

# Nonstationary Flood Frequency Analysis: A Mixed and Pooled Approach

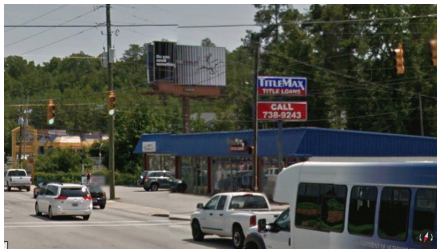
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# Columbia, SC: October 2015



Garners Ferry Road in Columbia, SC before and during the October 2015 flood.

Economists estimated the floods caused about \$12 billion damage on the state of South Carolina

Source: Sean Rayford/Getty Images

# River Gage



Gage #12041200: Hoh River at U.S. Highway 101 near Forks, WA

# Congaree River: Columbia, SC



Gervais Street Bridge, Columbia, SC

First version: 1827 to 1865

Second version: 1870 to 1928

Third version: 1928 to current

Flood gage about 0.2 miles south of current Gervais Street Bridge

# 1865: Columbia, SC



- Ruins, as seen from the State House, 1865.
- General Sherman's Union troops were slowed entering Columbia by a major flood on the Congaree River.

## Annual Peak Flows

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- Peak flows are measured in cubic feet per second (cfs)

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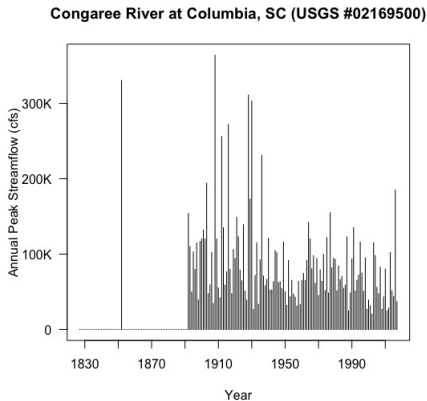
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## Historical Flood Data

Any observation of flood stage or conditions made before actual flood data were collected systematically

- Data collected from old newspapers, diaries, museums, libraries, etc.

# Congaree River: Columbia, SC (USGS #02169500)



Historic Floods: 1852, Possible historic floods: 1886, 1888

Flood Record: 1892 to 2017



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  - 1% chance flood is the 99th percentile of the fitted finite mixture model

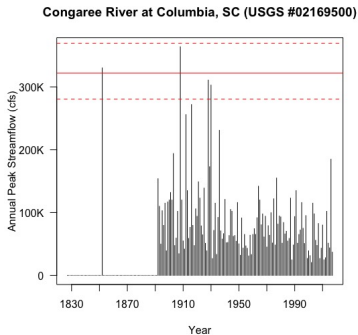


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  - assume that the 1853 to 1891 floods are all smaller than the 1852 flood
  - 1% chance flood is the 99th percentile of the fitted finite mixture model
  - Due to the complexity of the likelihood function, the standard error of the estimate of the 1% chance flood is produced solely from score functions (first partial derivatives)

# Initial Results: 1827 to 2017



## Parameter Estimates:

$$\hat{\mu}^T = (4.854, 5.480), \hat{\sigma}^T = (0.228, 0.0498), \hat{\tau} = 0.0278$$

**Point Estimate for 1% Chance Flood:** 321,972 cfs

**95% CI for 1% Chance Flood:** 280,568 cfs to 369,486 cfs

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Source: *Science*, Vol. 319, pp. 573-574, 1 February 2008, doi: 10.1126/science.1151915

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- Pool the results together.

This is the mixed and pooled approach:

- **Pooled:** Annual peak streamflows are identified to belong to a specific component (i.e., before a dam was built vs. after a dam was built) beforehand



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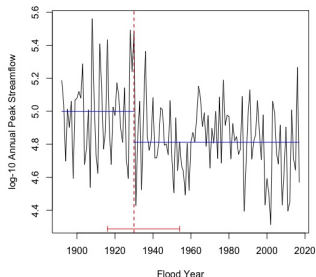
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- **Mixed:** Within each stationary series, it is not known ahead a time if the annual peak streamflow is from a specific component (i.e., was it due to tropical storms? Snow melt?)
  - This is estimated by the finite mixture models.

# Congaree River: 1892 to 2017



Results from strucchange package in R: two pooled components

- estimated change point is 1930 (95% CI: 1916 to 1954)
- 1930 – Dreher Shoals Dam completed about 10 miles west of flood gage/Columbia, SC
- 1892 to 1930 – pre-dam annual peak streamflows
  - The annual peak streamflow of the 1930 flood year occurred on October 3, 1929.
- 1931 to 2017 – post-dam annual peak streamflows

# Proposed Model

Assume that there are  $K - 1$  change points in the flood series. The pdf of the annual peak streamflows can be written as a linear combination of  $K$  finite mixture models.

$$p(y) = \sum_{k=1}^K \pi_k \left[ \sum_{j=1}^{J_k} \tau_{jk} f(y|\theta_{jk}) \right],$$

where

$$\sum_{k=1}^K \pi_k = 1, \sum_{j=1}^{J_k} \tau_{jk} = 1, \text{ and } \int_{\mathcal{Y}} f(y|\theta_{jk}) dy = 1$$

The likelihood function is

$$L(\eta) = \prod_{i=1}^n p(y_i) = \prod_{i=1}^n \left\{ \sum_{k=1}^K \pi_k \left[ \sum_{j=1}^{J_k} \tau_{jk} f(y_i|\theta_{jk}) \right] \right\},$$

where

$$\eta = (\theta_j, \tau_j), j = 1, \dots, J_k, k = 1, \dots, K$$

# Complete Data Likelihood & Log-Likelihood

The complete data,  $x_i, i = 1, \dots, n$ , are observed indirectly via:

$$x_i = (y_i, \mathbf{z}_i, \boldsymbol{\zeta}_i), i = 1, \dots, n$$

where each  $\mathbf{z}_i = (z_{i11}, \dots, z_{ijk})^T$  is an indicator vector of length  $jk$  with 1 in the position corresponding to the appropriate **mixing** component and zeroes elsewhere and  $\boldsymbol{\zeta}_i = (\zeta_{i1}, \dots, \zeta_{ik})^T$  is an indicator vector of length  $k$  with 1 in the position corresponding to the appropriate **pooling** component and zeroes elsewhere.

## Complete Data Likelihood:

$$g(\mathbf{x}|\boldsymbol{\eta}) = \prod_{i=1}^n \prod_{k=1}^K \prod_{j=1}^{J_k} \pi_k^{\zeta_{ik}} \tau_{jk}^{z_{ijk}\zeta_{ik}} f(y_i|\boldsymbol{\theta}_{jk})^{z_{ijk}\zeta_{ik}}$$

## Complete Data Log-Likelihood:

$$\log g(\mathbf{x}|\boldsymbol{\eta}) = \sum_{i=1}^n \sum_{k=1}^K \zeta_{ik} \log \pi_k + \sum_{i=1}^n \sum_{k=1}^K \sum_{j=1}^{J_k} [z_{ijk}\zeta_{ik} \log \tau_{jk} + z_{ijk}\zeta_{ik} \log f(y_i|\boldsymbol{\theta}_{jk})]$$

# A Simple Scenario...

The complete data log-likelihood can be “simplified” when  $K = 2$  and  $J_1 = J_2 = 2$ :

$$\begin{aligned}\log g(\mathbf{x}|\boldsymbol{\eta}) &= \sum_{i=1}^n [\zeta_i \log \pi + (1 - \zeta_i) \log (1 - \pi)] \\ &+ \sum_{i=1}^n [z_{i1} \zeta_i \log \tau_1 + (1 - z_{i1}) \zeta_i \log (1 - \tau_1) + z_{i0} (1 - \zeta_i) \log \tau_0 + (1 - z_{i0}) (1 - \zeta_i) \log (1 - \tau_0) \\ &+ z_{i1} \zeta_i \log f(y_i|\boldsymbol{\theta}_{11}) + (1 - z_{i1}) \zeta_i \log f(y_i|\boldsymbol{\theta}_{01}) + z_{i0} (1 - \zeta_i) \log f(y_i|\boldsymbol{\theta}_{10}) \\ &+ (1 - z_{i0}) (1 - \zeta_i) \log f(y_i|\boldsymbol{\theta}_{00})]\end{aligned}$$

The parameters,  $\boldsymbol{\eta} = (\tau_1, \tau_0, \boldsymbol{\theta}_{11}, \boldsymbol{\theta}_{10}, \boldsymbol{\theta}_{01}, \boldsymbol{\theta}_{00})$ , can be estimated using an ECM algorithm.

In fact, a separate ECM algorithm can be performed on each known pooling component of finite mixture models!

# Pooling of Finite Mixture Models: Congaree River Example

Analysis based on:

- observed annual peak flows: 1892 to 2017
- historic period: 1827 to 1891
- observed historic flood: 1852
- two known pooled components: 1827 to 1930, 1931 to 2017

**Pooling Weights (based off of 1892 to 2017 flood years):**

$$\pi^T = \left( \frac{39}{126} = 0.310, \frac{87}{126} = 0.690 \right)$$

**Parameter Estimates (first pooling component):**

$$\hat{\mu}^T = (4.945, 5.476), \hat{\sigma}^T = (0.222, 0.0440), \hat{\tau} = 0.0804$$

**Parameter Estimates (second pooling component):**

$$\hat{\mu}^T = (4.803, 4.970), \hat{\sigma}^T = (0.217, 0.00554), \hat{\tau} = 0.0595$$

**Point Estimate for 1% Chance Flood:** 314,424 cfs

**95% CI for 1% Chance Flood:** 279,633 cfs to 353,543 cfs