac{n\theta_1 + \theta - s}{\theta} \sum_{i=1}^5 \beta_i \lambda_i e^{-\lambda_i s} && \text{for } n\theta_1 \leq s \leq n\theta_1 + \theta, \quad n = 0, 1, 2, \dots, \\ \beta D(s) &= \frac{s - n\theta_1 + \theta}{\theta} \sum_{i=1}^5 \beta_i \lambda_i e^{-\lambda_i s} && \text{for } n\theta_1 - \theta \leq s \leq n\theta_1, \quad n = 1, 2, 3, \dots, \\ \beta D(s) &= 0 && \text{for } n\theta_1 + \theta \leq s \leq (n+1)\theta_1 - \theta, \quad n = 0, 1, 2, \dots. \end{aligned}$$

Equation (4) is now substituted into Eq. (1), and for P we set $P = P_0 e^{t/T}$. Then

$$\begin{aligned} \frac{T}{T} P_0 e^{t/T} &= (k_{ex} - \beta) P_0 e^{t/T} + \sum_{i=1}^5 \beta_i \lambda_i \left[\sum_{n=0}^{\infty} \int_{n\theta_1}^{n\theta_1 + \theta} \frac{n\theta_1 + \theta - s}{\theta} e^{-\lambda_i s} P_0 e^{(t-s)/T} ds \right. \\ &\quad \left. + \sum_{n=1}^{\infty} \int_{n\theta_1 - \theta}^{n\theta_1} \frac{s - n\theta_1 + \theta}{\theta} e^{-\lambda_i s} P_0 e^{(t-s)/T} ds \right]. \end{aligned}$$

The common factor $P_0 e^{t/T}$ cancels out. The substitution $\sigma = n\theta_1 + \theta - s$ transforms

$$\int_{n\theta_1}^{n\theta_1 + \theta} (n\theta_1 + \theta - s) \exp\{-[\lambda_i + (1/T)]s\} ds$$

into

$$\exp\{-n\theta_1 [\lambda_i + (1/T)]\} \exp\{-\theta [\lambda_i + (1/T)]\} \int_0^\theta \sigma \exp\{[\lambda_i + (1/T)]\sigma\} d\sigma,$$

and the substitution $\sigma = s - n\theta_1 + \theta$ transforms

$$\int_{n\theta_1 - \theta}^{n\theta_1} (s - n\theta_1 + \theta) \exp\{-[\lambda_i + (1/T)]s\} ds$$

into

$$\exp\{-n\theta_1 [\lambda_i + (1/T)]\} \exp\{\theta [\lambda_i + (1/T)]\} \int_0^\theta \sigma \exp\{-[\lambda_i + (1/T)]\sigma\} d\sigma.$$

The geometric series $\exp\{-n[\lambda_i + (1/T)]\theta_1\}$ can now be summed, and the integrals over σ evaluated by elementary methods. After performing all these operations, one obtains the following inhour formula:

$$(5) \quad k_{ex} = \frac{\tau}{T} + \beta - \frac{1}{\theta} \sum_{i=1}^5 \beta_i \lambda_i \frac{\mu_i \theta - 1 + e^{-\mu_i \theta}}{\mu_i^2 [1 - e^{-\mu_i \theta_1}]},$$

$$(6) \quad \mu_i = \lambda_i + (1/T).$$

β is obtained by integrating Eq. (3) from 0 to ∞ . Expressions are obtained which are of the same type as the ones just discussed, and which can be evaluated by the same methods. The result is

$$(7) \quad \beta = \sum_{i=1}^5 \beta_i \frac{\lambda_i \theta - 1 + e^{-\lambda_i \theta} - e^{-\lambda_i \theta_1} (\lambda_i \theta + 1) + e^{-\lambda_i (\theta_1 - \theta)}}{\theta \lambda_i (1 - e^{-\lambda_i \theta_1})}.$$

In spite of the formidable appearance of Eqs. (5), (6), and (7), it is easy to find, for any given θ and θ_1 , the value of k_{ex} which produces a given time constant T .

Furthermore, the following reasoning describes the general features of the equations. Consider first the dependence of k_{ex} on T . If $T = \infty$, $\mu_i = \lambda_i$, and the sum on the right of (5) is equal to β , k_{ex} is equal to zero. This corresponds to the state in which the reactor is just critical. If T becomes very small, the μ_i become very large and in the fraction on the right of (5) the numerator is dominated by $\mu_i\theta$ and the bracket in the denominator by 1. Hence the fraction tends to zero like θ/μ_i , as T goes to zero. If τ is very small, as it is in practice, T will be small as soon as k_{ex} exceeds β by a small amount. Then the complicated sum on the right of (5) is of little importance, and T is determined by $\tau/T = k_{ex} - \beta$, that is, the reactor period is inversely proportional to the excess of the reactivity over the reactivity corresponding to the "prompt critical" condition.

In the stationary-fuel reactor, the k_{ex} which makes the reactor prompt critical is given by $\sum \beta_i$. With circulating fuel, the reactor is prompt critical if $k_{ex} = \beta$, which is less than $\sum \beta_i$, that is, it takes less excess reactivity to make the circulating-fuel reactor prompt critical than to do the same thing to a stationary-fuel reactor. This is physically evident because the fuel circulation renders some of the delayed neutrons ineffective. That β is less than $\sum \beta_i$ can also be verified mathematically.

For T intermediate between very small positive values and ∞ , we consider again the analogy to the stationary-fuel reactor. Here the inhour formula reads:⁵

$$(8) \quad k_{ex} = \frac{\tau}{T} + \sum_{i=1}^5 \frac{\beta_i}{1 + \lambda_i T} .$$

For every positive k_{ex} there is one, and only one, positive time constant T , and vice versa. This is a consequence of the fact that k_{ex} is a monotonic decreasing function of T , for if this monotony did not exist, there could be several positive T values corresponding to a given value of k_{ex} , or vice versa. In the circulating-fuel reactor the situation is qualitatively the same; the fractions under the

⁵See Glasstone and Edlund, *loc. cit.*, p. 301, Eq. 10.29.1. See also preceding footnote.

sum in Eq. (5) are essentially of the form

$$\frac{x - 1 + e^{-x} - e^{-ax}(x + 1) + e^{-(a-1)x}}{x^2[1 - e^{-ax}]}$$

$$(x = \mu_i \theta_1, a = \theta_1/\theta) ,$$

and an expression of this form can be shown to be a monotonic decreasing function of positive x ;⁶ the expression is thus a monotonic increasing function of T [see Eq. (6)], and as T increases k_{ex} decreases monotonically, according to Eq. (5); for every positive k_{ex} there is one, and only one, positive T , and vice versa. This, of course, does not preclude that there exists for a given k_{ex} several negative T values, in addition to the one positive value. Negative T correspond, however, to decaying exponentials, which are of no importance if the rise in power is observed for a sufficiently long time.

Consider now the behavior of Eq. (5) with variation of θ , the transit time of the fuel through the reactor, and of θ_1 , the transit time of the fuel through the whole loop. If θ (and hence also θ_1) is very large compared to all $1/\lambda_i$ and $1/\mu_i$, Eq. (5) reduces to Eq. (8), the inhour formula for the stationary-fuel reactor. The circulation is so slow that the reactor behaves as if the fuel were stationary, inasmuch as all delayed neutrons, even the ones with the long-lived precursors, are given off inside the reacting zone, before much fuel reaches the outside. On the other hand, if θ_1 and, hence, also θ , is small compared to all $1/\lambda_i$, that is, if the transit time of the fuel through the complete loop is small compared to the mean life of even the short-lived delayed-neutron precursors, then for $T \gg \theta$

$$(9) \quad k_{ex} = \frac{\tau}{T} + \frac{\theta}{\theta_1} \sum_{i=1}^5 \frac{\beta_i}{1 + \lambda_i T} .$$

This is the same as the inhour formula for the stationary-fuel reactor, except that all the fission yields β_i are decreased by the factor θ/θ_1 . This is physically easy to understand, since θ/θ_1 is just the probability that a given delayed neutron is born inside the reactor.

Of interest is the intermediate case, in which θ

⁶W. K. Ergen, *The Behavior of Certain Functions Related to the Inhour Formula of Circulating Fuel Reactors*, ORNL CF-54-1-1 (Jan. 15, 1954).

is smaller than the mean life of the long-lived delayed-neutron precursors and larger than the mean life of the short-lived precursors. In that case, the long-delayed neutrons act approximately according to Eq. (9) and are reduced by the factor θ/θ_1 . On the other hand, the neutrons with the short-lived precursors behave approximately like Eq. (8) and are not appreciably reduced. Hence, a small excess reactivity enables the reactor to

increase its power without "waiting" for the not very abundant long-delayed neutrons. The reactor goes to fairly short time constants with surprisingly small excess reactivities. However, to make the reactor prompt critical, that is, to enable it to exponentiate without even the little-delayed neutrons, takes a substantial excess reactivity because of the almost undiminished amount of the latter neutrons.

Appendix J

CALIBRATION OF THE SHIM RODS

Three essentially independent methods were used to find the value of the shim rods in terms of reactivity. The first method involved an analysis of the counting rate data taken during the critical experiment, and the second was a calibration of shim rod No. 3 in terms of the regulating rod. The agreement between these two methods was very good. As a check on the general shape of the reactivity curves as a function of rod position, the rods were also calibrated by using the fission chambers. The various methods are discussed in detail below.

CALIBRATION FROM CRITICAL EXPERIMENT DATA

After about one-half the critical mass of uranium had been added to the system, the counting rates of the two fission chambers and the BF_3 counter were taken as a function of shim rod position for each subsequent fuel addition until criticality was reached (as described in the main body of this report, chap. 4). Because the fission chamber counting rates were subject to the phenomenon noted in Appendix H, only the BF_3 counter data were used in the rod calibration.

From the BF_3 counting rates for each rod position taken after a given fuel injection, the multiplication M was determined from the relationship

$$M = \frac{N}{N_0} ,$$

where

N = counting rate for a given fuel concentration and shim rod setting,

N_0 = counting rate before start of enrichment.

For each value of M the value of the multiplication factor k was determined:

$$k = 1 - \frac{1}{M} .$$

Figure 4.9 of Chapter 4 shows k plotted as a function of the uranium in the system for rod positions of 20, 25, 30, and 35 in.

The shim rod calibration was obtained from Fig. 4.9 by first making a cross plot of k against rod position at the critical mass, as shown in

Fig. J.1. Then, with this plot, a value of $(\Delta k/k)/\text{in.}$ was obtained for every 1-in. movement of the shim rods from no insertion to 16 in. of insertion of the rods. A plot of $(\Delta k/k)/\text{in.}$ as a function of rod position is given in Fig. J.2, and the data are tabulated in Table J.1.

In order to find the integrated reactivity, or total worth of the rods, in terms of $(\Delta k/k)$ as a function of the number of inches of insertion, the curve of Fig. J.2 was divided into three sections. Over each section the curves were fitted to a formula of the form

$$\alpha = Ad^2 + Bd + C ,$$

where $\alpha = (\Delta k/k)/\text{in.}$. The formula and its integral, which were applied to the three sections of the curve, are given in Table J.2. For each section, then, the integrated reactivity was found by integrating over the α curves. The integrated curves were of the form

$$\rho = \frac{\Delta k}{k} = A'd^3 + B'd^2 + C'd .$$

The three sections into which the curve of Fig. J.2

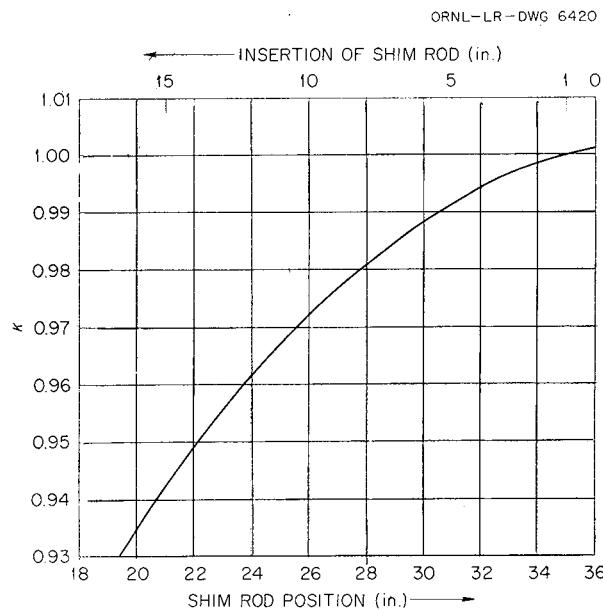


Fig. J.1. Shim Rod Position as a Function of k at Criticality.

TABLE J.1. CALIBRATION OF SHIM RODS FROM FUEL ADDITION DURING CRITICAL EXPERIMENT

Rod Position		Average Insertion of Shim Rods (in.)	Average k	Δk	Movement of Shim Rods, Δd (in.)	3 Rods [($\Delta k/k$)/in.]	Average per Rod [($\Delta k/k$)/in.]
Interval Taken (in.)	Average Rod Position (in.)						
36 to 35	35.5	0.5	1.0	0.001	1	0.001	0.00033
35 to 34	34.5	1.5	0.9992	0.0015	1	0.00150	0.00050
34 to 33	33.5	2.5	0.9975	0.0020	1	0.00200	0.00067
32 to 33	32.5	3.5	0.9953	0.0025	1	0.00251	0.00083
31 to 32	31.5	4.5	0.9926	0.0028	1	0.00282	0.00094
30 to 31	30.5	5.5	0.9895	0.0032	1	0.00323	0.00108
29 to 30	29.5	6.5	0.9862	0.0035	1	0.00355	0.00118
28 to 29	28.5	7.5	0.9825	0.0038	1	0.00387	0.00129
27 to 28	27.5	8.5	0.9785	0.0041	1	0.00419	0.00140
26 to 27	26.5	9.5	0.9743	0.0045	1	0.00462	0.00154
25 to 26	25.5	10.5	0.9695	0.0050	1	0.00516	0.00172
24 to 25	24.5	11.5	0.9643	0.0055	1	0.00570	0.00190
23 to 24	23.5	12.5	0.9585	0.0060	1	0.00626	0.00209
22 to 23	22.5	13.5	0.9523	0.0064	1	0.00672	0.00224
21 to 22	21.5	14.5	0.9458	0.0069	1	0.00730	0.00243
20 to 21	20.5	15.5	0.9386	0.0075	1	0.00799	0.00266

TABLE J.2. FORMULA (AND INTEGRAND) FITTED TO SHIM ROD SENSITIVITY CURVE

Formula No.	Range of Use (in.)	Type	Formula*
1	0 to 8	Differential	$\alpha = -0.0006d^2 + 0.0187d + 0.0239$
2	8 to 16	Differential	$\alpha = 0.0005d^2 + 0.0055d + 0.059$
3	16 to 18	Differential	$\alpha = -0.0045d^2 + 0.1655d - 1.221$
4	0 to 8	Integral	$\rho = -0.0002d^3 + 0.00935d^2 + 0.0239d$
5	8 to 16	Integral	$\rho = 0.000167d^3 + 0.00275d^2 + 0.059d$
6	16 to 18	Integral	$\rho = -0.0015d^3 + 0.0875d^2 - 1.221d$

* $\alpha = (\Delta k/k)$ /in.

$\rho = \Delta k/k$

was divided and the corresponding formulas which were fitted to the curve are given in Table J.2.

In the case of the integrated curves, the $\Delta k/k$ found by integration in the range of the curve was added to the total $\Delta k/k$ of the previous curve to give the total $\Delta k/k$ to the point of integration. The resulting worth, $(\Delta k/k)$, of the shim rods over the first 18 in. of their movement is shown in Fig. J.3 and the data are tabulated in Table J.3.

It should be noted that the last 2 in. of the curve

of Fig. J.2 (16 to 18 in.) was extrapolated. The basis for the extrapolation is the curve shown in Fig. D.4 of Appendix D, which is a calibration of an ARE regulating rod made during some preliminary experiments done in the Critical Experiments Facility. The shim rods were assumed to give the same type of curve.

If it were assumed that the last 18 in. of the shim rods gave a shape of $\Delta k/k$ vs rod insertion which was essentially the image of the first

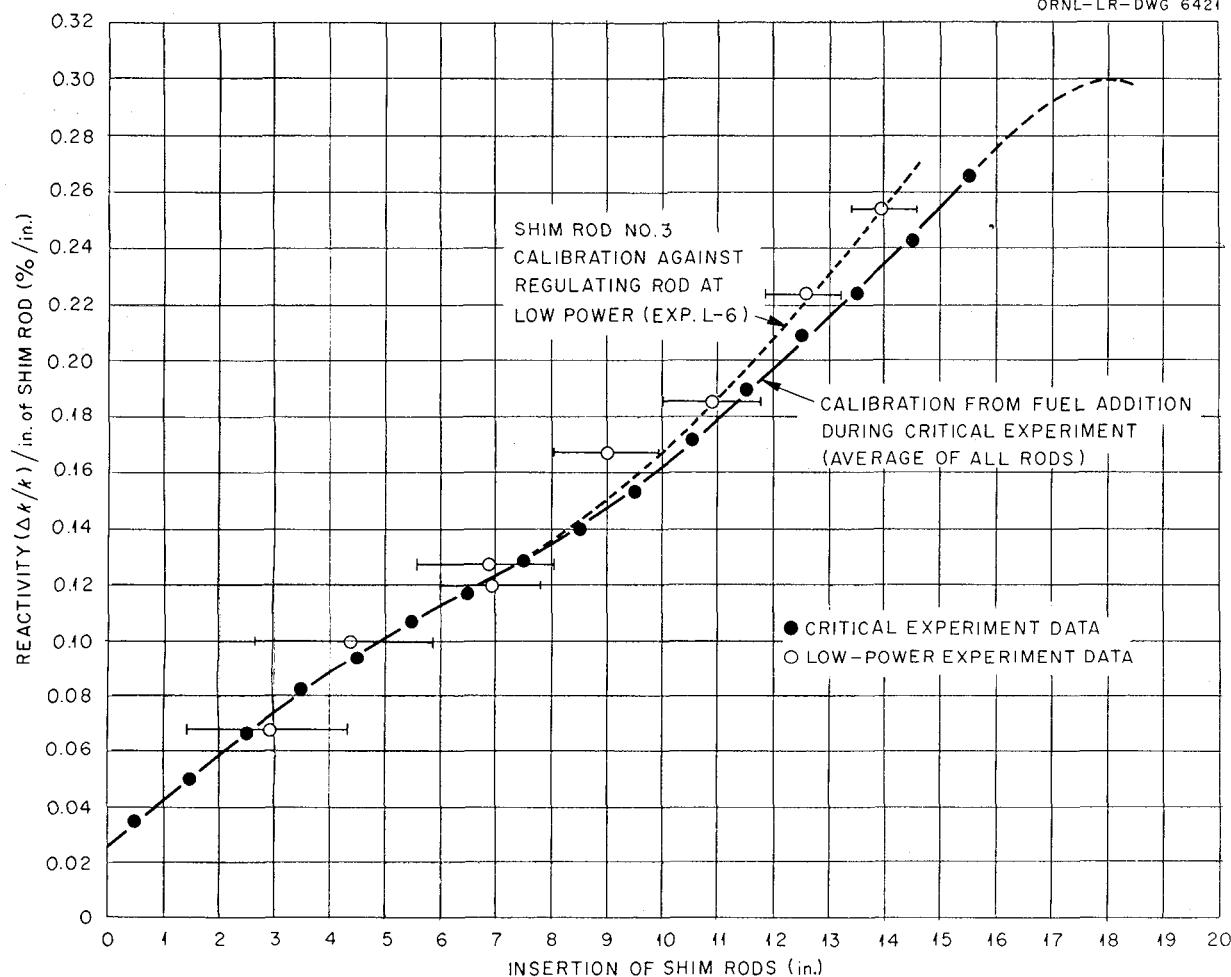


Fig. J.2. Differential Shim Rod Sensitivity.

18 in. (see Appendix D, Fig. D.3), then the total worth of a shim rod was 5.8% ($\Delta k/k$) and the total worth of all three rods was about 17% ($\Delta k/k$).

CALIBRATION AGAINST THE REGULATING ROD

In Exp. L-6, with the reactor at a power of 1 watt (nominal), shim rods Nos. 1 and 2 were set at predetermined positions. Then shim rod No. 3 was moved over various small increments of its travel and thus calibrated against the regulating rod. With the reactor on servo the regulating rod then moved automatically a compensating distance, this distance being roughly 10 in. of its travel. From the previous measurement of the worth of the regulating rod of ($\Delta k/k$)/in. of

0.033%/in. and the ratio of the movement of shim rod No. 3 and the regulating rod, a calibration of No. 3 shim rod was obtained over the first 14 inches of its travel (starting from the out position).

Figure J.2 shows the results of this method of calibration (dashed curve), and the data are listed in Table J.4. The agreement between the two methods of calibration was surprisingly good. Since the increments of shim rod movement were larger in this method than in the preceding method and since there were other sources of error, such as the error in the movement of the shim rod position indicators on the reactor console, no attempt was made to use this curve (dashed curve, Fig. J.2) to find the integrated value of $\Delta k/k$ over the rod.

TABLE J.3. CALCULATION OF SHIM ROD REACTIVITY FROM FUEL ADDITION

Insertion of Shim Rod, d (in.)	Differential Calibration						Integral Calibration				Over Range ^c of Formula	Total ^d
	d^2	d^3	Formula ^a	Ad^2	Bd	$(\Delta k/k)/\text{in.}$ (%/in.)	Formula ^b	$A'd^3$	$B'd^2$	$C'd$		
1	1	1	1	-0.0006	0.0187	0.0420	4	-0.0002	0.00935	0.0239	0.0331	0.0331
2	4	8	1	-0.0024	0.0374	0.0589	4	-0.0016	0.0374	0.0478	0.0836	0.0836
3	9	27	1	-0.0054	0.0561	0.0746	4	-0.0054	0.0842	0.0717	0.151	0.151
4	16	64	1	-0.0096	0.0748	0.0891	4	-0.0128	0.1496	0.0956	0.232	0.232
5	25	125	1	-0.0150	0.0935	0.102	4	-0.0250	0.2238	0.1195	0.328	0.328
6	36	216	1	-0.0216	0.112	0.114	4	-0.0432	0.3366	0.1434	0.437	0.437
7	49	343	1	-0.0294	0.131	0.125	4	-0.0686	0.4581	0.1673	0.557	0.557
8	64	512	1	-0.0384	0.150	0.135	4	-0.1024	0.5984	0.1912	0.687	0.687
			2	+0.032	0.0055	0.135	5	+0.0855	0.1760	0.4720	0	0.687
9	81	729	2	0.0405	0.0495	0.149	5	+0.1217	0.2228	0.5310	0.142	0.829
10	100	1000	2	0.0500	0.0550	0.164	5	0.1670	0.2750	0.5900	0.299	0.986
11	121	1331	2	0.0605	0.0605	0.180	5	0.2223	0.3328	0.6490	0.470	1.158
12	144	1728	2	0.0720	0.0660	0.197	5	0.2886	0.3960	0.7080	0.659	1.346
13	169	2197	2	0.0845	0.0715	0.215	5	0.3669	0.4648	0.7670	0.865	1.552
14	196	2744	2	0.0980	0.0720	0.234	5	0.4583	0.5390	0.8260	1.117	1.804
15	225	3375	2	0.1125	0.0825	0.254	5	0.5636	0.6187	0.8850	1.334	2.021
16	256	4096	2	0.1280	0.0880	0.275	5	0.6840	0.7040	0.9440	1.599	2.286
			3	-1.152	2.648	0.275	6	-6.144	21.184	-19.536	0	2.286
17	289	4913	3	-1.300	2.8135	0.292	6	-7.3695	23.9147	-20.757	0.3112	2.597
18	324	5832	3	-1.458	2.979	0.300	6	-8.7480	26.811	-21.978	0.612	2.898

^aDifferential formulas were of the form $(\Delta k/k) \text{ in.} = Ad^2 + Bd + c$ Formula 1: $(\Delta k/k)/\text{in.} = -0.0006d^2 + 0.0187d + 0.0239$ Formula 2: $(\Delta k/k)/\text{in.} = 0.0005d^2 + 0.0055d + 0.059$ Formula 3: $(\Delta k/k)/\text{in.} = -0.0045d^2 + 0.1655d - 1.221$ ^bIntegral formulas were of the form $\Delta k/k = A'd^3 + B'd^2 + C'd$ Formula 4: $\Delta k/k = -0.0002d^3 + 0.00935d^2 + 0.0239d$ Formula 5: $\Delta k/k = 0.000167d^3 + 0.00275d^2 + 0.059d$ Formula 6: $\Delta k/k = -0.0015d^3 + 0.08275d^2 - 1.221d$ ^c d_1 = lower limit of formula^d d_2 = position integrated toRanges: Formulas 1 and 4, $d = 0$ to 8 in.Formulas 2 and 5, $d = 8$ to 16 in.Formulas 3 and 6, $d = 16$ to 18 in.^dTotal $\Delta k/k$, adding area from each section

TABLE J.4. CALIBRATION OF SHIM ROD NO. 3 AGAINST REGULATING ROD

Experiment L-6

Run No.	Shim Rod	Shim Rod	Shim Rod No. 3				Regulating Rod			Shim Rod	Shim Rod
	No. 1 Position (in.)	No. 2 Position (in.)	Start Position (in.)	Stop Position (in.)	Average Position (in.)	Movement Δd_s (in.)	Start Position (in.)	Stop Position (in.)	Movement Δd_R (in.)	$= 0.033 \frac{\Delta d_R}{\Delta d_s}$ (%/in.)	Average Insertion (in.)
1A-1B	35.0	36.0	30.0	33.3	31.65	3.3	13.0	3.0	10.0	0.100	4.35
1C-1D	35.0	36.0	30.0	18.1	29.05	1.9	6.5	13.4	6.9	0.120	6.95
3-4	27.0	26.6	35.5	30.6	33.05	4.9	3.1	13.2	10.1	0.068	2.95
5-6	28.0	27.4	30.6	28.0	29.3	2.6	3.0	13.1	10.1	0.128	6.7
7-8	29.1	28.9	28.0	26.0	27.0	2.0	3.0	13.2	10.2	0.168	9.0
9-10	30.0	30.0	26.0	24.2	25.1	1.8	2.95	13.0	10.05	0.183	10.9
11-12	32.8	31.9	24.2	22.7	23.45	1.5	2.9	13.1	10.2	0.224	12.55
13-14	35.0	36.0	22.7	21.4	22.05	1.3	3.2	13.2	10.0	0.254	13.95

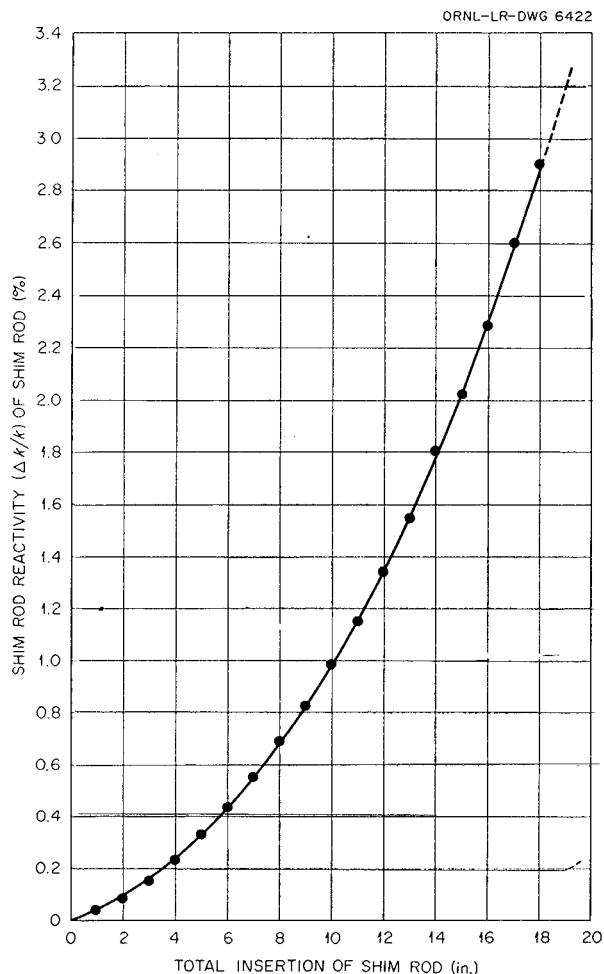


Fig. J.3. Integral Calibration of Shim Rods as a Function of Position.

CALIBRATION BY USING THE FISSION CHAMBERS

A third calibration of the shim rods was attempted during the critical experiments in which the counting rate of the neutron detectors was taken as a function of shim rod position for two different uranium concentrations.

The reactivity was then obtained from the counting rates by using the relationship

$$k = 1 - \frac{1}{M},$$

and a plot of k as a function of rod position then gave a check on the general shape of the curve. Figure J.4 shows the k vs rod position for fission chambers 1 and 2. Because the uranium concentration in the system was low for both the runs the fission chambers were showing a subcritical

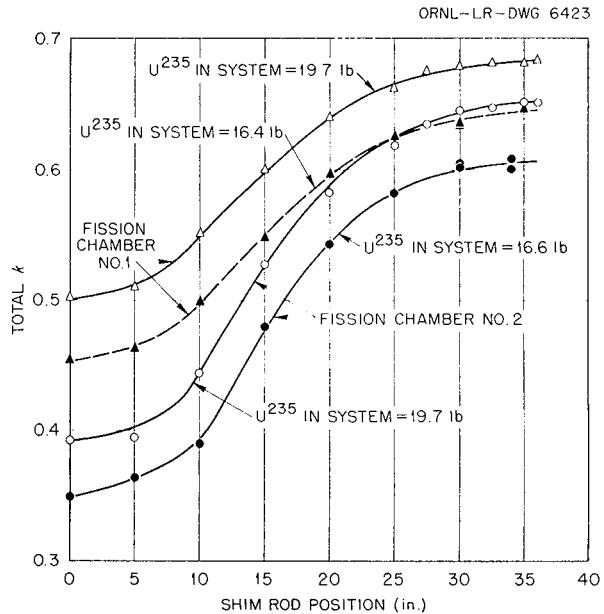


Fig. J.4. Calibration of Shim Rods from Fission Chamber Data.

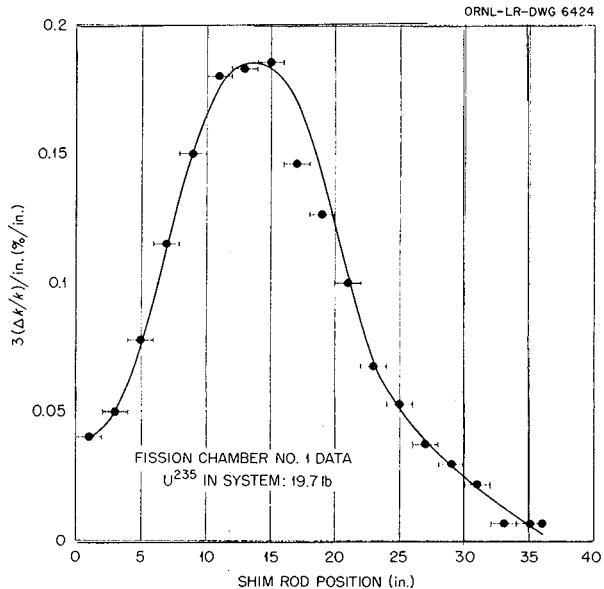


Fig. J.5. Reactivity as a Function of Shim Rod Position.

multiplication M greater than the actual value, as discussed in Appendix E. Therefore, the absolute values of k , as calculated from the counting rates, are in error. Nevertheless, the general shape of the curve is experimental verification of the curve shown in Fig. D.3 of Appendix D. Figure J.5 shows the value of $(\Delta k/k)/in.$ vs rod position,

as obtained from one of the curves of Fig. 4.10. Again, the general shape of this curve is about the same as shown in Fig. D.3 of Appendix D,

but its absolute magnitude is not meaningful.

The data from which Figs. 4.10 and 4.11 were plotted are given in Tables J.5 and J.6.

TABLE J.5. REACTIVITY OF THE SHIM RODS vs ROD POSITION

U ²³⁵ in System (lb)	Rod Position (in.)	Fission Chamber No. 1			Fission Chamber No. 2			BF ₃ Counter		
		Counting Rate N (counts/sec)	N ₀ /N	k	Counting Rate N (counts/sec)	N ₀ /N	k	Counting Rate N (counts/sec)	N ₀ /N	k
16.6	0	17.52	0.5457	0.4543	25.00	0.6512	0.3488	6.00	0.7483	0.2517
	5	17.60	0.5375	0.4625	25.52	0.6379	0.3621	6.05	0.742	0.258
	10	18.85	0.5019	0.4981	26.69	0.6100	0.3900	6.51	0.690	0.310
	15	20.93	0.4520	0.5480	31.33	0.5196	0.4804	6.40	0.702	0.298
	20	23.44	0.4036	0.5964	35.63	0.4569	0.5431	6.67	0.673	0.327
	25	25.23	0.3750	0.6250	38.91	0.4184	0.5816	7.01	0.640	0.360
	30	26.00	0.3638	0.6362	40.93	0.3978	0.6022			
	30	25.87	0.3657	0.6343	41.12	0.3952	0.6048	6.72	0.668	0.332
	35	26.83	0.3526	0.6474	41.76	0.3898	0.6011	6.80	0.660	0.340
	35	26.85	0.3523	0.6477	41.65	0.3909	0.6091	6.77	0.663	0.337
19.7	0	18.99	0.4982	0.5018	26.83	0.6068	0.3932	6.27	0.716	0.284
	5	19.31	0.4899	0.5101	26.88	0.6057	0.3943	6.43	0.698	0.302
	10	21.07	0.4490	0.5510	29.28	0.5560	0.444	6.56	0.684	0.316
	15	23.63	0.4003	0.5997	34.43	0.4728	0.5272	6.91	0.650	0.350
	20	26.21	0.3609	0.6391	38.99	0.4175	0.5825	7.04	0.638	0.362
	25	28.08	0.3369	0.6631	42.67	0.3815	0.6185	7.28	0.617	0.383
	27.5	29.23	0.3236	0.6764	44.59	0.3651	0.6349	7.15	0.628	0.372
	30	29.55	0.3201	0.6793	45.97	0.3541	0.6459	7.01	0.640	0.360
	32.5	29.76	0.3179	0.6821	46.19	0.3525	0.6475	7.04	0.638	0.362
	35	29.76	0.3179	0.6821	46.83	0.3476	0.6524	7.09	0.633	0.367
	36	29.90	0.3164	0.6836	46.81	0.3478	0.6522	7.16	0.627	0.373

TABLE J.6. REACTIVITY AS A FUNCTION OF SHIM ROD POSITION (FROM FISSION CHAMBER DATA)

U^{235} in System (lb)	Limits of d	d_{av}	k_{av}	Δk	Δd (in.)	$3(\Delta k/k)/in.$
19.7	0 to 2	1	0.502	0.04	2	0.0398
	2 to 4	3	0.5065	0.05	2	0.0494
	4 to 6	5	0.5125	0.08	2	0.0780
	6 to 8	7	0.523	0.12	2	0.1147
	8 to 10	9	0.532	0.16	2	0.1503
	10 to 12	11	0.555	0.20	2	0.1801
	12 to 14	13	0.574	0.21	2	0.1829
	14 to 16	15	0.596	0.22	2	0.1853
	16 to 18	17	0.6155	0.18	2	0.1462
	18 to 20	19	0.632	0.16	2	0.1266
	20 to 22	21	0.6465	0.13	2	0.1005
	22 to 24	23	0.6575	0.09	2	0.0684
	24 to 26	25	0.6655	0.07	2	0.0526
	26 to 28	27	0.6715	0.05	2	0.0372
	28 to 30	29	0.676	0.04	2	0.0296
	30 to 32	31	0.6795	0.03	2	0.0221
	32 to 34	33	0.6815	0.01	2	0.0073
	34 to 36	35	0.6825	0.01	2	0.0073

Appendix K

CORRELATION OF REACTOR AND LINE TEMPERATURES

An effect which was noted late in the operation of the ARE was that fuel and sodium line temperatures indicated in the basement disagreed quite radically with those recorded in the control room. It so happened that all the basement indicators gave line temperatures measured by thermocouples outside the reactor thermal shield, while the temperatures recorded in the control room were measured by thermocouples all located within the thermal shield. When this was first discovered it was thought that helium from the rod-cooling system blowing on the thermocouples inside the thermal shield was making them read low. Turning the rod cooling blowers on and off, however, was demonstrated to have no effect on the thermocouples, and therefore at the end of the experiment no positive explanation for these temperature discrepancies had been found.

This situation has created serious difficulties in trying to analyze the data for this report. There was evidence that the discrepancies were intensified during operation at high power. Nevertheless, when nearly isothermal conditions existed, it was found that the absolute magnitude of the measurements made by the thermocouple within the thermal shield were incorrect, but the rates of change obtained from the data were correct. The temperatures read on the basement instruments were considered to be correct for several reasons. First, the temperature indications available in the basement were much more numerous than those in the control room, and the thermocouple sensing elements for these indicators were all located along lines outside the thermal shield; the temperatures agreed with each other to ± 10 deg from the average. Equilibrium conditions prevailed across the pipes because of the insulation. Also, there were many reasons for the thermocouples to indicate higher than actual temperatures, but none for lower than actual indications.

In order to use the temperature data from the experiment it was necessary to correlate the temperature data obtained in the control room with those obtained in the basement. The correlations were then used to correct temperature data obtained in the control room.

The results of the temperature correlations for the fuel system are shown in Figs. K.1, K.2, and K.3. The agreement between the low-power line

temperatures (Fig. K.1) reflects the attention which was given to calibrating these thermocouples in the isothermal condition. The curves in Figs. K.2

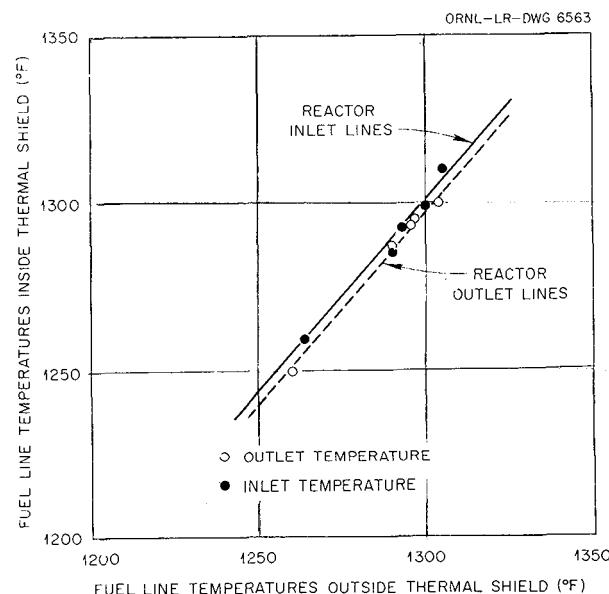


Fig. K.1. Correlation Between Fuel Line Temperatures Measured Inside and Outside the Reactor Thermal Shield During Subcritical and Low-Power Experiments.

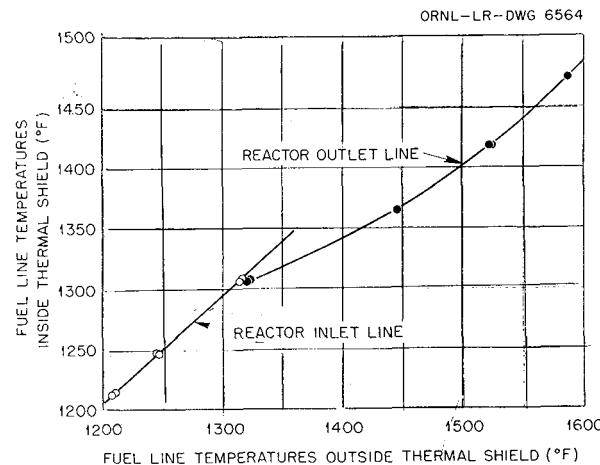


Fig. K.2. Correlation Between Fuel Line Temperatures Measured Inside and Outside the Reactor Thermal Shield During High-Power Experiments.

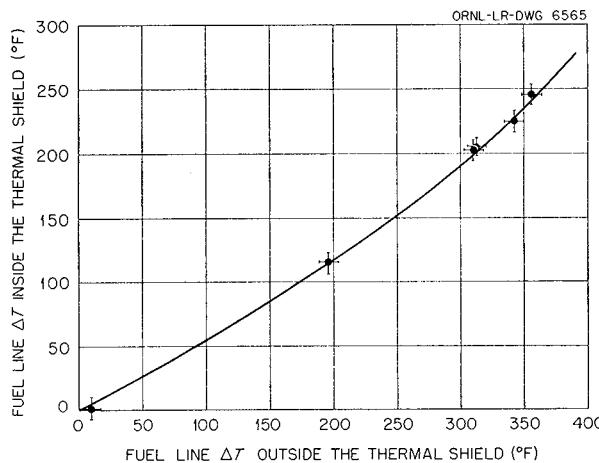


Fig. K.3. Correlation Between Fuel Temperature Differentials Measured Inside and Outside the Thermal Shield.

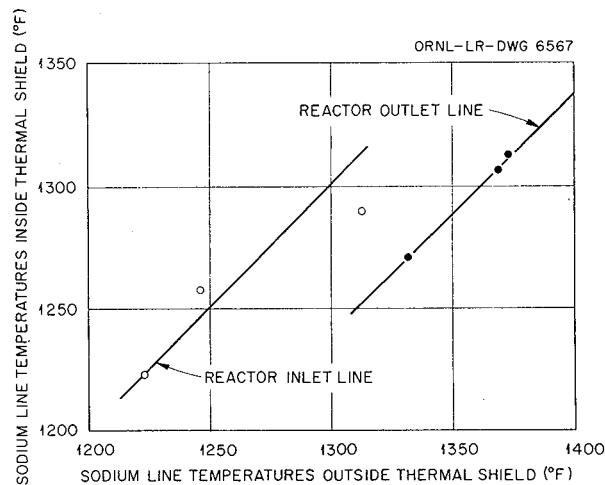


Fig. K.5. Correlation Between Sodium Line Temperatures Measured Inside and Outside the Thermal Shield During High-Power Experiments.

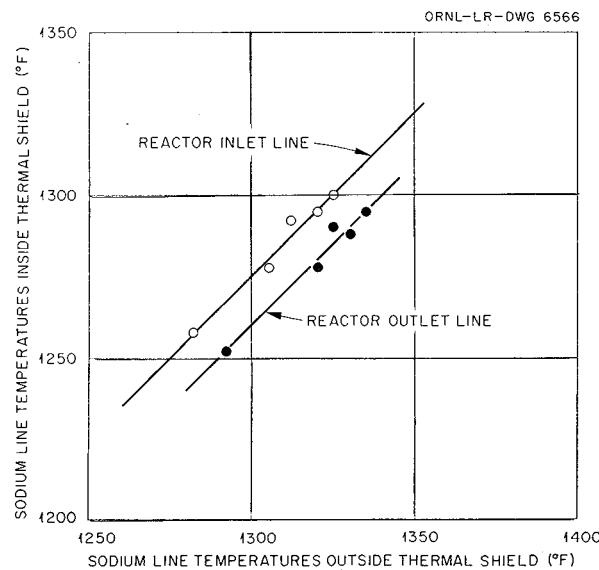


Fig. K.4. Correlation Between Sodium Line Temperatures Measured Inside and Outside the Thermal Shield During Low-Power Experiments.

and K.3, both of which were obtained from data taken during operation at high (>200 kw) power, show the anomaly in question.

The analogous data for the sodium system are shown in Figs. K.4, K.5, and K.6. It is evident from Fig. K.4 that an isothermal condition was never attained in the sodium system, since both

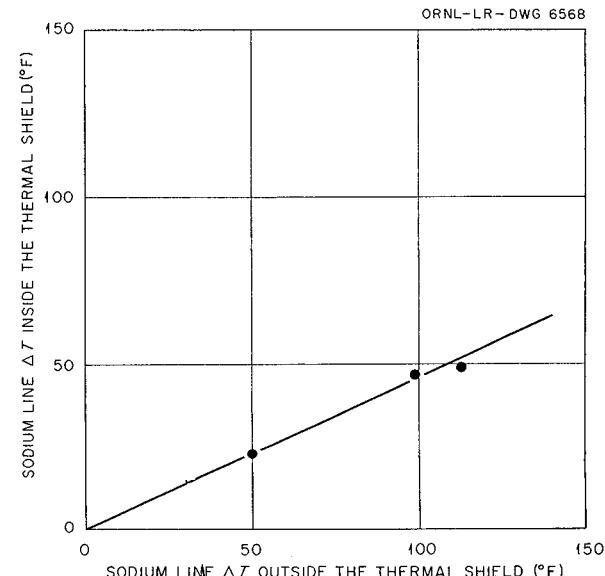


Fig. K.6. Correlation Between Sodium Temperature Differentials Measured Inside and Outside the Thermal Shield.

the inlet and the outlet line temperature correlations have slopes of 1 but intercepts of -25 and -40° F, respectively. This was probably the result of the long sodium inlet and outlet lines being used as a convenient means of adding heat to the system to maintain a thermal equilibrium in the reactor of $\sim 1300^{\circ}$ F. Good data for the high-power

correlations, Figs. K.5 and K.6, were rather scarce, but the curves shown are believed to be reasonable approximations to the actual correlation. The data in Fig. K.6 have been corrected for known error in the temperature differential at zero (or low) power. The correction, as applied, was to reduce the value of the temperature differential determined from the thermocouples outside the thermal shield by 10°F.

All the correlations were based upon data which were obtained during runs long enough for the establishment of equilibrium conditions in the system or at times when isothermal conditions prevailed. The most important conclusion that can be made from these data is that the temperature differentials across the reactor in both the fuel and sodium systems were about a factor of 2 low. In the fuel system the outlet line temperature changes read in the control room (inside pressure shell temperatures) were only one-half as great as the corresponding temperature changes read in the

basement (outside pressure shell temperatures). In the sodium system both outlet and inlet line temperature curves had different intercepts but the same slopes (as during the low-power runs).

All temperature data used in this report that pertained to operation at high power were corrected to agree with line temperatures obtained outside the thermal shield (basement readings) by using curves K.1 through K.6. Data from runs made under isothermal or equilibrium conditions where equal temperature differences were obtained on instruments either in the control room or in the basement needed no temperature corrections. The temperature correlation data from which the curves were obtained are presented in Tables K.1 and K.2. Because of the lack of coordination between the control room and basement operations during the experiment, much potentially useful data had to be discarded because the exact times of the readings were not known or the data were taken before equilibrium conditions were established.

TABLE K.1. FUEL LINE TEMPERATURES MEASURED BY THERMOCOUPLES INSIDE AND OUTSIDE THE REACTOR THERMAL SHIELD

Date	Time	Experiment No.	Fuel Inlet Line Temperatures (°F) (Line 120)		Fuel Outlet Line Temperatures (°F) (Line 111)		Temperature Differential (°F) ^c	
			Basement ^a	Control Room ^b	Basement ^a	Control Room ^b	Basement	Control Room
10/26	2115	Before operation	1290	1285	1290	1287	0	2
10/27	0630	Before operation	1293	1293	1296	1293	3	0
11/4	1100	L-1	1300	1299	1297	1295	-3	-4
11/6	0340	L-4	1305	1310	1304	1300	-1	-10
11/11	0300	H-11	1207	1212	1522	1418	315	206
	1215	H-11	1210	1214	1524	1418	314	204
11/12	0001	H-13	1316	1308	1323	1308	7	0
	0630	H-13	1315	1307	1320	1306	5	-1
	1003	H-14	1246 ^d	1243	1587	1475	341	232
11/13	0915	After operation	1264	1260	1260	1250	-4	-10

^aFuel line temperatures outside thermal shield.

^bFuel line temperatures inside thermal shield.

^cThermocouple differences for no-power runs indicate extent of thermocouple errors (highest is ± 10 deg) and therefore the accuracy of the readings.

^dEstimated.

**TABLE K.2. SODIUM LINE TEMPERATURES MEASURED BY THERMOCOUPLES INSIDE AND
OUTSIDE THE REACTOR THERMAL SHIELD**

Date	Time	Experiment No.	Sodium Inlet Line Temperatures (°F)		Sodium Outlet Line Temperatures (°F)		Temperature Differential (°F)	
			Basement	Control Room	Basement	Control Room	Basement	Control Room
10/26	2115	Before operation	1305	1278	1320	1278	15	0
10/27	0630	Before operation	1312	1292	1325	1290	13	2
11/4	1100	L-1	1320	1295	1330	1288	10	7
11/6	0400	L-4	1325	1300	1335	1295	10	5
11/11	0900	H-11	1223	1224	1332	1271	109	47
11/12	1003	H-14(1)	1246	1258	1369	1307	123	49
11/9	1907	H-3(7)	1313	1290	1373	1313	60	23
11/13	0915	After operation	1282	1258	1292	1252	10	-6

This points out the need in future operations of the scale of the ARE for some sort of timing device that would automatically stamp the date and time every few minutes on the charts of all recording instruments, and a more systematic method of

manually recording data for each experiment performed in which conditions are held constant long enough for all pertinent data to be recorded. These and other similar recommendations will be found in Chapter 7 of this report.

Appendix L

POWER DETERMINATION FROM HEAT EXTRACTION

The power level of the reactor was determined from the total heat extracted by the fuel and the sodium. Data for the heat extraction determination were obtained from continuous records of the reactor fuel inlet, outlet, and mean temperatures, the temperature differential across the reactor, and the flow rates of the fuel and the sodium. The flow rates could also be calculated from the pump speed, and there was independent experimental evidence from which a plot of speed vs flow rate was obtained. The power level of the reactor was calculated by use of heat capacities, flow rates, and temperature differentials for both sodium and fuel. It was found that the fuel and the sodium accounted for 99% of the extraction of power generated in the reactor. The data referred to above were all obtainable in the control room.

The controls for preheating and maintaining heat on the system were located in the basement, and along with these controls were temperature recorders and indicators for the whole system, exclusive of the reactor. The temperatures of both fuel and sodium lines to and from the reactor were also recorded in the basement. These basement data were used for a separate power extraction determination.

An independent source of power level information was also available, since the fuel and sodium were cooled by a helium stream flowing over a heat exchanger and the helium in turn was cooled by a helium-to-water heat exchanger. No flow or temperature measurements were made of the helium, but since the water exchangers were very close to the fuel or the sodium exchangers, all the heat that was taken out of the fuel and sodium should have appeared in the water. The water flow through these exchangers was metered by orifice-type flowmeters, and the outlet temperatures were measured by thermocouples in wells. The fuel loop exchangers and the two sodium loop exchangers were metered separately.

Up to the time of the 25-hr xenon run the reactor was operated at high power for very short periods of time, and the extracted power was determined from the control room data. During the 25-hr xenon run a comparison was made of the extracted power determined from the control room data, that determined from the basement data, and that from the water data (Table L.1). Large discrepancies

were found, and the indications were that the control room data were low.

The disagreement of the various data led to the examination of the inlet and outlet line temperatures, as described in Appendix K. During the xenon run the fuel outlet line temperatures were about 100°F higher than the fuel outlet manifold temperatures (control room data), and the fuel inlet line temperatures (basement data) were essentially the same as the fuel inlet manifold temperatures (control room data). The sodium outlet line temperature (basement data) was 60°F higher than the sodium outlet temperature at the reactor (control room data). (The only check on power extraction by the rod cooling system, which was only 1% of total power, was the water data for the rod cooling helium-to-water heat exchanger. In most discussions this 1% is neglected.)

The power extracted in both the fuel and the sodium systems has been calculated by using temperature data from several experiments, and the results are presented in Table L.2. There were three separate measurements of the fuel temperature differential available in the control room which were usually in fair agreement. The largest discrepancy was, as mentioned, between the control room data and the basement data. The temperature differential obtained from the basement data was an average result from a number of line thermocouples, while the control room data came from thermocouples located on the fuel headers inside the reactor thermal shield.

The so-called secondary heat balance was obtained by determining the heat dumped by the water from the various heat exchangers. These data are tabulated in Table L.3 for the high-power experiments.

The various estimates of reactor power from both primary and secondary heat extraction are then listed in Table L.4, together with the power estimated from the calibration of the nuclear instruments, that is, the log N recorder and the micro-microammeter. These latter instruments were normalized to agree with the primary extracted power as determined by the line temperature (basement data) during the xenon experiment (H-11). Equilibrium conditions were certainly attained during this 25-hr experiment and such error as there may be in using these data as the criteria for

TABLE L.1. COMPARISON OF POWER EXTRACTION DETERMINATIONS MADE FROM DATA OBTAINED DURING 25-hr XENON RUN

	Temperatures (°F)			Flow (gpm)	Power Extracted (Mw)	Total Power ^a Extracted (Mw)
	Inlet	Outlet	ΔT			
Fuel System						
Control room data	1212	1418	206	44	1.02	
Basement data	1209	1522	313	44	1.52	
Sodium System						
Control room data	1225	1271	46	153	0.244	
Basement data	1226	1335	109	153	0.577	
Total Power						
Control room data						1.28
Basement data						2.12
Water Data						
In fuel loop	61	117	56	205	1.68	
In sodium loop	61	114 ^b	53	38.3 ^b	0.588 ^c	
Total Power from Water Data						2.28

^aIncludes ~1% for rod cooling.

^bAverage for both loops.

^cSum of both loops.

TABLE L.2. PRIMARY POWER EXTRACTION

Experiment No.	Run No.	Control Room Data									Basement Data						
		Fuel System						Sodium System			Average Total Power Including Rod-Cooling Power (Mw)	Fuel System		Sodium System		Total Power Including Rod-Cooling Power (Mw)	
		Flow (gpm)	ΔT, Outlet Minus Inlet (°F)	ΔT, Recorder (°F)	ΔT, Tube Average (°F)	P _{ΔT} (Mw)	P _R (Mw)	P _{Na} (Mw)	Flow (gpm)	ΔT (°F)		ΔT (°F)	P _{fuel} (Mw)	ΔT (°F)	P _{Na} (Mw)	ΔT (°F)	P _{fuel} (Mw)
H-3	1	44½	40	33.5		0.196	0.163		153	0	0.199						
	2	44½	66	52		0.323	0.254			0	0.308						
	3	44½	115	116		0.562	0.567			0	0.584						
	4	44½	120	114	124	0.588	0.560	0.606	153	14	0.0734	0.678	198	0.970	45	0.236	1.23
	5	44½	230	231	239	1.128	1.129	1.17	153	10.5	0.0548	1.21					
	6	44½	237	234	243	1.16	1.145	1.19	152	10	0.0523	1.24	138	0.677	60	0.315	1.012
	7	44½	13	19	20	0.0653	0.0946	0.0975	152	22	0.115	0.221					
H-6		44½	236	240	245	1.158	1.175	1.198	152	3.5	0.0182	1.22	320	1.572			
H-8		45	266	225		1.31	1.111		153	21	0.110	1.34	293	1.452	75	0.394	1.87
H-11		44	206	213	211	0.984	1.017	1.018	153	46.4	0.244	1.27	313	1.520	110	0.577	2.12
H-13		44		10			0.0484		153	1.4	0.0073	0.0757	312	1.530	19	0.099	1.65
H-14		45	182	245		0.900	1.212		153	50	0.262	1.45	355	1.760	127	0.667	2.45

TABLE L.3. SECONDARY POWER EXTRACTION

Experiment No.	Run No.	Fuel Heat Exchanger			No. 1 Sodium Heat Exchanger			No. 2 Sodium Heat Exchanger			Rod-Cooling Heat Exchanger			Total Extracted Power Secondary System (Mw)
		Water Flow (gpm)	ΔT ($^{\circ}$ F)	P_{fuel} , Power (Mw)	Water Flow (gpm)	ΔT ($^{\circ}$ F)	$P_{Na'}$, Power (Mw)	Water Flow (gpm)	ΔT ($^{\circ}$ F)	$P_{Na'}$, Power (Mw)	Water Flow (gpm)	ΔT ($^{\circ}$ F)	$P_{R.C.}$, Power (Mw)	
H-3	1	204	13	0.389	38.4	0	0	38.4	0	0	17.3	3	0.0076	0.397
	2	204	13	0.389	38.4	0	0	38.4	0	0	17.3	3	0.0076	0.397
	3	204	30	0.897	38.4	0	0	38.4	0	0	17.3	3	0.0076	0.905
	4	204	29	0.866	38.4	26	0.146	38.4	21	0.1188	17.3	3	0.0076	1.14
	5	204	59	1.765	38.4	26	0.146	38.4	25	0.141	17.3	3	0.0076	2.06
	6	204	59	1.765	38.4	27	0.152	38.4	24	0.135	17.3	3	0.0076	2.06
	7	204	3	0.0903	38.4	26	0.146	38.4	25	0.141	17.3	2	0.0051	0.382
H-6		204												
H-8		206	63	1.901	38.0	37	0.207	38.4	40	0.226	17.3	3	0.0076	2.34
H-11		205	56	1.685	38.2	55	0.300	38.4	51	0.228	17.6	2	0.0052	2.28
H-13		205	3	0.0902	38	10	0.0561	38.4	1	0.0056	17.1			
H-14		204	63	1.883	38	57	0.318	38.4	56	0.316	16.9	6	0.0150	2.53

TABLE L.4. REACTOR POWER SUMMARY

Experiment No.	Run No.	Nuclear Power (Mw)		Primary Power (Mw)				Secondary Power (Mw); Water Heat Exchanger, P_W		
		Log N	Micromicroammeter	Control Room Data			P_B	P_W		
				$P_{\Delta T}$	P_R	$P_{av \Delta T}$				
H-3	1	0.449	0.425	0.216	0.183		0.199			0.3966
	2	0.449	0.463	0.343	0.274		0.308			0.3966
	3	0.848	0.910	0.582	0.587		0.584			0.9046
	4	0.923	0.988	0.681	0.653	0.699	0.678	1.23		1.1384
	5	2.47	2.05	1.20	1.20	1.24	1.21			2.0596
	6	2.12	2.34	1.23	1.22	1.26	1.24	1.012		2.0596
	7	0.281	0.288	0.200	0.230	0.232	0.221			0.3824
H-6		2.21	2.16	1.20	1.21	1.25	1.22	1.93		
H-8		2.12	2.38	1.44	1.24		1.34	1.87		2.342
H-11		2.12	2.12	1.25	1.28	1.28	1.27	2.12		2.278
H-13		0.125	0.151		0.0757		0.0757			0.1562
H-14		2.41	2.53	1.42	1.45	1.43		2.45		2.53

amount of extracted power is conservative, since the water heat balance at the same time showed the power to be 7% higher.

The sources of error in the various measurements of extracted power were associated with the tem-

perature measurements on the fuel and sodium lines at the reactor, which gave the reactor ΔT . These thermocouples were unique in several respects; that is, they were located within the reactor thermal shield; they were exposed to the reactor pressure

shell; they were exposed to high nuclear radiation fluxes, etc. These unique aspects immediately suggest several possible explanations for the erroneous temperature measurements. However, upon further examination, each of these aspects, with the dubious exception of nuclear radiation, has been shown to be incapable of producing the observed anomaly.

The control and shim rods and the fission chambers were cooled by forced helium circulation in the rod-cooling system. Part of the helium that was blown down through the rod tubes was deflected back up across the outlet manifold and between the pressure shell and the thermal shield. While it was thought that perhaps this was cooling the fuel outlet manifold thermocouples and making them read low, this was disproved when changing the speed of the blower or stopping it had no effect on the fuel outlet temperature.

It was thought that possibly the heat radiation from the fuel outlet manifold to the colder bottom of the pressure shell was great enough to actually lower the manifold wall temperatures 100°F below the fluid temperature. This has been disproved by heat transfer calculations. It was also thought that since the outlet fuel lines passed through the 2-in. plenum chamber that the resulting surface cooling of the fuel might account for the lower wall temperatures, although the mixed mean fuel temperature was considerably higher. This was also disproved when no increase in wall temperature was observed for thermocouples within the thermal shield but located progressively farther away from the pressure shell bottom.

It is of interest that after the final shutdown of the reactor, the fuel outlet line and fuel outlet manifold temperatures agreed; in other words, with no power generation the basement data and control room data agreed.

Appendix M

THERMODYNAMIC ANALYSES

Some two years before the Aircraft Reactor Experiment was placed in operation a comprehensive report was written on the "Thermodynamic and Heat Transfer Analysis of the Aircraft Reactor Experiment."¹ Not only was the design of the reactor system based, in part, on the studies culminating in that report, but the material therein served as a guide during the acceptance test of the experiment. Therefore a comparison of the calculated and the actual thermodynamic performance of the reactor system was attempted. It soon became apparent that the experimental data of the type needed for thermodynamic analyses were inadequate to permit a meaningful comparison with any of the calculated situations. Perhaps the most valid comparison may be made between the calculated insulation losses, the heater power input at equilibrium, and the heat removed by the space coolers. Even here the agreement is less than 50%. An illustration of the inefficacy of attempting to calculate such thermodynamic constants as the heat transfer coefficients of the fuel and the sodium is presented below.

INSULATION LOSSES, HEATER POWER INPUT, AND SPACE COOLER PERFORMANCE

At equilibrium the electrical heat required to maintain the system at a mean temperature of 1325°F should have been equivalent to the heat removed in the eight pit space coolers. The maximum amount of heat ever removed by the space coolers was the 250 kw attained with 66.5-gpm-total water flow with a temperature rise of 30°F. Although this value agrees very well with calculated¹ heat loss of 220 kw for the entire system (the reported value of 240 kw was calculated for an earlier design system and was reduced by about 20 kw for the actual system), the actual electrical power input to the heaters averaged around 375 kw after the system reached equilibrium.

There are several possible explanations for the discrepancies between the calculated heat loss, the electrical power input, and the heat removed by the space coolers. First, the calculated loss was low because it assumed idealized conditions

and not the actual insulation which had cracks, clips, etc. Second, the electrical heat load was high, since it did not allow for transformer, variac, and line losses. Also, the space cooler heat load may not have represented an equilibrium condition if the pit walls were still heating up and/or radiating heat.

EXPERIMENTAL VALUES OF HEAT TRANSFER COEFFICIENTS²

An attempt was made to calculate both the sodium and the fuel heat transfer coefficients from the measured values of temperatures and flows in the various heat transfer media, that is, fuel, sodium, helium, water. These data are given in Table M.1 for a typical operating condition.

The desired heat transfer coefficient should be determinable from the calculated values of the various thermal resistances in the heat exchangers. To obtain the thermal resistance on the fuel side or the sodium side of the respective heat exchangers, the helium side and metal resistances had to be subtracted from the over-all resistance. The expression for the over-all resistance is

$$R_T = \frac{1}{(U_0 A)} = \frac{q}{A^2 \Delta T},$$

where

U = over-all heat transfer coefficient,

A = area across which heat is transferred,

q = rate of heat transfer,

ΔT = over-all temperature difference.

A knowledge of the inlet and outlet temperatures on the helium side of the heat exchanger is required by the above expression, and lack of this information immediately introduces a large uncertainty in the results. Of greater importance, however, is the relative magnitude of the resistances involved. The calculated ratio for the fuel-to-helium exchanger is

$$\frac{R_{He}}{R_f} = 10.3,$$

where R_{He} is the resistance on the helium side

¹B. Lubarsky and B. L. Greenstreet, *Thermodynamic and Heat Transfer Analysis of the Aircraft Reactor Experiment*, ORNL-1535 (Aug. 10, 1953).

²H. H. Hoffman, Physical Properties Group, Reactor Experimental Engineering Division.

TABLE M.1. EXPERIMENTAL HEAT TRANSFER DATA IN FUEL AND SODIUM LOOPS

	Primary Coolant				Helium				Water			
	Flow (gpm)	Temperature (°F)		Flow* (cfm)	Temperature (°F)		Flow (gpm)	Temperature (°F)		Flow (gpm)	Temperature (°F)	
		Inlet	Outlet		Inlet	Outlet		Inlet	Outlet		Inlet	Outlet
Fuel loop	44 ($\pm 5\%$)	1209 ± 10	1522 ± 10	8000 ($\pm 30\%$)	No data	No data	194 ($\pm 5\%$)	61 ± 2	117 ± 2			
Sodium loop	152 ($\pm 1\%$)	1225 ± 10	1335 ± 10	1700 ($\pm 20\%$)	No data	No data	76.6 ($\pm 1\%$)	61 ± 2	114 ± 2			

*Estimated.

and R_f is the resistance on the fuel side, and for the sodium-to-helium exchanger is

$$\frac{R_{He}}{R_{Na}} = 65 .$$

The liquid-side resistance is

$$R_l = R_T - (R_{He} + R_m) ,$$

where R_m is the wall resistance. Hence, the liquid-side thermal resistance is the small difference between two much larger numbers. A small error in R_T or R_{He} is greatly magnified in R_l . Unfortunately, the error in R_{He} is not small, being perhaps as great as 60%. Thus, except for over-all heat balances, little useful heat transfer information can be extracted from the available data on the ARE heat exchangers.

Appendix N

COMPARISON OF REACTOR POWER DETERMINATIONS

W. K. Ergen

In order to get an estimate of the reactor power and to be able to calibrate the instruments, the ARE was run for 1 hr at a power which was estimated, at the time, to be 10 watts (exp. L-4). A sample of the fuel was then withdrawn and the gamma activity was compared with that of a sample which had been irradiated at a known power level in the Bulk Shielding Reactor (BSR). This method of power determination is discussed in Appendix H.

A curve showing the gamma counting rate of a BSR-irradiated sample as a function of time after shutdown had been obtained. The irradiation time was 1 hr at a constant power of 1 w. From this curve a decay curve corresponding to the actual power history of the ARE was synthesized by taking into account not only the "10-watt" run, but also the previous lower power operation.

When this synthetic curve was compared with the one obtained from measurements on the ARE sample, the shapes of the curves did not agree, the ARE curve having a smaller slope than the synthetic curve. Also, the power determined by this method was lower than the power ultimately determined by the heat balance. Both these effects can be explained in a qualitative manner by the loss of some of the radioactive fission fragments from the ARE sample. This would reduce the total radioactivity of the sample and hence the apparent power level. Furthermore, the loss of radioactive fission fragments would reduce the counting rate at short times after irradiation more than at long times, because among the most volatile fission fragments are the strong gamma emitters that have relatively short half lives (notably, 2.77-hr Kr⁸⁸). This would flatten the slope of the decay curve of the ARE sample.

It has not been possible so far to treat this matter in a quantitative way, but in order to eliminate some computational complications a sample was irradiated in the BSR under conditions exactly duplicating the power history of the ARE, except for a proportionality factor. A comparison of the decay curve of this sample and that of the ARE sample is shown in Fig. N.1. The BSR sample contained 0.1166 g of U²³⁵; the fission cross section at the temperature of the BSR is 509 barns.¹ The BSR power at the final 1-hr irradiation was

10 w, corresponding to a flux² of 1.7×10^8 n/cm²·sec, and a self-shielding factor, estimated to be 0.8, had to be applied to this sample. Hence, during the 1-hr irradiation there were

$$\begin{aligned} 0.1166 \text{ g} &\times 0.6 \times 10^{24} \text{ atoms/g-atom} \times 509 \\ &\times 10^{-24} \text{ fissions/(atoms} \cdot \text{n/cm}^2) \times 1.7 \\ &\times 10^8 \text{ n/cm}^2 \cdot \text{sec} \times 0.8/235 \text{ g/g-atom} \\ &= 20.6 \times 10^6 \text{ fissions/sec} . \end{aligned}$$

The ARE sample contained 0.1177 g of U²³⁵ and the total U²³⁵ in the ARE at the time of the run was 59.1 kg. The reactor power, as determined later by the heat balance, was actually 27 w, instead of the expected 10 w. Hence there were

$$\begin{aligned} 27 \text{ w} &\times 3.1 \times 10^{10} \text{ fissions/w-sec} \times 0.1177 \text{ g} \\ &\hline 59,100 \text{ g} \\ &= 1.66 \times 10^6 \text{ fissions/sec} \end{aligned}$$

in the ARE sample.

The ratio of the radioactivities of the BSR sample and the ARE sample should thus have been $20.6/1.66 = 12.4$. As may be seen from Fig. N.1, the measured ratio is 27 at 1 hr 40 min, and 17.5 at 38½ hr. As pointed out above, the discrepancy can be explained by the loss of radioactive fission fragments from the ARE sample.

A small amount of the radioactivity of either sample was contributed by the capsule and the fuel carrier, especially the sodium content of the carrier. This was measured by irradiating a non-uranium-bearing capsule with carrier, and counting its radioactivity. However, since this correction proved to be small and since both samples contained about the same amount of uranium in the same amount of carrier, the results would not be appreciably affected.

¹J. L. Meem, L. B. Holland, and G. M. McCommon, *Determination of the Power of the Bulk Shielding Reactor, Part III. Measurement of the Energy Released per Fission*, ORNL-1537 (Feb. 15, 1954).

²E. B. Johnson, private communication.

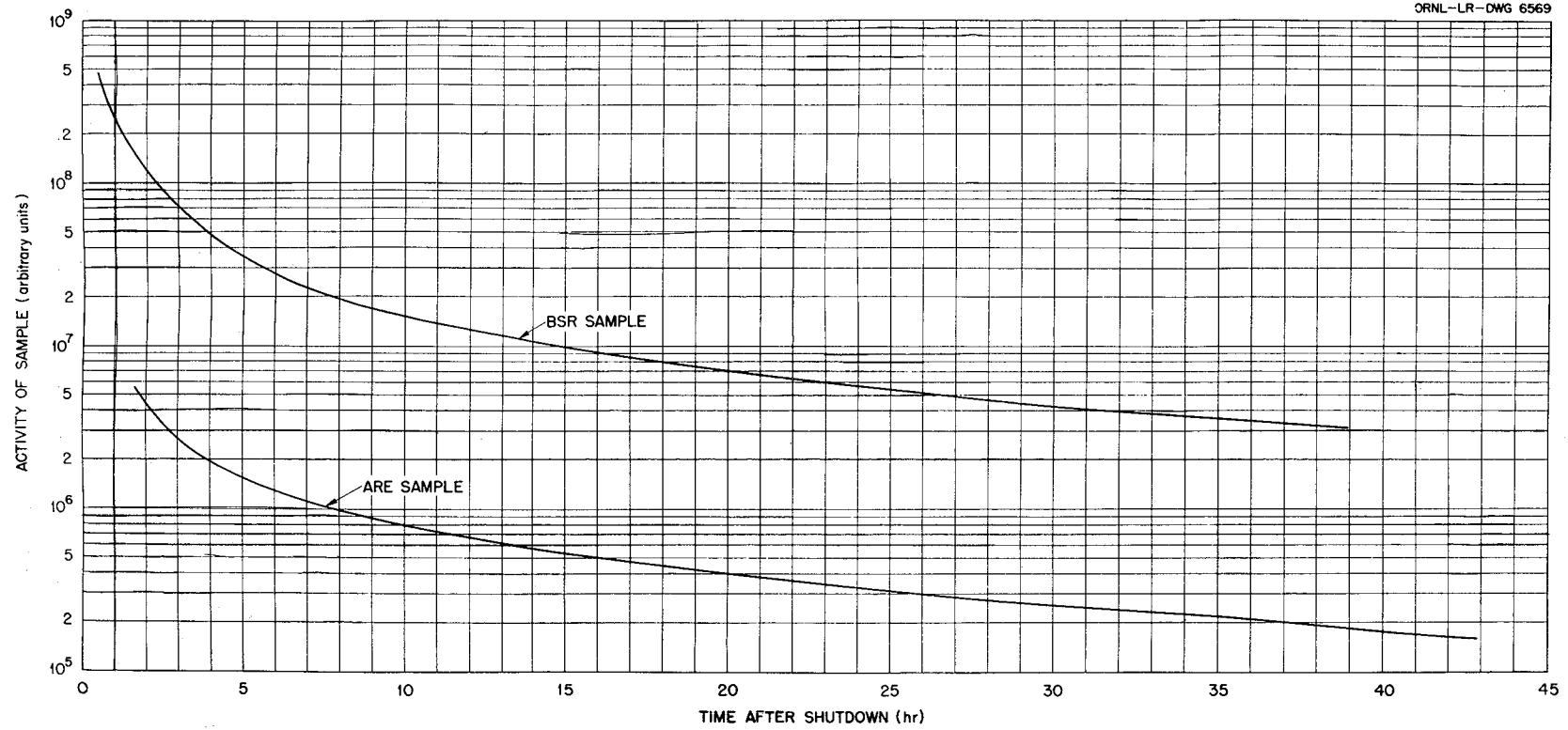


Fig. N.1. Decay of Irradiated Fuel Samples.

Appendix O

ANALYSIS OF TEMPERATURE COEFFICIENT MEASUREMENTS

IMPORTANCE OF THE FUEL TEMPERATURE COEFFICIENT

One of the most desirable features of a circulating-fuel reactor is its inherent stability because of the strong negative temperature coefficient of reactivity. This was conclusively demonstrated by the ARE. It had been predicted, on the basis of the temperature dependence of the density, which was

$$\rho \text{ (g/cm}^3\text{)} = 3.98 - 0.00093T \text{ (}^{\circ}\text{F)}$$

for the final fuel concentration in the reactor, that the ARE fuel would have a negative temperature coefficient of sizable magnitude. At the operating temperature of 1300°F the fuel density was 3.33 g/cm^3 . The resulting mass reactivity coefficient was

$$(\Delta M/M)/^{\circ}\text{F} = -\frac{0.00052}{3.33} = -1.56 \times 10^{-4}/^{\circ}\text{F},$$

and, for $\Delta k/k = 0.236 \Delta M/M$, the predicted temperature coefficient that would result from the changing density of the fuel alone was

$$(\Delta k/k)/^{\circ}\text{F} = -3.68 \times 10^{-5}/^{\circ}\text{F}.$$

Actually, as was stated in the body of this report (cf., Fig. 6.4), the fuel temperature coefficient was $-9.8 \times 10^{-5}/^{\circ}\text{F}$.

As long as the over-all temperature coefficient of a reactor is negative, the reactor will be a slave to the load demand. However, the fuel temperature coefficient was the important factor for reactor control in the ARE because it took a significant time for the bulk of the material of the reactor to change temperature and, therefore, for the over-all coefficient to be felt. In experiment H-5 (cf., Fig. 6.4), it was found that the fuel temperature coefficient predominated for 6 min.

EFFECT OF GEOMETRY IN THE ARE

When the reactor was allowed to heat up by nuclear power, as in experiment H-5, the measurements of the temperature coefficient were quite definitive. The experiments in which the heat extraction by the helium blower was suddenly increased, i.e., experiments E-2, L-8, and H-4, did not give clear-cut results. In fact, it was noticed throughout the operation that whenever the fuel

loop helium blower speed was increased there was always a sudden marked increase in reactivity. In attempting to determine this instantaneous temperature coefficient by observing the rod movement by the servo as a function of the fuel temperature, values of the fuel temperature coefficient of a magnitude much larger than -9.8×10^{-5} could be obtained.

The change in the apparent temperature coefficient as a function of time during experiment H-4 is shown in Fig. O.1. The time intervals chosen were of 15-sec duration. The apparent peak temperature coefficient of reactivity was in excess of $-3.5 \times 10^{-4} (\Delta k/k)/^{\circ}\text{F}$, and after 5 min the coefficient leveled out to a value of about -6×10^{-5} . A more complete discussion of this experiment is given below in the section on "High-Power Measurements of Temperature Coefficients of Reactivity," in which the time lag of the thermocouples is taken into account. Two coefficients were obtained: an initial fuel temperature coefficient and an over-all coefficient, which was the asymptotic value (-6×10^{-5}) given by Fig. O.1.

The effect shown in Fig. O.1 was due partly to geometrical considerations. By reference to Figs. 2.2 and 2.3, it can be seen that as the fuel entered the reactor it passed through the tubes closest to

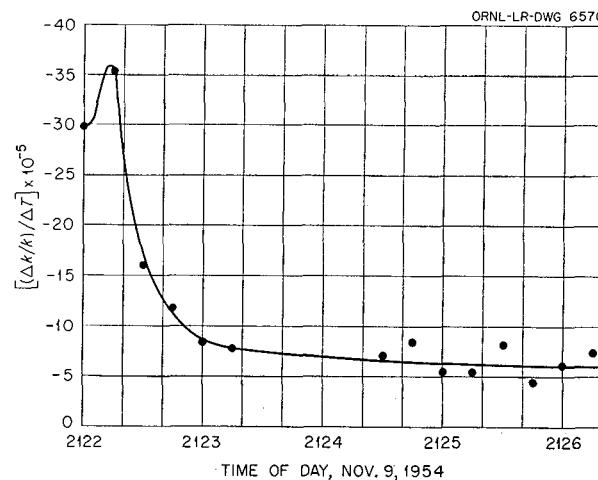


Fig. O.1. Variation in Apparent Temperature Coefficient of Reactivity with Time. Experiment H-4.

the center where the reactivity effect was greatest. With a sudden increase in heat extraction, a slug of cooled fuel initially entered the center of the core and caused a large reactivity change. Since the mean reactor temperature was the average temperature of all the fuel tubes, a comparison of the initial rate of rod insertion by the servo with the initial rate of change of the mean reactor temperature could give an apparent temperature coefficient much larger than its actual value. For example, in experiment L-8 (cf., Figs. 5.13 and 5.14) a comparison of the slopes of the rod position curve and the mean temperature curve near the beginning of the run was made. If it is assumed that the temperature response of the thermocouples lagged behind the response of the regulating rod movement, it is interesting to compare the points of steepest slope for the two curves. By using the slope from Fig. 5.13 at time 0218:30, and the slope from the mean temperature curve (Fig. 5.14) at 0220, a temperature coefficient of -1.6×10^{-4} $(\Delta k/k)/^{\circ}\text{F}$ is obtained, as opposed to the actual fuel temperature coefficient of -9.8×10^{-5} . A detailed discussion of this experiment is given in the section on "Low-Power Measurements of Temperature Coefficients of Reactivity." This effect was characteristic of the geometry of the ARE but not necessarily of circulating-fuel reactors in general.

TIME LAG CONSIDERATIONS

As mentioned above and in the "Reactor Kinetics" section of Chapter 6, one of the most consistently noted phenomena of the ARE operation was the time lag in reactor temperature response during every phase of the experiment. These time lag effects can be partly explained by the geometry effect just described; and, in this sense, the time lag is not a true time lag but only an apparent lag due to the differences in location and response of the thermocouples and the neutron detectors (and, hence, regulating rod movements¹). Other possible causes for the time lags were the fuel transit time around the system, the heat transfer phenomenon within the reactor, the design and location of thermocouples, and a mass-temperature inertia effect. These effects were all discussed briefly in the section on "Reactor Kinetics," Chapter 6.

Whether or not the time lag was all or partly real is academic. The fact that it did give an observed effect during many phases of the ARE operation made it mandatory to take the lag into account in interpreting much of the data. The manner in which this was actually done was to assume that the response of the thermocouples lagged behind the nuclear response of the reactor (by as much as $2\frac{1}{2}$ min for low-power operation and by about 1 min during the high-power regime) in those experiments in which the equilibrium between the reactor and its load was upset (i.e., rapid fuel cooling rates). The thermocouple readings were then "moved up" by that amount, and the new readings were compared with the appropriate nuclear instrument observation. For those experiments in which equilibrium prevailed, but in which cooling was taking place, it was only necessary to correct for temperature readings (cf., app. K).

The temperature coefficient measurements were probably more affected by the temperature-time lags than any other single type of measurement made on the ARE, mainly because of the short duration of the experiments and their great dependence on time correlations (for example, correlations between regulating rod motion and mean temperature changes). The results of temperature coefficient measurements which contained time lag corrections were not included in the main body of the report because such corrections needed to be discussed in detail inappropriate to the context of the report. These experiments are described in the following sections of this appendix.

SUBCRITICAL MEASUREMENT OF TEMPERATURE COEFFICIENT

The subcritical measurement of the temperature coefficient (exp. E-2) was described in Chapter 4. Briefly, the procedure followed was to cool the fuel by raising the heat barriers on the fuel heat exchangers, turning on the fuel helium blowers, and then observing the increase in multiplication with the two fission chambers and the BF_3 counter. The BF_3 counting rate was so low that the statistics were poor; therefore, the fission chamber data had to be used. The subcritical multiplication of the fission chambers was then subject to the phenomenon discussed in Appendix E. In this experiment the cooling was rapid and equilibrium conditions were not attained. Consequently, in order to find a value of the temperature coefficient from these measurements, it was necessary to

¹The regulating rod was controlled by a flux servo mechanism which received its error signal from a neutron detector (cf., App. C).

apply three corrections: a correction for the fission chamber multiplication error, a time lag correction, and a temperature correction of control room observed temperatures (app. K).

Throughout the subcritical experiments ample data were taken simultaneously on the BF_3 counter and the two fission chambers for a correlation plot between the counting rates of the BF_3 counter and the fission chamber to be easily obtained, as shown in Fig. O.2. A plot of the raw data obtained from the fission chambers before corrections were applied is shown in Fig. O.3,² which shows the counting rates of the chambers plotted as a function of the reactor mean temperature. The hysteresis effect is the result of the time lag. The progress of the experiment can be read from the curves by starting on the right side at 1004 and proceeding counterclockwise around the loops. The fuel blower was turned on at 1004 and allowed to cool the fuel for 5 min, after which the blower was turned off and the system then slowly returned to its initial condition. The fission chamber counting rates increased while the blower was on and decreased after the blower was turned off again in immediate response to the cooling. The reactor mean temperature change, on the other hand, lagged behind both when the blower was turned on and when it was turned off. The blower was turned off shortly after 1009, but even though the counting rate started to decrease immediately, the reactor mean temperature continued to fall for approximately 2½ min before it began to show a warming trend. Undoubtedly the fuel temperature did actually follow closely the changes introduced by the blower (otherwise the counting rate changes would not have been observed as promptly as they were), but because of the various effects noted in this appendix and in the "Reactor Kinetics" section of Chapter 4 the thermocouples were slow in responding. If the thermocouples had shown instant response there would have been no hysteresis effect observed, and the plot of k vs mean temperature would have been a straight line with a negative slope proportional to the temperature coefficient.

The plot of k vs mean temperature was obtained by applying the three corrections noted above in

²This plot is actually a cross plot of the curves of Fig. 4.5, which show both the counting rate and reactor mean temperature plotted as a function of time.

the following way. The first correction was applied by changing the fission chamber data to BF_3 counter data by using the curves of Fig. O.2. The resulting points obtained from each fission chamber were averaged and then plotted on a time scale along with the reactor mean temperature to produce a plot similar to the curves of Fig. 4.5. The maximum of the counting rate curve and the minimum of the temperature curve were then matched up (the temperature curve was effectively moved up 2½ min in time), and new temperatures were read from the temperature curve corresponding to the time that the counts were taken. From the counting rates the multiplication factor $k = 1 - (1/M)$ was determined for each point, and then a plot of k as a function of mean temperature was drawn up, as shown in Fig. O.4. A straight line could reasonably be drawn through the points.

The third and final correction to be applied to the mean temperature was obtained from Appendix K. Since this experiment was one in which the fuel was cooled rapidly and equilibrium conditions were not met, the curves of Fig. K.2 are applicable. From Fig. K.2 it can be shown that a change of 1°F in the true mean temperature corresponds to a change of 1.40°F in the mean temperature read from the control room instruments. Thus the mean temperature change observed had to be increased by a factor of 1.4. A measurement of the slope of the curve of Fig. O.4 gives a $(\Delta k/k)/\Delta T$ of 1.65×10^{-4} . The average k over the plot is 0.922. By applying the factor 1.4 to the observed mean temperature change, the fuel temperature coefficient was calculated to be

$$\alpha = (\Delta k/k)/\Delta T = \frac{-1.65 \times 10^{-4}}{0.922 \times 1.4} = -1.28 \times 10^{-4} .$$

This value is about 30% higher than that given by the results of experiment H-5, but it is in fair agreement in consideration of all the necessary corrections. A consideration of the errors involved showed that the maximum error was of the order of magnitude of 2.4×10^{-5} . Therefore,

$$\alpha = -(1.28 \pm 0.24) \times 10^{-4} .$$

If the lower limit of this value is taken, the agreement between this value and the accepted value is fairly good. This experiment did not yield an over-all temperature coefficient.

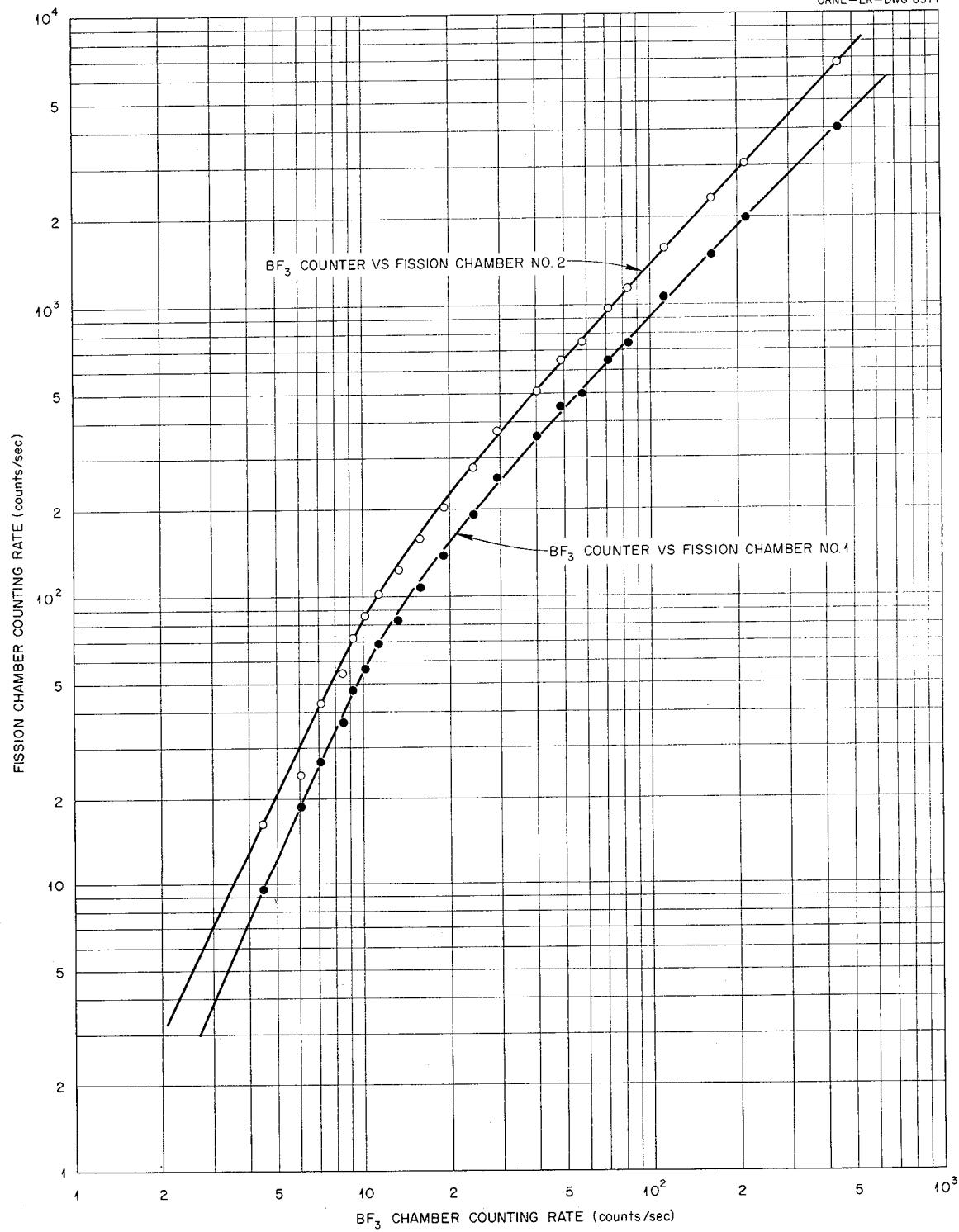


Fig. O.2. Correlation Between the Counting Rates of the BF₃ Counter and the Two Fission Chambers.

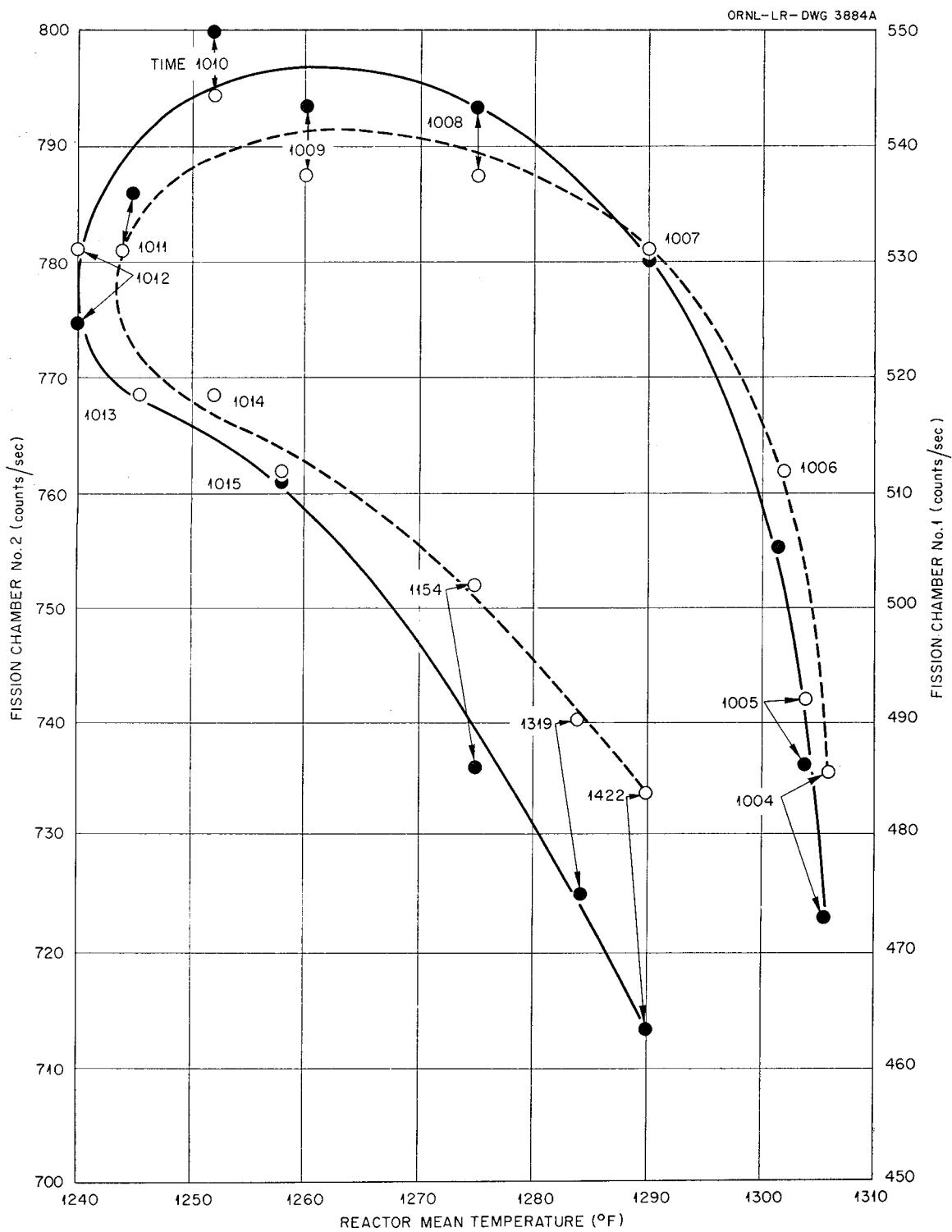


Fig. O.3. Subcritical Measurement of Temperature Coefficient of Reactivity (Uncorrected Fission Chamber Data).

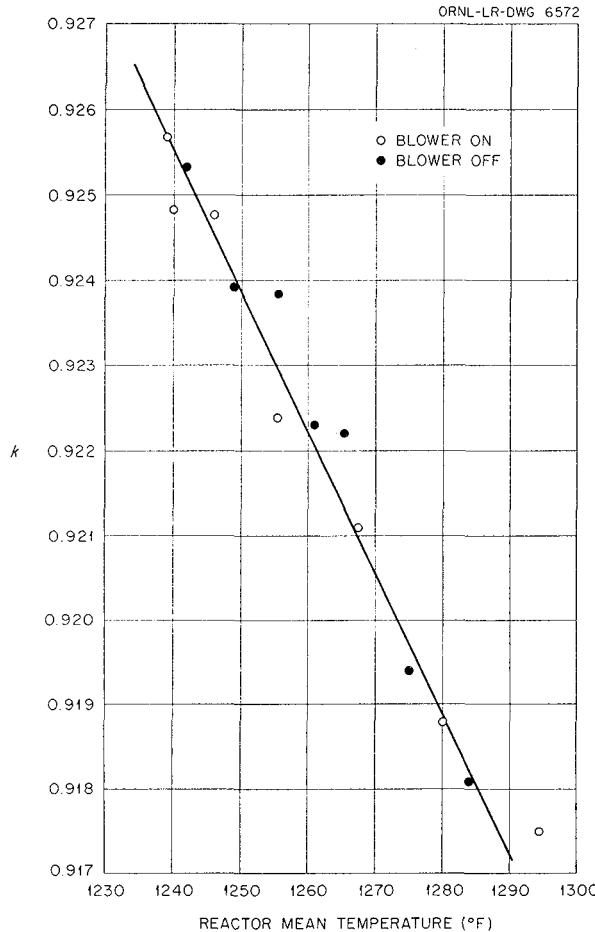


Fig. 0.4. Reactivity as a Function of Reactor Mean Temperature as Determined from the Sub-critical Temperature Coefficient Measurement. Experiment E-2.

LOW-POWER MEASUREMENTS OF TEMPERATURE COEFFICIENTS OF REACTIVITY

The low-power measurements of the temperature coefficients of reactivity were similar to the sub-critical measurements, except that with the reactor critical and on servo at 1-w power, reactivity introduced by cooling the fuel was observed by a change in the regulating rod position. The experiment is described in Chapter 5.

As shown in Fig. 0.5, which is a plot of the regulating rod position vs the observed mean temperature during the experiment, a hysteresis phenomenon was obtained. It is significant that no time lags needed to be taken into account in the interpretation of this data, because the experiment proceeded slowly enough for equilibrium conditions to prevail. However, since this was a cooling experiment, a temperature correction had to be applied. Cooling took place along the lower half of the figure and heating occurred along the upper portion. Each of the curves had an initial steep slope corresponding to an initial fuel temperature coefficient and a less steep slope from which an over-all reactivity coefficient was found.

After correction for the mean temperature readings, the average of the two initial slopes gave a fuel temperature coefficient of reactivity of -9.9×10^{-5} , and the other slopes gave an average over-all reactivity coefficient of about -5.8×10^{-5} . These values agree well with the accepted values of -9.8×10^{-5} and -6.1×10^{-5} for the fuel and over-all temperature coefficients of reactivity, respectively.

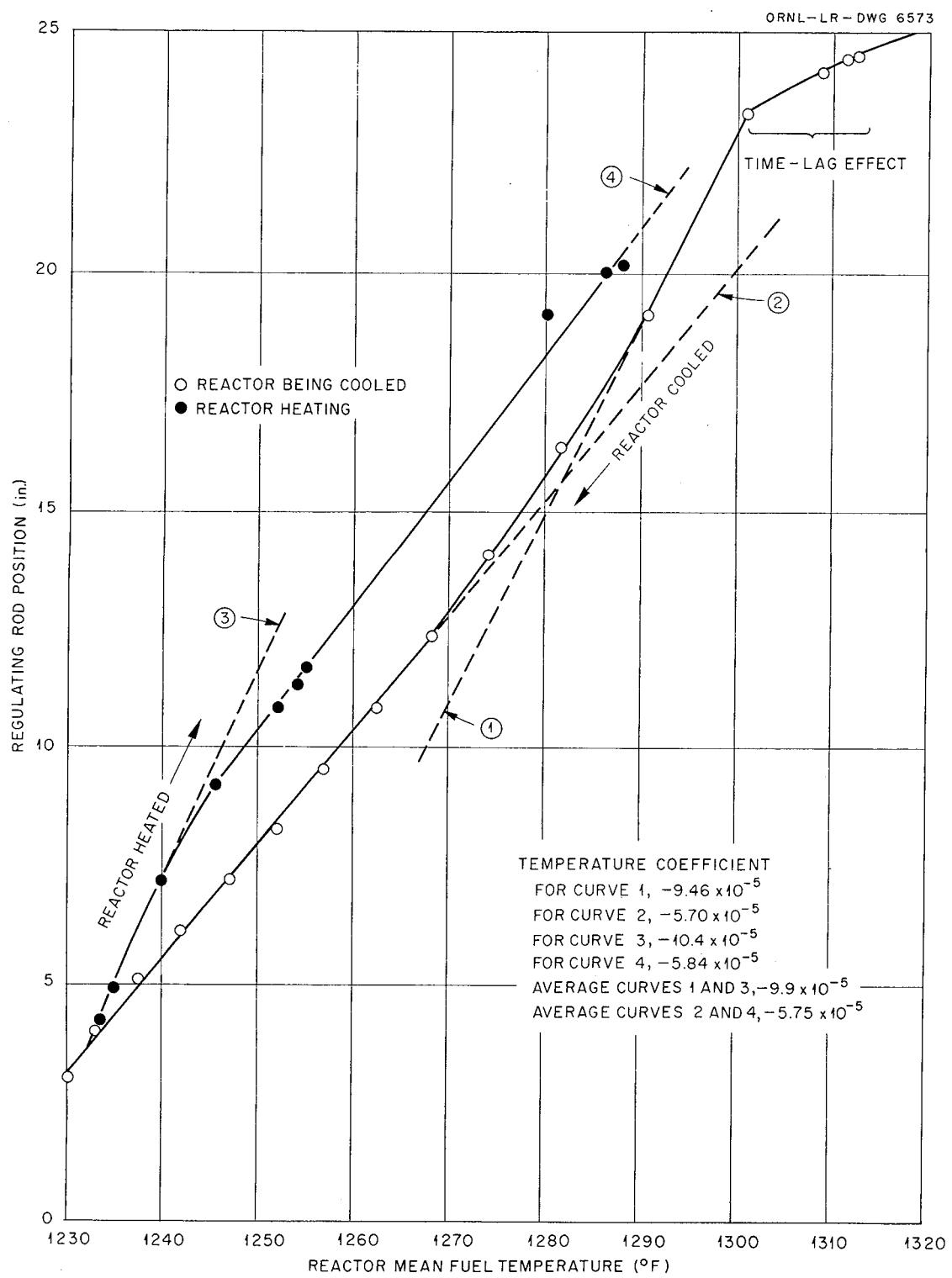


Fig. O.5. Regulating Rod Position as a Function of Observed Reactor Mean Temperature During Experiment L-5.

HIGH-POWER MEASUREMENTS OF TEMPERATURE COEFFICIENTS OF REACTIVITY

During the high-power operations an experiment was conducted at a power of 100 kw which was similar to the low-power experiment just described. The fuel helium blower was turned on with the reactor on servo, and the fuel was cooled. However, the action took place so rapidly that a 1-min time lag³ of the fuel mean temperature had to be accounted for in plotting the data in addition to the temperature correction. Figure O.6, in which the regulating rod movement is plotted as a function of the mean fuel temperature, shows the experimental measurements. Two distinct slopes were observed that corresponded to an initial fuel temperature coefficient and to an over-all temperature coefficient of reactivity.

From the steep slope (curve No. 1) a fuel temperature coefficient of -1.17×10^{-4} ($\Delta k/k$)/ $^{\circ}\text{F}$ was obtained, and from the other slope an over-all coefficient of -5.9×10^{-5} ($\Delta k/k$)/ $^{\circ}\text{F}$ was found. These two values are in fair agreement with the accepted values of -9.8×10^{-5} and -6.1×10^{-5} for these coefficients.

³Time lags at high power operation were observed to be shorter than those at low or no power. For a discussion, see Chapter 4.

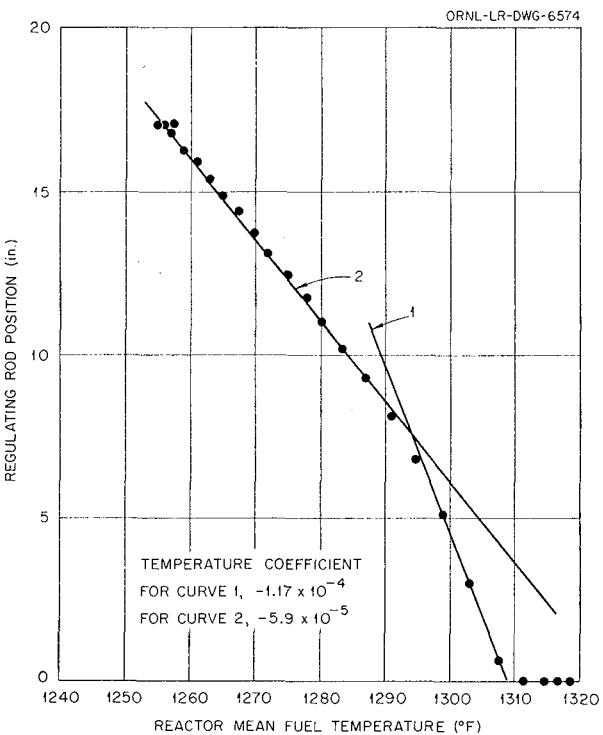


Fig. O.6. Regulating Rod Position as a Function of Reactor Mean Fuel Temperature for Experiment H-4.

Appendix P

THEORETICAL XENON POISONING

The xenon poisoning which existed in the ARE was determined experimentally to be an almost negligible amount. It was therefore of interest to compute the amount of such poisoning that would have been present if no xenon had been lost due to off-gassing of the fuel so that a measure of the effectiveness of the off-gassing process could be obtained.

The poisoning by Xe^{135} , when the xenon content has reached equilibrium, is given by¹

$$(1) \quad P_0 = \frac{\sigma_2(\gamma_1 + \gamma_2)\phi_0}{(\lambda_2 + \sigma_2\phi_0)} \left(\frac{\Sigma_f}{\Sigma_u} \right),$$

where

P_0 = the ratio of the number of thermal neutrons adsorbed in the xenon to those adsorbed in the fuel,

σ_2 = microscopic xenon cross section for thermal-neutron absorption,

$(\gamma_1 + \gamma_2)$ = the total fractional yield of Xe^{135} from fission, both from iodine decay and direct Xe formation = 0.059,

λ_2 = the decay constant for Xe^{135} = $2.1 \times 10^{-5}/sec$,

Σ_f/Σ_u = the ratio of the macroscopic thermal-neutron cross section for fission to that for absorption, for U^{235} $\Sigma_f/\Sigma_u = 0.84$,

ϕ_0 = the average thermal-neutron flux in the fuel (since the entire fuel volume, 5.33 ft^3 , is equally exposed to this flux, although there is only 1.37 ft^3 of fuel in the core at one time, the average flux in the fuel is $1.37/5.33$ or 0.26 times the average flux in the reactor, which is 0.7×10^{13}).

The Xe^{135} absorption cross section, σ_2 , is smaller in the ARE than at room temperature, because the average neutron energy in the ARE exceeds the average neutron energy corresponding to room temperature and because the Xe^{135} absorption cross section drops off rapidly with

¹S. Glasstone and M. C. Edlund, *The Elements of Nuclear Reactor Theory*, D. Van Nostrand Co., Inc., New York (1952), p 333, 11.57.2.

increasing neutron energy. R. R. Bate, R. R. Coveyou, and R. W. Osborn investigated the neutron energy distribution in an absorbing infinite moderator by using the Monte Carlo method and the Oracle. By assuming a constant scattering cross section and a constant $1/v$ absorption cross section, they found that the neutron energy distribution is well represented by a Maxwellian distribution corresponding to an effective temperature, T_e , provided

$$\kappa = \sqrt{\frac{2}{3}} \frac{\Sigma_a}{\Sigma_s} < 0.06 ,$$

where the macroscopic absorption cross section Σ_a is measured at the moderator temperature and Σ_s is the macroscopic scattering cross section. The effective temperature

$$T_e = T_m(1 + \alpha A \kappa) ,$$

where T_m is the moderator temperature, α is a constant approximately equal to 0.9, and A is the atomic weight of the moderator.

The present state of the theory does not permit consideration of the inhomogeneous distribution of the various constituents of the ARE core, and therefore the main constituents were considered to be evenly distributed over the core. The nuclei per cubic centimeter were thus

Oxygen	5.5×10^{22}
Beryllium	5.5×10^{22}
U^{235}	7.8×10^{19}

Other elements made only a negligible contribution to the cross section of the core. The following cross sections were used:

Oxygen, scattering	4 barns
Beryllium, scattering	7 barns
Uranium, absorption	360 barns ²

²Obtained by converting the room temperature value of the cross section to the value at the reactor operating temperature by multiplying by the square root of the ratio of the temperatures:

$$630 \text{ (barns)} \times \sqrt{\frac{293 \text{ }(^{\circ}\text{K})}{1033 \text{ }(^{\circ}\text{K})}} = 360 \text{ (barns)} .$$

Thus

$$\kappa = \sqrt{\frac{2}{3}} \frac{360 \times 7.8 \times 10^{19}}{(4 + 7) \times 5.55 \times 10^{22}} = 0.038 .$$

For the atomic weight, A , the average of the values for beryllium and oxygen, 12.5, was assumed. Thus

$$\begin{aligned} T_e &= 1033[1 + (0.9 \times 12.5 \times 0.038)] \\ &= 1474^\circ\text{K} \\ &= 2200^\circ\text{F} . \end{aligned}$$

The Xe^{135} absorption cross section in the reactor was then determined, as shown in Table P.1, which gives the energy intervals of the neutrons, E_i , the fraction of neutrons in these energy intervals according to the Maxwell-Boltzman distribution, $n(E_i)/n$, and the total Xe^{135} cross section, σ_t , for each energy interval,³ from which the average Xe^{135} cross section is obtained. In the energy range in question the xenon adsorption cross section is approximately equal to the total xenon cross section, σ_t . As shown in Table P.1, the value of this cross section is 1.335×10^6 barns or $1.335 \times 10^{-18} \text{ cm}^2$.

The anticipated xenon poisoning during the 25-hr xenon run (exp. H-11) may then be computed from Eq. 1 by using the value determined above for the Xe^{135} absorption cross section:

$$\begin{aligned} P_0 &= \frac{1.3 \times 10^{-18} \times 0.059 \times 0.7 \times 10^{13} \times 0.26}{(2.1 \times 10^{-5}) + (1.3 \times 10^{-18} \times 0.7 \times 10^{13} \times 0.26)} \times 0.84 \\ &= \frac{0.0117 \times 10^{-5}}{(2.1 + 0.24) \times 10^{-5}} = \frac{0.0117}{2.34} = 0.005 . \end{aligned}$$

This value has to be corrected because about one-third of the fissions occur at energies above thermal and therefore have only little competition from xenon absorption. Furthermore, the reactivity loss due to poison was about 8% of that computed above because of the absorption in other poisons

TABLE P.1. Xe^{135} ABSORPTION CROSS SECTION IN THE REACTOR

E_i (ev)	$f = \frac{n(E_i)}{n}$	ΔE	$\sigma_t^{Xe}(E_i)$ (barns)	$f \times \sigma_t^{Xe}(E_i)$ (barns)
0.02	0.060		2.50×10^6	0.150×10^6
0.04	0.073		2.75×10^6	0.200×10^6
0.06	0.076		3.25×10^6	0.248×10^6
0.08	0.075		3.30×10^6	0.248×10^6
0.10	0.072		2.82×10^6	0.201×10^6
0.12	0.067		1.92×10^6	0.129×10^6
0.14	0.062		1.27×10^6	0.079×10^6
0.16	0.057		0.75×10^6	0.042×10^6
0.18	0.051		0.45×10^6	0.023×10^6
0.20	0.046		0.32×10^6	0.015×10^6
Average σ_t^{Xe}				1.335×10^6

(such as Inconel, etc.), and during the 25 hr of operation, if the xenon had all stayed in the fuel it would have reached 69% of its equilibrium concentration.⁴ By applying these various corrections, it is found that the xenon poisoning in the ARE at the end of the 25-hr run should have

been 0.2% in $\Delta k/k$ if no xenon had been off-gassed.

³BNL-170.

⁴Glasstone and Edlund, *op. cit.*, p 333.

Appendix Q

OPERATIONAL DIFFICULTIES

The operational difficulties described here are only those which occurred during the nuclear phase of the operation, that is, from October 30 to November 12, the period of time covered by this report. With a system as large, as complex, and as unique as that which constituted the ARE, it is amazing that so few difficulties developed during the crucial stages of the operation. Furthermore, such troubles were, without exception, not of a serious nature. This is in large measure attributable to the long period of installation and testing¹ which preceded the nuclear operation, the safety features inherent in the system, and the quality of workmanship which went into its construction. All major difficulties and impediments which arose are discussed below and are grouped by systems, with special regard for chronology of occurrence.

ENRICHMENT SYSTEM

As mentioned previously, the fuel enrichment system was changed (shortly before the critical experiment was to begin) from a remotely operated two-stage system, in which the transfer was to start with all the fuel concentrate in a single container, to a manually operated two-stage system, in which small batches of the available concentrate were transferred, one at a time. A portion of the equipment used is shown in Fig. Q.1. Although this change resulted in an improvement both in safety and control, the temperature control of the manually operated system was persistently difficult. Furthermore, in order to avoid plugged lines because of the concentrate freezing at cold spots, the lines had to be continuously purged with gas and the exit gas lines then plugged as a result of concentrate-vapor condensation. Both these difficulties could have been avoided with proper design.

The temperature control was a greater problem here than anywhere else in the system because of the small ($\frac{5}{16}$ and $\frac{3}{8}$ in.) tubing used in the transfer lines and an inferior technique of heater installation. This problem was aggravated by the virtual inaccessibility of the connection between the transfer line and the pump at the time the system was revised. The final heater arrangement used, which proved to be satisfactory, consisted of

double tracing of the line with calrod heaters staggered so that successive pairs of calrods did not meet at the same point. Even with this arrangement, thermocouples were necessary at every heater junction and each calrod or each pair of calrods should have had a separate control.

After it became an established part of the enrichment procedure to continuously bleed gas through the transfer line into the pump (in order to keep the line clear), the gas was vented through an extra line at the pump. The extra line was not properly heated and soon plugged with vapor condensate. It then became necessary to use the primary pump vent system which had a vapor trap. By reducing the bleed gas flow to a minimum, this vent system could be used without becoming plugged with vapor condensate.

The transfer line to the pump served adequately throughout the critical experiment, although it had to be reworked four times either because of the formation of plugs or the development of leaks (in Swagelok connections where the line was cut and replaced). During the last injection for rod calibration the transfer line again became plugged at the fitting through the pump flange. This fitting was a resistance-heated concentric-tubing arrangement which provided an entrance for the 1300°F transfer line through the 700°F pump flange. The oxidized fuel from previous leaks had shorted the heating circuit, and the fitting had therefore cooled and plugged. Attempts to clear the fitting caused it to leak; the leak was sealed but the fitting was then inoperable.

The final injection of concentrate, which was required for burnup at power, xenon poison, etc., was therefore made through the fuel sampling line. A special batch of concentrate was prepared and pressurized into the pump through the sample line. This technique worked satisfactorily but had previously been avoided because the line had not been designed to attain the high temperatures >1200°F required by the melting point of the concentrate. Furthermore, the sample line was attached to the pump below the liquid level in the pump, and if a leak had developed in the line a sizeable spill would have resulted.

¹Design and Installation of the Aircraft Reactor Experiment, ORNL-1844 (to be issued).

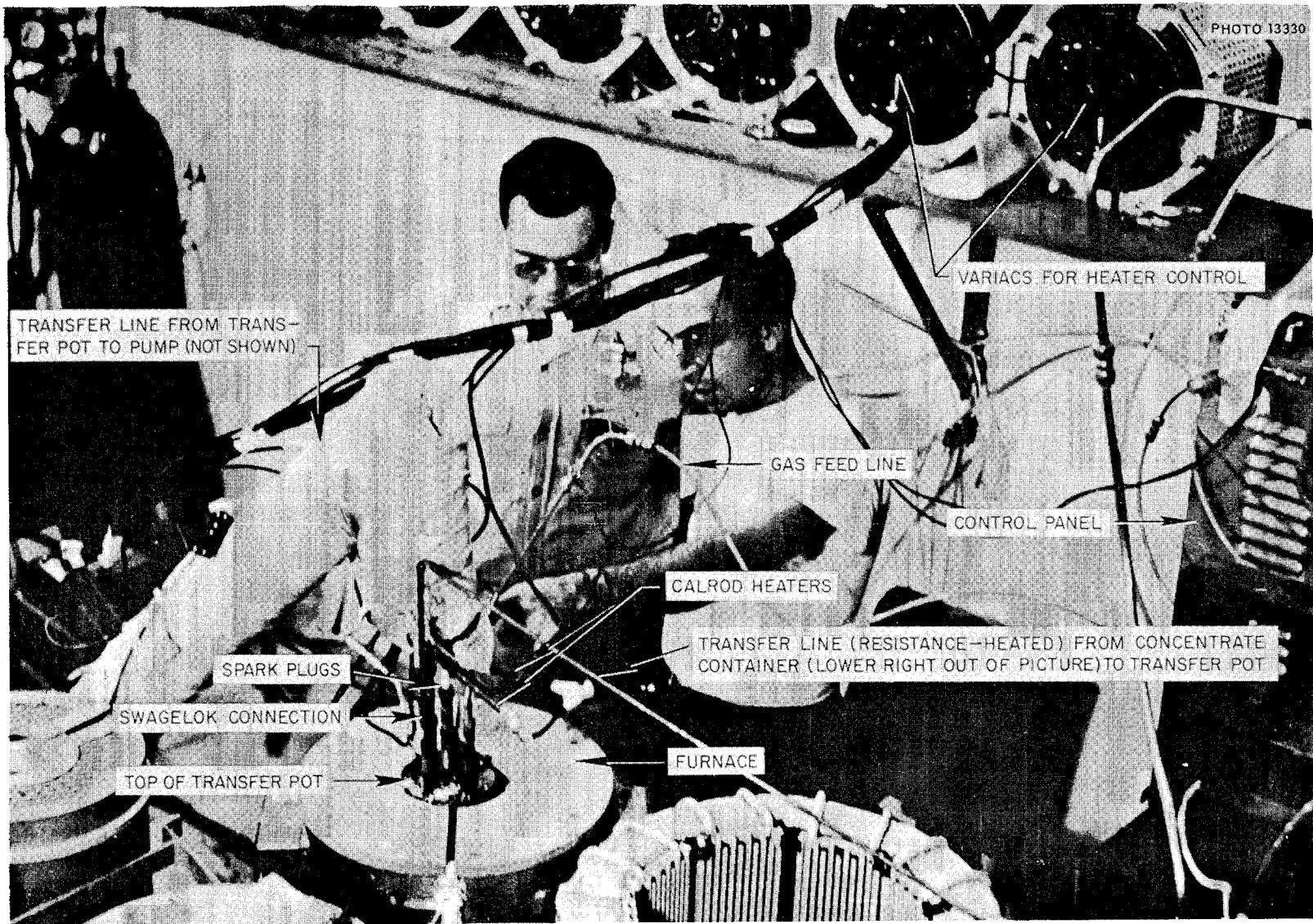


Fig. Q.1. Enrichment System Transfer Pot and Transfer Lines.

PROCESS INSTRUMENTATION

For an appreciation of the generally excellent performance of the instrumentation, knowledge of the number and complexity of the instruments is required. There were at least 27 strip recorders (mostly multipoint), 5 circular recorders, 7 indicating controllers, 9 temperature indicators (with from 48 to 96 points apiece), about 50 spark plugs, 20 ammeters, 40 pressure gages, 16 pressure regulators, 20 pressure transmitters, and numerous flow recorder indicators and alarms, voltmeters, tachometers, and assorted miscellaneous instruments. Furthermore, many of these were employed in systems circulating fuel and sodium at temperatures up to 1600°F. Since all instruments were subject to routine inspection and service, petty difficulties were kept to a minimum.

In the course of nuclear operation, only the following instruments gave cause for particular concern: fuel flowmeter, main fuel pump level indicator, several sodium system spark plugs, fuel pressure transmitter, and several pump tachometer generators. Of these only the tachometer generator "failures" were not caused by the materials and temperatures being instrumented. The tachometers, as installed, were belt driven rather than direct-coupled and were not designed to withstand the side bearing loads to which they were subjected. The tachometers were replaced, however, before the pits were sealed, and they performed satisfactorily during the high-power operation.

The fuel flowmeter and the fuel pump level indicator were similar instruments in which a float or bob was attached to a long tapered iron core suspended in a "dead leg." Coils were mounted outside the dead leg which located the position of the core. The position of the core could be interpreted as a measure either of fuel level or of fuel flow up past the bob. The coil current, however, was very sensitive to the fuel temperature, which had to be maintained above the fuel melting point. In addition to the temperature sensitivity, several coils (spare coils were provided on each instrument) opened up during the experiment, presumably due to oxidation of the coil-to-lead wire connection. The fuel flowmeter oscillated rapidly over a 10-gpm range throughout the later stages of the experiment, although the electronics of the instrument appeared to be in order. On the other hand, operation of the main fuel pump level indicator was satisfactory up to the last day of operation, at which time the spare coil opened up (the main coil

had previously opened). It is felt that these instruments would have performed satisfactorily if the iron core were designed to move in a trapped gas leg above the float rather than in a dead leg below the float so that the operating temperature could be reduced. Furthermore, the coil reading should be "balanced out" to eliminate the temperature sensitivity.

Of the numerous spark plugs which were employed in the various fuel and sodium tanks as the measure or check on the liquid level, only three of those in the sodium system showed a persistent tendency to short. These shorts could not always be cleared by "short-burning," but they frequently cleared themselves as the liquid level dropped. Although the probes were located in a riser above the tank top to minimize shorts, the shorts could probably have been eliminated by using larger clearances than were afforded by the use of $\frac{1}{8}$ -in.-OD probes in a $\frac{1}{2}$ -in.-IPS pipe riser.

The high-temperature fuel system pressure transmitters suffered a zero shift during the course of the experiment. These transmitters employed bellows through which the liquid pressure was transmitted to gas. It is probable that the bellows were distorted at times when the gas and liquid pressure were not balanced as a result of operational errors or plugged gas supply lines. In any case, the gas ports in the transmitter occasionally plugged, and a zero shift in the instrument was observed.

In view of the large number of thermocouples in use throughout the experiment (in the neighborhood of 1000), it is not surprising that a small number were in error. However, those which gave incorrect indications included some of the most important ones associated with the entire experiment. As discussed in Appendix K there was serious disagreement between line thermocouples inside and outside the reactor thermal shield, although it would appear that they both should have given the same indication. Other misleading temperature readings were obtained from the thermocouples on the tubes in the fuel-to-helium heat exchangers. These thermocouples were not properly shielded from the helium flow and read low.

Although most of the thermocouple installations were designed to measure equilibrium temperatures and did so satisfactorily for a number of experiments involving fast transients, it was important that the response of the thermocouples be $> 10^{\circ}\text{F}$ per sec in order to correlate the changes in fluid

temperatures with nuclear changes. Unfortunately it is not certain that this was the case, and, in addition, in certain instances, as with one of the thermocouples on each of the reactor ΔT and reactor mean temperature instruments, the thermocouples were mounted on electrical insulators which increased the thermal lags.

The above discussion covers most of the instrumentation difficulties that arose. This is not meant to imply, for example, that all the 800-odd thermocouples lasted throughout the experiment; there were open thermocouples scattered throughout the system. Furthermore, the instrument mechanics were kept busy; when not doing installation work, they were usually involved in routine service and maintenance work.

NUCLEAR INSTRUMENTATION AND CONTROLS

It is difficult in the case of the nuclear instruments to separate operation problems from those inherent in routine installation and debugging, since these latter operations were continued right up to the time the instruments were needed. However, during actual operation, all nuclear instrumentation performed satisfactorily. The control mechanism operated as designed, except that one shim rod had a higher hold current (it was supported by an electromagnet) than the other two. This situation was improved by cleaning the magnet face and filtering the gas surrounding the magnet.

ANNUNCIATORS

The control system included an annunciator panel which anticipated potential troubles and indicated off-design conditions by a light and an alarm. During the course of the experiment, certain annuncicators consistently gave false indications, and therefore the bells (but not the lights) of these annunciators were finally disconnected. Included were the standby sodium pump lubrication system flow, the standby fuel pump cooling water flow, the fuel heat exchanger water flow, and the fuel heat exchanger low-temperature alarm. The first three annunciators had mercury switches which were either improperly mounted or set too close to the design condition, but the fuel heat exchanger low temperature alarm error was due to faulty thermocouple indication; that is, instead of indicating fuel temperature, the thermocouple, which was located in the cooling gas stream, read low.

HEATERS AND HEATER CONTROLS

During the time the system was being heated, the heater system power was over 500 kw. This heat was transferred to the piping and other components by the assorted ceramic heaters, calrods, and strip heaters that covered every square inch of fuel and sodium piping, as well as all system components which contained these liquids. Although there were numerous heater failures resulting from mechanical abuse up until the time the pits were sealed, all known failures were repaired before the pit was sealed. Only four heater circuits were known to be inoperable at the time the reactor was scrammed — two heaters showed open, two shorted.

Except for the fuel enrichment system in which the heating situation was aggravated by the higher temperatures as well as the small lines, the available heat was adequate everywhere. The control of the various heater circuits was, however, initially very poor; it consisted of four voltage buses to which the various loads could be connected plus variacs for valve and instrument heaters. However, in order to obtain satisfactory heater control for all elements of the system, 13 additional regulators were installed in addition to numerous additional variacs. With the additional regulators it was possible to split up the heater load to get the proper temperatures throughout the system without overloading any distribution panel. Even with the helium annulus, one function of which was to distribute the external heat uniformly, it must be concluded as extremely desirable, if not an absolute necessity, that all components of any such complex high-temperature system be provided with independently controlled heater units in order to achieve the desired system equilibrium temperature.

SYSTEM COMPONENTS

The only major components of either the sodium or fuel system which caused any concern during the nuclear operation were the sodium valves (several of which leaked) and the fuel pump (from which emanated a noise originally believed to originate in the pump bearings). In addition, there were problems associated with plugged gas valves and overloaded motor relays.

The sodium valves that leaked were the two pairs that isolated the main and standby pumps and at least one of the fill valves in the lines to the three sodium fill tanks. The leakage across

the pump isolation valves was eliminated from concern by maintaining the pressure in the inoperative pump at the value required to balance with the system pressures. The leak (or leaks) in the fill valves was of the order of $\frac{1}{2}$ to 1 ft³ of sodium per day, and was periodically made up by refilling the system from one of the fill tanks. In the course of these operations, two tanks eventually became empty, and it was then apparent that most of the leakage had been through the valve to the third tank. This leakage was initially abetted by the high (~ 50 psi) pressure drop across the valve, but even though the pressure difference was reduced to 5 to 10 psi the leakage rate appeared to increase during the run.

It was of interest, as well as fortunate for the ultimate success of the project, that the fuel carrier fill valves were tight. However, in the fuel system, only two valves were opened during the filling operation and only one of these had to seal in order to prevent leakage. This valve did seal, and it was opened only one other time, i.e., when the system was dumped.

Each sodium pump (main and standby) and each fuel pump (main and standby) was provided with four microphone pickups to detect bearing noises. Shortly after the fuel system had been filled with the fuel carrier, the noise level detected on one of the main fuel pump pickups jumped an order of magnitude, while that on the other increased substantially. At the time the noise was believed to be due to a flat spot on a bearing, and operation was therefore watched very closely. When the noise level did not increase further (in fact, it tended to decrease), it was decided to continue the experiment without replacing the pump (a very difficult job which could conceivably have resulted in contamination of the fuel system). The pump operated satisfactorily throughout the experiment. Subsequent review of the pump design and behavior of the noise level indicated that the noise probably originated at the pump discharge where a sleeve was welded inside the system to effect a slip connection between the pump discharge duct from the impeller housing and the exit pipe, which was welded to the pump casing. Vibration of the sleeve in the slip joint could account for all the noise.

Although the vent header was heated from the fuel and sodium systems to the vapor trap filled with NaK (which was provided to remove certain fission products but also removed sodium vapor),

the temperature control of the header and the individual vent lines connected to it was not adequate to maintain the line above the sodium melting point and yet not exceed the maximum temperature limit (400°F) of the solenoid and diaphragm gas valves. Consequently, these vent lines became restricted by the condensation of sodium vapor. It was apparent that a higher temperature valve would have been desirable, that the gas line connecting the tank to the header should have been installed so that it could drain back into the tank, and, also, that good temperature control of the line and valve should have been provided. As it was, exceptionally long times were required to vent the sodium tanks through the normal vent valves. It would have been necessary to use the emergency vent system, which was still operable at the end of the experiment, if a fast dump had been required.

In addition to the above failures or shortcomings, there were numerous problems of less serious nature in connection with auxiliary equipment, motor overloads, water pipes which froze and split, and air dryers which burned out. However, nothing occurred in such a manner or at such a time as to have any significant bearing on the conduct of the experiment.

LEAKS

The only sodium or fluoride leaks that occurred have already been discussed. These included one minor sodium leak in the sodium purification system (discussed in chap. 3, "Prenuclear Operation") and two fuel concentrate leaks from the enrichment system. That neither the reactor fuel system nor sodium system leaked is a tribute to the quality of the workmanship in both welding and inspection that went into the fabrication of these systems. In all, there were over 266 welded joints exposed to the fluoride mixture, and over 225 welded joints were exposed to the sodium.

In contrast to the liquid systems, there were several leaks in gas systems. It is felt that these leaks would not have occurred if the gas systems had been fabricated according to the standards used for the liquid systems. The notable gas leaks were from the fuel pumps into the pits, from the helium ducts in the heat exchangers into the pits, and from the pits into the building through the various pit bulkheads, as well as the chamber which housed the reactor controls.

The combination of the leak out of the fuel pump and that out of the pits required that the pits be maintained at subatmospheric pressures in order to prevent gaseous activity from contaminating the building. Accordingly, the pit pressure was lowered by about 6 in. H₂O by using portable compressors which discharged the gaseous activity some 1000 ft south of the ARE building. The activity was of such a low magnitude that, coupled with favorable meteorological conditions, it was possible to

operate in this manner for the last four days of the experiment.

The leaks out of the helium ducts in the fuel and sodium heat exchangers resulted in a maximum helium concentration in the ducts of the order of 50%, and to maintain even this low concentration, it was necessary to use excessive helium supply rates, i.e., 15 cfm to the ducts alone and another 10 cfm to the instruments.

Appendix R

INTEGRATED POWER

The total integrated power obtained from the operation of the Aircraft Reactor Experiment does not have any particular significance in terms of the operational life of the system. However, a total integrated power of 100 Mw was more or less arbitrarily specified as one of the nominal objectives of the experiment. While at the time the experiment was concluded it was estimated that this, as well as all other objectives of the experiment, had been met, the estimate was based on a crude evaluation of reactor power. Since subsequent analyses of the data have permitted a reasonably accurate determination of the reactor power, it is of interest to reappraise the estimated value of the total integrated power.

The total integrated power could be determined from either the nuclear power or the extracted power (cf., section on "Reactor Kinetics" in chap. 6). The power curves, which should have equivalent integrals, could be obtained from any of a number of continuously recording instruments, i.e., the nuclear power from either the micromicroammeter or log N meter, and the extracted power from any of the several temperature differential recorders in the fuel and sodium circuits. The total integrated power has been determined both from integration of a nuclear power curve ($\log N$) and from the sum of the extracted power in both the sodium and fuel circuits, as determined by the temperature differentials in each system together with their respective flows (which were held constant). For both power determinations a calculation of the associated error was made.

EXTRACTED POWER

The integrated extracted power was determined from the charts which continuously recorded the temperature differential (ΔT) in each system. As a matter of convenience the sodium system ΔT was taken from a 24-hr circular chart, while the fuel ΔT was taken from one of the six Brown strip charts which recorded, in the control room, the ΔT across each of the six parallel fuel circuits through the reactor. The individual circuit recorders had a much slower chart speed than that of the over-all ΔT recorder and were therefore much easier to read. To keep the results well within the accuracy of the whole experiment, tube No. 4 was selected for the determination because

the chart trace very closely corresponded to that of the over-all fuel ΔT across the reactor. From Fig. K.3, Appendix K, the control-room-recorded ΔT was converted to what was accepted as the correct ΔT . The power extraction was then calculated and plotted against time in Fig. R.1.

The sodium ΔT across the reactor was obtained from the circular charts of the recorders located in the control room. These ΔT 's were also corrected by using Fig. K.6, Appendix K, and the plot of the power extracted by the sodium as a function of time is also shown in Fig. R.1 on the same abscissa as that of the fuel plot. The total integrated (extracted) power, i.e., the sum of the area under both the fuel and sodium system power curves, was then determined by using a planimeter; it was found to be 97 Mw-hr.

A calculation was also made of the magnitude of the "maximum" possible error in the determination of the reactor power. The power equation, which was calculated for both the fuel and sodium systems, was

$$P = kf \Delta T ,$$

where

P = reactor power,

k = a constant containing heat capacity and conversion units,

f = flow rate of fuel or sodium,

ΔT = temperature difference across reactor.

The consequent error equation is

$$\Delta P = kf \Delta(\Delta T) + k \Delta T \Delta f + f \Delta T \Delta k ,$$

where

Δk = maximum error in the heat capacity,

Δf = maximum error in the flow rate,

$\Delta(\Delta T)$ = maximum error in the temperature difference.

Nominal average values of these factors for the fuel system were

$$f = 46 \text{ gpm}$$

$$\Delta T = 350^\circ\text{F}$$

$$k = 0.11 \text{ kw/day gpm}$$

$$\Delta f = 2 \text{ gpm} \approx 5\%$$

$$\Delta(\Delta T) = 10^\circ\text{F} \approx 3\%$$

$$\Delta k = 0.011 \approx 10\%$$

Therefore

$$\Delta P \text{ (for fuel system)} = 20\%$$

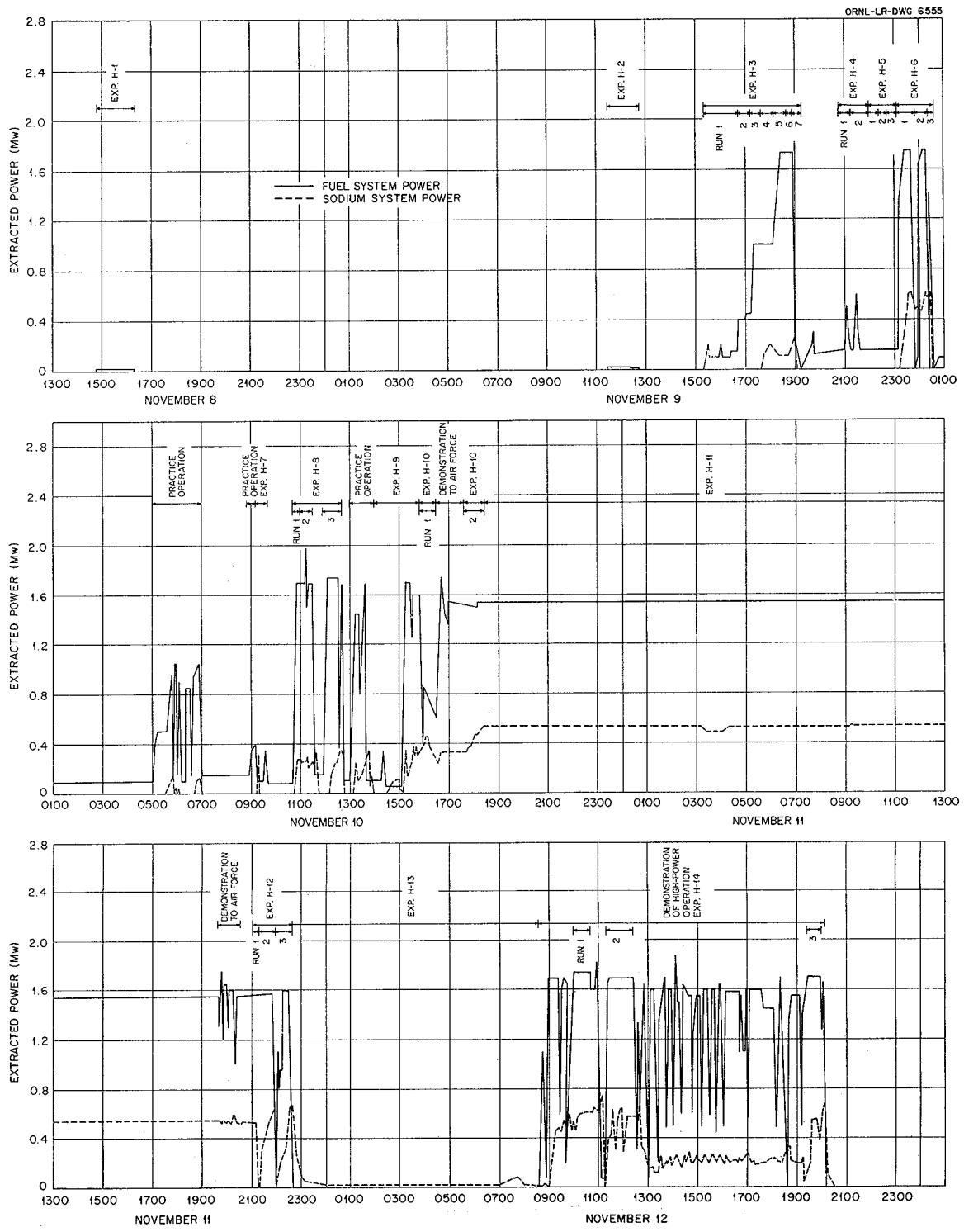


Fig. R.1. Power-Time Curve.

The values for the sodium system were

$$\begin{aligned}f &= 152 \text{ gpm} \\ \Delta T &= 50^\circ\text{F} \\ k &= 0.0343 \text{ kw/day.gpm} \\ \Delta f &= 4 \text{ gpm} \approx 3\% \\ \Delta(\Delta T) &= 10^\circ\text{F} \approx 20\% \\ \Delta k &= 0\end{aligned}$$

Therefore

$$\Delta P \text{ (for sodium system)} = 11\%$$

The weighted, over-all percentage error was therefore

$$\frac{\Delta P}{P} = \frac{P_f \times 0.20}{P} + \frac{P_s \times 0.11}{P} = 17\%,$$

where P_f and P_s are the power extracted in the fuel and sodium systems. The errors made in the power integration by using the ΔT chart are only those associated with the determination of power extraction. Since Fig. R.1 is a reproduction of the ΔT trace and it was integrated by using the planimeter, any integrating errors were assumed to have been averaged out. Therefore, the error that applies to the integrated extracted power is the 17% that is applicable to the power level determination; therefore the integrated extracted power was

$$97 \pm 16.5 \text{ Mw-hr}.$$

NUCLEAR POWER

During most of the time the reactor was operating at any appreciable power level, the nuclear power level was kept fairly constant and was recorded in the log book. During the times the power level was either not constant or not recorded in the log book, the nuclear power was determined from the log N recorder chart by integrating the area under the power trace. (The log N trace was used rather than the micromicroammeter because no record was kept of the micromicroammeter shunt value as a multiplying factor.) Since the log N chart gave a log of power vs time plot, exact integration under the curve would have been an extremely difficult task; accordingly, the area under the curve was integrated graphically. The curved portions of the trace were approximated by straight lines, and an average log N value was determined for each line segment. It was assumed that there were as many positive as negative errors in this method and that the errors cancelled out. The total integrated power was then obtained

by adding up all the incremental areas which were in terms of average log N units times time.

From the 25-hr constant-power xenon run a relation between the log N reading and the extracted power was obtained. It was found that $22.5 \log N \text{ units} = 2.12 \text{ Mw}$, or $10.6 \log N \text{ units} = 1 \text{ Mw}$; therefore

$$\frac{\log N}{10.6} \times \text{time (hr)} = \text{Mw-hr}$$

for any segment under the curve. By using this correlation between actual power and log N reading, the total integrated nuclear power was calculated to be 96.6 Mw-hr. This value of the integrated nuclear power, Q , as determined from the log N chart, was, in effect, found from the following relation

$$Q = MC \Delta t,$$

where

M = average log N recorded value over an increment of time Δt ,

Δt = increment of time in hours,

C = a constant which converts the log N value to Mw-hr.

The constant, C , in the expression is equal to the percentage error in the extracted power level determination, which was calculated in the preceding section to be 17%. Therefore the error in C is $(0.17)(1/10.6) = 0.016$. The 74-hr period of high-power operation was divided into two parts, one part being the 25-hr period of constant power during the xenon run and the remainder being the 49-hr period of variable power. The errors were of different magnitude for each part, since during the xenon run there was no error in time or in the determination of the average value of M .

For the 25-hr xenon run the integrated power was 53 Mw-hr. Thus

$$\begin{aligned}M &= 22.5 \log N \text{ units} \\ \Delta t &= 25 \text{ hr} \\ C &= 0.094 \text{ Mw}/\log N \\ \Delta M &= 0 \\ \Delta(\Delta t) &= 0 \\ \Delta C &= 0.016 \approx 17\%\end{aligned}$$

Therefore

$$\Delta Q_1 = MC \Delta(\Delta t) + M \Delta C \Delta t + \Delta M C \Delta t = 9 \text{ Mw-hr}.$$

For the balance of the operating time (49 hr) and integrated power (43.6 Mw-hr), the average M must

be determined as

$$\bar{M} = \frac{Q}{Ct} = \frac{43.6}{(0.094)(49)} = 9.46$$

and for ΔQ_2

$$\bar{M} = 9.46 \log N \text{ units}$$

$$\Delta t = 49 \text{ hr}$$

$$C = 0.094 \text{ Mw}/\log N$$

$$\Delta M = 1$$

$$\Delta(\Delta t) = 1 \text{ hr}$$

$$\Delta C = 0.016 \approx 17\%$$

$$\Delta Q_2 = MC \Delta(\Delta t) + M \Delta C \Delta t + \Delta M C \Delta t = 12.8 \text{ Mw-hr.}$$

The total error was therefore

$$\Delta Q = 12.8 + 9.0 = 21.8 \text{ Mw-hr or } 22.5\% .$$

The total extracted nuclear power then was

$$96.6 \pm 21.8 \text{ Mw-hr.}$$

Appendix S

INTERPRETATION OF OBSERVED REACTOR PERIODS DURING TRANSIENTS

When excess reactivity is being introduced into a reactor at a given rate, the period meter will show a period which is not a true period but a combination of the true period and its time rate of change. If the time rate of change of the period is known, then the true period may be found by the following means.

First, it is assumed that whenever any excess reactivity is introduced into the reactor the power will rise according to the following equation:

$$P = P_0 e^{\lambda t},$$

where

P_0 = initial power,

$\lambda = 1/\tau$,

τ = reactor period,

t = time power is increasing.

Then, to introduce a time rate of change of the period, the power is expressed in the form of an infinite series

$$P = P_0 \left(1 + \lambda t + \frac{\lambda^2 t^2}{2!} + \dots \right).$$

If the higher order terms are neglected, the rate of change of power is

$$\frac{dP}{dt} = P_0 \left(\lambda + t \frac{d\lambda}{dt} \right),$$

and therefore

$$\lambda = \frac{1}{P_0} \left(\frac{dP}{dt} - t \frac{d\lambda}{dt} \right)$$

and

$$\tau = \frac{P_0}{\left(\frac{dP}{dt} - t \frac{d\lambda}{dt} \right)}.$$

In experiment H-8 (cf., chap. 6) it was noted that when the regulating rod was withdrawn the period observed was not a true period and that it kept changing over the 35 sec it took the regulating rod to travel its full distance. For a calculation of the true period, the following values were taken from Fig. 6.10 and Table 6.4:

$$P_0 = 2.34 \text{ Mw},$$

$$P = 3.94 \text{ Mw},$$

$$\tau_1 = 25 \text{ sec (initial period observed)},$$

$$\tau_2 = 50 \text{ sec (final period observed)},$$

$$t = 35 \text{ sec.}$$

From these values, it was found that

$$\frac{dP}{dt} = 0.0457 \text{ Mw/sec}$$

and

$$t \frac{d\lambda}{dt} = 35 \left(\frac{\frac{1}{50} - \frac{1}{25}}{35} \right) = -0.02.$$

Therefore

$$\tau \approx \frac{2.34}{0.0457 + 0.02} = 36 \text{ sec}.$$

This calculated value for the true period corresponds fairly closely to the period of 42 sec measured from the slope of the log N recorder trace.

Appendix T NUCLEAR LOG

The following information was copied verbatim from the nuclear log book. The only material omitted was the running uranium inventory, which was kept during the critical experiment, and several calculations and graphs, which were inserted in the log book in an attempt to interpret the data. All the omitted information is presented in much better form elsewhere in this report.

The reactor power data referred to in the log are not consistent, because the power was estimated first from a calculation of flux at the chambers, subsequently from the activation of a fuel sample, and finally from the extracted power. If it is assumed that the extracted power value is correct, the original estimate was a factor of 2.7 low and that calculated from the fuel activation was a factor of 2 low. In the log book, all power levels mentioned through experiment L-8 were based on the original estimate; from experiment L-9 to H-14, all power levels were based on the fuel activation; and it was not until after high-power runs 1 and 2 of experiment H-14 that correct power levels were listed.

EXPERIMENT E-1

October 30, 1954

Objective: Bring the Reactor Critical

Run	Time	
1	1425	Zero fuel flow.
	1500	Main fuel pump started to bleed down to minimum prime level.
	1507	Main fuel pump at minimum prime level. System volume is now $4.64 + 0.18 = 4.82 \text{ ft}^3$ (calculated).
2		Started adding lot from can 6.
	1539	First 5-lb lot going into pump.
	1545	It was noticed that pips on the fission chamber occurred in about 2-min intervals (pump rpm, 520).
	1554	Second 5-lb batch going in.
	1558	Third 5-lb batch going in. Interval is exactly 2 min. This gives a flow of 18.8 gpm for a pump speed of 520 rpm.
	1603	Fourth 5-lb batch going in.
	1610	Fifth 5-lb batch going in.
	1614	Last of first 30-lb lot going in.
	1623	Speeded up pump. Roughly 26 counts/sec on fission chamber 1 and 40 counts/sec on fission chamber 2. 500 rpm on pump.
	1625	Pump speed 1100 rpm.
	1720	Sample 6 taken from pump for analysis.
~1730		Shim rods up, control rod down, fission chambers down. { fission chamber 1 26.74 counts/sec fission chamber 2 41.86 counts/sec BF ₃ 6.93 counts/sec
		These count rates checked very well with count rate meters.
~1750		Shim rods down, control rod down, fission chambers down. { fission chamber 1 18.74 counts/sec fission chamber 2 24.18 counts/sec BF ₃ 6.03 counts/sec
1812		Rods started up. Control rod back to 8-in. out.
~1827		Rods out and count started prior to taking source out of core.
		Source in core { fission chamber 1 27.1 counts/sec fission chamber 2 42.0 counts/sec BF ₃ 6.97 counts/sec
1845		Source out of core { fission chamber 1 1.49 counts/sec fission chamber 2 2.24 counts/sec BF ₃ 13.44 counts/sec
1855		Source in core { fission chamber 1 27.01 counts/sec fission chamber 2 42.59 counts/sec BF ₃ 6.82 counts/sec
3	1912	Started adding lot from can 7.
	1920	Started transferring first 5-lb.
	1930	Plugged line from transfer tank to pump.
	2015	Chemists report that uranium concentration of sample 6 taken at 1720 is 2.47 ± 0.01 wt %.

EXPERIMENT E-1 (continued)

October 31, 1954

Run	Time	
(3)	0035	Attempt to clear line from transfer tank to pump.
	0230	Still unsuccessful.
	2000	New transfer line into main fuel pump installed.
	2006	Sample 7 drawn off for analysis.
	2230	Analysis of sample 7 taken at 2006 shows 1.84 ± 0.04 wt % total uranium. Grimes estimates that no appreciable concentrate was transferred last night (i.e., Saturday night) at the time the line plugged. Therefore, this sample should be representative of run 2 and supersedes the previous sample which showed 2.47% (see above).
	2300	Starting transfer of first 5 lb of 25 lb in can 7.
	2307	0.78 min between pips = 43 gpm, indicator on rotameter shows 46 gpm.
	2315	Transfer line plugged again.
		November 1, 1954
	0008	Rods inserted.
	1315	From data on rod position vs count rate, rods appear to be ineffective above 30 in.
	1320	Plug removed from transfer line. Can 7 is still attached to the system. It is estimated that 5 of the 25 lb in can 7 were injected last night. The other 20 lb are now to be injected in 5-lb batches.
	1335	Started transfer of second 5 lb of 25 lb in can 7. Interval between pips on fission chamber 2 was 30 sec. Pips are becoming hard to see.
	1349	Started transfer of third 5 lb. Interval between pips ~ 0.86 min.
	1403	Started transfer of fourth 5 lb.
	1413	Started transfer of last batch from can 7.
	1415	Transfer of 25 lb from can 7 completed. Interval between pips ~ 0.79 min.
	1421	Withdrew rods from 30 to 35 in. Three 10-min counts taken.
	1505	Rods inserted.
	1615	Set log N to come on scale at an estimated 2×10^{-3} w.
	1617	Sample 8 taken for analysis.
4	1707	First 5 lb of 30 lb from can 8 transferred.
	1720	Second 5 lb transferred.
	1731	Third 5 lb transferred.
	1742	Fourth 5 lb transferred.
	1753	Fifth 5 lb transferred.
	1804	Sixth (final) 5 lb from can 8 transferred.
	1838	Analysis of sample 8 taken at 1617 shows 3.45 ± 0.01 wt % total uranium.
	1900	Rods inserted. Check on noise on pile period recorder started.
	1940	Pile period meter shows microphonics. Epler put log N back on normal setting. Log N should come on scale $\sim 1/2$ w.
	2028	Taking sample of fuel system, sample 9.

EXPERIMENT E-1 (continued)

November 1, 1954

Run	Time	
5	2112	First 5 lb from can 9 transferred.
	2123	Second 5 lb transferred.
	2133	Third 5 lb transferred.
	2142	Fourth 5 lb transferred.
	2153	Fifth 5 lb transferred.
	2203	Sixth (final) 5 lb transferred.
	2255	Chemists report 5.43 wt % total uranium for sample 9 taken at 2028.

November 2, 1954

6	0104	First 5 lb from can 10 transferred.
	0117	Second 5 lb transferred.
	0128	Third 5 lb transferred. Two 5-min counts taken.
	0153	Fourth 5 lb transferred.
	0202	Fifth 5 lb transferred.
	0213	Sixth (final) 5 lb transferred.
7	0506	First 5 lb from can 12 transferred.
	0521	Second 5 lb transferred.
	0533	Third 5 lb transferred. Two 5-min counts taken.
	0551	Fourth 5 lb transferred.
	0600	Fifth 5 lb transferred.
	0610	Sixth (final) 5 lb transferred.
8	0831	First 5 lb from can 5 injected. Leak in line occurred.

EXPERIMENT E-2

Objective: Preliminary Measurement of Temperature Coefficient

1003	Heat barriers started up.
1005	Heat barriers up.
1005	Blower started.
1005:10	Blower up to 275 rpm.
1010	Blower off. Water heat exchanger rose 25°F. Manometer reading 5.65 in.; corresponds to ~170 gpm.
1615	Sample from fuel system taken. This is sample 10.
1820	Results from sample 10 show 9.58 ± 0.08% uranium.
2015	Sample 11 taken for analysis.
2020	Referring back to run 8, experiment E-1: It is estimated that 5.5 lb from can 5 went into transfer tank. Approximately 0.2 lb was lost in the leak and 5.3 lb went into the system. Counts vs shim rod position were taken at 5-in. intervals on shim rods. Time of day was 1442 to 1512.
2215	Sample 11 showed 9.54 ± 0.08% total uranium.

November 3, 1954

0136	Second 5 lb batch from can 5 injected. Rods at 20 in. Counts taken at intervals for each 5 in. of rod withdrawal.
0152	Rods inserted to 20 in.
0205	Injection nozzle shorted.

EXPERIMENT E-2 (continued)

November 3, 1954

Run	Time	
(8)	0226	Third 5 lb batch from can 5 injected. Rods at 20 in. Counts taken as rods withdrawn.
	0256	Final batch from can 5 injected. Chemists estimate about $2\frac{1}{2}$ lb. Counts taken as rods withdrawn.
9	0459	First batch consisting of 5.5 lb from can 11 injected. Rods at 20 in. Counts taken as rods withdrawn.
	0523	Remainder of can 11 injected. Rods at 20 in. Counts taken as rods withdrawn.
10	0836	5.5 lb from can 22 injected. Rods at 20 in. Counts taken as rods withdrawn.
	0911	Second 5.5 lb from can 22 injected. Counts taken as rods withdrawn.
	0941	Completing injection from can 22. Can 22 empty. Counts taken as rods withdrawn.
	1018	Reactor monitored. Reads ~6 mr/hr.
11	1110	5.5 lb from can 31 injected. Rods at 20 in. Counts taken as rods withdrawn.
	1147	Second 5.5 lb from can 31 injected. Rods at 20 in.
	1230	Fission chamber 2 withdrawn 2 orders of magnitude.
	1245	Balance of can 31 injected. Rods at 20 in. Counts taken as rods withdrawn.
12	1453	5.5 lb from can 20 injected. Rods at 20 in. Counts taken as rods withdrawn.
		Source withdrawn - reactor subcritical.
	1536	Second 5.5 lb from can 20 injected. Rods at 20 in. Counts taken as rods withdrawn.
	1545	Reactor critical.
	1547	Control given to servo.
	1603	Radiation survey made. Reactor reads 750 mr/hr at side; ~10 mr/hr on grill above main fuel pump.
	1604	Reactor shut down.
	1626	Shim rods brought out to about 18 in. with source in core.

November 4, 1954

- 0830 Sample 12 taken.
0840 Sample 13 taken.

EXPERIMENT L-1

**Objective: One-Hour Run at 1 w¹ (Estimated) to Determine Power Level;
Radiation Level Check**

- 1107 Shim rods coming out.
1118:40 Reactor up and leveled out. Estimated 1 watt.¹ On servo.
Micromicroammeter 1×10^{-9} ; 48.6 on Brown recorder.
1218:40 Reactor scrammed.
1250 Sample 14 taken.
1300 Sample 15 taken.
1400 Estimated power from sample 15, 1.6 w.² Count was low. Must be repeated at 10 w.

¹Actual power subsequently determined to be 2.7 w.

²See Appendix H, "Power Determination from Fuel Activation."

EXPERIMENT L-1 (continued)

November 4, 1954

Run	Time	Four samples taken from the fuel system since going critical. Analyzed as follows:		
	Time	Sample No.	Uranium (total) (wt %)	
	0830	12	12.11	± 0.10
	0840	13	12.21	± 0.12
	1250	14	12.27	± 0.08
	1300	15	12.24	± 0.12

EXPERIMENT L-2**Objective: Rod Calibration vs Fuel Addition**

0		Reactor brought critical before injecting first penguin.
	1651	Rods coming out.
	1657	Reactor up to ~1 w. Regulating rod at 13.1 in.
	1707	Reactor subcritical.
1	1710	Penguin 11 injected.
	1746	Reactor up to ~1 w. Regulating rod at 10.6 in. Rod moved 2.5 in., from 13.1 to 10.6 in.
	1758	Readjusted rods. Regulating rod at 13.0 in.
	1804	Reactor subcritical.
	1814	Penguin 19 put in furnace.
2	2009	Penguin 19 injected. Time between pips, 0.75 min.
	2018	Reactor up to ~1 w. Rod at 5.7 in.
	2024	Reactor scrammed.
	2030	Started changing from rod 4 (19.2 g/cm) to rod 5 (36 g/cm). Counts on fission chambers and BF_3 taken before changing rod.

EXPERIMENT L-3

2230 Fuel system characteristics were obtained.

EXPERIMENT L-2 (continued)

November 5, 1954

3	0142	Started withdrawing rods.
	0158	Up to ~1 w.
	0210	Reactor subcritical.
	0235	Up to ~1 w again. Temperature had drifted. Regulating rod position, 12.1 in.
	0240	Reactor subcritical.
	0245	Penguin 4 injected.
	0250	Reactor at ~1 w again. Regulating rod position, 12.1 in.
	0252	Reactor subcritical. Apparently penguin didn't come over (no dip line).
	0346	Reactor at ~1 w. Regulating rod position, 11.5 in.
	0350	Reactor subcritical.
	0354	Penguin 14 injected.
	0357	Reactor at ~1 w. Regulating rod position, 9.9 in.
	0401	Reactor subcritical. Regulating rod movement, 1.6 in.

EXPERIMENT L-2 (continued)

November 5, 1954

Run	Time	
4	0429	Reactor at ~1 w. Regulating rod position, 9.7 in.
	0431	Reactor subcritical.
	0439	Penguin 16 injected.
	0442	Reactor at ~1 w. Regulating rod position, 7.8 in. Rod moved 1.9 in.
	0445	Reactor subcritical.
5	0519	Reactor at ~1 w. Regulating rod position, 7.65 in.
	0524	Reactor subcritical.
	0529	Penguin 13 injected.
	0536	Reactor critical at ~1 w. Regulating rod position, 6.80 in.
	0542	Reactor subcritical.
6	0607	Reactor critical at ~1 w. Regulating rod position, 6.5 in.
	0612	Reactor subcritical.
	0619	Penguin 5 injected.
	0626	Reactor critical. Regulating rod position, 5.50 in.
	0631	Reactor subcritical.
	0715	Shim rods 1 and 2 inserted. Reactor shut down due to increase in radiation level above fuel pump tank upon adding concentrate to pump. During fuel addition for run 9 the background picked up to ~50 mr/hr and, on run 5 addition, increased to 55 mr/hr. The normal background at the point of measurement being ~1 mr/hr.
	1015	Trimming pump level to normal operating probe level.
	1040	Trimming pump level to estimated $\frac{1}{4}$ in. below normal operating probe.
	1105	Took fuel sample 16.

EXPERIMENT L-2-A

Objective: Test on Activity of Vent Lines by Operating Reactor at ~1 w for ~10 min and then Venting as Though Adding Fuel

1350	Preliminary data recorded.
1403	Rods 1 and 2 being withdrawn.
1413	Rods at 30 in., rod 2 being withdrawn. Fission chamber 1 at full scale.
1414	Period meter shows slight period, ~400 sec.
1416	Rod 2 at upper limit. Rod 1 being withdrawn.
1417	Period meter reaches 100 to 50 sec. Log N reading, 2×10^{-4} . Fission chamber 2 at 500 counts/sec. Rod 1 at upper limit Regulating rod being withdrawn.
1418	Micromicroammeter reading, 10. Fission chamber 2 at 1000 counts/sec. Log N, 3×10^{-4} . Period, ~400 sec.

EXPERIMENT L-2-A (continued)

November 5, 1954

Run	Time									
(6)	1420	Log N , 5×10^{-4} Fission chamber 2, 2×10^3 . Micromicroammeter, 20. Period, ~400 to 100 sec.								
	1421	On servo. Micromicroammeter, 38. Log N , 10^3 . Fission chamber 2, 3.5×10^3 counts/sec.								
	1432	Regulating rod inserted. Shim rods 2 and 1 inserted.								
	1515	Log N and period channel normal and operating correctly except 5-sec period reverse is disconnected for duration of calibration run.								
	1940	The activity observed at 0715 was explained during the run 1420 to 1432 as activity in the vent line from the pump.								
	1945	Analysis of sample 16 taken at 1105 after the 70-lb removal gave: <table> <tr> <td>Total Uranium</td> <td>12.54 wt % uranium or 11.7% U²³⁵</td> </tr> <tr> <td>Chromium</td> <td>372 ppm</td> </tr> <tr> <td>Iron</td> <td>5 ppm</td> </tr> <tr> <td>Nickel</td> <td><5 ppm</td> </tr> </table>	Total Uranium	12.54 wt % uranium or 11.7% U ²³⁵	Chromium	372 ppm	Iron	5 ppm	Nickel	<5 ppm
Total Uranium	12.54 wt % uranium or 11.7% U ²³⁵									
Chromium	372 ppm									
Iron	5 ppm									
Nickel	<5 ppm									

EXPERIMENT L-2 (continued)

7	1947	Started pulling shims.
	2002	Up to ~1 w.
	2009	Reactor subcritical.
	2014	Move shim rods - must reset. Started pulling shims.
	2016	Up to ~1 w. Regulating rod position, 6.9 in.
	2020	Shim rods going in.
	2025	Penguin 15 injected.
	2032	Up to ~1 w. Regulating rod position, 6.2 in.
	2050	Shim rods going in. Regulating rod movement, 0.7 in.
8	2148	Up to power of ~1 w. Regulating rod position, 6.8 in.
	2156	Reactor subcritical. Shim rods going in.
	2204	Penguin 18 injected.
	2211	Up to ~1 w. Regulating rod position, 5.7 in.
	2220	Shim rods going in. Reactor subcritical. Regulating rod movement, 0.6 in.
9	2238	Started up to ~1 w.
	2242	Reactor at ~1 w. Regulating rod position, 6.9 in.
	2250	Shim rods going in. Reactor subcritical.
	2258	Penguin 17 injected.
	2305	Reactor at ~1 w. Regulating rod position, 3.3 in.
	2312	Shim rods going in. Reactor subcritical.
10	2332	Reactor at power of ~1 w. Regulating rod position, 13.5 in.
	2340	Shim rods going in.
	2345	Penguin 12 injected.
	2352	Reactor critical at ~1 w. Regulating rod position, 12.95 to 13.0.
	2400	Shim rods going in. Reactor subcritical.

EXPERIMENT L-2 (continued)

November 6, 1954

Run	Time	
11	0020	Reactor critical. Adjusted regulating rod to ~3.5 in. with shims 1 and 2.
	0026	Shim rods inserted. Reactor subcritical.
	0100	Developed gas leak in injection system during injection of penguin 10.
	0212	Leak repaired; apparently penguin 10 was injected at 0100. Rods coming out.
	0223	Reactor critical. Regulating rod position, ~2.44 in.
	0228	Reactor scrammed.

EXPERIMENT L-4

Objective: One-Hour Run at 10 w to Make Radiation Survey and Observe Pile Period

0305	Shim rods coming out.
0315	Leveled off manually at ~0.1 w. Regulating rod position, 7 in.
0318	Pulled regulating rod to 8 in.
0320:11	10 w estimated power. ³ Rod moved from 6.8 to 7.9 on chart paper. 40-sec period according to the chart. Flux servo demand, 500. Micromicroammeter 51 on range 1×10^{-8} .
0420:11	Reactor scrammed after ~1 hr at 10 w estimated power. Pile period from slope of log N, 51 sec.
0505	Sample 16 taken.
0516	Sample 17 taken.
0524	Sample 18 taken.

EXPERIMENT L-5

Objective: Calibration of Regulating Rod from Reactor Periods

1	0651	Leveled out at ~1 w. Shim 3 at 30 in. Regulating rod at 13 in. Shim 3 at 33.3 in. Regulating rod at 3 in. Shim 3 at 30 in. Regulating rod at 6.5 in. Shim 3 at 28.1 in. Regulating rod at 13.4 in.
2	0705	Pulled regulating rod from 6.53 to 8.61 in. Period, 22.1 sec.
3	0925	Shim rods coming out.
	0934	Reactor at 1 w.
	0939	Reactor subcritical.
	0940	Pump stopped.
	0942	Reactor at 1 w.
	0945	Pulled regulating rod.
	0947	Reactor scrammed at ~50 w.
	0948	Pump started. From log N, 21.3-sec period. From recorder: regulating rod moved from 6.61 to 12.66.

³Actual power subsequently determined to be 27 w.

EXPERIMENT L-2 (continued)

November 7, 1954

Run	Time		Rod Position (in.)			
			Regulating Rod	1	2	3
12	0136	Reactor up to ~1 w.	8	32.8	32.4	32.1
	0138	Reactor subcritical.				
	0231	Start injection from cans 120 and 125.				
	0237	Injection completed.				
	0245	Reactor up to ~1 w.	8	28.2	28.2	27.8
	0249	Reactor shutdown.				
	0423	Sample 19 taken for chemical analysis. All fuel injection and sampling lines removed from pump. It is estimated that the liquid level is about 0.1 ft ³ below the normal operating level probe; therefore final system volume ⁴ is 5.35 ft ³ .				
		Results on sample 19:				
		Uranium (total)	13.59 ± 0.08 wt %			
		Chromium	445 ppm			

EXPERIMENT L-5 (continued)

4	1605	Up to 1 w.
	1611	Pulled regulating rod.
	1613	Scrammed at 100 w. Wrong paper on log N. By super-imposing proper paper got 27.2 sec.
		Regulating rod withdrawal from 2.80 to 4.80 in., from Brown.
5	1804	Up to 1 w.
	1808	Pulled regulating rod.
	1810	Scrammed at 100 w. From log N, period is 22.4 sec; Δk/k, 0.06%.
6	2020	Up to 1 w. Pump at 48 gpm.
	2022	Reactor subcritical.
	2024	Pump stopped, zero flow.
	2026	Up to 1 w.
	2034	Pulled regulating rod.
	2036	Reactor scrammed at 60 w.
	2037	Started pump. Period, 23.0 sec from slope on log N. Rod moved from 2.60 to 8.70 in., or 6.1 in.
7	2201	Reactor up to 1 w.
	2208	Pulled regulating rod.
	2210	Scrammed at 100 w. Period, 20.6 sec from slope on log N. Rod moved from 4.19 to 6.27 in., or 2.08 in. (Brown)

EXPERIMENT L-6

Objective: Calibration of Shim Rods vs Regulating Rod

1		One set of data taken before final fuel addition.
2	2307	Up to 1 w. Data recorded.
	2353	End of run.

⁴Inventory gave 5.33 ft³ for the volume of the fluoride in the system.

EXPERIMENT L-5 (continued)

November 7, 1954

Run	Time	
8	2353	Start of run, reactor already at 1 w.
	2358	Pulled regulating rod.
	2400	Scrammed at 200 w. Period, 23.0 sec from slope on log N. Regulating rod moved from 8.32 to 10.38 in., or 2.06 in.

EXPERIMENT L-7

November 8, 1954

Objective: Effect of Fuel Flow Rate on Delayed Neutrons

	0147	Up to 1-w power.
1	0050	Fuel Flow rate, 48 gpm. Regulating rod position, 12.2 in.
2	0057	Fuel Flow rate, 41 gpm. Regulating rod position, 11.5 in.
3	0107	Fuel Flow rate, 34 gpm. Regulating rod position, 11.0 in.
4	0110	Fuel Flow rate, 30.5 gpm. Regulating rod position, 10.5 in.
5	0113	Fuel Flow rate, 25 gpm. Regulating rod position, 10.0 in.
6	0115	Fuel Flow rate, 20 gpm. Regulating rod position, 9.35 in.
7	0117	Fuel Flow rate, 16 gpm. Regulating rod position, 9.0 in.
8	0119	Fuel Flow rate, 0 gpm. Regulating rod position, <2 (off-scale). Reset shims.
9	0122	Fuel Flow rate, 11.7 gpm. Regulating rod position, 12.3 in.
10	0125	Fuel Flow rate, 0 gpm. Regulating rod position, 3.6 in.
11	0127	Fuel Flow rate, 12 gpm. Regulating rod position, 12.2 in. Reset shims.
12	0131	Fuel Flow rate, 12 gpm. Regulating rod position, 3.7 in.
13	0136	Fuel Flow rate, 43.5 gpm. Regulating rod position, 6.45 in.
14	0139	Fuel Flow rate, 37.5 gpm. Regulating rod position, 8.0 in. Stopped sodium flow.
15	0141	Fuel Flow rate, 37.5 gpm. Regulating rod position, 7.9 in.
	0142	End of experiment.

EXPERIMENT L-8

Objective: Measure Reactor Temperature Coefficient

1	0142	Reactor already up to 1 w.
	0157	Took data.
2	0214	Start prime mover.
	0215	Started raising barrier doors.
	0218	Helium blower, 255 rpm.
	0221	Readjust shims to put regulating rod to top of scale.
	0222	Heat exchanger water flow, 195 gpm. Temperature rise, 62 to 76°F. Steady state.
	0230	Low heat exchanger reverse. Prime mover off.
	0231	Barrier doors down.
3	0233	Took data.

EXPERIMENT L-8 (continued)

November 8, 1954

Run	Time	
(3)	0242	Readjusted shims. Regulating rod position, 3.15 in. Reactor mean, 1257°F.
	0700	Regulating rod position now 9.55 in., moved 6.40 in. since 0242 when final rod adjustment was made. Reactor mean temperature, 1286°F; 29°F rise since 0242.
	0950	End of experiment.

EXPERIMENT L-9

Objective: Set Reactor at 1 kw and Adjust Chambers

1	0950	Reactor already at 1 w.
	0954	Took data.
	1004	Pulled safety chamber 1.
	1010	Raised power to ~20 w.
	1018	Raised power to ~40 w.
2	1028	Started pulling log N chamber.
	1033	Reactor scrammed.
	1101	40-w nominal power.
3	1106	Pulled log N chamber all the way within shield.
4	1113	Pulled log N out of shield about 20 in.
5	1116	Data recorded.
	1128	Raised power to ~400 w.
6	1132	On manual. Pulling micromicroammeter chamber.
7	1150	Set micromicroammeter to exactly 500 w.
8	1155	Micromicroammeter 50 on 1×10^{-8} ; corresponds to 500 w.
	1159	Put reactor on 30-sec period and let safety chambers scram reactor.

EXPERIMENT H-1

Objective: Approach to Power (10-kw run)

	1445	Instruments on scale
	1448	Reactor up to 10 kw.
1	1452	Took data.
	1505	Pulled safety chambers.
2	1525	Took data.
3	1611	Took data.
	1619	Scrammed. Fission gases in basement.

EXPERIMENT H-2

November 9, 1954

Objective: 10-kw Run to Monitor Gas Activity

	1125	Instruments on scale.
	1127	Up to 10 kw.
1	1138	Data taken.
2	1208	Data taken.
	1224	Decreased power to 5 kw.

EXPERIMENT H-2 (continued)

November 9, 1954

Run	Time	
3	1227	Data taken.
4	1245	Data taken.
	1246	Reactor scrammed. During run, the estimated pit activity from RIA-4 was $0.032 \mu\text{c}/\text{cm}^3$.

EXPERIMENT H-3**Objective:** 100-kw Run

1	1520	Instruments on scale. Period, ~ 17 sec.
	1523	Reactor at ~ 100 kw.
	1526	Fuel and sodium system barrier doors raised. Fuel system prime mover started.
	1529	Blower at ~ 300 rpm.
	1530	Safety chambers scrammed reactor at ~ 130 kw.
	1551	Instruments on scale. Period, ~ 30 sec.
	1600	Reactor scrammed by safety level (set too low).
	1621	Instruments on scale. Period, ~ 27 sec.
	1625	Reactor on servo at 50 kw. Safety chambers reset.
	1626	Reactor off servo. Power raised.
	1643	Power leveled out at ~ 250 kw. Data taken.
2	1656	Elevated mean temperature (withdrew shim rods). Changed scales on reactor ΔT .
	1704	Data taken.
3	1715	Power raised to ~ 500 kw.
	1727	Data taken.
4	1740	Front sodium system blower brought to ~ 500 rpm.
	1749	Back sodium system blower brought to ~ 500 rpm.
	1801	Data taken.
5	1810	Increased power.
	1820	1-Mw nominal power.
	1825	Data taken.
6	1845	Data taken.
7	1854	Reduced power.
	1900	Fuel system blower off.
	1907	Data taken, ~ 115 kw.
	1915	Rods going in.
	1919	Sodium system blowers off.
	1938	Started increasing power.
	1945	Reactor power, 50 kw.
	2027	Reactor power, ~ 100 kw.

EXPERIMENT H-4**Objective:** Fuel and Reactor Temperature Coefficient Determinations

1	2045	Reactor power level at about 100 kw.
	2100	Turned on fuel system helium blower, 350 rpm.
	2102	Readjusted shims.
	2103	Blower off.

EXPERIMENT H-4

November 9, 1954

Run	Time	
2	2121	Fuel system blower on, 340 rpm.
	2124	Readjusted shim.
	2126:30	Prime mover off. Servo off.
	2129	End of run.
	2156	Reactor at 10 kw.

EXPERIMENT H-5

Objective: Overall Reactor Temperature Coefficient Determination

Reactor at 100 kw on flux servo. Allowed to heat up from 1260 to 1313°F.

1	2225	Data taken.
2	2243	Data taken.
3	2300	Data taken.

EXPERIMENT H-6

Objective: Startup on Temperature Coefficient

1	2307	Increased power.
	2315	Power, ~1.3 Mw (fuel system blower speed at maximum).
	2327	Took data.
	2339	Reduced power to ~200 kw. Pressure shell temperature getting high.
	2348	Inserted shims to drop reactor mean temperature.
	2353	Ran blower up from 0 to 1700 rpm (maximum speed).
	2400	Mark charts.
	2405	Ran regulating rod in from 7 in.; then pulled out all the way.

November 10, 1954

2	0016	Reduced fuel system helium blower speed to zero.
	0019	Inserted regulating rod from 14 to 2 in. Reactor subcritical.
	0026	Ran fuel system helium blower speed from 0 to 1700 rpm.
	0028	Low heat exchanger temperature reverse.
	0033	Stopped fuel system helium blower.
	0037	Inserted shim rods and reduced power. Stopped sodium system helium blowers.
	0106	Reactor left at 10 to 100 kw to maintain temperature on fuel lines.
	0115	Reactor scrammed due to calibration of fuel flowmeter.
	0137	Reactor power at ~100 kw.
	0204	Reactor mean temperature at ~1300°F; power at ~75 kw and falling slowly due to heating of fuel. 5.25 in. of regulating rod movement \equiv ~30°F temperature rise $\equiv 5.5 \times 10^{-5} (\Delta k/k)/^{\circ}\text{F}$.

PRACTICE OPERATION

Objective: To Familiarize Crews with Reactor Operation

0503	Reactor power, ~250 kw.
0538	Reactor power, ~500 kw.
0545	Stopped fuel and sodium system blowers. Power leveled at ~50 kw.
0548	All blowers back on at about 500 rpm.

PRACTICE OPERATION (continued)

November 10, 1954

Run	Time	
(2)	0552	Reactor power, ~750 kw.
	0554	All blowers off.
	0600	Blowers on. Power, ~750 kw.
	0602	Blowers off.
	0615	Reactor power, ~500 w.
	0625	Reactor power, ~100 kw.
	0630	Reactor power, ~50 kw.
	0844	Reactor power, ~50 kw. Took data.
	0852	Started fuel system blower prime mover.
	0855	Started fuel system blower.
	0858	Leveled off power at ~200 kw.
	0905	K. Z. Morgan reports short-lived air activity in crane bay.
	0909	Blower off. Prime mover off. End of experiment. Reactor leveled out at ~50 kw.

EXPERIMENT H-7

Objective: Sodium Temperature Coefficient Determination

0914	Ran sodium system helium blowers from 0 to ~2000 rpm.
0917	Stopped sodium system blowers. Peak power, ~150 kw.
0924	Leveled out. Charts pulled. Sodium temperature coefficient is negative.

EXPERIMENT H-8

Objective: Measure Effect of a Dollar of Reactivity

1	1040	Reactor power, ~50 kw. Started sodium system blowers.
	1045	Reactor power, ~1 Mw.
	1057	Took data.
2	1110	Pulled regulating rod one dollar in 0.61 min.
	1114	Inserted regulating rod one dollar. Charts pulled.
	1128	Scrammed while pulling charts.
	1150	Reactor power, ~150 kw.
	1200	Reactor power, ~1 Mw.
	1206	Sodium system blowers up to 1000 rpm each.
	1229	Reduced blower speed to zero.
	1241	Reactor power, ~100 kw.

PRACTICE OPERATION (continued)

1300	Blowers started. Blowers at 500 rpm.
1305	Reactor power, ~500 kw. Extracted power, ~570 kw.
1310	Blowers to 1000 rpm.
1313	Reactor power, ~900 kw.
1315	Regulating rod withdrawn 2 in. Extracted power, 920 kw (fuel) + 96 kw (sodium) = 1.016 Mw.

EXPERIMENT H-9

November 10, 1954

Objective: Overall Reactor Temperature Coefficient Determination

Run	Time	
(2)	1400	Reactor power, 300 kw. Fuel mean temperature raised to 1350°F.
	1422	Reactor on servo at 36 kw. Front sodium system blower on, 600 rpm. Reactor cooling.
	1452	Regulating rod reached lower limit.
	1458	Reactor at 100 kw on servo.
	1505	Going up to 1 Mw.
	1515	Mean temperature was raised to 1350°F; now lowered to 1325°F to avoid hot places on lines.
	1523	Mean temperature lowered to 1315°F at which point low heat exchanger temperature interlock reversed helium blowers.

EXPERIMENT H-10

Objective: Moderator Temperature Coefficient Determination

1	1550	Lowered reactor to ~400 kw.
	1600	Fuel temperature, 1317°F; regulating rod position, 7.2 in.; reactor outlet sodium temperature, 1280°F; reactor power, 500 kw.
	1605	Front sodium system blower, 870 rpm. Back sodium system blower, 1260 rpm.
	1606	Reduced back sodium system blower speed to 870 rpm. Regulating rod position, 7.5 in.; fuel temperature, 1317°F; sodium temperature, 1280°F.
	1611	Temperatures same as at 1606. Regulating rod position, 8.3 in.
	1613	Front sodium system blower speed reduced to 670 rpm; back sodium system blower speed to 850 rpm. Regulating rod position, 8.7 in.; fuel temperature, 1319°F; sodium temperature, 1278°F.
	1625	Front blower at 650 rpm; back blower at 640 rpm. Regulating rod position, 7.6 in.; sodium temperature, 1278°F.
	1630	Reactor power at 1 Mw for demonstration to Air Force personnel.
2	1735	Regulating rod position, 8.0 in.; reactor mean temperature 1313°F; front blower at 960 rpm; back blower at 1050 rpm; sodium inlet temperature, 1265°F (thermocouple 3-CR-1) sodium outlet temperature, 1282°F (thermocouple 3-CR-5).
	1737:30	Front blower at 1180 rpm.
	1745	Reactor mean temperature, 1314°F; regulating rod position, 8.0 in. Front blower at 1160 rpm; back blower at 1050 rpm. Sodium inlet temperature, 1255°F; sodium outlet temperature, 1280°F.
	1747	Back blower at 1280 rpm.
	1752	Reactor mean temperature, 1313°F. Regulating rod position, 7.6 in. Front blower at 1170 rpm; back blower at 1260 rpm. Sodium inlet temperature, 1248°F; sodium outlet temperature, 1278°F.
	1755	Front blower raised to 1350 rpm.
	1802	Regulating rod position, 6.6 in. Reactor mean temperature, 1308°F. Front blower at 1340 rpm; back blower at 1250 rpm. Sodium inlet temperature, 1238°F; sodium outlet temperature, 1272°F.
	1805	Front blower raised to 1490 rpm.
	1808	Regulating rod withdrawn 1.3 in. to regain 5°F lost in reactor mean temperature. Rod position = 7.3.

EXPERIMENT H-10 (continued)

November 10, 1954

Run	Time	
(2)	1812	Regulating rod position, 8.4 in. Reactor mean temperature, 1311°F. Front blower at 1480 rpm; back blower at 1240 rpm. Sodium inlet temperature, 1230°F; sodium outlet temperature, 1268°F.
	1816	Back blower speed changed to 1500 rpm.
	1825	Regulating rod position, 8.9 in. Reactor mean temperature, 1313°F. Front blower at 1470 rpm; back sodium blower at 1480 rpm. Sodium inlet temperature, 1225°F; sodium outlet temperature, 1268°F.

EXPERIMENT H-11

Objectives: 25-Hour Run at Full Power to Observe Xenon Poisoning

- 1935 Since 1825, the reactor has been steady at 90% full power on servo; it is now off servo. The 25-hr xenon run is considered to have started at 1825.

November 11, 1954

0304	Cooling water flow to back sodium heat exchanger decreased. Sodium ΔT fell $\sim 3^{\circ}\text{F}$. No explanation as yet.
0400	Drop in sodium ΔT due to heaters for annulus helium being shut off.
0635	Withdrew regulating rod from 10.3 to 10.4 in. Reactor mean temperature dropped to 1309°F from an initial temperature of 1311°F.
0750	Regulating rod withdrawn from 10.4 to 10.5 in.
0825	Micromicroammeter took a small dip (53 to 52) for no apparent reason.
0915	Adding helium to sodium and fuel system ducts.
0925	Fuel flowmeter coils calibrate OK. There is a possibility of something binding in the Rotameter to give the erratic readings. Switched to operation on No. 3 coil.
1020	Regulating rod withdrawn ~ 0.05 in. Indicator now reading 9.25 in.
1100	Pile period shows unexplained excursion to 400 sec.
1130	Noticed fluctuations in the fuel pump ammeter recorder corresponding to fluctuations in the Rotameter chart. These fluctuations appear to be between 9.0 and $9\frac{3}{4}$ amp.
1145	Noticed same pump current and flow level fluctuations as at 1130.
1206	Switched back to No. 5 coil on fuel flow Rotameter.
1435	Regulating rod withdrawn 0.1 in.
1445	For the past $\frac{3}{4}$ hr have noticed corresponding fluctuations in the following instruments: fuel flow Rotameter, fuel motor current recorder, period meter, log N recorder, safety levels 1 and 2, reactor ΔT , the six individual tube ΔT 's, and the micromicroammeter. All these fluctuations at present are small, especially on the micro-microammeter. The largest fluctuations appear to be on the pump motor current, between 9 and 10 amp; the pile period meter, ∞ to ± 400 sec; and the six ΔT recorders, ± 2 to 3°F . No extraneous audio noise has been detected. Noticed increase in fuel pump pressure since 0800 of 0.2 psi. At 0800 pressure was 0.2 psi, at present it is 0.4 psi.

EXPERIMENT H-11 (continued)

November 11, 1954

Run	Time	
(2)	1935	End of xenon run. Regulating rod has been withdrawn ~0.3 in., which corresponds to 0.01% $\Delta k/k$ as compared to ~0.30% $\Delta k/k$ if all xenon had stayed in system. Had demonstration for Air Force personnel, mostly 1-Mw nominal power.
	2032	Set reactor back to original condition left at 1935.

EXPERIMENT H-12

Objective: Stop Sodium System Blower and Observe Effect on Power

1	2105	Took data.
2	2113	Sodium system blower motors off.
	2119	Took data. Blowers back on. Maximum deviation of micromicroammeter was from 53 to 45, 15%.
	2150	Reduced power by cutting off fuel system blower.
	2155	Reduced speed on sodium system blower.
	2158	Regulating rod inserted; reactor power, ~10 kw.
	2200	Started fuel system blower motor.
	2201	Started fuel system helium blower.
	2204	Approached low heat exchanger temperature reverse (1150°F) which shut off fuel system blower motor. Withdrew regulating rod.
	2210	Reactor power back up to 1 Mw.
	2230	Cut off fuel system blower. Cooling reactor with sodium system blowers only.
	2237	Reactor power, ~100 kw.

EXPERIMENT H-13

Objective: Measure Xenon Buildup at $\frac{1}{10}$ Full Power

2237 Consider experiment to have started at 2237 at $\frac{1}{10}$ full power, i.e., ~100 kw.

November 12, 1954

0605	Regulating rod withdrawn from 5.05 to 5.15 in. Reactor mean temperature dropped from 1304 to ~1303°F.
0735	Sodium ΔT up due to addition of helium in rod cooling system. Reactor mean temperature down to 1302°F.
0835	No appreciable xenon buildup. End of experiment.

EXPERIMENT H-14

Objective: Determine Maximum Reactor Power and Characteristics of Power Operation

0837	Demonstration of reactor operation.
0855	Reactor power up to 1 Mw. Maximum fuel system helium flow. Reactor mean temperature, ~1340°F.
0907	No. 2 rod cooling helium blower on slow speed. Helium pressure, 25 in. H_2O .
0910	No. 2 rod cooling blower off. Helium pressure, 9 in. H_2O .
0917	No. 2 rod cooling blower on.

EXPERIMENT H-14 (continued)

November 12, 1954

Run	Time	
(2)	0919	No. 2 rod cooling blower off. Small wobble in ΔT probably due to helium blowing on thermocouple. No systematic effect on microammeter can be observed.
	0922	Started demonstration. Average reactor power, ~ 1 Mw.
	0935	Demonstration ended. Reactor power back to 1 Mw.
1	1015	Reactor mean temperature raised to 1350°F.
	1055	Fuel system blower off.
	1102	Power leveled off at ~ 350 kw. Sodium system blowers off.
	1109	Power leveled off at ~ 210 kw. Rod cooling blowers off.
	1110	Power leveled off at 200 kw.
	1111:30	Started bringing reactor up to full power.
	1112	14-sec period observed.
	1113	Heat exchanger outlet temperature reduced from 1380 to 1175°F. Log N from 4 to 30.
	1115	Back to power of >1 Mw.
	1117	Moved shim and regulating rods to obtain new heat balance.
2	1125	Sodium system blower speed up to 2000 rpm. Extracted power: from fuel, 1920 kw; from rod cooling, 20 kw; from sodium, 653 kw; total, 2.6 Mw.
	1140	No. 2 rod cooling blower started.
	1150	Front sodium system blower off; reactor power reduced to ~ 100 kw.
	1230	Reactor mean temperature and power leveled off; power, ~ 1.5 Mw.
	1244	Reduced fuel system helium blower speed to minimum.
	1306	Fuel ΔT nearly constant.
	1306	Raised fuel system helium blower speed to maximum.
	1308	Fuel ΔT essentially restored.
	1325	Fuel system blower turned on; speed reached 1500 rpm.
	1326	Blower speed reduced to 1000 rpm.
	1330	Reactor ΔT about 200°F.
	1331	Regulating rod withdrawn to raise mean temperature from 1320 to 1325°F.
	1334	Regulating rod inserted to lower mean temperature from 1325 to 1320°F.
	1336	Regulating rod withdrawn to raise mean temperature.
	1350	After demonstration, power leveled off to 1.5 Mw.
	1400	Demonstration of reactor operation.
	1615	End of demonstration of reactor operation. Reactor run more or less steadily at 2 Mw until time for scram.
3	1930	Reactor power up to ~ 2.5 Mw.
	2004	Reactor scammed.

Appendix U

THE ARE BUILDING

The ARE building, shown in Fig. U.1, is a mill type of structure that was designed to house the ARE and the necessary facilities for its operation. The building has a full basement 80 by 105 ft, a crane bay 42 by 105 ft, and a one-story service wing 38 by 105 ft. The reactor and the necessary heat disposal systems were located in shielded pits in the part of the basement serviced by the crane. One half the main floor area was open to the reactor and heat exchanger pits in the basement below; the other one half housed the control room, office space, shops, and change rooms.

In one half the basement were the shielded reactor and heat exchanger pits; the other one half of the basement was service area and miscellaneous heater and control panels. The control room, office space, and some shops were located

on the first floor over the service area. The first floor does not extend over the one half of the basement that contains the pits. The crane is a floor-operated, 10-ton, bridge crane having a maximum lift of 25 ft above the main floor level. Plan and elevation drawings of the building are shown in Figs. U.2 and U.3.

The entire reactor system was contained in three interconnected pits: one for the reactor, another for the heat exchangers and pumps, and a third for the fuel dump tanks. These pits, which were sealed at the top by shielding blocks, were located in the large crane bay of the building. The crane bay was separated from the control room and offices, and the heating and air conditioning systems maintained the control room at a slightly higher pressure than that of the crane bay.

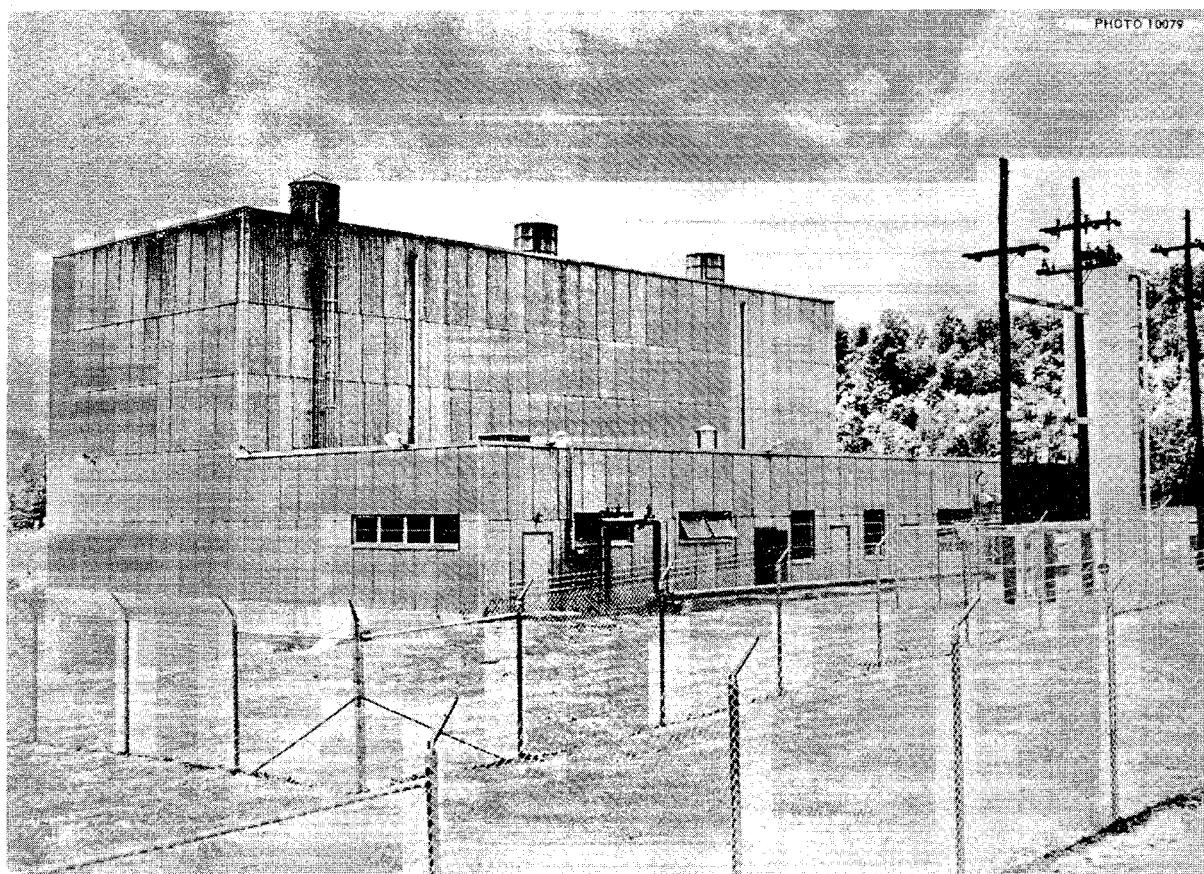


Fig. U.1. The ARE Building.

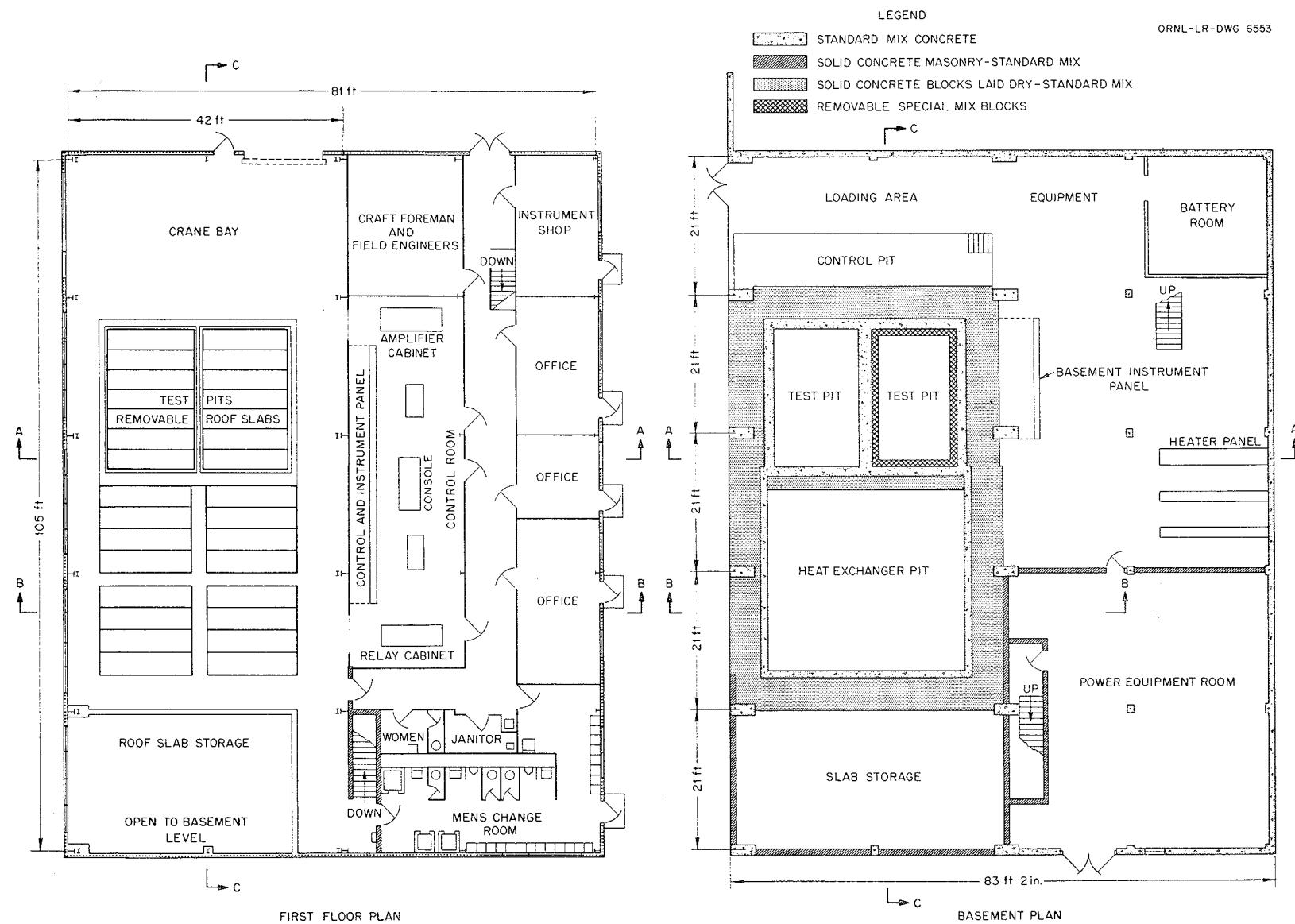
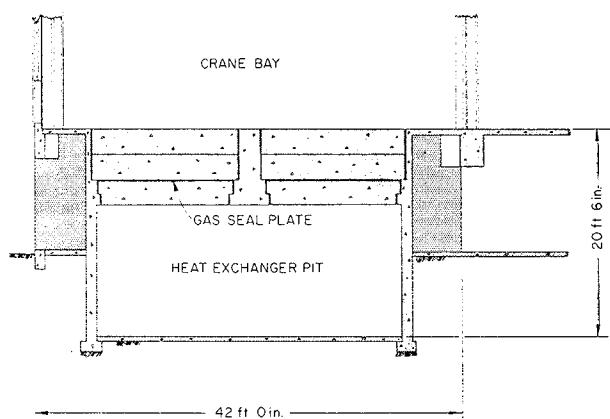
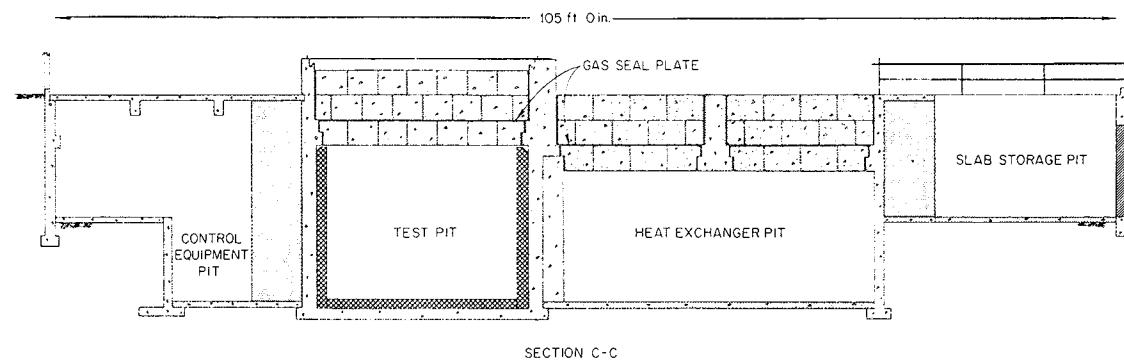
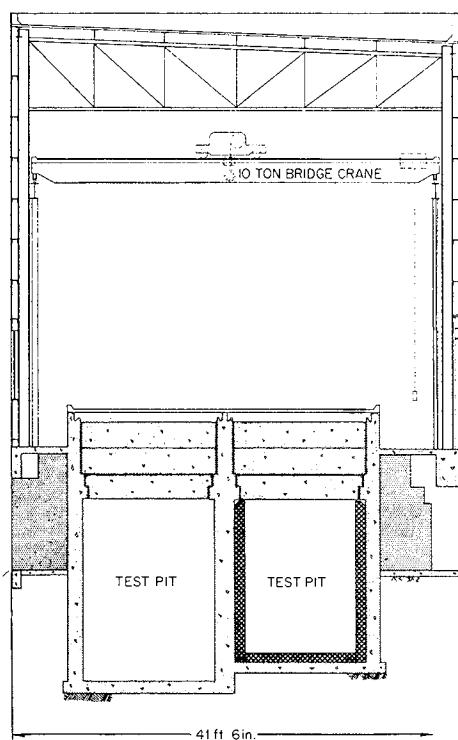


Fig. U.2. Plan of the ARE Building.

LEGEND

- STANDARD MIX CONCRETE
- SOLID CONCRETE MASONRY - STANDARD MIX
- SOLID CONCRETE BLOCKS LAID DRY - STANDARD MIX
- REMOVABLE SPECIAL MIX BLOCKS

ORNL-LR-DWG 6554



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