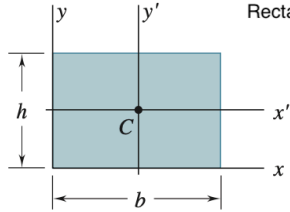
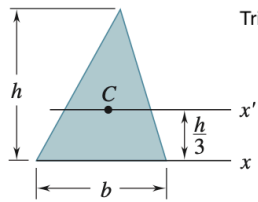
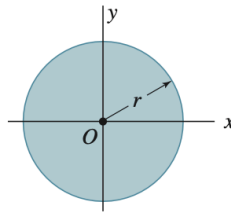
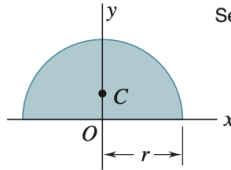
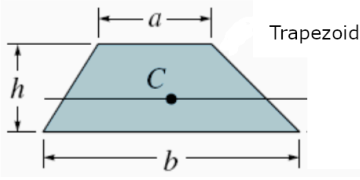
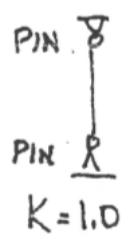


CE 112 Exams Forumula Sheet

Axial Load		Stress in Pressure Vessel	
Max In-Plane Shear Stress	$\sigma_n = \frac{P}{A}$	Cylinder	$\sigma_1 = \frac{Pr}{t}$
Displacement			$\sigma_2 = \frac{Pr}{2t}$
$\sigma = E\epsilon$	$\delta = \int_0^L \frac{P(x)}{A(x)E}dx$	Sphere	$\sigma_1 = \sigma_2 = \frac{Pr}{2t}$
$\delta_{th} = \alpha \Delta TL$	$\delta = \frac{PL}{AE}$	Stress Transformation	
Torsion	$\tau = G\gamma$	$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2}cos2\theta + \tau_{xy}sin2\theta$	
Shear Stress in a circular shaft	$\tau = \frac{Tp}{J}$	$\tau_{x'y'} = -\left(\frac{\sigma_x + \sigma_y}{2}\right)sin2\theta + \tau_{xy}cos2\theta$	
J for solid circle	$J = \frac{\pi}{2}C^4$		
J for hollow circle	$J = \frac{\pi}{2}(C_o^4 - C_i^4)$	Principal Stress	
Angle of Twist	$\phi = \int_0^L \frac{T(x)}{J(x)G}dx$	$tan2\theta_p = \frac{\tau_{xy}}{\frac{1}{2}(\sigma_x - \sigma_y)}$	
	$\phi = \frac{TL}{JG}$	$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$	
		Max In-Plane Shear Stress	
		$tan2\theta_s = -\frac{\frac{1}{2}(\sigma_x - \sigma_y)}{\tau_{xy}}$	
Bending			
Normal Stress	$\sigma = -\frac{My}{I}$	$\tau_{max} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$	
Shear		Absolute Maximum Shear Stress	
Average Shear Stress	$\tau_{avg} = \frac{V}{A}$	$\tau_{ max } = \frac{\sigma_x + \sigma_y}{2}$	
Transverse (Bending) Shear Stress	$\tau = \frac{VQ}{It}$	$\sigma_{avg} = \frac{\sigma_{max} + \sigma_{min}}{2}$	

Shear Flow	$q = \frac{VQ}{I}$	Geometric Properties of Shapes	
Material Properties			$\bar{I}_{x'} = \frac{1}{12}bh^3$ $\bar{I}_{y'} = \frac{1}{12}b^3h$ $A = bh$
Poisson's Ratio	$\nu = -\frac{\epsilon_{tran}}{\epsilon_{long}}$		$\bar{I}_{x'} = \frac{1}{36}bh^3$ $A = \frac{1}{2}bh$
Relations between w, V, M			$\bar{I}_x = \bar{I}_y = \frac{1}{4}\pi r^4$ $J_O = \frac{1}{2}\pi r^4$ $A = \pi r^2$
Elastic Curve	$\frac{dV}{dx} = -w(x)$ $\frac{dM}{dx} = V$ $\frac{l}{\rho} = \frac{M}{EI}$ $EI \frac{d^4v}{dx^4} = -\omega(x)$ $EI \frac{d^3v}{dx^3} = V(x)$ $EI \frac{d^2v}{dx^2} = M(x)$		$I_x = I_y = \frac{1}{8}\pi r^4$ $J_O = \frac{1}{4}\pi r^4$ $A = \frac{\pi r^2}{2}$
Buckling			$C_x = \frac{h}{2}$ $C_y = \frac{1}{3} \left(\frac{2a+b}{a+b} \right) h$ $A = \frac{1}{2}h(a+b)$
Effective Length Factor, K		Parallel Axis Theorem	
		$I_{x'} = I_x + Ad^2$	