

Popular Electronics

WORLD'S LARGEST-SELLING ELECTRONICS MAGAZINE

APRIL 1980/95¢

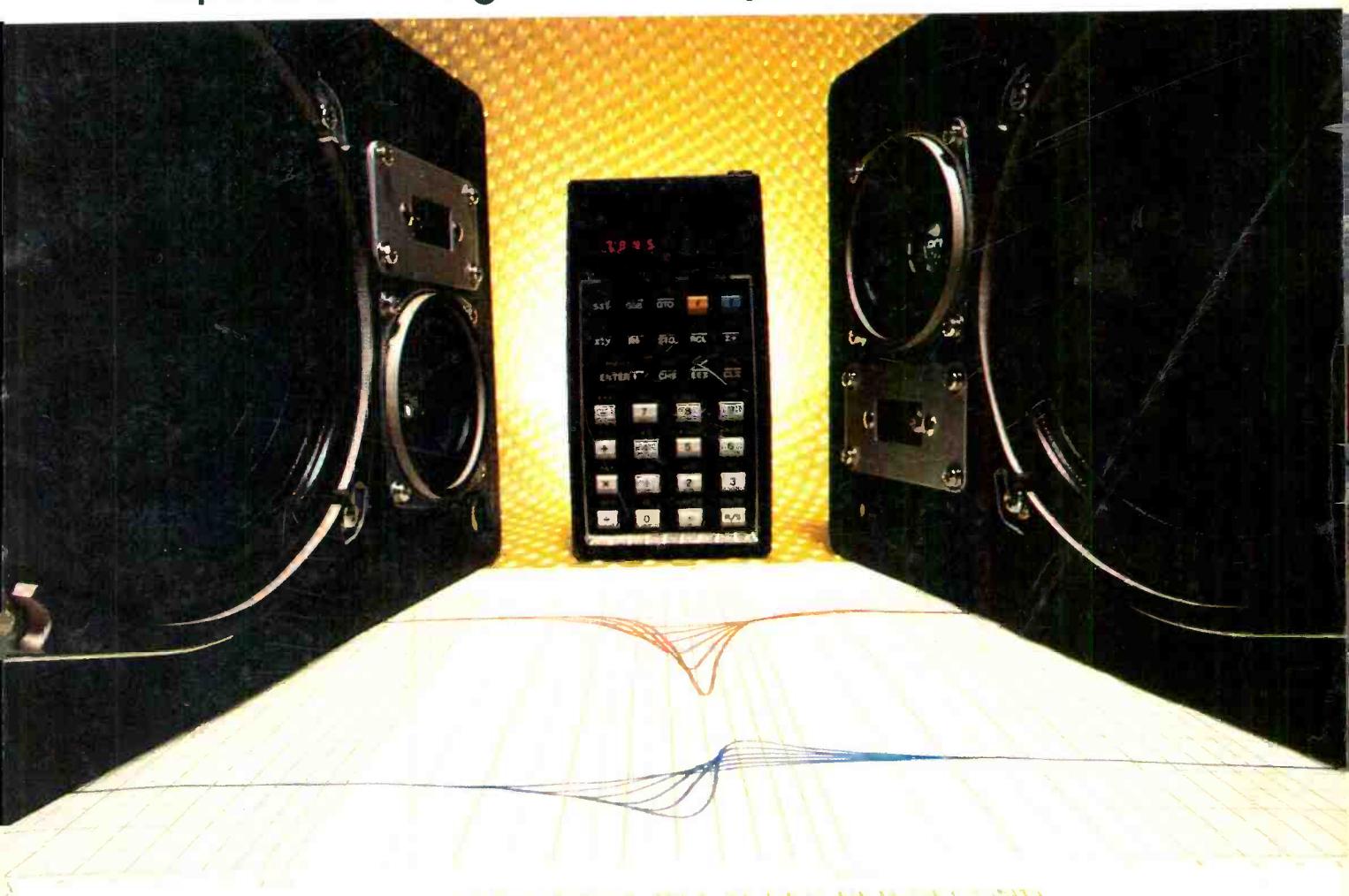
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Popular Electronics



What kind of man owns his own computer?

Rather revolutionary, the whole idea of owning your own computer? Not if you're a diplomat, printer, scientist, inventor... or a kite designer, too. Today there's Apple Computer. It's designed to be a *personal* computer. To uncomplicate your life. And make you more effective.

It's a wise man who owns an Apple.

If your time means money, Apple can help you make more of it. In an age of specialists, the most successful specialists stay away from uncreative drudgery. That's where Apple comes in.

Apple is a real computer, right to the core. So just like big computers, it manages data, crunches numbers, keeps records, processes your information and prints reports. You concentrate on what you do best. And let Apple do the rest. Apple makes that easy with three programming languages—including Pascal—that let you be your own software expert.

Apple, the computer worth not waiting for.

Time waiting for access to your company's big mainframe is time wasted. What you need in your department—



on your desk—is a computer that answers only to you... Apple Computer. It's less expensive than timesharing. More dependable than distributed processing.

Far more flexible than centralized EDP. And, at less than \$2500 (as shown), downright affordable.

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Friendly Comparison

Can JS&A offer a better telephone answering unit than the first one we introduced? Here's the story of American competition at its finest.



We've seen them all. Every telephone answering unit has its advantages and disadvantages.

So when JS&A selected our first telephone answering unit three years ago and called it the best remote system available, it soon became one of the most popular units on the market. Since 1976, JS&A has sold thousands of them.

SERIOUS COMPETITION

But that was three years ago. It finally took an enterprising company called Olympia to develop and introduce what we would call the first serious competition to our first telephone answerer.

So JS&A had a dilemma. Here we were, with an excellent relationship with a major supplier, and yet our reputation demands that we offer our customers only the most advanced products. Do we continue to carry both units, or do we break off relations completely and introduce a competitive model? To make the decision more difficult, you first have to understand the new technology in the Olympia unit.

A FAIR COMPARISON

The Olympia Master Telephone Recorder is a microprocessor-based system with a few features that make it a more advanced unit than the industry leader.

But to provide a fair comparison, there are a few disadvantages with the Olympia. The Olympia does not have a call counter that tells you at a glance how many calls you've received. And its outgoing announcement is not recorded as fast as with our first unit. But there are so many other features and advanced technology that the Olympia deserves your consideration.

ERASE OR SAVE

Most remote units and the Olympia have remote pagers. When you want to retrieve your messages, simply hold the pager up to the telephone, press a button, and the telephone answering unit rewinds to the start of your first message and plays them back.

That's great. But there was a disadvantage to the others. After you listened to your messages, you could not rewind. If you wanted to rewind to the beginning of the tape, you had to call your unit a second time. That's only a slight problem if you're calling locally from a phone booth, but very costly when you're calling long distance. And if you don't call back right away and rewind, you have another problem. Later, you'll have to listen to all those messages you previously heard because the unit doesn't know where the old messages stop and the new ones start.

The new Olympia Master Recorder has solved that problem. You have a choice. You can either hang up after you've heard your

messages or you can rewind them to the beginning while you're on the phone.

NO MESSAGE/LAST MESSAGE

Let's say you call in and there are no messages for you. The Olympia has a special beep tone that tells you the moment you call in that there is no message. Or let's say there are three messages waiting for you. After the three messages are played back, another beep tone signals you that you've finished your last message. There is no provision like this on any of the popularly priced units.

YOUR OWN TAPE

The Olympia uses one commercially available cassette tape that will last a few years with normal use. Today's most popular unit uses a built-in tape that will last five years, and costs \$17 to replace. With the Olympia unit, you remove the old cassette and pop in the new one which shouldn't cost more than \$2.

TAPE SPEED

It costs time and money to listen to your old messages and to rewind. So the Olympia not only improved the concept by giving you a choice, they also improved the tape rewind speed. Now, when you retrieve your calls, your rewind time is faster than many other systems and as fast as the system we formerly sold.

Not only is the Olympia faster, but it measures only 2 1/4" x 6" x 10" and weighs only 36 ounces. You can place your phone on top of the unit or next to it without cluttering your desk.

We could probably present reasons why the Olympia Master Recorder will pay for itself with just the time you save retrieving messages—but there's more.

SINGLE SYSTEM

You record your outgoing announcement on one track of the cassette tape and you receive your incoming messages on the other side. This single cassette approach reduced the costs of the Olympia below those of the conventional recorders that required two separate record and playback systems. And like other units, when you play back your tape, you hear only your incoming messages—never the outgoing announcement.

To record an outgoing announcement, you simply press the record button and talk into a microphone supplied with the unit. The unit will record a 17 second outgoing announcement and a 30 second incoming message. Our previous unit records a 20 second outgoing announcement and a 30 second incoming message.

AND THEN THERE'S VALUE

Our previous unit sold for \$269.95. The Olympia sells for only \$169.95—a \$100 savings before you even start to use the system.

But don't take our word for it. Order an Olympia from us on our 30-day telephone answering test. Personally see how quickly you can retrieve or rewind your messages without having to call in twice. See how this compact unit fits on your desk. And above all, note the quality and workmanship of this fine piece of equipment.

Then after 30 days of messages, decide if you want to keep your unit. If not, no problem. Just return your unit for a prompt and courteous refund including your \$3.50 postage and handling.

If you decide to keep it, great. You'll own the most advanced unit of its kind. The Olympia Master Recorder is sold exclusively by JS&A. We're America's largest single source of space-age products, and we have sold more telephone answering units than many of our competitors combined. We know the market.

MULTI-NATIONAL CORPORATION

Olympia is a multi-national corporation with eight national factory service and service-by-mail facilities—further assurance that your modest investment is well protected.

To order your Olympia, send a check for **\$169.95** plus \$3.50 postage and handling made payable to JS&A Group, Inc. (Illinois residents add 5% sales tax.) Credit card buyers may call our toll-free number below. We'll send your unit complete with recording microphone, one cassette tape, remote pager, AC adapter, instructions, and a 90-day limited warranty—everything you'll need for your 30-day test.

When we realized that the Olympia was the unit we should market, we called our previous supplier and told them of our decision.

In today's changing times, technology does not stand still. Despite our excellent relationship with our previous supplier, we felt it our obligation to introduce today's most advanced products—even at the risk of losing a valuable supplier.

If you're considering a new telephone answering unit, we can't recommend a better system than the Olympia Master Recorder. Why not order one at no obligation today?

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The easiest, least expensive way to generate spectacular multi-color graphics, sharp two-color alphanumerics: Your computer, a color tv set and the Percom Electric Crayon™.

Add the Electric Crayon™ to your system and your keyboard becomes a palette, the tv screen your medium.

You dab and stroke using one-key commands to create dazzling full-color drawings, eye-catching charts and diagrams.

Or you run any of innumerable programs. Your own BASIC language programs that generate dynamic pyrotechnic images, laugh-provoking animations.

From a combined alphanumerics-semographics mode to a high resolution 256- by 192-element full graphics mode, the microprocessor-controlled Electric Crayon™ is capable of generating 10 distinctly different display modes.

Colors are brilliant and true, and up to eight are available depending on the mode.

As shipped, the Electric Crayon™ interfaces a TRS-80* computer. It may be easily

adapted for interfacing to any computer or to an ordinary parallel ASCII keyboard.

But that's not all

The Electric Crayon is not just a color graphics generator/controller.

It is also a complete self-contained control computer. With built-in provision for 1K-byte of on-board program RAM, an EPROM chip for extending EGOS™, its on-board ROM graphics OS, and a dual bidirectional eight-bit port — over and above the computer/keyboard port — for peripherals. The applications are endless.

Shipped with EGOS™, 1K-byte of display memory and a comprehensive user's manual that includes an assembly language listing of EGOS™ and listings of BASIC demo programs, the Electric Crayon™ costs only \$249.95.

Options include:

- LEVEL II BASIC color graphics programs on minidiskette: \$17.95.
- A 34-conductor ribbon cable to interconnect the Electric Crayon™ to a TRS-80*: \$24.95.
- RAM chips for adding refresh memory for higher density graphics modes: \$29.95 per K-byte.
- Electric Crayon™ Sketchpad, a sketching grid of proportioned picture elements (pixels) in a tv aspect ratio. For 128 x 192 or 256 x 192 graphics modes. 11-inch by 17-inch, 25-sheet pads: \$3.95 per pad.

SYSTEM REQUIREMENTS: the video circuitry of the Electric Crayon™ provides direct drive input to a video monitor or modified tv set. An internal up-modulator for rf antenna input may be constructed by adding inexpensive components to the existing video circuitry.

Prices and specifications subject to change without notice.

TM = trademark of Percom Data Company, Inc.

* = trademark of Tandy Radio Shack Corporation which has no relationship to Percom Data Company.

Get into computer color graphics the easy, low-cost way with a Percom Electric Crayon™. Available at Percom dealers nationwide. Call toll-free, **1-800-527-1592**, for the address of your nearest dealer, or to order direct if there is no Percom dealer in your area.

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(214) 272-3421

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About the cover:

This month's loudspeaker focus examines the problems of testing, specifying and evaluating loudspeakers.

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ZIFF-DAVIS PUBLISHING COMPANY
Editorial and Executive Offices
One Park Avenue, New York, New York 10016
212-725-3500
Joseph E. Mesics
Published (725-3568)
Richard F. Govatski
Advertising Manager (725-3939)
Bonnie B. Kaiser
Eastern Ad. Mgr., (725-3580)
Midwestern Office
Ted Welch
Suite 1400, 180 N. Michigan Ave.,
Chicago, IL 60601 (312-346-2600)
Western Office
3460 Wilshire Blvd., Los Angeles, CA 90054
213-387-2100
Western Representative: Norm Schindler
Jon Marshall
7050 Owensmouth Ave., #209
Canoga Park, CA 91303 (213-999-1414)
Japan: James Yagi, Oji Palace Aoyama,
6-25, Minami Aoyama, 6 Chome, Minato-Ku,
Tokyo, 407-1930/6821-582-2851
ZIFF-DAVIS PUBLISHING COMPANY
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Editorial

NEW ELECTRONIC PRODUCTS ON THE HORIZON

The Winter Consumer Electronics Show, where some 950 exhibitors displayed electronic products they hope dealers will buy for resale to you, is over. As far as the introduction of new products was concerned, the Show was unimpressive. Most of the models on display were carryovers from last year's line or warmed-over versions of same. Even the new products shown had a mix of new "for real" and prototype models.

A refreshingly healthy number of computers were on hand, though the only wholly new one was the first general showing of Hewlett-Packard's HP-85 typewriter-size unit (see "New Products" section). Commodore Business Machines demonstrated a few systems that were for show rather than for sale at this time. These included a 16-color video system and a "touch the CRT screen with a finger" input control. We also observed Personal Software's VisCalc™ software program in action, which is also available for use with an Apple II or II-plus computer. It's an impressive program that turns a personal computer into a highly efficient electronic worksheet that organizes and displays information on a screen for business and engineering applications.

Apple introduced "Apple Writer," a software package to convert the Apple II into a word processor (\$75), and "Graphics Tablet," an intelligent graphics input subsystem that's extremely powerful. APF added an expansion interface to its personal computer, while Ohio Scientific, Atari, and Compucolor boosted their software libraries.

Noncomputer microprocessor technology was evident in a number of products. For example, we observed that more voice synthesizing systems are being adopted for general consumer products. Sharp's prototype digital clock tells the time verbally, and a "talking" calculator verbally confirms each key operation; Windert's under-\$100 "Talking Watch" tells the time as well as voicing a brief message; Quasar's prototype microwave oven issued cooking times by "voice"; Texas Instruments added three Solid State Speech™ modules to its "Speak & Spell" learning aids and a new version of S&S is scheduled to be introduced that includes sound effects; and Timely Products, Chicago, demonstrated a \$38 retail door chime with 24 tunes that can be dialed.

A host of electronic handheld and board games were demonstrated by many companies, including a gin card game (Mattel Electronics); a handheld video game cassette system called "Microvision" (Milton Bradley); two-player handheld football and basketball games (Coleco Industries); "Odyssey²," an over-30-games programmable video game system from Magnavox; Waddingtons' two-player soccer and hockey games; Entex's "Mac Mini-Computer" for children (4K ROM, 1.5K RAM and full keyboard).

A handful of electronic chess and backgammon games was on display, too. Chafitz' "Grand Master" Auto Response Board chess program (Sargon 2.5) was especially interesting as moves need not be keyed to alphanumeric markings or pushbuttons. The system automatically senses chesspiece moves and responses are by lighted LEDs on squares.

Wireless telephones and telephone accessories were clearly upbeat items, with more companies in the field than ever before. These included new wireless entries by Electra, APF and Cobra, among others. Ford Industries introduced its Code-A-Phone 1400 remote command telephone system, which includes a pocket coder that allows the owner to call from any telephone to pick up recorded messages at home. Fracom/Rovaphone's new Rovette® cordless phone system eliminated the traditional whip antenna, with a flexible antenna in the handset coil cord replacing it. And Canada's Dictograph Corp., an intercom maker, has entered a \$100 Phone Controller™ that stores up to 30 different 16-digit numbers for single-touch dialing and has LED phone-number readout and automatic redial, among other features.

Major products in the fields of audio, video cassette, radar, car stereo, et al., were on display, of course, each demonstrating some refinements. These will be covered in other sections of PE over the next few months.

NOW AVAILABLE!

WATT WIZARD™

POWER FACTOR CONTROLLER CUTS
THE COST OF RUNNING ELECTRIC
APPLIANCES BY AS MUCH AS
50% -- AND YOU CAN EVEN SEE THE
SAVINGS!

For over a year now, in magazines and newspapers the world over, there have been enthusiastic write-ups on a remarkable new device that can cut your electric bill while helping the U.S. save huge quantities of fuel.

"The NASA/Nola power saver," wrote a *Popular Science* senior editor, "was developed by Frank Nola at NASA's George C. Marshall Flight Center as an offshoot of a program to reduce power consumption in spacecraft motors. Nola calls it a PFC — power-factor controller. I prefer to call it a power saver, however, because that's what it does."

NASA TESTED IT

According to Clyde S. Jones of NASA, "The device has been tested at Marshall Center on over 40 types of motors, with power savings ranging up to 60%, depending on the loading. The motors tested were both single-phase and three-phase, ranging from 1/2 H.P. to 5 H.P. Most motors will show up to 40-to-50% savings when running lightly loaded or unloaded, and some will show 5-to-7% savings at rated load."

NASA's Technical Support Package showed the test results and noted that "The Power Factor Controller applies to induction type electric motors — the most commonly used type in all major home appliances and the most commonly used by industry."

HOW IT SAVES POWER

Popular Electronics explained it this way: "AC induction motors characteristically run at a nearly constant speed that's fixed by power-line frequency and independent of load and supply voltage. When heavily loaded, the motor draws line current that is nearly in phase with the applied voltage... Under light load conditions, the motor develops less torque by allowing more lag between the voltage and current. This reduces the power factor while leaving the current essentially the same in magnitude.

"Though the low power factor means that conversion of electricity to mechanical power is small, the large current causes considerable (heat) losses in the supply lines and motor windings. This is what reduces efficiency.

"To minimize this waste, Nola's device monitors the motor's power factor and, when it detects light load conditions, it reduces the supply voltage... The current, now more nearly in phase with the voltage, therefore does as much useful work as before, but it and the voltage are smaller, resulting in a net savings of electric power."

THE SAVINGS CAN ADD UP

Like everything else, the cost of electric power keeps going up. Not only is the basic rate you pay going up, the power companies have now added on a "fuel adjustment" charge to help pay for running their generators. In 1980, 1981 and beyond, you'll pay more and more for the privilege of running your electric appliances.



MERCURY
1980 ©

National Aeronautics
and Space Administration
Patent No. 4,052,648

Right now, the typical consumer pays about \$8 per month to operate a 16.5 cu. ft. frost-free freezer... \$10 to run a 17.5 cu. ft. frost-free refrigerator... \$8.25 for an attic fan operating 12 hours a day... and about \$60 for an air conditioner used during summer months. It's not hard to figure out what you're paying per year just to run one of these appliances. And in many parts of the country, the cost is even higher.

That's why Nola's power saver can soon pay for itself, then start reducing your electric bills — the amount of savings, of course, depending on which appliance(s) you use it with.

There's just one catch. Until now, the device has not been available — except for industrial models prices at \$80 or more.

INTRODUCING THE WATT WIZARD

Cynex, an American manufacturer of electrical and electronic products and a prime contractor for the U.S. Government, has been licensed by NASA to manufacture Frank Nola's power saver. Cynex calls it the Watt Wizard.

"The Watt Wizard," says Ray Beauchea, the firm's Marketing Director, "regulates the voltage fed into an induction motor, reducing or boosting power as required, when loads go up or down. Simply stated, it makes motors run more efficiently, especially when idling. It reduces motor heat, affording longer motor life and reducing the amount of air conditioning required for cooling (rooms) in summer months. It saves electric power, because kilowatt hours are greatly reduced. And it causes the motor to run quieter."

SIMPLE TO USE

Cynex makes several models of the Watt Wizard (all with solid state design), including the 110 V AC plug-in model we're offering. It's for single phase fractional H.P. motors (less than 1 H.P.) which is the type used in most made-for-the-home freezers, refrigerators, window and attic fans, swimming pool pumps, furnace fans, vacuum cleaners, sewing machines, power drills, etc.

Simply plug the Watt Wizard into any electric outlet, then plug the appliance into the Watt Wizard. There's no wiring required. Unlike some competitor's models (if and when available), the appliance does not have to be turned on before being plugged into the power saver. You can leave the appliance — whether on or off — plugged into the Watt Wizard all the time. Or you can move the Watt Wizard to various locations, depending on which appliance is being used. (Better yet, order several Watt Wizards.)

OTHER MODELS AVAILABLE

Air conditioners, washers and dryers require wire-in model. If you lack mechanical skill, you probably need an electrician to install it. We also offer it in 220 VAC single or three-phase.

ADVANCE FEATURES

The Watt Wizard also includes two more unique features. It's fused, so if you accidentally overload the device, it won't burn out. Just change the fuse, which is available at any auto supply store.

And the Watt Wizard features an LED readout, so you can actually tell, at any moment, exactly how much power you're saving — 10%, 20%, 30%, 40% or 50%.

There's a "Power On" light, too. And the Watt Wizard comes with the manufacturer's 1-year limited warranty.

LOW COST — AND A TAX CREDIT

We're offering the Watt Wizard for only \$39.95, with immediate delivery. Want two? Then it's just \$37.95 each. Or splurge and get three at \$34.95 each. Wire-in models for heavy duty motors are \$6 more for each unit. Add just \$2.50 postage/handling for each order (not each unit).

And next year, when you fill out your tax return, you can deduct a full 15% energy tax credit — for additional savings.

30-DAY MONEY-BACK GUARANTEE

Try the Watt Wizard for up to 30 days. If not completely satisfied, return it (insured) for a full refund.

The sooner you send for the Watt Wizard, the more you can save on your electric bills. To order, send your check or money order to the address below. Or charge it to your Visa, MasterCharge, American Express or Carte Blanche credit card. If using your charge card, you can also order via our toll-free phone number:

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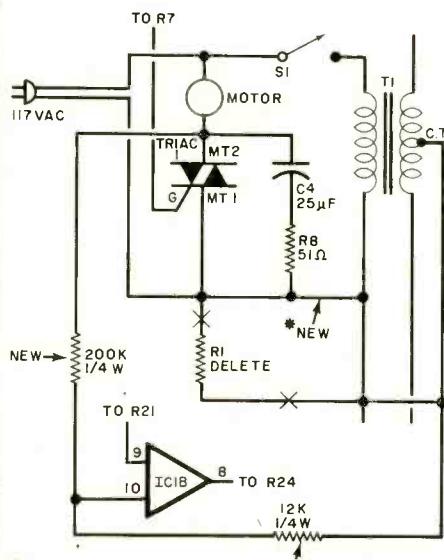
Letters

RELAY POWER SAVINGS

"An Experimenter's Guide to Relay Control" in your February issue was an excellent short course, which I clipped out and put in my book of handy circuits. However, there is a way of achieving significant power saving in relay circuits that was not mentioned. I first read about it in an article by John R. Nelson, of Motorola, in *Electronics* magazine, dated Dec. 9, 1976. Essentially, the idea is to reduce the voltage necessary to actuate a relay by adding the voltage across a charged capacitor to the normal source. Then, once the relay is energized, the source is sufficient to hold it in. Thus, a 26-V relay can be energized from a 12-V supply by adding a charged 15- μ F capacitor in series with the coil and a transistor. When a switch is closed to apply the 12 V, it also turns on the transistor to discharge the capacitor and increase voltage across the coil. Variations in the circuit can be made to suit various relays.—J.M. Burwell, Fort Rucker, AL.

IMPROVED NASA MOTOR CONTROLLER

The designer of the circuit that appeared in my article ("NASA Motor-Control Circuit Cuts Electric Cost," October 1979) has brought to my attention a simple modification which eliminates the need for the cumbersome fixed resistor R_1 (0.02 ohm, 5 watts). With the change (shown below), the only factors



*NOTE: ERRONEOUSLY INCLUDED IN SCHEMATIC OF ORIGINAL CIRCUIT; NOW PART OF MODIFICATION

that limit the size of the motor to be controlled are the current rating of *TRIAC1* and the heat-dissipating capability of the heat sink on which it is actually mounted.

The modified circuit replaces R_1 with a jumper to the bottom of *T1*'s primary and has two new fixed resistors that form a voltage divider between the bottom of the primary and *MT2* of *TRIAC1*. The tap of the voltage divider is connected to the noninverting input of *IC1B* (pin 10). Instead of sampling motor current by means of the voltage drop across R_1 , the modified circuit samples it by means of the voltage drop across the intrinsic resistance of *TRIAC1*. The voltage divider attenuates this voltage to a level below that of the op amp's power supply.—Myles H. Marks, Pittsburg, PA.

REACT TEAMS HEALTHY

The reference in your December "Personal Electronics News" column to REACT's financial needs and recommendations that contributions be sent for our Emergency Fund is most helpful and appreciated. However, we have been advised by a number of our REACT Teams throughout the country that, while our Headquarters operations as REACT International, Inc. are having difficulties, we still have hundreds of local REACT Teams throughout the country which are thriving, growing and serving the public in an increasingly more valuable way every day.

The REACT program is most successful and visible at the local level where we have very active Teams. The Emergency Funding Drive is ending with some success thanks to you and other publishers as well as the outstanding response we have received from local REACT Teams everywhere.—Gerald H. Reese, Managing Director, REACT International, Chicago, IL.

NUCLEAR POWER ADVOCATE

The nuclear power plant illustration on the cover of your January 1980 issue portrays a gloomy nuclear power plant of impending doom. This portrayal is untrue and unwarranted... singles out nuclear power plants as the only source of radiation that the "personal radiation monitor" (PRM) may be used to detect. However, your article lists several other sources of radiation, including "many New England fireplaces." Why not illustrate a New England fireplace on your cover?

The Kemeny commission has reported that the offsite radiation dose attributable to the (Three-Mile Island) incident was so low that any potential health effects will be minimal, leading to a projected cancer-death potential from zero to less than 10. Therefore, when you mentioned the TMI incident and resulting radiation release, you should have included "though very-low-level" just as you did in making reference to radiation emitted from New England fireplaces.—M. L. Nelson, Nuclear Engineer, Babcock and Wilcox Co., Lynchburg, VA.

If one were to illustrate a home on fire with a smoke alarm in the foreground it does not imply that people should not live in homes. The radiation release from TMI was indeed very-low-level.—Ed.

AMBIENCE FOR STEREO

Adding two extra loudspeakers to provide "ambience" via the Hafler system, as described in the "Stereo Scene" in your October 1979 and January 1980 issues, is a

great idea. But the effect can be further improved, using an even simpler setup that works on all stereo recordings and does not require the listener to sit near the center of the room. The rear speakers, connected in parallel with the front ones, should be placed on their backs, facing the ceiling. Their diffuse reflections provide a stronger feeling of spaciousness. Crossing the left to the right and vice versa at the rear prevents the sound from seeming to come from the side walls. The back speakers can be relatively inexpensive and their levels can be controlled by L-pads or simple 5-watt pots with values around 27 ohms.

This system is called "S-cubed" and is used in all General Motors cars having factory-installed stereo radios with the four-speaker option. (Ford and Chrysler are not interchanging L and R at the rear.)—*Daniel Shanefield, Princeton, NJ.*

AUDIO ARTIST CONNECTIONS

On page 61 of the December issue, in the "Audio Artist" article, the gate, source, and drain of Q1 are not marked. The markings given on the component placement on page 62 would not seem to agree logically with the schematic. —*Mike Ringenberger, Martinsville, IN.*

There are two versions of the TO-92 case for FETs. For the one shown in the component layout, the outline is correct and the circuit would work but interchange the labeling of the drain and source.—Ed.

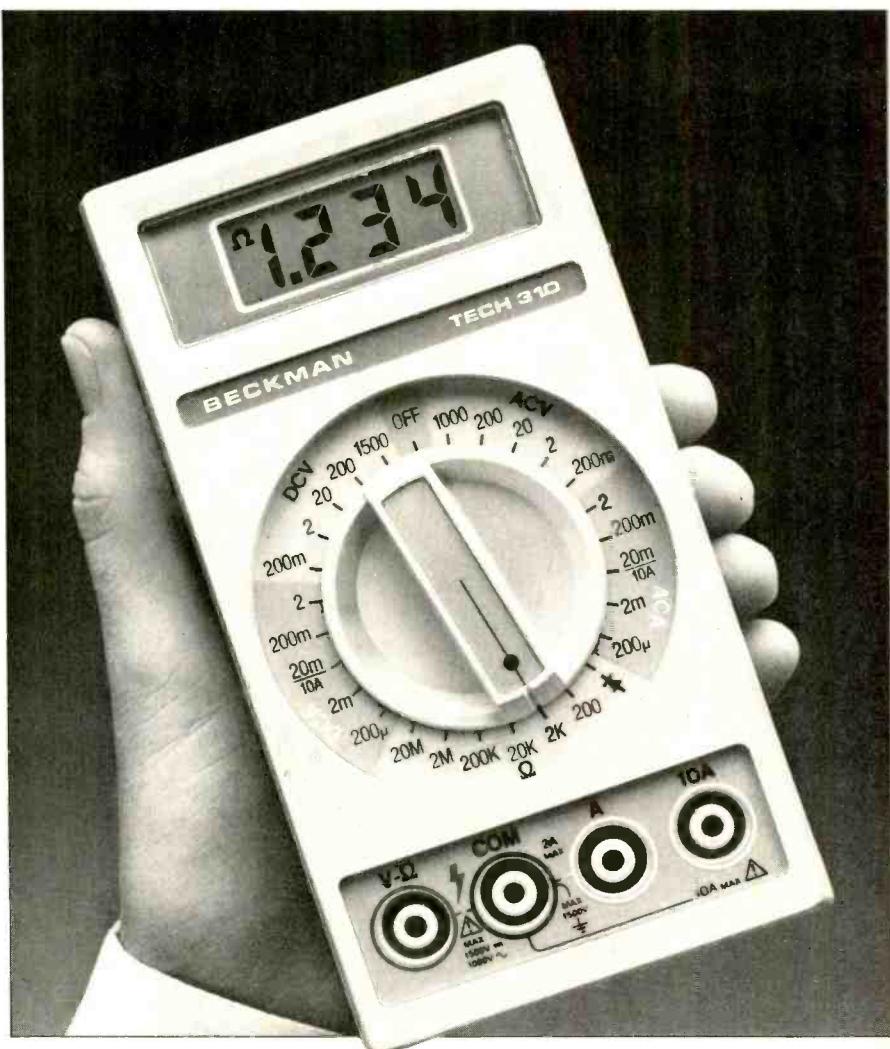
PEDOMETER MODIFICATION

Readers who build the "Electronic Pedometer for Joggers" (August 1979) may wish to keep a running tally in miles rather than steps. To do this, simply use the number of miles per step as the constant instead of 1. For example, if you find it takes you 1250 steps to jog a mile, the miles per step would be this number's reciprocal, or 0.0008. To enter this constant, use the key sequence CLR, +, .0008. If your calculator has a reciprocal key, use the sequence CLR, +, 1/x. The calculator can be reset to zero or preset to any number without reentering the constant simply by pressing 0 or entering any other number without pressing CLR or any arithmetic-operation key. —*Stephan Bush, Kingston, NY.*



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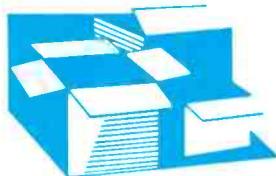
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BECKMAN

CIRCLE NO. 7 ON FREE INFORMATION CARD



New Products

Additional information on new products covered in this section is available from the manufacturers. Either circle the item's code number on the Free Information Card or write to the manufacturer at the address given.

Hewlett-Packard Personal Computer

Hewlett-Packard's new HP-85 computer is a self-contained system that combines a computer, five-inch CRT, alpha keyboard and 20-key numeric pad, a thermal printer, and an H-P tape drive to accommodate H-P



Data Cartridges. Interactive graphics are built-in with a graphics mode for video display and for the printer. The system has 16,000 bytes of read/write memory, with 14,500 bytes available. Memory can be expanded to 32,000 bytes (30,500 available) by plugging in an optional memory module. H-P's BASIC language is said to offer 12-digit accuracy, versatile string operations, convenient editing, 42 predefined functions, four levels of program security and flexible output formatting. The graphics system (with a 256-by-192 dot field) allows data to be plotted, displayed, and preserved on the built-in printer. The keyboard serves four functions: entering alpha data; entering numbers and doing arithmetic operations; program development using "soft" keys; and display, editing, and system control keys. In the alphanumeric mode, the CRT display has a maximum of 16 lines of 32 characters. Four I/O ports permit expansion for disc drives, plotters, etc. Dimensions are 16" W X 18" L X 6" H (40 X 46 X 15.5 cm); weight is 20 lb (9 kg). \$3250.

CIRCLE NO. 84 ON FREE INFORMATION CARD

Bose Ambiance System

The new Bose Spatial Expander® is designed to work with the company's Spatial Control Receiver, two 901 Series IV

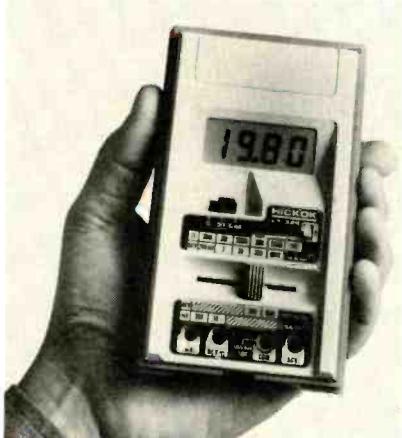


speakers and two Direct/Reflecting speakers. The Spatial Expander uses a charge-couple device (CCD) time-delay process to delay sound from the rear speakers. The result is said to create a lifelike ambience without detrimental effects.

CIRCLE NO. 85 ON FREE INFORMATION CARD

Hickok Hand-Held DVOM

The new one-hand-operation LX 304 DVOM from Hickok has a 1/2"-high, 3 1/2-digit LCD display and is claimed to be able to withstand a four-foot drop without loss of accuracy. It features automatic polarity,



zero, and overrange indication; automatic decimal point; battery indicator; and diode and transistor testing capability. It's rated at 0.5% accuracy on dc voltage ranges. Resistance ranges are from 200 ohms to 20 megohms and dc voltage from 200 mV to 1 kV. Current ranges are 200 mA and 1 A; ac voltage ranges are 200 and 600 rms. Test leads store in a built-in closed compartment. \$89.95.

CIRCLE NO. 86 ON FREE INFORMATION CARD

Computer "Electric Crayon"

Percom's new Electric Crayon generates computer-operated color graphics and control on either a color TV receiver or monitor. It includes a ROM operating system, (EGOS®) which accepts single-character commands directly from a parallel ASCII keyboard or program generated from a computer. It interfaces with a TRS-80, but can be adapted to any computer. The system has provision for 1K of on-board RAM, an EPROM chip for extending EGOS and a second dual bidirectional 8-bit port for peripherals. Ten display modes include alphanumeric-semographics, a second higher-density semographics, and eight



graphics modes. Up to eight colors can be generated. With highest density, display resolution is 256 by 192 picture elements. System enclosure is 2 1/2" H X 9" D X 12" W (6.4 X 23 X 30 cm). \$249.95.

CIRCLE NO. 87 ON FREE INFORMATION CARD

Digital Readout AM/FM Receiver

Among the features of Sony's top-of-the-line 55-watt/channel STR-V55 AM/Stereo FM receiver is its frequency synthesis tuning system with a claimed tuning accuracy of better than 0.002% and fluorescent digital frequency readout for both FM and AM. A microprocessor tuning system with "Feather Touch" controls offers four station-selection methods: "Manual" for stepping up or down the FM scale; "Auto" to move up or down scale to the next available station; "Memory Preset" to select one of eight stations entered into memory; and "Memory Scan" to stop for 3.5 sec-



onds at each station in memory. Memory is retained even when power is removed, and provision is made for inserting tiny cards to indicate what stations are in memory. The power amp's pulse power supply is said to keep TIM and IM below 0.02%. In addition, output transistors are claimed to deliver cutoff frequencies between 50 and 80 MHz. Other features include a three-position muting sensitivity level, two tape monitor circuits, a five-LED signal-strength display, a low filter that takes effect at 15 Hz, an audio mute that lowers volume by 20 dB. Dimensions are 5 1/4" H X 17" W X 14 7/8" D (13.5 X 43 X 37 cm); weight is 15 lb (6.8 kg). \$500.

CIRCLE NO. 88 ON FREE INFORMATION CARD

"Intelligent" Printer

The HY-Q 1000™ by XYMEC, is a daisy-wheel printer for use with computers. It uses five built-in microprocessors and is said to be capable of eliminating the need for much complex computer software. The

THE WORLD AT YOUR FINGERTIPS



printer can be plugged into any computer and will automatically convert simple codes into instructions for right justification, proportional spacing, automatic title centering, automatic decimal-point location, and other common text formatting functions. It also has Quadra-Pitch™ (10, 12, or 15 characters per inch, or proportional spacing) up to 198 characters per line, 100 printable characters in five languages, and a choice of 21 different type styles in five different colors. White characters can also be printed on a black background. The printer uses an Olivetti electronic typewriter which can perform various functions by use of a 1024-character memory, including often-used phrases, tabs etc. \$2495.

CIRCLE NO. 89 ON FREE INFORMATION CARD

Selectable-Current Circuit Breaker

Intended for use in building and testing breadboard circuits, the Model 101 Breaker Box, by the Long Range Co., can be varied to trip with currents between 250 mA



and 7.75 A in 250-mA steps. There is also a 10-mA setting for testing "dry" or no-current circuits. The unit reacts to overcurrents of ac or either polarity of dc in about 10 milliseconds. Toggle switches point toward current values selected and a tripped condition is indicated by a lighted red LED.

CIRCLE NO. 91 ON FREE INFORMATION CARD

VCR with 14-Day Programmer

Zenith's new "Video Director-Programmable" VCR (Model VR9700J) is a Beta-format machine that can record up to four programs on four different channels at four different times during a 14-day period. Other features of the five-hour VCR are a weekly repeat which allows a program to

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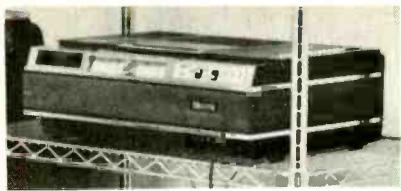
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be recorded once a week until the tape runs out, automatic electronic-pulse indexing, triple-speed play for review of material with a picture on the screen, and remote control with pause/stop action. Audio dub allows sound to be recorded from an outside source onto previously recorded tapes. \$1350.

CIRCLE NO. 92 ON FREE INFORMATION CARD

Mobile Digital Scanner

Regency Electronics' Model "Touch M100" is a digitally synthesized, 10-channel scanning radio for both mobile and home use. It covers the low, amateur and

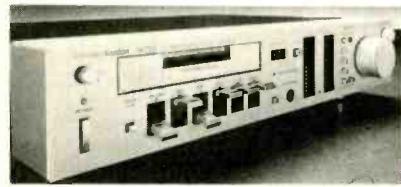


high vhf bands, and uhf band from 440 MHz to 512 MHz. Features include a search mode that can sample a band for calls, channel-one priority, digital display, scan and search delay, and brightness control for day or night use. Scanning rate is 15 channels/second.

CIRCLE NO. 93 ON FREE INFORMATION CARD

Harman Kardon Adds Dolby HX System

The hk705 cassette deck has been introduced into the Harman Kardon line of separate components. It features Dolby headroom extention (HX), said to improve high-frequency dynamic headroom by 10 dB, as well as Dolby B. The deck is equipped to



handle all current types of tape, including metal. Sendust Alloy tape heads are used, and LED record level indicators are provided. Rated specifications include: 0.04% wow and flutter (NAB wrms); 0.9% THD; 20-19,000 Hz ± 3 dB (metal tape) frequency response; -68 dB S/N (A-weighted, metal tape, Dolby in); channel crosstalk over 65 dB and channel separation over 38 dB. Dimensions are 15.2" W X 2.9" H X 12.6" D (385 X 72.5 X 320 mm); and weight is 13.7 lb (6.2 kg).

CIRCLE NO. 94 ON FREE INFORMATION CARD

Low-Cost ASCII Keyboards

RCA has introduced two ASCII-encoded keyboards with flexible-membrane key switches that are utilized to prevent liquids or dust from affecting operation. Model VP-601 is a 58-key typewriter-format board, while Model VP-611 has 74 keys with typewriter format plus 16 keys for numeric entry. The switches have positive-press action plus a tone generator to give aural keypress feedback. Boards operate from a single 5-volt dc supply and include a LED power-on indicator. The buffered seven-bit output is TTL and CMOS compatible. The boards also include two-key-rollover circuitry. The VP-601 is \$65; VP-611, \$80.

CIRCLE NO. 95 ON FREE INFORMATION CARD

Loudspeaker Uses New Cone Material

Wharfedale's TSR 110 speaker system uses a vertical-line, linear-phase arrangement with two 200-mm (7.87-in.) bass/midrange drivers operating in conjunction with one 25-mm (0.98-in.) soft-dome tweeter. The two lower drivers operate in tandem in an acoustic-suspension enclo-



sure up to about 300 Hz. Between 300 and 3500 Hz, the upper driver only is energized; there is an 18-dB/octave crossover to the treble unit. The bass/midrange cones are molded of a mineral-filled homopolymer said to have an exceptionally high stiffness-to-weight ratio. A continuously variable treble control adjusts the output in the range from 3000 to 20,000 Hz. Claimed frequency range is 35 to 25,000 Hz, with a power rating of 15 to 140 watts. The walnut-veneer enclosure has a detachable grille and measures 27.5" X 13.1" X 13.2" (695 X 332 X 335 mm).

CIRCLE NO. 96 ON FREE INFORMATION CARD

Antler Base-Loaded Antennas

Antler's two-way radio "Pro" Line of base-loaded antennas includes four models covering ranges of 30-36 MHz, 36-42 MHz,



45-50 MHz, and 130-174 MHz plus a 3/4-wave roof-mount antenna tuned to resonate between 108 and 174 M Hz. The latter is for use by city dwellers who have low-clearance problems. The four base-loaded models are provided with cutting charts to obtain accurate frequencies. They are available with a variety of mounting arrangements; shock springs are optional.

CIRCLE NO. 97 ON FREE INFORMATION CARD

Turntable "Flattens" Warps

Onkyo's new CP-1030F turntable is a single-play, fully automatic, direct-drive model with a quartz-lock speed control and a specially designed low-mass carbon-fiber



tonearm said to give optimum results with today's high-compliance cartridges. Low-frequency resonance of the arm and a typical high-compliance cartridge is controlled well enough, according to Onkyo, to allow warped records to be played with a minimum of distortion. In addition, the turntable has a rated signal-to-noise ratio of 75 dB and wow and flutter less than 0.03% (WRMS). Reliability of the unit is said to be enhanced by the use of an additional motor dedicated to tonearm functions. A set of LED indicators show what functions are engaged. \$315.

CIRCLE NO. 98 ON FREE INFORMATION CARD

Digital Encoder Interface

Sensor Technology has introduced an incremental encoder, the Digipot®, which provides an interface manually with a digi-

Not Just Another Limited Area Motion Detector!

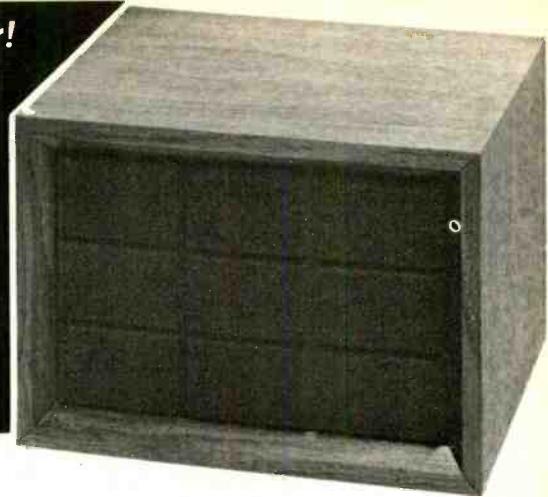
guardex

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Protects Every Square Inch Of Your Building

Turns On Lights Automatically

Powerful Electronic Siren



Low Cost Computerized Burglar Alarm System Home - Office - Business

NO INSTALLATION

Just plug the Guardex 8000 alarm system in, make several simple control adjustments to suit your particular building and it works! There are no other wires to run. This totally self-contained burglar alarm can completely seal off every square inch of the surface of your building. It protects doors, windows, and what most alarms miss...your roof, walls and floors.

HOW CAN ONE SMALL COMPUTER PROTECT MY WHOLE BUILDING?

Guardex 8000 Alarm System works on the principle of audio discrimination. This, put simply, is the process of electronically separating normal everyday sounds, such as voices, telephones, etc. from break-in type noises such as breaking glass, prying metal, or forcing a door open. The Guardex 8000 protects one story homes and offices up to 2000 square feet and open commercial buildings up to 10,000 square feet. The Guardex 9300 with wireless remote sensor capability is available for multi-story homes and offices or single story with more than 2000 square feet. Call the factory for more detailed information.

TURNS ON LIGHTS AUTOMATICALLY

When the first break-in type sound is detected, the system will instantly turn on lights, radio, or other electronic equipment that you have plugged into the back of the alarm. These lights or other equipment will remain on for a period of five minutes, then automatically turn off.

POWERFUL ELECTRONIC SIREN

The Guardex 8000 alarm is equipped with a loud built-in siren. If during the five minute period the lights or other electronic equipment has been activated, a second break-in sound is detected, (it can be only a second or two after the first break-in sound) the built-in siren will start blasting for 90 seconds. At the end of approximately 90 seconds the siren will shut off and the alarm listens again. If another break-in sound is heard, the siren will come on for another 90 seconds. If no other break-in sound is detected, the siren will stay off and at the end of the five minute period the lights will shut off and the alarm instantly resets.



The rear control panel contains two standard AC plug receptacles for a table lamp, spot lights, radio, etc.; terminals for connecting optional outside siren and back-up battery (not included); entry delay time control and sensitivity control.

The Guardex 8000 Alarm System is walnut grained and disguised to look like a small stereo speaker (6 3/4" x 9 3/4" x 8") and weighs less than 6 1/2 pounds.

EXIT AND ENTRY DELAY

The Guardex 8000 alarm has a built-in exit delay allowing you approximately one minute to lock up and leave the building before the alarm is armed. When you enter your building you may find that just your normal entering sounds activate the siren. You may delay it from starting for up to 30 seconds by turning up the siren entry delay control.

BATTERY BACK-UP

Burglars rarely cut power. However, to give you total protection from a burglar and possible power failure, our alarm has provisions for a battery back-up. (Batteries not included). 12 volt lantern batteries are available at most hardware stores.

THE BURGLARY PROBLEM

The F.B.I. statistics show that at the present rate, one out of every four Americans are going to be burglarized. That is not a very pleasant fact, but it is true. You have a greater chance of being burglarized than being a victim of a fire or automobile accident. The time is now to help protect yourself and your valuables with a Guardex 8000 alarm system.

OUTSIDE SIREN

The Guardex 8000 alarm is equipped with a loud, built-in siren, but if you desire an additional siren to mount outside or in an area away from the main alarm, they are available with 50 feet of wire for \$24.95. (Connecting terminals are provided on the back of the alarm).

30 DAY NO RISK TRIAL

This is your opportunity to purchase an alarm system directly from the factory for only \$199.95. Try it in your home or business for thirty days without risking one cent. Put our Guardex 8000 alarm to your own test. See for yourself! It will protect every window and door from break-in. If you are not completely satisfied, return the alarm within 30 days for a complete refund. To order your Guardex 8000 alarm, CALL TOLL FREE to charge your credit card or send your check to Guardian Electronics, Inc. in the amount of \$199.95. If you want the optional outside siren, add \$24.94. (California residents add 6% sales tax.)

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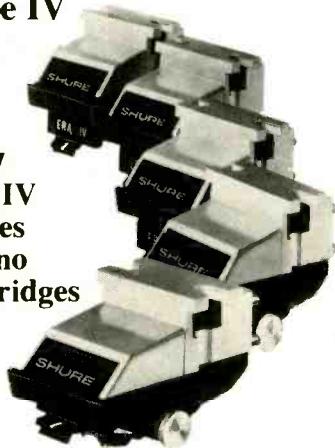
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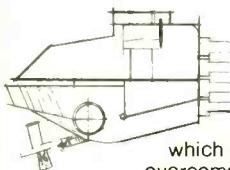
Westlake Village, Calif. 91361

**fact:
five new Shure Cartridges
feature the technological
breakthroughs of the V15
Type IV**

**the
M97
Era IV
Series
phono
cartridges**



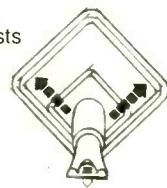
Shure has written a new chapter in the history of affordable hi-fi by making the space-age technological breakthroughs of the incomparable V15 Type IV available in a complete line of high-performance, moderately-priced cartridges: the M97 Era IV Series Phono Cartridges, available with five different interchangeable stylus configurations to fit every system and every budget.



Dynamic Stabilizer—

which simultaneously overcomes record-warp caused problems, provides electrostatic neutralization of the record surface, and effectively removes dust and lint from the record.

SIDE-GUARD, which responds to side thrusts on the stylus by withdrawing the entire stylus shank and tip safely into the stylus housing before it can bend.



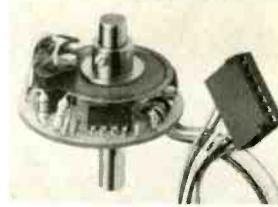
And, the unique telescoped stylus assembly which results in lower effective stylus mass and dramatically improved trackability.

There is even an M97 cartridge that offers the low distortion Hyperelliptical stylus!

NEW! M97 Series Era IV Phono Cartridges...Five new invitations to the new era in hi-fi.

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Manufacturers of high fidelity components,
microphones, sound systems and related circuitry.

CIRCLE NO. 53 ON FREE INFORMATION CARD



tal system. Connected to an up/down counter, the unit is claimed to offer unlimited resolution in the form of an n-bit word which can be arbitrarily long. The same up/down counter can also be used as a memory for a D/A converter. Direct interfacing to a microprocessor is possible through an I/O routine over two bitlines. Applications include positioning of X/Y tables, N/C machines, inputs to volume controls, or control of stepping motors. \$39.90. Address: Sensor Technology, 21012 Lassen St., Chatsworth, CA 91311.

New Cassette Tapes

RKO Tape Corp. has added Ultrachrome and XD general-purpose tapes to its line of audio cassette tapes. Ultrachrome is said to be a second-generation chromium-dioxide tape with a frequency response flat ± 0.2 dB out to 20 kHz. It is claimed to



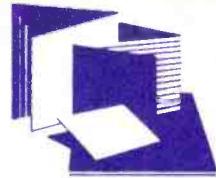
equal metal tape in response, distortion and S/N. The XD, according to RKO, is formulated for the musical midrange, where its headroom is said to be 78% greater than average with a significantly higher S/N. Ultrachrome is \$5.76 for C-90, \$3.96 for C-60; XD, \$3.66 and \$2.60 (also available in C-45 at \$2.36).

CIRCLE NO. 99 ON FREE INFORMATION CARD

Analyzer / Equalizer

Soundcraftsmen's new Model AE2420-R "Scan-Alyzer" / Equalizer contains differential comparator circuitry said to be able to measure room equalization with an accuracy of ± 0.1 dB. The equalizer and analyzer sections both use active bandpass filters on octave centers ranging from 30 to 15,360 Hz. Rated boost/cut capability ranges from ± 12 to ± 16 dB in each band, depending on setting of adjacent controls. Harmonic and IM distortion are reported to be less than 0.01%, and S/N, 100 dB, all at 2-V output. In addition, the analyzer section contains its own pink-noise source and a microphone preamp. Dimensions are 5 1/4" H X 19" W X 11 1/4" D (13.5 X 49 X 29 cm); weight is 20 lb (9.1 kg). \$500.

CIRCLE NO. 100 ON FREE INFORMATION CARD



New Literature

COMPUTER SOFTWARE YELLOW PAGES

All Micro Architect business software for the TRS-80 is listed in the 12-page TRS Yellow Pages guide. Issue 1.4 features a sophisticated data base manager for the TRS-80. Two stamped, long, self-addressed envelopes must accompany request. Address: Micro Architect, 96 Dothan St., Arlington, MA 02174.

CB ANTENNA CATALOG

"Firestik" CB antennas and accessories are described in the company's new product catalog. Featured is the Firestik top-loaded, helically wire-wound fiberglass CB antennas for mobile and base station use. Also included is the company's line of antenna mounts. Address: "Firestik" Antenna Company, 2614 East Adams, Phoenix, AZ 85034.

TECHNICAL HANDBOOK FOR FANS

"The Fan Catalog" is a 92-page handbook (No. EF3) from IMC Magnetics describing over 140 types of propeller and tubeaxial airmovers for dc, 60-Hz, 400-Hz, and multi-frequency applications. Capacities range from 13 to 1600 cu ft/min. Complete specifications and dimensions are provided. Address: IMC Marketing Div., 570 Main St., Westbury, NY 11590.

HAMTRONICS KIT CATALOG

The 24-page 1980 catalog from Hamtronics features a variety of kits for the radio amateur or radio service shop person. Included are a 435-MHz transmitting converter, a uhf FM receiver, an AM receiver for aircraft and DX warning, a weather tone alert receiver module, and various linear amplifiers for vhf and uhf. Address: Hamtronics, Inc., 65F Moul Rd., Hilton, NY 14468.

CAR SPEAKER SYSTEMS

A new booklet published by Audiovox, "The Dynamics of Speaker Placement in an Automobile," describes the differences in sound effects which can be obtained by placing speakers in different locations; the matching of speakers to the rest of the system; and how to get optimum sound from car stereo. Address: Audiovox Corp., 150 Marcus Blvd., Hauppauge, NY 11787.

DATA COMMUNICATIONS CALENDAR

The 1980 "Sherry Says" Data Communication Calendar provides pertinent information in the data communications field—major trade shows and conferences and historical events. The calendar is designed to be hung on the wall, and there is space in the squares to write in daily schedule. Address: Corporate Relations Dept. Racal-Milgo, Inc., 8600 N.W. 41st St., Miami, FL 33166.

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OMNISONIC IMAGERY™ IS HERE!

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CIRCLE NO. 62 ON FREE INFORMATION CARD



Stereo Scene

By Harold A. Rodgers
Executive Editor

AMPLIFIER TECHNOLOGY, DISTORTION, ETC.

RARELY WILL one find an audible difference in the performance of two neighboring receivers in a line. This applies with particular force to the power amplifier sections. The reasons why the foregoing is true depend on the two fundamental properties of amplifiers: power output and distortion. A higher-powered amplifier is worthwhile only by virtue of the fact that it allows music to be played louder without the peaks being clipped. In typical use, an amplifier—even when driving fairly inefficient speakers—will loaf along at an average power of 1 watt or less. Every now and then, at intervals of a few hundred milliseconds or so, a peak 10 to 20 dB above the average level comes along. To reproduce this properly—that is without limiting and cutting off the top of the waveform—the amplifier must increase its output for an instant by a factor of 10 to 100. Although the intervals during which these demands are made are very short, the ability of the amplifier to satisfy them makes all the difference. Most of the nasty sound that an overdriven amplifier produces is from just such clipping of peaks.

Now let's look at a hypothetical (but representative) line of receivers. Typically, their rated output power might be spaced at something like 25, 40, 60, and 90 watts as we move up in single steps, and very often we would find the spacing even closer. Next, let's change these absolute powers into

decibels—which give a more accurate reflection of auditory effect—using, for convenience, the lowest-powered model as the zero reference. The figures become 0, 2, 3.8, and 5.6 dB. Granted, the power an amplifier can deliver in handling a short peak is considerably more than its steady-state rating. In units of similar design, however, the extra power generally turns out to be a constant percentage of the steady-state ratings, so the difference remains the same when it is expressed in decibels.

It has been rather solidly established that even the most astute listener will not notice level differences in music unless they exceed 3 dB. (Designers of stepped audio attenuators implicitly endorse this view, as such devices rarely have steps smaller than 2 dB between adjacent positions, the control at this point being in effect continuous.) Therefore, it follows that, if we play the same music on any adjacent pair in our hypothetical line of receivers at a level just below clipping, there will be no perceptible difference in loudness. In fact, even if one skips a receiver in the series and listens very carefully, the difference will usually be very slight. There are other factors such as convenience features, a better FM section, or more elaborate tone controls that might make a single step upward worth taking. But as far as power goes, the message is clear: take big jumps or stay where you are.

What About Distortion? Although a few receiver manufacturers make a point of having identical distortion ratings for the power-amplifier sections throughout the line, most give reduced percentages at higher price points. Unfortunately, there is no real ground for considering these reductions significant in audible terms. As a matter of fact, it is questionable whether any distortion specifications in today's component amplifiers are audibly meaningful.

First, we can establish fairly easily that small changes in distortion can be ignored completely. We already illustrated that changes in level of a *desired signal* are inconsequential if they are smaller than about 3 dB. Obviously, the same principle applies to distortion. Therefore, given a unit rated at, say, 0.1%, its competitor would have to be rated at 0.07% (3 dB lower) before it could possibly sound any better. (Distortion percentages are, for some reason, calculated on the basis of voltage, not power.) And remember, by ignoring the presence of the test signal, we are being very pessimistic.

The Role of Masking. The presence of the fundamental (the tone being distorted, so to speak) makes any harmonic distortion products even less audible. As shown in the graph, the presence of a 400-Hz tone at a level 80 dB above its own audibility threshold raises the audibility threshold for a 4000-Hz tone (its 10th harmonic) by 20 dB. This is a factor of 100. Studies done directly on the audibility of distortion by Robert Carver and others showed that, under the most severe conditions—broad spectrum crossover distortion and pure tones, the threshold of audibility for distortion was around 0.15%, a level considered almost gross by today's standards. When music is used as a test signal, audibility thresholds consistently rise to something on the order of several percent.

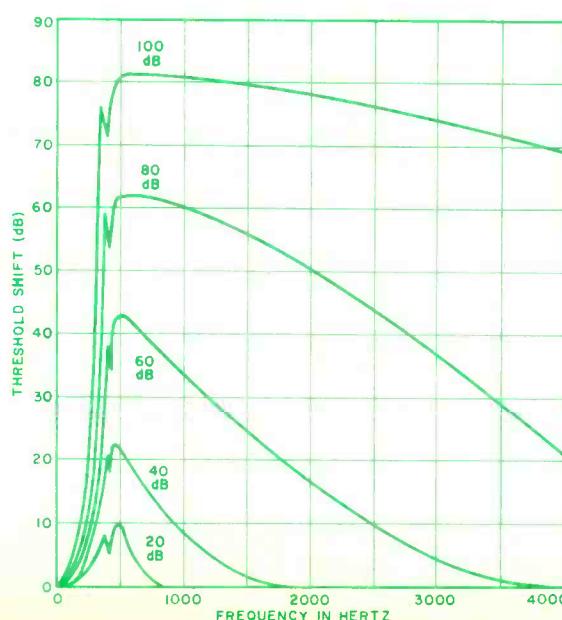
Intermodulation distortion represents what, superficially at least, looks like a more difficult challenge. It can, after all, produce spurious tones that are lower in frequency than the lowest tone present in the test signal. Consequently, it's more difficult to mask. For practical purposes, however, it should be remembered that such tones, if produced by musical fundamentals, will tend to lie in a range where the ear is not terribly sensitive. The same applies to transient intermodulation distortion (TIM), which the work of Walter Jung and others suggests can be detected in steady-state tests if proper methods are used. A better name for the phenomenon might be high-frequency distortion. In any case, it is well to remember that distortion-audibility studies using music include the effects of harmonic, intermodulation, and—if they truly exist—transient distortions. There is no practical way to separate them.

I had hoped at one point to look for ways in which amplifier distortion might be weighted for audibility. On the basis of the admittedly limited research that I did, that step seems quite unnecessary. What sense can it make to rate the relative audibility of influences that are inaudible in the meanest of present-day component amplifiers?

Do Amplifiers All Sound Alike? Not necessarily. They still differ in how much power they can deliver before overload, in internally generated noise, and in ability to tolerate

(Continued on page 20)

Masking effect of a 400-Hz tone at various levels. The traces indicate how much the audibility threshold is raised at other frequencies when the 400-Hz tone is present.



JBL'S NEW L150: ITS BOTTOM PUTS IT ON TOP.

JBL's new L150 takes you deeper into the low frequencies of music without taking you deeper into your budget.

This short-tower, floor-standing loudspeaker system produces bass with depth, power and transparency that comes incredibly close to a live performance.



A completely new 12" driver was created for the L150. It has an innovative magnetic assembly, the result of years of research at JBL. It uses a stiff, heavy cone that's been coated with an exclusive camping formulation for optimum mass and density.

And it has an unusually large 3" voice coil, which aids the L150's efficiency and its ability to respond to transients.



(peaks, climaxes and sudden spurts) in music. There's seven more to the L150's bottom—a 12" passive radiator. It looks like a driver but it's not. We use it to replace a large volume of air and contribute to the production of true, deep bass. Bass without boom.

If you're impressed with the L150's lows, you'll be equally impressed with its highs and mids. Its powerful 1" high-frequency

dome radiator provides wide dispersion throughout its range. And a 5" midrange transducer handles high volume levels without distorting.

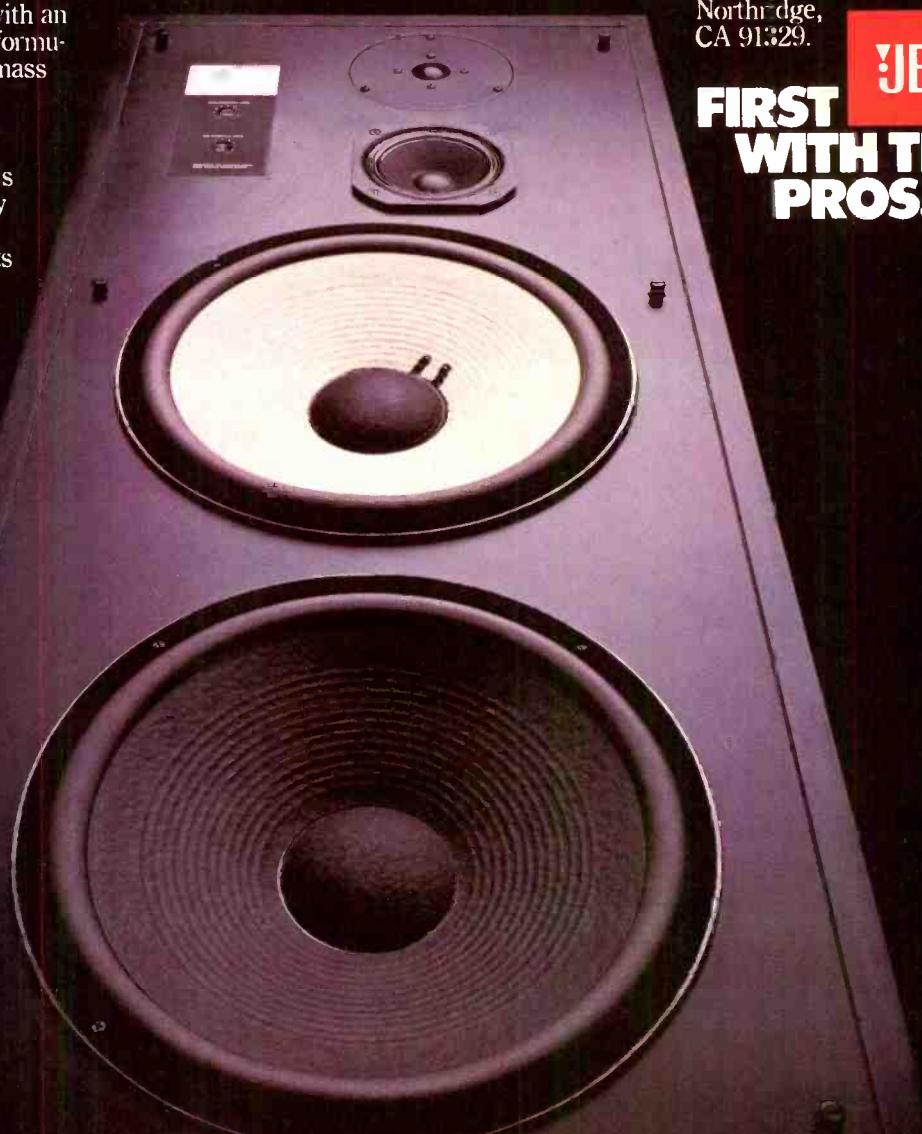
The maximum power recommended is 300 watts per channel.

The L150's other attributes include typical JBL accuracy—the kind that recording professionals rely on. Maximum power/flat frequency response. High efficiency. And extraordinary time/phase accuracy.

Before you believe that you can't afford a floor system, listen to an L150. While its bottom is tops, its price isn't.

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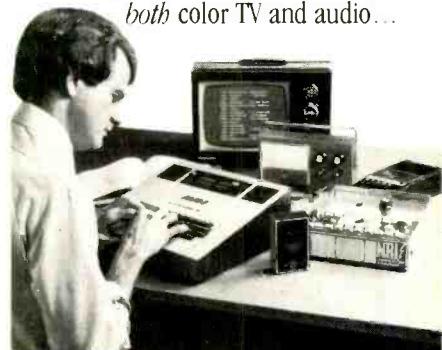
As part of your training in NRI's Master Course in TV/Audio/Video Systems Servicing, you actually assemble and keep NRI's exclusive designed-for-learning 25"

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(Summary of survey on request.)

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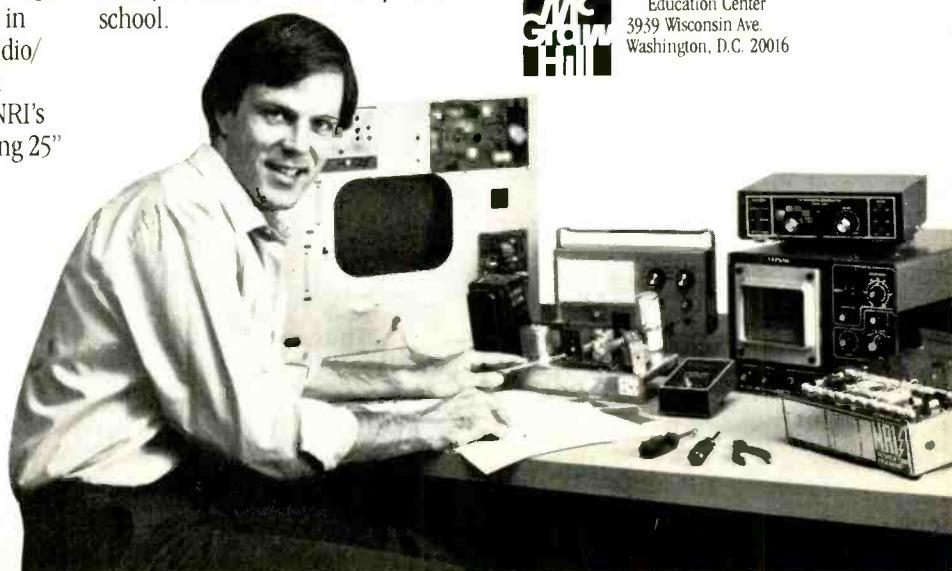
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STEREO SCENE *continued*

loads of very low impedance and/or highly reactive character without overloading or becoming unstable. The last point is just now beginning to get the attention it deserves.

Other points of difference include: ruggedness, quality of construction and parts selection, and the ability of automatic protection systems to operate without objectionable effects on sound quality. Designing in such characteristics can generate expenses that appreciably affect the price of the product.

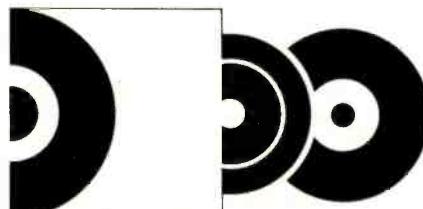
As for distortion, the next time someone tries to frighten or cajole you into considering it as a selling point, tell him you'd rather know how the moon's gravity affects the power-transformer windings. That probably makes more difference. ◇

ABBEY ROAD. **The Beatles.** Mobile Fidelity MFSL 1-023. Like others in the MFSL Superdisc series, this is a re-release, but with a difference. The original master tape is used, and the new master disc is cut at half speed. To top it all off, disc manufacture is very careful. In this case, the result is a superior rendition of a classic. The new production gives a clear insight into the antediluvian mixing techniques available to the Beatles and, also, into how artistically they used what they had. (Bach got by with some pretty crude instruments, too.) Curiously, the vocal is less prominent than I remember its being in the original production, an effect I noticed on some other Mobile Fidelity discs. Here, that characteristic is especially welcome, as there is a lot of fascinating instrumental.

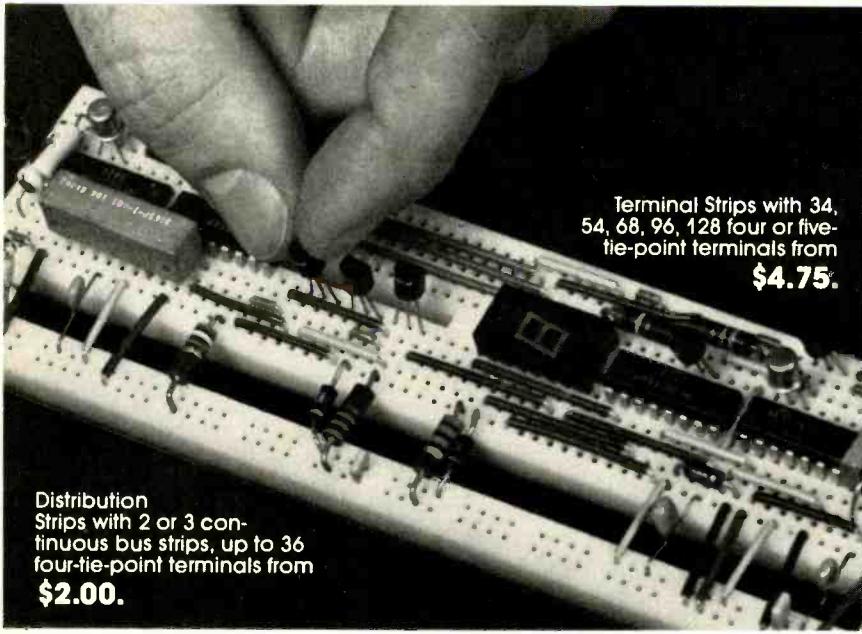
SONIC FIREWORKS: MUSIC FOR ORGAN, BRASS, AND PERCUSSION, VOLS I, II, **Richard Morris with the Atlanta Brass Ensemble.** Crystal Clear CCS-7010, 7011. This is a direct-mastered production with a big sound. What seems quite unusual about it is that the massiveness and opacity often found in recordings of large, loud ensembles is absent here. Details stand out nicely in even the most heavily scored passages. The playing sounds accurate and spirited, and generally brings the music off well. What seems a bit unfortunate, though, is that most of the works presented are transcriptions. Some were originally for neither organ nor brass, and in the rest one or the other seems grafted on as an afterthought. Surely music composed for organ and brass is not as hard to find as all that.

DON SEBESKY: THREE WORKS FOR JAZZ SOLOISTS AND SYMPHONY ORCHESTRA, **Harry Rabinowitz, with the Royal Philharmonic Orchestra and soloists.** Gryphon G-2-791. Attempts to fuse jazz and symphonic music into a single medium have always been a bit problematic. Somehow the two seem to conflict, each getting in the way of the other. Most of the successful works using such combinations belong properly in one genre or the other: jazz borrowing from symphonic or vice versa. While Sebesky's shows quite a lot of imaginativeness in his approach and generates many delightful minutes of listening, the junctions between music à la Bartok and jazz and music à la Stravinsky and jazz don't seem to work. The transition sounds nonorganic and sometimes almost arbitrary. Most successful, I think is Sebastian's Theme, which comes off as a kind of jazz meditation on material from J. S. Bach. Interestingly, this is the least symphonic-sounding of the three works presented. The recording quality is first-rate, with a nice sense of perspective and depth.

THE BEEGEES MUSIC Carmen Dragon conducting the Glendale Symphony Orchestra. Orinda ORC500. This is a pleasant bit of lightweight fluff, prepared with the utmost in professionalism and very neatly recorded via a digital process. It embraces a bit of disco, a bit of rock, a bit of MOR—all with the rough edges polished away by lush orchestral arrangements. "Exciting" does not seem like the word to describe this release. "Entertaining" is more like it.



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But at Pioneer, we believe, that if you're going to pay \$200 for a turntable, you shouldn't just get one of these features. You should get all of them.



PIONEER'S SOPHISTICATED SUSPENSION SYSTEM ELIMINATES SHAKE, RATTLE AND ROLL.

While other turntables with some of these advancements may look the same as the PL-400 on paper, they don't sound at all alike in your home. Because all these advancements act together to keep an imperfect environment, like your home, from getting in the way of perfect sound.

In your home, simply slamming a door can be more jarring to your turntable than it is to you.

Pioneer's PL-400 has a sophisticated suspension system that isolates the platter and tone arm from the rest of

the turntable. Which means you can shake, rattle and roll a lot more with a lot less worry that your turntable is doing the same thing.

The PL-400 also has the world's thinnest direct drive motor. This ultra-thin motor does a lot more than give the PL-400 an ultra-sleek appearance. It keeps the turntable platter perfectly steady at all times. Though platter wobbling isn't a problem that can be easily seen on most turntables, it can be easily heard. It results in shifts of musical pitch. Something the PL-400 is never bothered with.

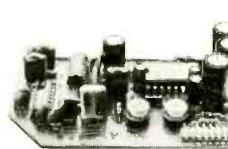
What's more, the PL-400 also has Quartz control like that found in the finest Swiss watches. Which means you're guaranteed to get the maximum in rotational accuracy.

So if you want a turntable that sounds great, there's any number you can buy. But if you also want the price to sound great, there's only one.

The fully-automatic Pioneer PL-400. We bring it back alive.

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CIRCLE NO. 48 ON FREE INFORMATION CARD

Julian Hirsch Audio Reports



Dual Model CS606 direct-drive single-play turntable with Ultra Low Mass tonearm



The new Dual CS606 is a direct-drive, single-play turntable with automatic shut-down at the end of a record.

It features Dual's ULM (Ultra Low Mass) tonearm, whose exceptionally low 5.5-gram mass can be complemented by an optional Dual/Ortofon ULM55E cartridge. The combined effective mass of the two is 8 grams, a new low for an integrated record player system. Any cartridges weighing between 2 and 9 grams and having standard $\frac{1}{2}$ -inch mounting centers can be installed in the ULM arm. An additional feature of the CS606's tonearm is its tuned counterweight, which can be adjusted to damp (at least partially) the low-frequency resonance of any cartridge used in the ULM arm.

Springs support the unit on its plastic base, the sides of which are finished in a simulated wood grain. The hinged plastic dust cover is easily removable. Total weight of the Dual CS606 is $14\frac{1}{4}$ lb (6.6 kg). With the cover lowered, it measures $16\frac{3}{4}''$ W \times $14\frac{1}{2}''$ D \times $5\frac{3}{4}''$ H (421 X 368 X 146 mm). Suggested retail price less cartridge is \$279.95. With the Dual/Ortofon ULM55E cartridge, it is \$390.

General Description. The platter has four rows of stroboscope dots cast into its rim for the $33\frac{1}{3}$ - and 45-rpm speeds with power-line frequencies of 50 or 60 Hz. They are lit by an LED mounted next to the outer edge of the platter. A small knob near the platter selects the operating

speed, and another provides a vernier pitch control.

To start the platter rotating, it is only necessary to move the tonearm from its rest. With the cuing lever in its "up" position, the arm can be moved horizontally until a light detent is felt at the lead-in diameter for a 12-inch record (a second detent marks the set-down point for a 7-inch record). The cuing action lowers the tonearm gently. A knob near the cuing lever disables the arm detents. Lifting the arm and returning it to its rest during play shuts off the motor; arm return and shutoff are automatic at the end of a record.

The straight ULM tonearm is constructed of small-diameter tubing and has a headshell designed for minimum mass. As the headshell is not detachable, the tonearm wiring must be connected to the cartridge pins before it is mounted in the arm. The counterweight has a scale around its circumference calibrated from 7 to 14 (apparently the resonant frequency of the internally suspended mass whose position is shifted within the counterweight as its main body is rotated). The instruction booklet includes a chart on which the mass and compliance of any cartridge to be used in the ULM arm can be located. From that information, one can determine the setting of the antiresonance filter that best cancels the increase in output that occurs at the resonant frequency of the stylus system and the effective mass of the arm and cartridge.

The gimbal arm mount has been retained from earlier Dual turntables, along with a side-mounted control that applies

vertical tracking force by means of a spring around the vertical pivot axis. The force scale is calibrated at 0.1 gram intervals from 1.5 to 3 grams. Antiskating with separate scales for conical and elliptical stylis is provided.

Test Results. We tested the CS606 with the ULM55E cartridge, which is designed to give its flattest frequency response when loaded by about 400 picofarads across the standard 47,000-ohm termination (this information is not stated anywhere in the instruction manual or the descriptive material on the cartridge). The CS606 tonearm and cable wiring had a capacitance of about 185 picofarads between each signal line and ground, so that preamp input capacitance of 200 to 250 pF should provide an optimum load for the cartridge. That is a fairly common input capacitance for phono circuits, although values range from less than 10 to more than 500 pF.

With the tonearm carefully balanced according to instructions, tracking force was within 0.1 gram of the indicated value. Tracking error was less than 0.5 degree per inch over the playing surface of a 12-inch record. The total effective mass of the arm and cartridge was only 7.5 grams, and the low-frequency resonance was at approximately 13 Hz. Due to the broad tolerances in the measurement, the differences between this and the manufacturer's data cannot be deemed significant.

The counterweight's antiresonator had a moderate effect on the playback output in the vicinity of resonance. In fact, when the antiresonant counterweight was set to 11.5 (the recommended point for this cartridge), it nulled the resonant peak almost completely, but narrowness of the notch left an appreciable rise in output above and below resonance. Measurements of the low-frequency response, made with the antiresonator set to its limits as well as as to the recommended value showed a typical output rise of 6 to 8 dB in the range of 11 to 14 Hz, remaining measurable as high as 25 Hz. In each case, however, the recommended setting gave the maximum reduction of output rise at the exact resonant frequency.

To check the Dual ULM arm with a cartridge more massive than the ULM55E, but highly compliant, we installed a Stanton 881S. This was complicated by the fact that the connecting clips on the tonearm wires were too small for the pins on the 881S. As they could not readily be unsoldered, we soldered larger clips to the original ones. It was also necessary to use one of the two additional counterweights that screw onto the rear of the regular one to balance the 5.7-gram mass of the 881S.

Low-frequency resonance measurements with the Denon 7001-A test record showed a resonant frequency near 10 Hz



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Here's the first calculator chronograph that can be operated easily with your fingertips. No need to use a stylus or pen; the keys are far enough apart that even the broadest fingers can work them.

Now you can add, subtract, multiply, divide—perform chain calculations up to six places, plus decimal. Numbers appear in crisp liquid crystal digits. There's even an indicator that tells you exactly which function is being performed.

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You also get two time zones; the second zone can be set for 12 or 24-hour time (especially useful for frequent travelers). Hours, minutes and seconds are displayed with reliable ± 15 second-a-month quartz precision. AM/PM indicator is always visible.

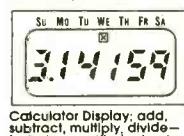
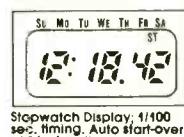
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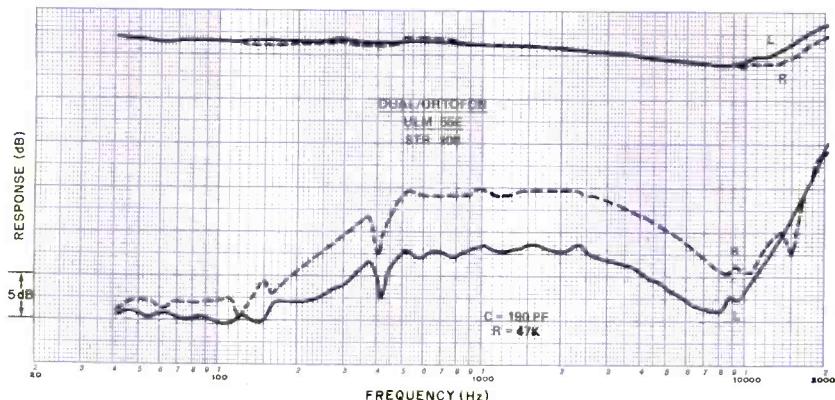
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Frequency response and crosstalk for left and right channels.

with the 881S. Since the setting of the antiresonator on the counterweight had an appreciable effect on the apparent resonant frequency, the figures are somewhat in doubt for both cartridges. Some of the antiresonator settings gave a peak around 8 to 9 Hz on the left channel, while the right channel seemed to peak at about 10 Hz. The Shure Audio Obstacle Course-ERA IV low-frequency resonance test gave similar indications. Maximum arm movement occurred from 8 to 10 Hz depending on the antiresonator setting. The antiresonator performed dramatically with this record, a setting of 11 giving best all-around stabilization around the stabilization of the arm.

Turntable flutter was $\pm 0.06\%$ weighted peak (CCIR) and 0.05% weighted rms (JIS), with 5 and 20 Hz dominating the spectrum. Unweighted rumble was -31 dB, measuring a good -60 dB with ARLL weighting. Maximum rumble energy was at about 7 or 8 Hz. Speed could be adjusted over a range of $+4.5\%$ to -6% with the vernier knob. The instruction manual says that there are separate pitch controls for each speed, but this appears to be an error. There is only one control and slight re-adjustment may be needed when changing speeds. On our test unit, however, the two speeds were very close to correct at the same setting.

The cueing device worked very smoothly, with negligible outward drift of the tonearm during descent—even with the antiskating at 2.5. End-of-play sequence took only 3.3

seconds from automatic arm lift to motor shut-off.

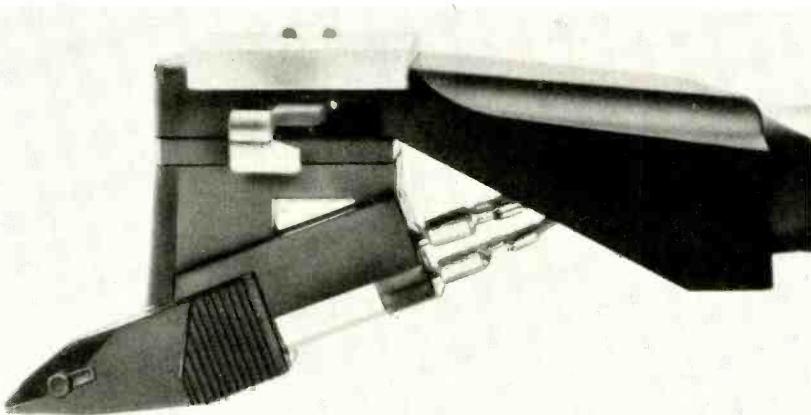
We also took data on the ULM55E cartridge, which, in addition to its very low mass, behaved very well when operated near the upper end of its rated tracking force range. At 1.5 and 1.75 grams, the tracking limits were respectively 60 and 70 micrometers on the German Hi Fi Institute test record. This fell to only 40 micrometers at 1 gram. Tracking distortion with

20,000 Hz. Channel separation was about 20 dB in the midrange, 25 dB at 10,000 Hz, and 12 dB at 20,000 Hz.

User Comment. The general handling characteristics of the Dual CS606 were excellent. For practical purposes, it can be considered as a "smart" player and easy to use because of its record diameter indexing feature and automatic shutoff.

The tonearm and pickup system give the CS606 the ability to play warped records that are completely unusable on conventional record players. Even a severe warp that would normally throw the pickup into the air will usually give no more than a slight "thump" when it is played, and most warps are undetectable by ear. Some, though not all, of these benefits are retained even when pickups other than the ULM55E are used.

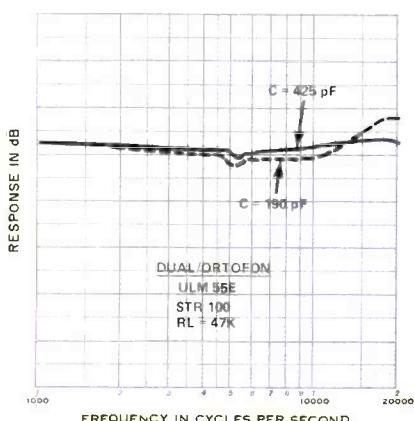
The compliant spring mounting of the record player on its base gives it relatively good immunity to base-conducted vibration that could cause acoustic feedback. Except for a single transmission response at about 35 Hz, the CS606 had almost no resonances in the audio range when driven through its mounting feet. We consider its isolation somewhat better than average for a direct-drive turntable.



Optional Dual/Ortofon ULM55E cartridge.

Shure TTR 102 and 103 records was relatively low, with no evidence of serious mistracking even at the highest levels. At a 1.5-gram force, the cartridge could track everything on the Shure ERA III record, although a touch of strain was evident on level 5 of the sibilance section. The more stringent ERA IV record caused audible mistracking on level 5 of most sections; level 4 usually played without difficulty.

The stylus vertical angle was 24 degrees. Square-wave response on the 1000-Hz square waves of the CBS STR112 record was very clean, with a slight overshoot and a couple of cycles of well-damped ringing at about 20,000 Hz. Frequency response (with the CBS STR100 record) was very flat up to 10,000 Hz and rose to about $+3$ dB at 20,000 Hz, when the cartridge was terminated by the CS606 cable capacitance (about 190 picofarads) and a 47,000-ohm resistance. A total of about 425 picofarads flattened out the high end very nicely, resulting in a response flat within ± 1 dB from 40 to



High-end frequency response with CS606 cable capacitance (190 pF) and with 425 pF.

We found the stroboscope illumination system less than helpful in viewing the 60-Hz 33 1/3-rpm marks. Fluorescent room lighting was better for setting this speed.

Because of the design of the ULM arm, anyone who habitually switches cartridges will find the CS606 more than a little frustrating. The fact that the signal cables are color-coded grey and brown with no channel identification doesn't help, and the connectors are too small for the pins on many cartridges. On the other hand, the ULM55E cartridge offers good value in its price range and is an excellent companion to the ULM tonearm. It comes properly installed and positioned when ordered with the CS606.

In short, the Dual CS606 is first-rate in its concept, construction, and ease of use. With its companion pickup, it offers superb warp-tracking capabilities. To provide that, along with fine overall performance, convenient operation, and a good price is, in our mind, an impressive achievement.

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(MORE HIRSCH REPORTS ON PAGE 31)



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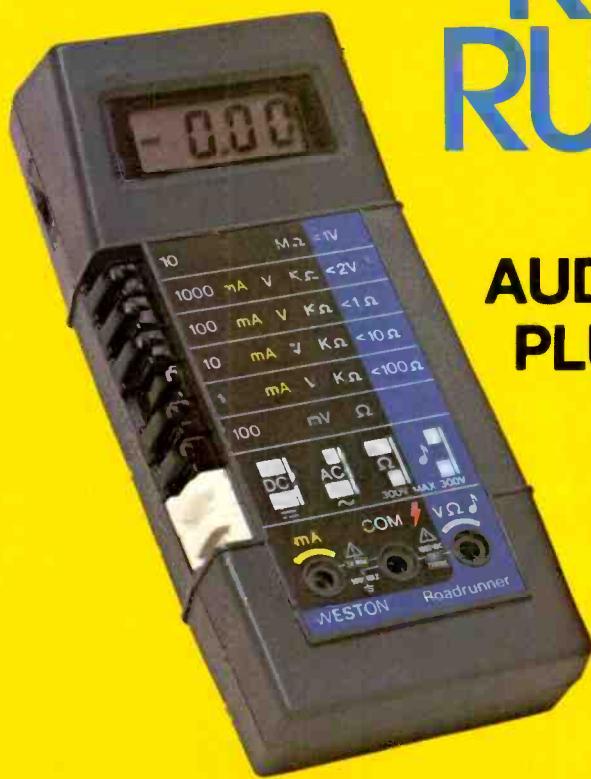
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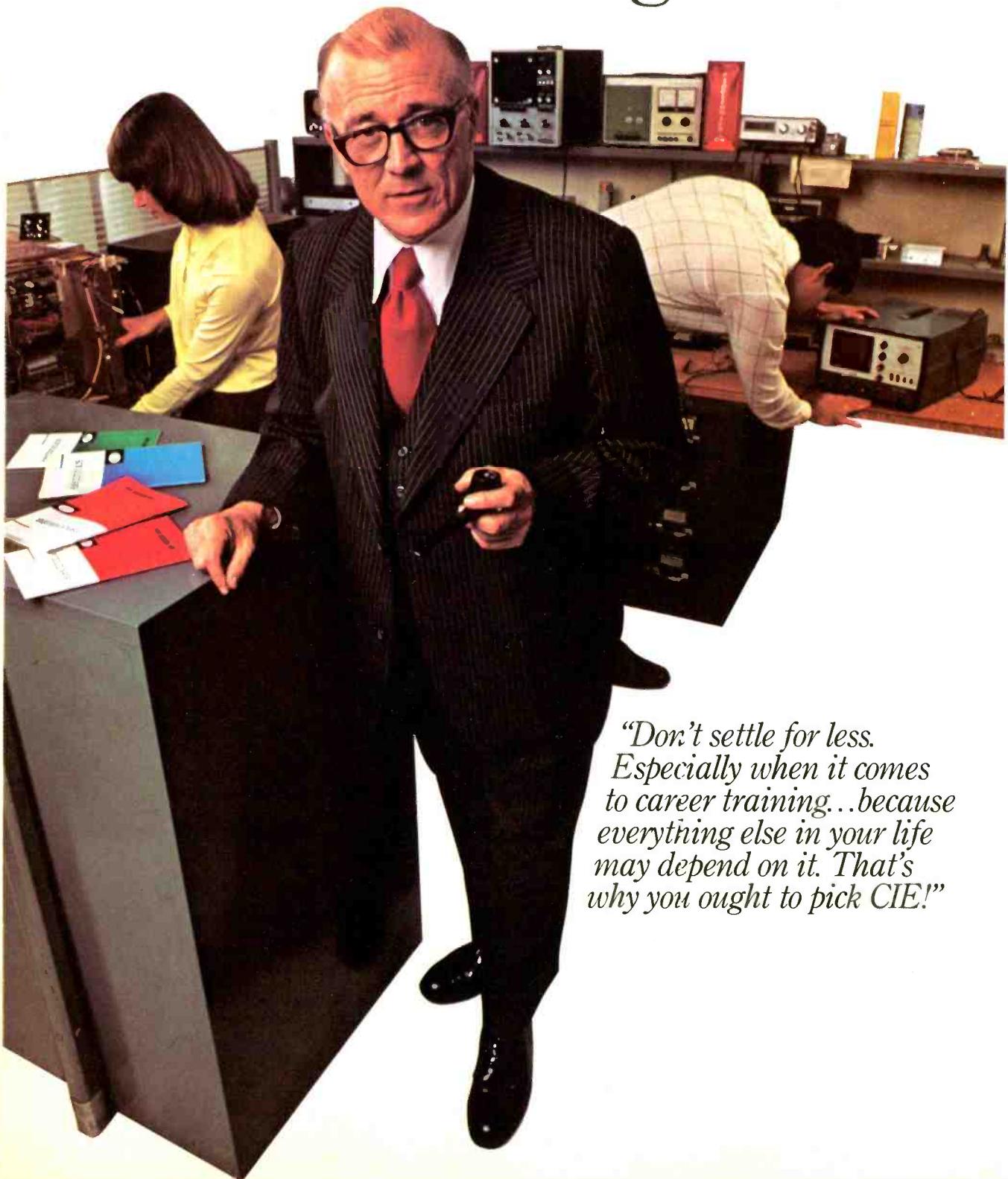
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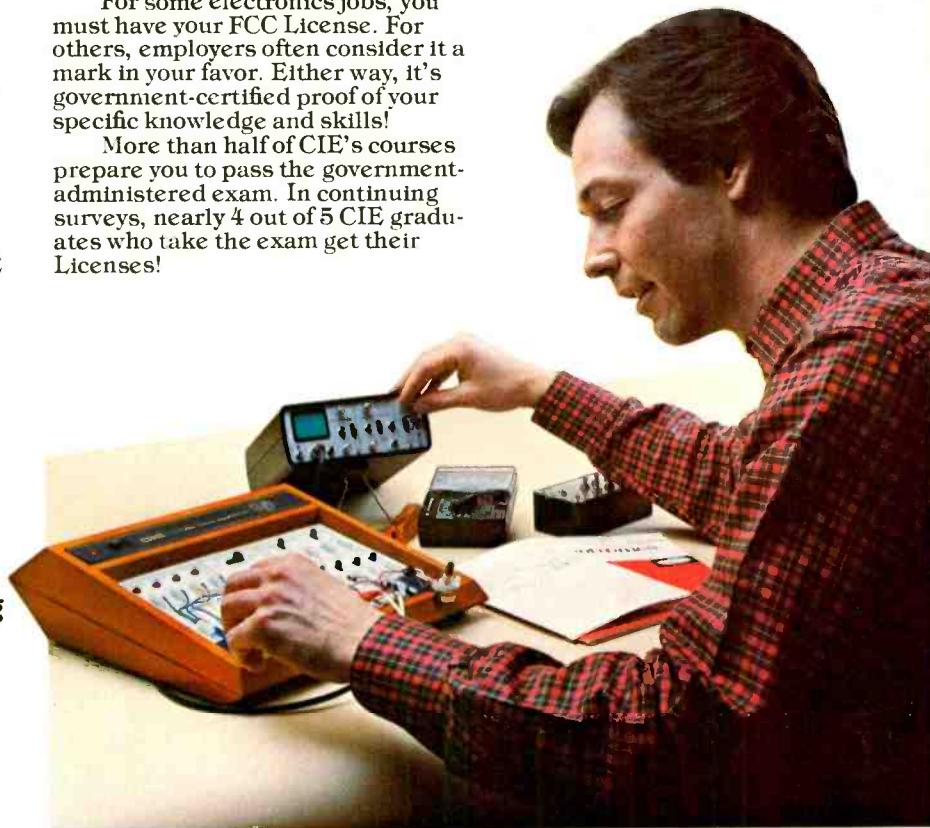
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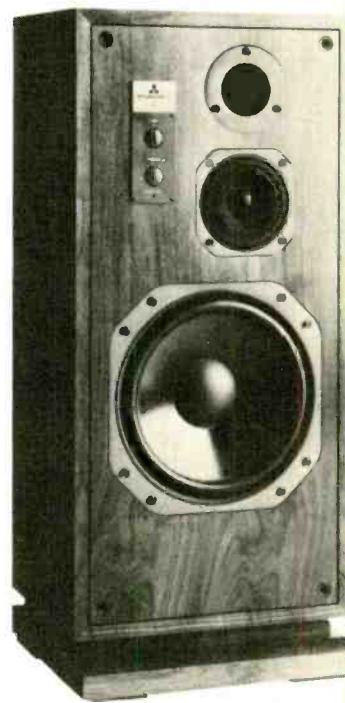
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Mitsubishi Model MS-40 three-way, floor-standing speaker system



HIRSCH-HOUCK LABS REPORT

Heading Mitsubishi's line of speaker systems is the floor-standing Model MS-40. Its 12" (30-cm) diameter woofer is

housed in a sealed enclosure and operates up to 600 Hz, where there is a 12-dB/octave crossover to a 4" (10-cm) midrange cone driver housed in a sealed subenclosure. The second crossover is to a 1½" (4-cm) dome driver at 5 kHz with an 18-dB/octave slope.

The handsome walnut-veneered enclosure measures 34⁵/₈" H X 15³/₈" W X 14⁵/₁₆" D (88 X 39 X 36.3 cm) and weighs 77 lb (35 kg). Suggested retail price is \$550.

General Description. The woofer is located about a third of the way up the front panel of the enclosure; the midrange and high-frequency drivers are positioned slightly off the vertical center line of the speaker board. Manufactured in mirror-image pairs, the speaker systems are designed for left- and right-channel operation, with the off-center drivers positioned toward the center of the listening area. Near the high-frequency drivers is a small panel with switches to adjust the levels of the two high-frequency drivers in 2-dB

steps from +2 to -4 dB and a small red LED that comes on when the system is driven to excessive levels.

The dark brown grille cloth is stretched on a wooden frame, the whole held in place by plastic snaps and supported ¾" (19.1 mm) away from the front panel. The front panel is free of bevels or recesses, and the drivers are mounted flush with its front surface to minimize diffraction effects. Spring-loaded connecting clips and a recessed pushbutton switch for resetting the system's protective circuit are located on the rear panel.

The protective circuit monitors the current passing through the drivers. Should this current become excessive, the circuit operates a fast-acting relay that greatly reduces the volume and simultaneously lights the LED on the front panel.

Nominal system impedance is rated at 6 ohms and, by IEC standards, the system can handle up to 150 watts without damage. Rated sound pressure level (SPL) is 87 dB at a distance of 1 meter with 1 watt of driving power.

One of the more novel features of the MS-40 is its honeycomb woofer construction. The honeycomb is formed of aluminum foil 20 micrometers thick, and each "cell" is 3¹/₁₆" (4.8 mm) wide and ¹/₈" (3.2 mm) deep. Bonded to each side of the honeycomb is a layer of glass-fiber reinforced plastic 100 micrometers thick. The complete structure forms a straight-sided cone that is far more rigid and lighter than paper. However, internal losses are similar to those of paper, damping the internal resonances that can occur with metallic cone materials. Mitsubishi's computer analysis of the cone indicates that it is far less subject to flexural vibration than a paper cone of similar dimensions. Additionally, the construction gives immunity to atmospheric changes that can affect the physical characteristics of paper.

Set within a cone-like recess formed by its butyl rubber edge suspension, the dome tweeter is claimed to give excellent dispersion qualities. Almost the entire interior of the MS-40 cabinet is filled with sound absorbent material, as is the midrange driver subenclosure.

Laboratory Measurements. When we spliced the semireverberant-field frequency response of the MS-40 to its close-miked bass response, the result was an unusually flat, smooth curve that varied only about ± 1.5 dB from 40 Hz to 20 kHz. A broad bass rise of about 2 dB occurred at 60 Hz, a slightly smaller rise at 1 kHz. There was a slight but definite upward

slope of the curve from about 4 to 20 kHz, where the output was up some 3 dB relative to the midrange level.

Slight departures from flatness of this magnitude are usually considered to be within the measurement tolerances of our test method and would hardly be worthy of mention. In this case, however, we were especially interested to note that the typical frequency-response curves published in Mitsubishi brochures for the speaker system had exactly the same features, specifically a bump at 1 kHz and the high-frequency rise. (Since it was made in a very large anechoic chamber, Mitsubishi's bass curve could not be expected to match ours exactly.)

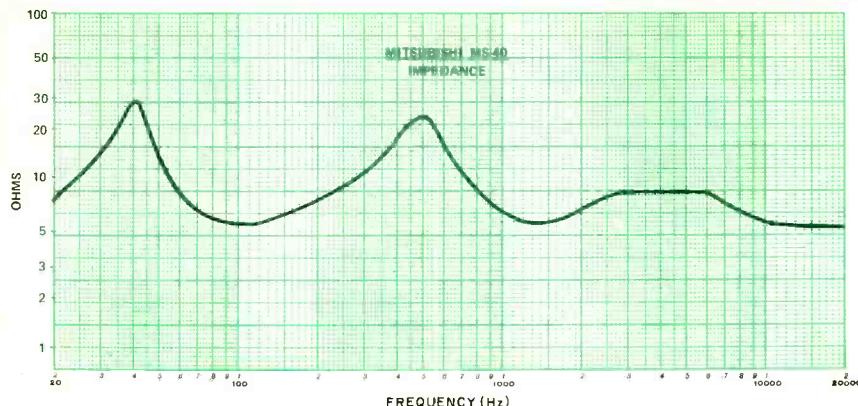
The dome tweeter had exceptionally wide horizontal dispersion, with the measured curves from the left and right speaker systems differing by less than 2 dB all the way up to 20 kHz. (The microphone was on the axis of the left system and about 30° off the axis of the right speaker.) Less than the indicated range was available from the level adjustment controls, which boosted the output by about 1 dB and cut it by 1.5 to 2 dB at the extreme settings. Only frequencies above 5 kHz were affected by the treble control, while the midrange control operated between 600 Hz and 5 kHz. As might be expected, the audible effect of these switches was very subtle.

Impedance was correctly rated at 6 ohms, which was the measured minimum impedance at 100 Hz and 1.3 kHz, and above 10 kHz. Impedance maxima were 30 ohms at 40 Hz and 22 ohms at 500 Hz. Speaker sensitivity, 89 dB at a 1-meter distance with a driving signal of 2.83 volts of random noise in an octave centered at 1 kHz, was relatively high for an acoustic-suspension speaker system.

Low-frequency distortion, at a 2.83-volt level (1 watt into 8 ohms) was very low in the midbass range: 0.13% at 100 Hz to 0.5% at 50 Hz, rising to 3.2% at 35 Hz and 6.3% at 30 Hz. A 10-dB power increase resulted in distortion readings ranging from 0.28% at 100 Hz to 0.89% at 50 Hz and to 6.3% at 35 Hz. The toneburst response was generally good, being relatively free of ringing and other distortions over the full range of the system and fairly independent of microphone positioning.

User Comment. The Mitsubishi MS-40 is a very fine system, with very low distortion and smooth, extended frequency response that is rare in loudspeakers. Listening to a pair of MS-40s for some time, we tried to identify a sound quality that would particularly characterize them, but never found any.

Because of their weight, we were not tempted to move the MS-40s around to judge the effect, if any, of their asymmetrical driver placement on the sound. We would expect it to be minimal at best, since the high-frequency/midrange driver axis is less than 2½" (63.5 mm) off the center axis of the front panel. In view of the emphasis Mitsubishi places on the flat, nonbeveled speaker board and flush-mounted drivers, it seemed strange to find the grille, with its wooden frame, supported in front of the speaker board so as



Impedance curve shows rated 6 ohms at 100 Hz and 1.3 kHz and above 10 kHz.

to place a 3/4" wide slot along each side of the speaker front. The effects of this, if any, were not audible to us, nor did we hear any change in sound with the grille in place and removed; but it does suggest that some of the other "steps" taken to

minimize diffraction may not have been entirely necessary.

We found the MS-40 to be a relatively uncolored speaker system, whose neutrality, though a virtue to a purist, might not appeal to a listener who prefers such pop-

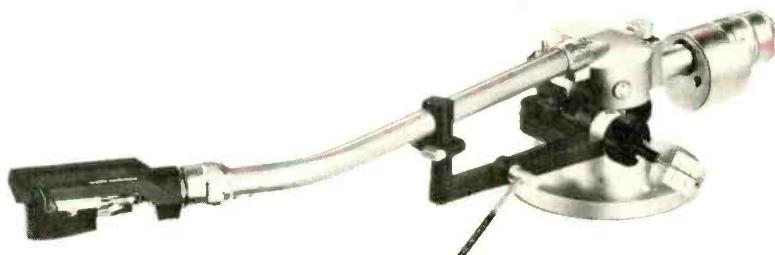
ular colorations as a soft, heavy bass or sizzling highs. The low bass is certainly all there, but it is tightly controlled, and the treble is clear without being "tinkly."

We checked out the overload protection system with a moderate-powered amplifier (70 watts per channel) which, when driven beyond clipping, shut down both speaker systems. The acoustic levels were, at that point, well in excess of what was tolerable. Under reasonable conditions of drive, the system is capable of generous acoustic output. Sounds can be heard after the relay has operated, but they are weak and distorted. A push on the reset button on the rear of the cabinet restores normal operation, leaving the speaker system in good condition.

Our overall assessment of the Mitsubishi MS-40 is that it is a high-caliber speaker system with unusually low coloration and very good dynamic range. Its price seems reasonable in light of its performance both in our lab and under actual listening conditions.

CIRCLE NO. 102 ON FREE INFORMATION CARD

Audio-Technica Model AT-1010 tonearm features adjustable damping device



Designed to enable a cartridge to trace the most difficult recorded passages, the Audio-Technica AT-1010 tonearm is free from many of the limitations normally imposed by interactions between cartridge and arm. One of its special features is an adjustable damping device for controlling the effect of low-frequency arm/cartridge resonance. The tonearm's shape and its relationship to the pivot axes are designed to minimize warp wow and frequency intermodulation (FIM) distortions that can be generated when record warps alter the normal tracking geometry.

A template simplifies locating the arm base relative to the center of the turntable. Other installation aids included are used

for setting stylus overhang for minimum tracking error and tilting the cartridge so that its stylus is perpendicular to the surface of the record. The headshell accepts almost any cartridge that has 1/2" (12.7-mm) mounting centers and weighs between 4 and 14 grams (14 to 24 grams for a cartridge mounted in its own headshell). The headshell is the standard 4-pin plugin type with locking ring. Suggested retail price is \$350.

General Description. The J-shaped aluminum tonearm tube is about 9 1/2" (241.3 mm) long, from pivot to turntable center, and moves on precision ball bearings. Made of die-cast magnesium alloy, the MS-10 headshell has a rubber-covered top to damp out resonant modes. Position of the plug in the end of the shell can be

adjusted over a range of at least 3 mm, by loosening a setscrew, to permit setting stylus overhang.

Unlike most headshells, that of the MS-10 is not slotted. Instead, it has three pairs of tapped holes for the cartridge mounting screws. Normally, the center pair of holes is used, but if correct stylus position cannot be reached by adjusting plug position, one of the other sets of holes will make this possible.

The arm tube is located above the vertical pivots, to locate the stylus in the plane of the pivots when playing a record. This minimizes warp wow and any change of vertical stylus angle that might occur when the pickup rides over a record warp.

The counterweight carries the tracking-force scale, calibrated from 0 to 2.5 grams at 0.1-gram intervals, and is threaded onto the rear extension of the arm tube. The rear of the arm tube is elastically isolated from the front portion. Hence, the suspended mass can supply antiresonant compensation for the main low-frequency resonance between total effective arm/cartridge mass and the compliance of the cantilever mount. A small knob on top of the arm pivot structure provides adjustable damping of the low-frequency resonance, apparently varying the stiffness of the elastic coupling between the two sections of the tube.

Extending to one side of the pivot is a balance weight that compensates for any lateral unbalance that might cause a side torque on the arm if the turntable is not leveled. Balance weight position is determined by total head shell and cartridge mass. Within the lateral balance weight is another "gyrobalance" weight that can be shifted vertically to alter the vertical swing

period of the arm. Its function is to minimize the up and down motion of the arm when playing warped records. As Audio-Technica points out, neither the lateral nor the gyrobalance would be needed, nor would they have any effect, if the turntable were level and the record were unwarped, but they serve a useful purpose in the more usual case where neither ideal condition exists.

Antiskating compensation is applied to the tonearm by a pivoted lever extending from the right side of the base. A weight on the lever can be set for elliptical, line-contact, or spherical stylus shapes, and the entire assembly rotates to set a number that matches the tracking force opposite an index mark. Angular position of the weight changes with arm location on the record. We assume that the operating principle of the Audio-Technica device is similar to the "weight-on-a-string" mechanisms used on other tonearms.

The arm-lift cueing lever, on a support that extends forward of the arm base, raises and lowers the tonearm with a very smooth, damped motion in both directions. The arm rest is built into the forward part of the support and includes a lock button to prevent the arm from being accidentally dislodged.

Although installing a tonearm on a motorboard is rarely easy, accessories supplied with the AT-1010 make this a relatively foolproof operation. A template

locates the base of the arm, which can be fastened to the motorboard with wood screws or bolts and nuts (both supplied). We suggest making the clearance hole for the arm post a little larger than the indicated 23 mm, since only a limited range of cartridge adjustment is possible when setting stylus overhang. Final arm position is set with the aid of a plastic gauge inserted into the socket in the end of the arm and located exactly over the turntable center spindle. Arm height is adjustable over a considerable range to accommodate almost any cartridge and turntable dimensions. When arm and headshell have been installed, the shell is rotated with the aid of another plastic gauge to make the stylus perpendicular to the record, as viewed from the front.

The signal cable assembly furnished with the AT-1010 has a plug that securely locks into a socket at the bottom of the arm post. At the free ends of the cable are high-quality gold-plated phono plugs. Audio-Technica points out that all wiring in the arm and cables is made of high-conductivity sterling silver, and all internal electrical contacts are gold-plated.

Laboratory Measurements. We installed the AT-1010 on a good-quality turntable, with an ADCOM XC-LT moving-coil cartridge in the headshell. We followed the instructions carefully and setup procedure went smoothly. Tracking force was set to

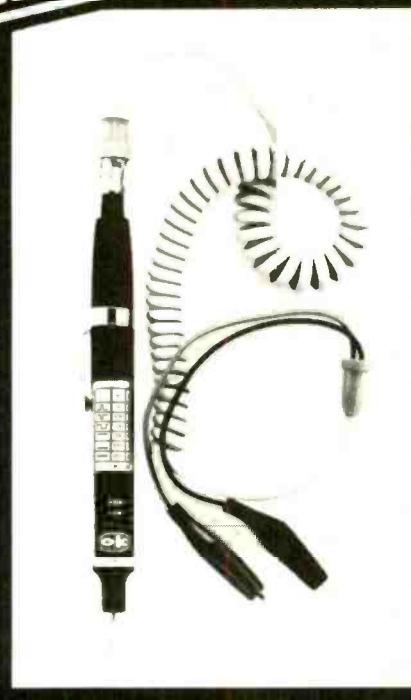
the 1.8 grams needed by the cartridge.

Tracking-force scale calibrations were accurate within 5% to 8% over the full range of adjustment, with a typical error of less than 0.1 gram. Rated at 1.5° maximum, the tracking error reached that value at radii of 3" and 6" (76.2 and 152.4 mm). More to the point, the error was always less than 0.5° /in. of radius and over much of the record was too small to measure.

Antiskating compensation had to be set to its maximum of 2.5 grams to give equal distortion in both channels when we operated the cartridge at a 1.8-gram vertical force. The setting is not critical, but like most antiskating systems this one should be set slightly higher than the tracking force. The cueing device worked with exceptional smoothness, partly because of the slight time delay between movement of the lever and first motion of the arm. It is impossible to move the arm suddenly with this system. However, there was a moderate outward drift during descent, caused by antiskating torque. About 14 seconds of a record was repeated each time the arm was raised and lowered with the cueing device.

Effective arm mass, less cartridge, was about 18 grams, which is an average figure for tonearms of conventional design. We measured the low-frequency arm/cartridge resonance with the adjustable damping set to minimum and maximum limits and observed no change in resonance

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response, which was at about 9 Hz and had an amplitude of about 5 dB. Capacitance to ground in the arm and cable wiring was about 90 picofarads per channel, and the interchannel capacitance was a low 2 picofarads.

User Comment. If one were to judge the AT-1010 tonearm solely from the measurements we have described, there would appear to be little to distinguish it from most other arms, many of them less costly. The workmanship of the Audio-Technica arm is exemplary, but one chooses a tonearm for how effectively it permits records to be played, not merely for its styling or construction.

We played a number of records with the combination of the AT-1010 arm and the ADCOM cartridge, and they certainly sounded excellent. This was inconclusive, since the cartridge was also new to us, and undoubtedly had more to do with the final sound than did the arm.

Since the design of the AT-1010 places unusual emphasis on control of arm motion when playing warped records, and under the influence of the low-frequency arm/cartridge resonance, we concentrated on those performance aspects. The results of our tests were, to say the least, surprising and gratifying.

The variable damping control had no effect on the measured output in the vicinity of resonance or on visible displacement

of the arm or sound when we played our collection of badly warped records. The same comment applies to the adjustment of the lateral balance and gyrobalance weights, neither of which had any detectable effect on the system. (Of course, we carefully leveled our turntable before making our tests, which would account for the lack of measurable, visible, or audible effects. These features are built into the tonearm to deal with less-than-ideal conditions, as when the turntable is not level.)

We did not expect the tonearm to cope too effectively with our badly warped records, that in the past have tossed every combination with effective mass comparable to the AT-1010 and ADCOM completely off the disc. Most often, the AT-1010 behaved as though the warp was simply not present. It lifted to follow the warp, and seemed to cling to the record as it descended the trailing side. Usually, not even a "thump" was heard from the speakers. Clearly, the damping was highly effective, and the 9-Hz resonance frequency was close to the optimum for tracking most record warps. Warps we used ranged from a once per revolution with a 10-mm amplitude to shorter warps that imparted a quick but violent "jiggle" to the pickup.

To isolate as much as possible the properties of the arm from those of the cartridge, we substituted an Audio-Technica AT-25, a highly compliant cartridge in

its own headshell that tracks at 1 gram and could be expected to significantly lower arm resonance (we did not measure resonance with this cartridge). Results were almost identical, although there was more visible arm motion every time it passed a warp and an occasional backward skipping of one groove under the influence of the antiskating torque. However, no tonearm and cartridge combination with an effective mass of more than 20 grams had ever been able to play these records without groove jumping or an audible wow.

Our conclusion, then, is that the geometry of the AT-1010 arm—including the various balance devices, relationship of the stylus to the vertical pivot axis, and any damping supplied by the decoupled rear section of the arm—gives this tonearm an above-average ability to play difficult records. Although we were unable to detect any variation in the arm's performance over the full range of adjustment of these damping and control features, it is possible that under some circumstances they could have made a difference. In any case, it is reassuring to know that, even with random settings of most of its adjustments, and with cartridges of high or low compliance, the AT-1010 can give superior tracking of less-than-perfect records. This arm's price carries with it a corresponding level of performance.

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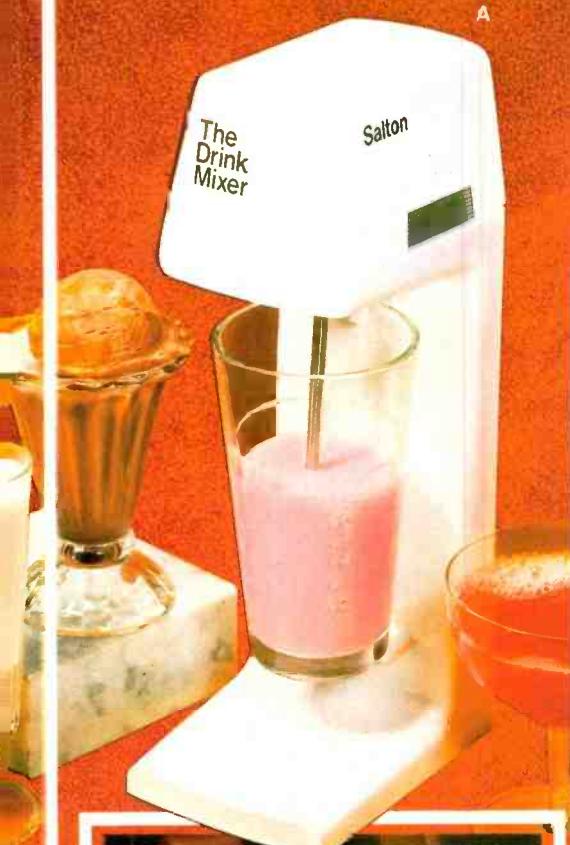
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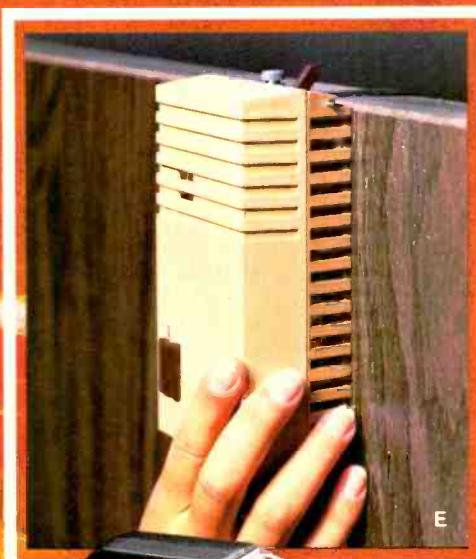
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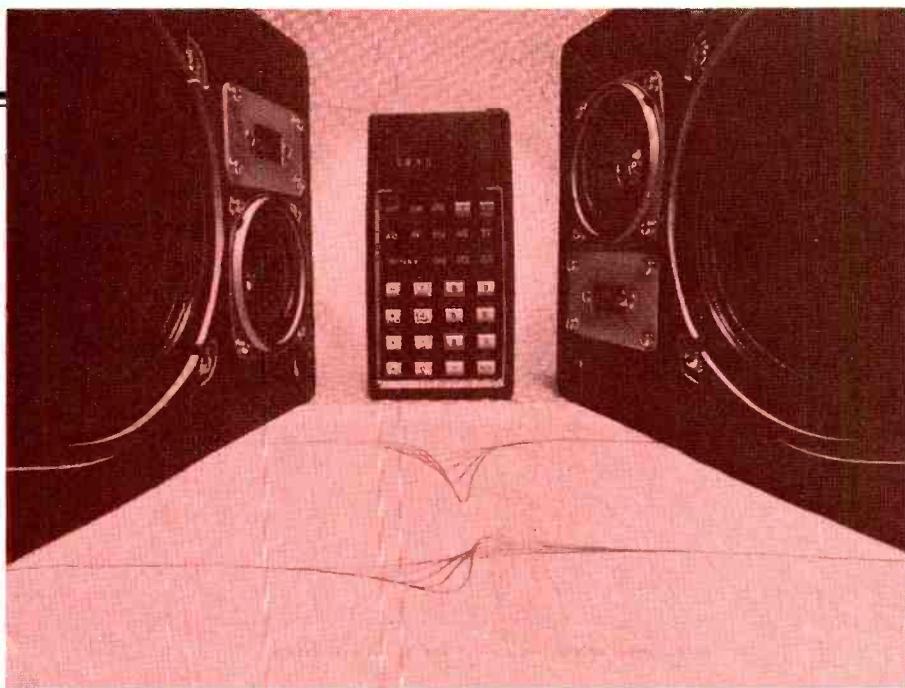
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Focus On **LOUDSPEAKERS**

● Enveloping audio transducers in an air of mystery seems almost a time-honored tradition. Loudspeakers, phono cartridges, and, to a lesser extent, microphones are often viewed as though their selection and use involved some kind of ineffable magic not to be understood by mortals or—worse—quantified.

Loudspeakers, are the most mysterious of the lot, for while measurements are dutifully made and data published, meaningful correlation between these and the sound of the product seem most notably absent. Though the idea may horrify some, it is not unreasonable to select, say, a power amplifier on the basis of its specs. But only a devoted optimist would buy a loudspeaker that way.

The first two articles of this Focus are aimed at applying some science to the loudspeaker conundrum, hoping to find out how the present situation came about and how it may be altered in the future. Two highly qualified authors discuss, each in the light of his own expertise and point of view, the problems of quantifying and predicting the audible performance of loudspeakers. Neither has fully resolved matters; in fact, while each does provide some answers, new questions seem far more numerous. Both point out, however, some interesting directions for exploration.

Part III of this section is a construction project for a three-way electronic crossover.—*Harold A. Rodgers, Executive Editor*

The Conflict Between Sound and Specs

BY DANIEL QUEEN

Daniel Queen Associates, Chicago, IL

I.

The Objective View

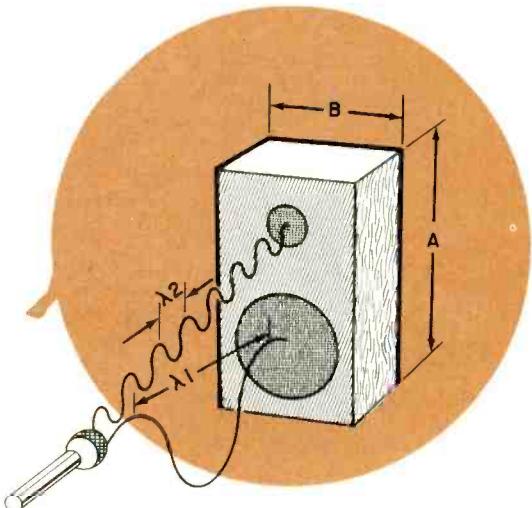


Fig. 1. The microphone is in the far field for the short-wavelength (λ_2) radiation of the tweeter. But when λ_1 , the wavelength of the woofer radiation is comparable with cabinet dimensions A and B, the microphone is in the near field. Balance between the drivers can be falsified by such microphone placement.

RARELY can the audible performance of a loudspeaker be accurately deduced from its published specifications or any of the measurements customarily made. Normally any correlation between the two appears more accidental than otherwise. It seems ironic, therefore, that controversy surrounds a point as abstruse as amplifier slew rate when seemingly elementary matters of measuring frequency response and distortion in loudspeakers are far from settled.

One way to measure the effective performance of a loudspeaker would be to place the microphones in the ears of a listener. But what listener? And in what listening room? Such questions make a loudspeaker more difficult to measure than an amplifier, recorder, or even a turntable and phono cartridge. In fact, the loudspeaker measurement encompasses most of the problems of those components and several more.

Frequency Response. A loudspeaker is analogous to an antenna. In fact, the laws defining the radiation patterns of the two are virtually identical. Nevertheless, the loudspeaker, for several reasons, is the more complex device.

While an antenna radiates a narrow band of frequencies into a fairly well-defined space, a loudspeaker must radiate any frequency in a 10-octave band into a room that may have one of a myriad of shapes and sizes. An antenna equivalent to a loudspeaker would be designed to operate on any tower with constant gain from 1.0 MHz to 1.0 GHz—i.e., broadcast to microwave—without varying its coverage pattern.

Obviously, then, the on-axis data usually given by manufacturers are only expedient simplifications. At best, they are useful only to compare loudspeakers for production quality control; at worst, they can seriously mislead the prospective buyer. To come even close to characterizing a speaker, a great many more measurements are needed.

To measure any one quantity, or variable, it is necessary to concentrate on it alone, holding all others constant. Those held constant are called parameters. In an electrical measurement, parameters may include characteristics such as supply voltage, ambient temperature and humidity, and load impedance. Parameters of loudspeaker measurement, in addition to these, include boundary conditions, positions of the speaker and sensing device, measurement time, and even the size and shape of the sensing device.

Traditional practice has minimized boundary conditions by measuring in an anechoic chamber. In such an environment, reflections are of negligible amplitude. Next, on the assumption that listeners will place themselves on the central axis of the loudspeaker, an on-axis microphone position is chosen. Such conditions should yield measurements which can be reproduced at many different facilities and which, though limited in the information they provide, can be applied to any loudspeaker.

However, the next assumption is that a single measuring distance may be used—usually three meters (or 10 ft. in some U.S. specifications) from the face of the loudspeaker. In the often published EIA sensitivity specification, the measurement at this distance is then extrapolated to 30 feet. Implicit in this extrapolation is

both the realization and the disregard by the writers of the EIA standard that three meters is not in the "far field" of a loudspeaker whose dimensions are appreciable fractions of that distance. Thus, another parameter is introduced: the size of the loudspeaker. To properly understand its importance, we must first examine another concept.

Sound Fields. There are three ways to look at the sound fields in the path from a loudspeaker to a listener. The first depends on the loudspeaker and listener themselves and the second on the environment (boundary conditions) in which they are placed. The loudspeaker and listener have a *near field* and a *far field*. The size of these fields as a function of distance increases with wavelength. (See Fig. 1.) At any one frequency and in one direction from the source, it can be determined whether one is in the near or the far field. In the absence of reflections, output will change inconsistently with increasing distance in the near field, whereas in the far field it will drop 6 dB per doubling of distance (more precisely, 20 dB for a tenfold increase). Thus, the disregarded assumption in the EIA specification is that a near-field measurement of a loudspeaker can be extrapolated to the far field.

The second way to describe sound fields is in terms of the environment in which the loudspeaker and listener are placed. Three fields are generated: the direct, the early-reflected, and the late-reflected fields. The direct field is formed of rays directly from the speaker that the listener intercepts (or might intercept) before they are reflected. This is the only field present in a perfect anechoic chamber. The early and late reflected fields are defined in relation to characteristics of human hearing. A reflection arriving late enough to be heard as distinct echo is described as late; if early enough to seem fused with the direct sound, it is described as early. (See Fig. 2)

A third set of fields—the spatial fields—is also defined by the boundary conditions. They are categorized by the segment of a sphere through which sound can radiate from (or towards) the device under measurement. Mounted in the center of an ideal anechoic chamber, it radiates into a free field, 4π - or full-space. A speaker set in an infinite wall radiates into 2π - or half-space; at a wall-floor intersection it works into π - or quarter-space; in a corner, it would radiate into eighth-space. This is shown in Fig. 3. If there are an infinite number of reflections from random directions, it radiates into a perfect reverberant-field, full-space. Like the near field, the spatial fields are also functions of wavelength and radiator size.

What Measurements to Use. "Anechoic" free-field measurement is based on the idea that only the direct-field is of importance in listening. In contrast, the method of frequency-response measurement called "power response", made in a true or calculated reverberant field, assumes that only the reflected sound is important. It also does not differentiate between the early- and late-reflection fields. But a measurement system should be based on correspondence to the actual listening situation. Are we sensitive to direct sound, early sound, or late sound? Do we listen to a loud-

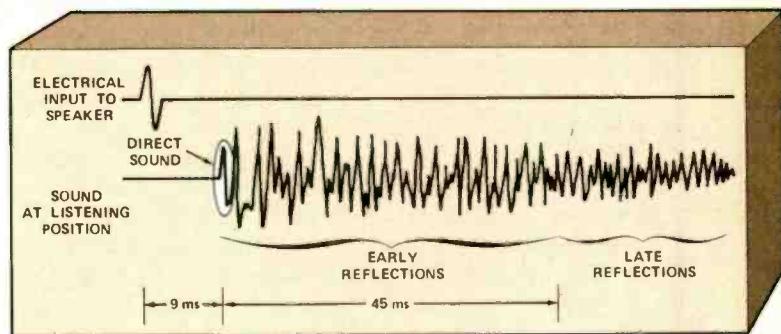


Fig. 2. A single-cycle input to a speaker in a normally "live" room produces a drawn-out train of impulses as numerous room reflections reach the measuring microphone.

speaker in its near field or its far field? In a half-space or full-space? Unfortunately, the answer is: all of the above. Although acoustical scientists differ as to relative importance of these fields, they agree that the listening experience involves them all.

There is no question that much of the directional information of the loudspeaker comes from its direct field and early reflections. In living-room size listening spaces, it is also possible that much of the perceived spectral balance of the loudspeaker comes from the direct field and the early sound that dominate such a room to the relative exclusion of late sound. On the other hand, in a large space, there is a great deal of late sound and relatively few early reflections. Thus, a loudspeaker which sounds pleasant in a small room

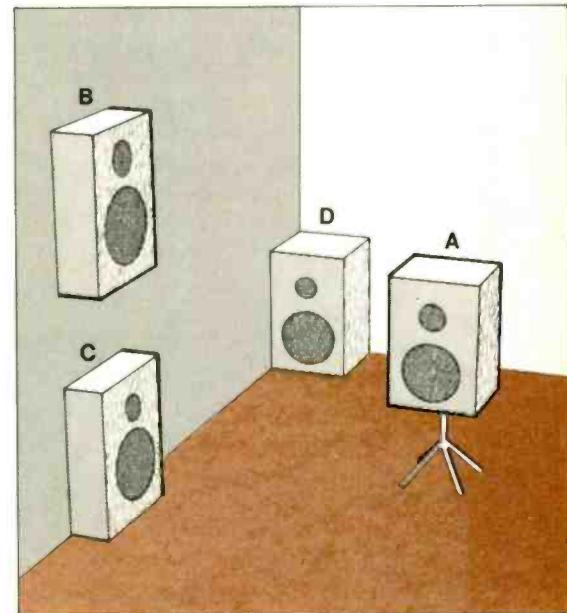


Fig. 3. Spatial fields of a loudspeaker. Loudspeaker A radiates into full-space, B into half-space, C into quarter-space, and D into eighth-space. These designations are approximate in that the dimensions of the drivers are ignored. In a practical case, D, for example, may have its response altered by positioning of the woofer in eighth-space, while the tweeter (because of its dimensions) is in full-space.

may be very poor in an auditorium, and vice versa.

In regard to distance, a very small loudspeaker system would almost always be listened to in the far field. However, larger systems may actually be intended to be heard in the near field. This would certainly be true of large planar or panel-type speakers used in small rooms. Thus, by juggling all these parameters, one can generate a plethora of efficiency and frequency-response data for a loudspeaker. A manufacturer could possibly be tempted to publish the best curve he dared and adjust measuring parameters to produce that curve. However, a more useful approach would be to base the choice of parameters on the design of the speaker and the intended listening conditions.

Distortion. Distortion products are generally unwanted frequencies elicited in response to a test signal. If one regards the task of quantifying them as a special type of frequency response measurement, the problems are at once apparent. All of the difficulties already mentioned apply, along with a few more that can cause distortion products to be temporally or spatially displaced with respect to the test signal. Worse yet, some, like turbulence noise in a bass vent, contain many incoherent frequencies so that there are few clues as to where to look for them in the spectrum.

Time delay is representative of distortion that is position-sensitive. A loudspeaker can have its drivers fixed on a panel with respect to one another so that the time of sound arrival is constant with frequency at an on-axis position. Yet there may be serious time errors as one moves to either side. Similarly, frequency modulation (FM) distortion, which occurs when a driver radiating a high frequency is moved back and forth by a low frequency and thus varies the high frequency by Doppler effect, can be substantial on-axis but less off-axis. If the listener receives a large amount of early sound reflected from all directions toward which the loudspeaker radiates, on-axis measurement of FM may not match the real listening conditions.

Distortion arising from cone motion causes another problem. Frequency response is usually measured at small signal levels. However, the loudspeaker must radiate large signals too. A good frequency response for small signals may deteriorate as power increases, or distortion may rise to the point where the

response at some frequencies is no longer useful.

Perhaps the nondirectionality of bass frequencies will free us of positional problems—but is such output really nondirectional? Certainly, if we attach a tire pump to the room and increase the static pressure, the pressure will equalize quickly throughout the room. That would be the dc, 0 hertz, or infinite wavelength condition. But as wavelengths approach finite size, directional effects occur. The question is: the finite size of what? The cone . . . the baffle . . . the wall behind? Again, the answer is all of the above.

Often, the bass characteristics of a loudspeaker are measured in the near-field. It can be shown that where wavelengths are substantially larger than the dimensions of the speaker in the cabinet, the near-field and far-field response are essentially equivalent. However, a microphone in the near field of a woofer must be very close to the cone. The limitation to very small cone excursions as a result of this positioning rules out measuring the large-signal properties of the loudspeaker. Furthermore, radiation from a vent or spurious emissions from the cabinet walls will not be included in the measurement. It becomes necessary to make measurements of all of these sources, both in amplitude and phase, and then to mathematically calculate the total radiated power. This is particularly complicated when the near-field technique is used to measure distortion. If the microphone is far enough from the cone to allow full excursion at the fundamental frequency, it may be in far field for the distortion products, which have smaller wavelengths. Differences in the distortion from vents or cabinet sides will also become difficult or tedious to calculate.

The Test Signal. Once a satisfactory set of testing parameters has been decided upon, it is necessary to make a choice of input signal. This is a critical matter, for a poorly chosen test signal can make interpretation of the results difficult or impossible.

For example, if a frequency-response test is made in a free-field environment, a swept sine wave is an adequate test signal. However, in a reverberant field, a sinusoidal signal would superimpose the standing waves of the room on the speaker response. A warble tone or broadband noise signal would overcome this difficulty; but, as both of these signals vary with time, averaging is required. Not only will it be necessary to decide upon the details of the averaging (time constant, etc.), but also the bandwidth covered by the warble or the noise. The goal is to smooth out variations contributed by the room while preserving the salient features of the loudspeaker.

Most reverberant-field responses, such as those called power responses, are made with long averaging times in one-third octave bands. The rationale is that third-octave bands are close to what is called critical bands of masking. These are interpreted as the bandwidth of noise in which an equal-power pure tone would be just detectable by a human listener. Unfortunately, critical bands have been shown to be considerably narrower than third-octave bands particularly in the region where hearing is most sensitive (roughly 800 Hz to 5 kHz). To make measurements that would accurately reflect variations in the narrowest critical bands, it

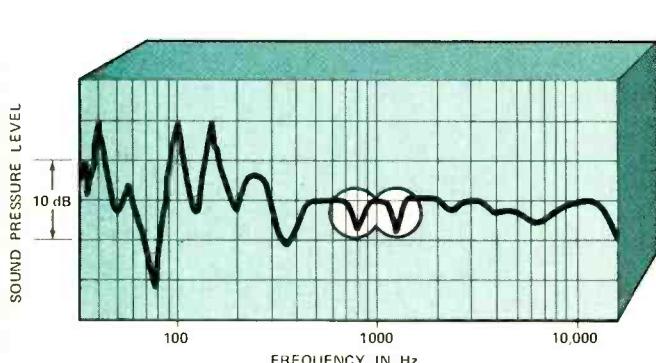


Fig. 4. Human hearing is rather tolerant of frequency-response variations at low frequencies and might often let peaks and dips below 200 Hz pass unnoticed. Smaller dips (unshaded area) in the midrange would be far more disturbing.

would be necessary to use one-tenth octave noise bands. Figure 4 shows that, while fairly large variations in the upper bass frequencies may pass undetected, our hearing is very intolerant of variations in the 800-to-5000-Hz range.

Similarly, any analysis of absolute phase and time differences—or any other variables—must be related to the detectability of these variations by human ears in the listening room. The analysis must indicate how this detectability will vary with the positions of the listener and loudspeaker in the room.

The Input Side. So far, we have only discussed the speaker's output, but interface with an amplifier is also a necessity. The usual measure of this interface is the loudspeaker impedance, which is often cited as a single figure. However, it is well-known that this impedance varies substantially with frequency and, more important, becomes more or less reactive. Thus, an amplifier may be confronted with a resistive load at some portions of the range and almost purely reactive loads over other portions. Depending on the amplifier design, such variations may cause such ills as prema-

ture clipping, distortion, and instability. It is possible, therefore, that a loudspeaker will sound excellent with one amplifier and raucus with another not capable of withstanding severe impedance variations. A complete impedance curve, then, would show not only the magnitude of the impedance but its phase as well.

In Conclusion. It might be tempting to conclude that quantitative specification of loudspeaker performance is virtually impossible, but the truth is that the process is merely very difficult. Most manufacturers' literature has little significance. Nevertheless, many of the shortcomings of these data are known and can be overcome. As measurements now being made in loudspeaker development laboratories are correlated with subjective responses, the relations between these hitherto mutually exclusive domains are becoming better known. Thus, the correct parameters for loudspeaker measurement will gradually become known and reflected in standardized measurements. Given this, it will eventually become possible to publish specifications that indeed indicate the subjective quality of a loudspeaker system. ◇

FOR MOST listeners, high-fidelity music reproduction means duplicating the sensation of being at an actual performance. This is usually what we remember about the first time we heard high-fidelity equipment: realism. But realism cannot be measured; it is subjective, inside the listener. It is the feeling that the experience we are having corresponds to another, earlier experience that is being duplicated.

Sooner or later, most seekers after high-fidelity music reproduction discover that different loudspeakers of reputable manufacturers reproduce what should be the same sounds quite differently. Some decide to judge which is the best to buy by listening and comparing the realism of one speaker system to that of another. Others equate realism with accuracy—that is, objectively measurable fidelity—and try to choose the loudspeaker they are going to buy by comparing published specifications, which means, most often, frequency response.

Anyone trying to make a purchasing decision on the basis of manufacturers' published specifications needs a good sense of humor. One speaker system, listed at \$7000, is said to have a frequency response from 25 to 18,000 Hz, ± 2 dB. These are good specs, but a darned high price. And how about one that goes from 26 to 25,000 Hz, ± 2 dB, and costs only \$150? Another spans 27 to 25,000 Hz, no dB, for \$149; you save a dollar over the closest competition, but lose a hertz and get no dB. Yet another, for \$2200, responds from 13 to 52,000 Hz—that's right, 52,000. How can they do it for so much less than \$7000? Probably by leaving out the number of plus or minus dB.

II.

BY ROBERT BERKOVITZ

Teledyne Acoustic Research, Norwood, MA

The Subjective View

Measurements vs Reality. Listeners want specifications, and so they get them—the best that manufacturers can provide. But do frequency-response measurements have anything to do with the way in which loudspeaker systems are used by their owners? To measure the frequency response of a loudspeaker, it is fed an electric signal containing all audible frequencies in exactly equal amounts. A microphone picks up the output of the loudspeaker and delivers a corresponding electric signal to measuring equipment. If the loudspeaker reproduces signals accurately, then the measuring equipment will show equal levels at all audible frequencies. At least, that is the idea expressed in its simplest form.

Even without much technical understanding, one soon notices that frequency-response data from manufacturers is always quite impressive. Lower-priced speaker systems show a little less bass or treble than higher-priced units, but still seem nearly perfect. If these published data are correct, all loudspeakers should sound alike. Why don't they?

Without a doubt, engineers learn a great deal about

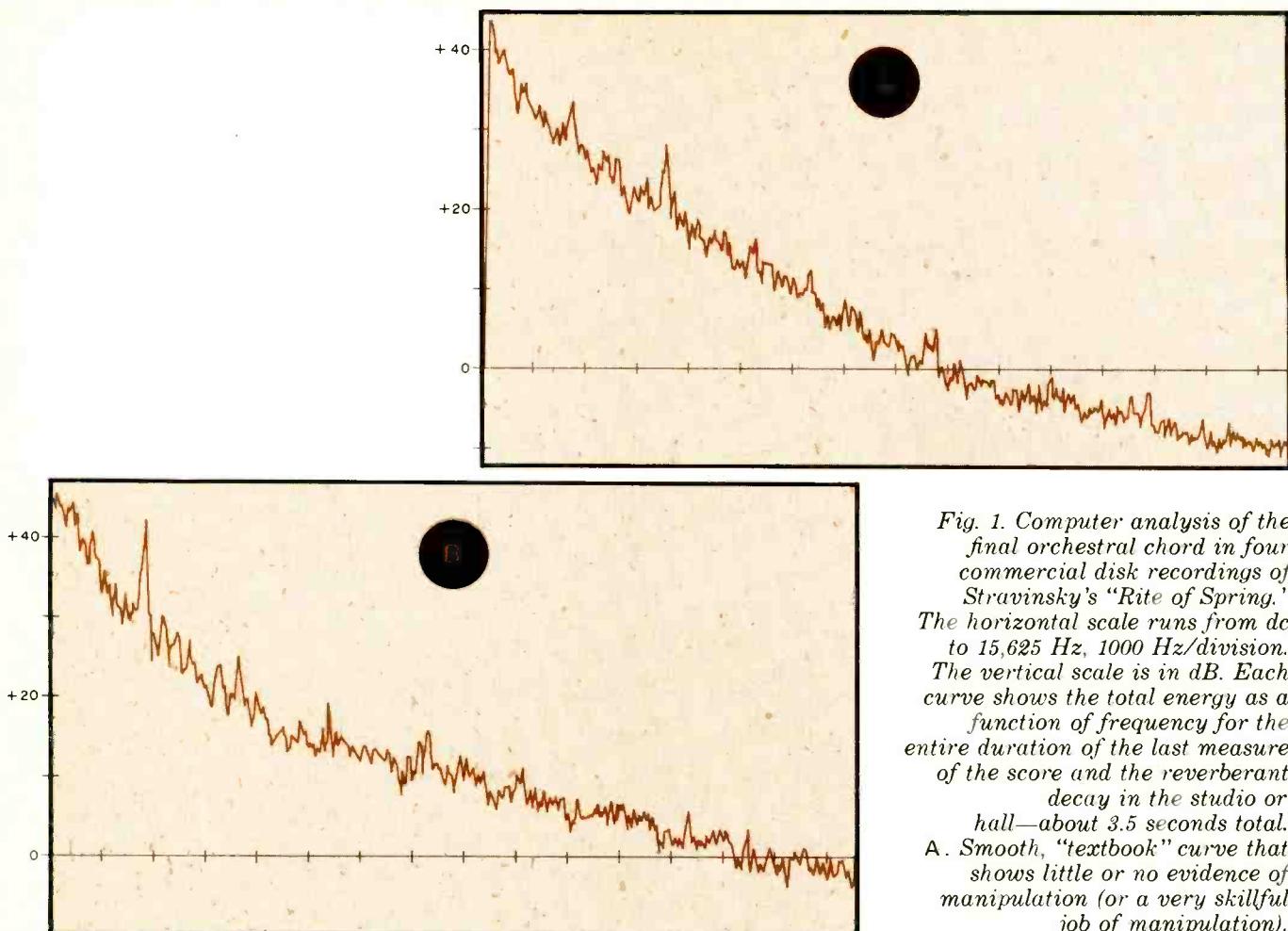


Fig. 1. Computer analysis of the final orchestral chord in four commercial disk recordings of Stravinsky's "Rite of Spring." The horizontal scale runs from dc to 15,625 Hz, 1000 Hz/division. The vertical scale is in dB. Each curve shows the total energy as a function of frequency for the entire duration of the last measure of the score and the reverberant decay in the studio or hall—about 3.5 seconds total.

A. Smooth, "textbook" curve that shows little or no evidence of manipulation (or a very skillful job of manipulation).

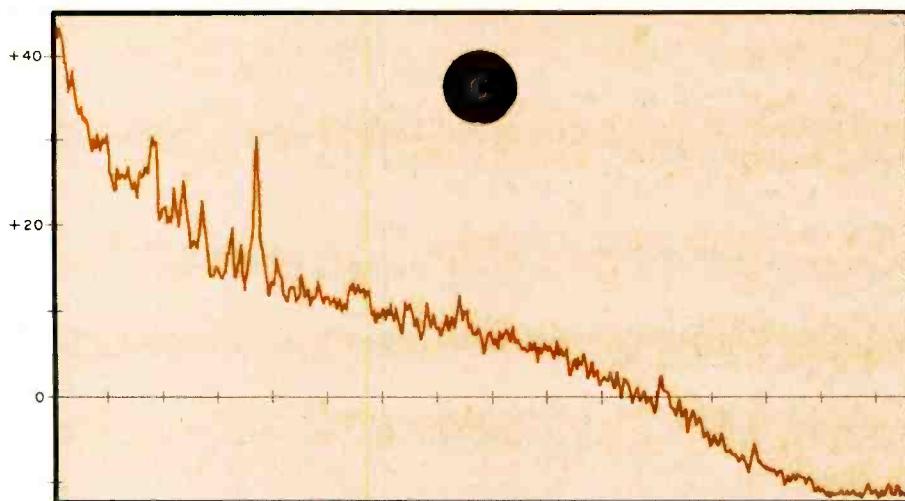
loudspeakers by measuring them during development. But typical engineering data tell listeners very little about how a loudspeaker is likely to sound. Here is a partial list of reasons:

1. Frequency-response measurements are usually made with a microphone directly in front of and one meter away from the loudspeaker. With this positioning it is often possible for even a small movement of the microphone to affect the frequency-response curve. Listeners normally are much farther away and, because of stereo placement, at an angle of at least 15 to 20 degrees to the speaker's center line.
2. Measurements are made on single speakers despite the fact that they are used in pairs. Driver layout and cabinet shape can make listening to two speakers different from listening to one.
3. Human ears, unlike test microphones, are not omnidirectional. Causing various frequencies to arrive at the listener's head from different directions will make loudspeakers sound different, but the microphone will not notice.
4. Listeners, because they have two ears, can analyze sounds and extract information that test microphones cannot detect—the direction from which a sound seems to come and the distance and apparent size of its source.
5. Some frequency-response measurements are made in typical listening rooms or special reverberant

rooms that integrate the sound power radiated by the loudspeaker in all directions. Such measurements "homogenize" the direct and reverberant sound reaching the microphone, losing a distinction that materially affects listening quality.

6. Engineering measurements made in typical test chambers fail to indicate the effects of interaction between a speaker system and the room in which it will be used. These include interference by sound reflected from the wall behind the speaker and the influence of side-wall, floor and ceiling reflections on the size of the sonic image.

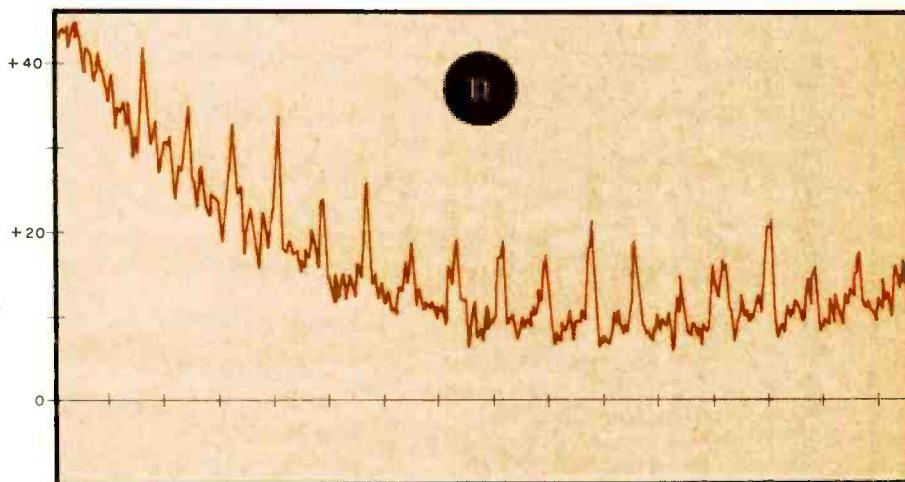
The list can be extended, but it is long enough to make this point: engineers spend much of their time and effort measuring the *loudspeaker*, while listeners are most interested in the *sound field* created by the loudspeaker under typical listening conditions. Manufacturers' frequency-response measurements can be quite correct without telling much about how a loudspeaker will sound. Moreover, it is probably impossible to find out how a loudspeaker will sound on an objective, scientific basis, using the types of measurement—computerized or not—upon which almost all manufacturers depend. Indeed, most computer-made loudspeaker measurements reveal nothing that engineers are unable to learn with conventional analog equipment. They simply provide the same data more quickly, conveniently, or elegantly.



B. Smooth curve showing evidence of high-frequency boost. Relative level at 10,000 Hz is about 10 dB higher than in A. Curve apparently breaks at about 5500 Hz.

C. Odd shape appears to be result of substantial high-frequency boost between 5000 and 12,000 Hz. Steep descent at low frequencies implies some bass boost.

D. Remarkable spectrum shows strong, precisely spaced brass instrument overtones and a surprising amount of high-frequency emphasis compared to other recordings. Alignment with other curves at low frequencies shows about 20-dB boost at 15,000 Hz.



A "Thought Experiment." If objective measurements cannot tell which loudspeaker is nearest to perfection, can listening tests give the answer? Before taking up this question, let's try to define the problem in a simple, scientific way.

Suppose that we had a *perfect* high-fidelity system. How would we know? We could set up microphones in our listening room and play a recording; while we played it, we would re-record it. Then we would compare the original recording with our recording of the recording. If we could hear absolutely no difference between the two recordings, we would have to conclude that our high-fidelity system was perfect. One problem remains. Where do we get the recording with which to begin?

Let's change the rules a bit to see if we can come closer to a practical answer, at least in our imaginary laboratory. Suppose that a soundproof wall is built across the middle of a large room, and a hole the size of a loudspeaker system is cut through it. We place musicians on one side of the wall and a listener on the other. When the musicians play, the purest high-fidelity sound—the real thing—comes through the hole and the listener hears it. Two holes can be used for stereo. Next, we put a speaker system into the hole, closing it, and connect a microphone, facing the musicians, through an amplifier to the loudspeaker, which faces the listener. The reproduction is perfect when the lis-

tener cannot tell the difference between the loudspeaker and the hole in the wall.

This is as far as the analogy is usually taken, but let's go one step further. Suppose we dismiss the musicians and substitute a recording made when the microphone was in place, played through the same kind of loudspeaker as we have mounted in the wall. Now the listener has to tell whether the loudspeaker is reproducing itself or live music. Would it work?

Probably not. We might come close, but there would be no way to tell how close. The problem concerns the size of the hole in the wall and the size of the microphone. Since the microphone is only about an inch in diameter, it picks up only a tiny sample of the sound field produced by the musicians or the loudspeaker. In fact, the sample is so restricted that it tells us nothing about the direction from which various frequencies arrive or where they go next. The sound level at one point in space is all that the microphone can relate to us. Unfortunately, the sound field on the other side of the wall is far too complicated for accurate representation by such a tiny sample.

Radiation from the loudspeaker develops in a complete, three-dimensional pattern, some frequencies in one direction and other frequencies all around, some mainly to the right and left and others only forward, but none of this has anything to do with the original sound. The directional information can't be coming from the

microphone; the loudspeaker just makes it all up! Unless the radiation pattern of the loudspeaker exactly matches that of the source, we will never be able to carry out our experiment successfully.

Why Does High Fidelity Work? After all this, it must be said that some recordings, played through some loudspeakers, sound realistic enough to make one's hair stand on end. If measurements are not going to give us the answer and tell us which speaker system is most accurate, we may have to go back to subjective listening comparisons, using good high-fidelity recordings. But we are assuming that recordings can be made accurately just as we assumed, at first, that loudspeakers can be measured accurately. A recording can be considered a measurement of a performance. How do the people who make a commercial recording know when it is accurate . . . or inaccurate? Simply: they listen to the master tape through loudspeakers and change the frequency response of the recording until they think it *sounds* right.

Without information about the record we are playing, there is no way to know how a loudspeaker should sound. The kind of information we want is hardly likely to be printed on album covers; but, with a little time and skill, we can let a computer analyze the frequency content of different recordings and compare them to each other, if not to an absolute standard. The results, shown in Fig. 1, will not encourage perfectionists, but they do indicate the danger of assuming that one's favorite "test record" can be a reliable index of objective loudspeaker performance.

Measuring the sound produced by musical instruments is no easier than measuring the sound coming from a loudspeaker. So many factors other than uniform frequency response enter into a listener's judgment of the realism of the result that the producer in the recording studio, even with access to the most elaborate and expensive apparatus, must rely on manipula-

tion to obtain a result he finds acceptable. Yet some of the manipulations on records are undoubtedly unacceptable to many serious music listeners. Perhaps more could be accomplished by improved microphone design or more careful positioning of microphones at recording sessions. Until better understanding of some of the objective problems of music recording and reproduction is achieved, however, equalization is likely to remain the most economical yet powerful tool the producer can use to adjust the sound of a recording.

Spatial Hearing and Cross-Correlation. The solution to the loudspeaker puzzle probably does not lie in improving existing methods of measurement, but rather in devising new, more meaningful ways of obtaining and interpreting data about loudspeakers. Given a good loudspeaker to begin with, the listener who is so inclined can easily manipulate its frequency response with tone controls or an equalizer. What is much harder to change—and may be the invariant property that gives a loudspeaker system its acoustic identity—is the way in which its three-dimensional radiation pattern interacts with the listener's auditory system. We need a better understanding of those properties of a loudspeaker's radiation that are used by a listener's brain to tell something about the size, shape, distance and direction of the sound being reproduced.

The human hearing system locates the direction of a source of sound in several ways. One is by estimating the time interval between the arrival of a sound at one ear and its arrival at the other ear. Nobody knows exactly how this is done in the brain, but one widely believed idea is that the process involves something called a "correlation matrix"—a web of nerves interconnected in such a way as to continuously monitor the incoming energy at each frequency for matching variations in level. As proposed by Jeffress and Licklider, distinguished researchers in this field who independently suggested ways such a system might work, the

TABLE	
± DELAY	AZIMUTH
100 µs	11 DEGREES
150 µs	17 DEGREES
220 µs	25 DEGREES
260 µs	30 DEGREES
300 µs	35 DEGREES
340 µs	40 DEGREES
380 µs	45 DEGREES

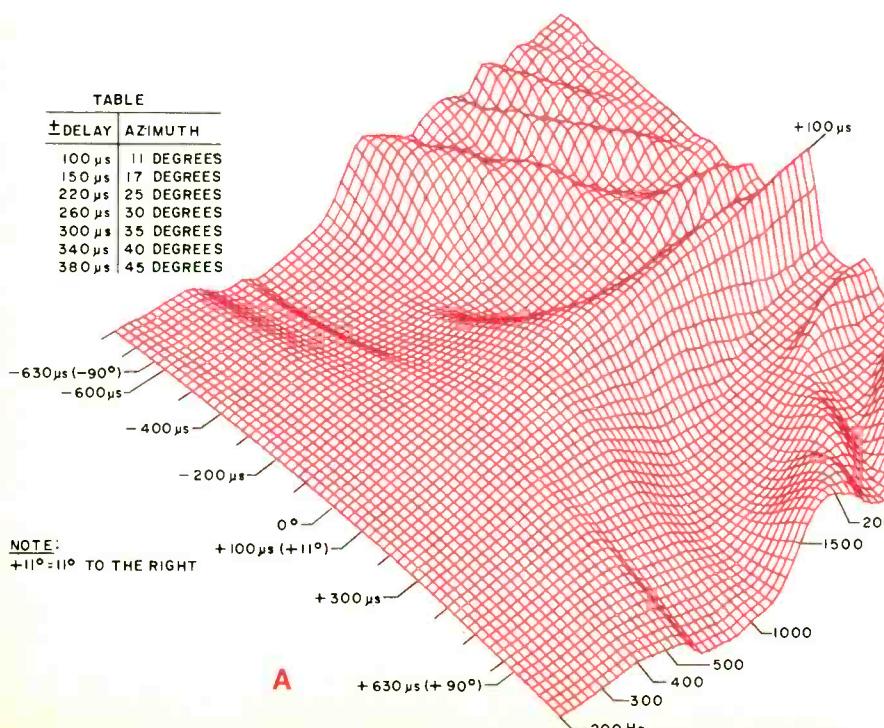


Fig. 2. Examples of kind of plot produced by AR's "robot listener" system. Automatic computer drawing shows how well signals at both ears match at varying time delays. Zero delay would correspond to source directly in front of listener; 90° to right or left would produce a peak at ± 630 microseconds. Speaker system A has drivers aligned vertically on front of cabinet; system B uses driver units on three cabinet sides. Like the human hearing system, A shows little directional infor-

correlation matrix has a number of output taps corresponding to different amounts of time delay. At a given frequency, the highest output is obtained from the tap corresponding to the delay time of either the left or right ear signal that gives the best match of the two.

My colleagues and I have experimented with an artificial human head, with specially constructed microphones implanted inside ears modelled after those human beings. The microphones' output is linked to a laboratory computer (and associated peripheral equipment) programmed to simulate some of the known properties of the inner ear and the neural networks in the human brain that analyze auditory data. We can interrogate our robot listener to ask it to draw a picture of what it has heard. Figure 2 shows one kind of picture produced in this way. The plot represents the cross-correlation of the signals received by the two "ears" as a function of frequency, after the individual signals have been processed to account for the response of the basilar membrane, a part of the inner ear. A trained observer will see that various features of the human hearing mechanism are indeed present in the computer simulation. Comparison of the model's data to data from experiments with human listeners confirms that our biological sensors and signal-processing networks closely approach the ideal efficiency that could be expected of such a system. The sensitivity is surprising. In some experiments, human hearing has proved capable of finding the azimuth of a sound source to within less than one degree.

Nonlinear Processing in Hearing. Despite its extreme sensitivity to some characteristics of sounds, the ear transforms and alters the incoming signal very early in the auditory process. One change is the separation of a sound into its constituent frequencies, that is, spectral analysis. Another is half-wave rectification, which probably takes place after frequency analysis. These changes would destroy little actual information

about a sound but would possibly assist localization. Transmission of information in the central nervous system, where processing takes place, appears to be statistically oriented, rather than discrete and quantitatively precise as in a computer.

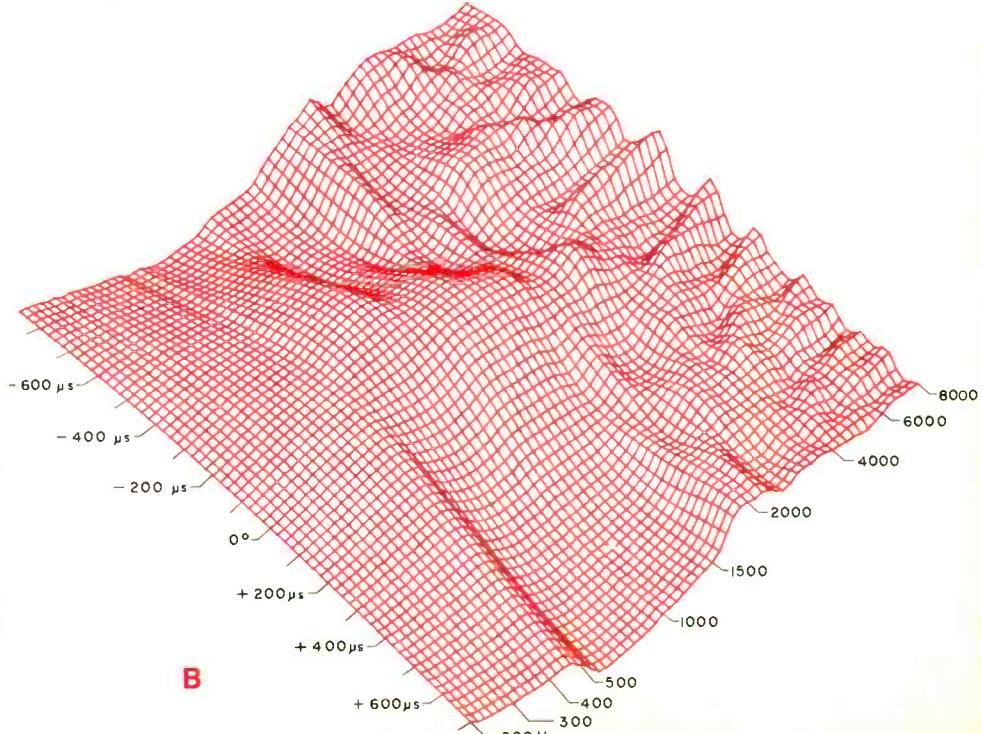
The significance of these nonlinear effects in music reproduction is not common knowledge, except to readers of specialized journals and texts on the subject. However, the importance of such effects should be clear to anyone who has heard an "ambience" or "time-delay" system. Without being able to add any genuine information at all, such systems, often by mere



Artificial head used at AR and many other laboratories is made by Neumann, German manufacturer of professional condenser microphones. Units are built with specially designed coupling chambers between ear canal and microphone capsule, to match electrical output as closely as possible to acoustical signal at human eardrum.

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delayed repetition of the original sound through added speakers, impressively augment the subjective impression of realism. Some listeners have observed that a mediocre system with "time-delay" can be more satisfying than a high-quality system without such an accessory, despite the fact that the additional sound can only *decrease* the objective accuracy with which the recording is reproduced.

The Future. For some years, at least, progress in audio might depend on the work of neurophysiologists and psychologists, rather than on refinement of hardware along conventional lines. Eventually perhaps, the results will justify the application of their hard-won knowledge to our special concern by bringing everyone

greater pleasure and enjoyment from music. The search for improved understanding is also one of the most exciting and potentially rewarding applications of computers and digital simulation to audio. By applying techniques from the field of artificial intelligence—feature detection and pattern recognition—we may soon be able to make objective measurements of the spatial fields generated by a loudspeaker in terms of a listener's perception. When we are able to measure such qualities objectively, we can begin to design speaker systems in which these variables are controlled. This, in turn, would give us much greater control over the listener's subjective impression—which is, as we said at the outset, the fundamental principle of high-fidelity music reproduction. ◇

A 3-Way Drive System for Speakers

Active crossover divides the audio spectrum for individual drivers before power amplification

BY J.F.P. MARCHAND

IN TRADITIONAL multiway loudspeaker systems, the division of the driving signal into frequency ranges suitable for the several drivers is performed after power amplification. The crossover or dividing network is composed of a set of passive components—inductors, capacitors, and resistors—interposed between the power amplifier output terminals and the input terminals of the individual transducers.

From the point of view of economy, this approach is advantageous, but it is not without difficulties. One is that the dividing network must handle appreciable power. This means that the passive components (the inductors are most problematic) must behave in a linear manner at high current levels if distortion products are not to be generated. Optimal design often raises the cost of the passive components and causes some of the economic advantage to evaporate.

Another drawback of particular concern to the home constructor is that a high-level network capable of performing well with the drivers to which it is added can be very difficult to design. The reason is that most tables and formulas for the filter-section design are based on the assumption that the network will be terminated by a purely resistive load, while the driver impedances usually contain significant, frequency-dependent reactive components.

Clearly, it would be advantageous to eliminate this problem. We can do this with no loss of performance by multamping the system and taking advantage of the fact that the power amplifiers act as buffers between the filters and the drivers. Another benefit is that, with

several power amplifiers sharing the load, the demands made on each of them are less stringent than when a single unit must do the whole job. For example, since bass frequencies cannot intermodulate with treble frequencies in loud passages, a particularly audible form of distortion is minimized. Also, the bass power amp can have a relatively low slew rate and cause no problems, as it will not see rapidly changing signals. A treble amp, on the other hand, can have a low damping factor, with less feedback and fewer problems.

The Filters. A schematic diagram of the active crossover for one audio channel appears in Fig. 1. While other types of filters can give good results in this application, the 18-dB/octave active Butterworth filters used here offer a desirable combination of steep slopes and good phase response. Rolling off the drivers rapidly helps to suppress any anomalous behavior they may exhibit as the extremes of their useful ranges are approached. Using as sharp a network as this between a power amplifier and the drivers is often avoided because of expense. In a design of this type, however, the extra cost is minimal.

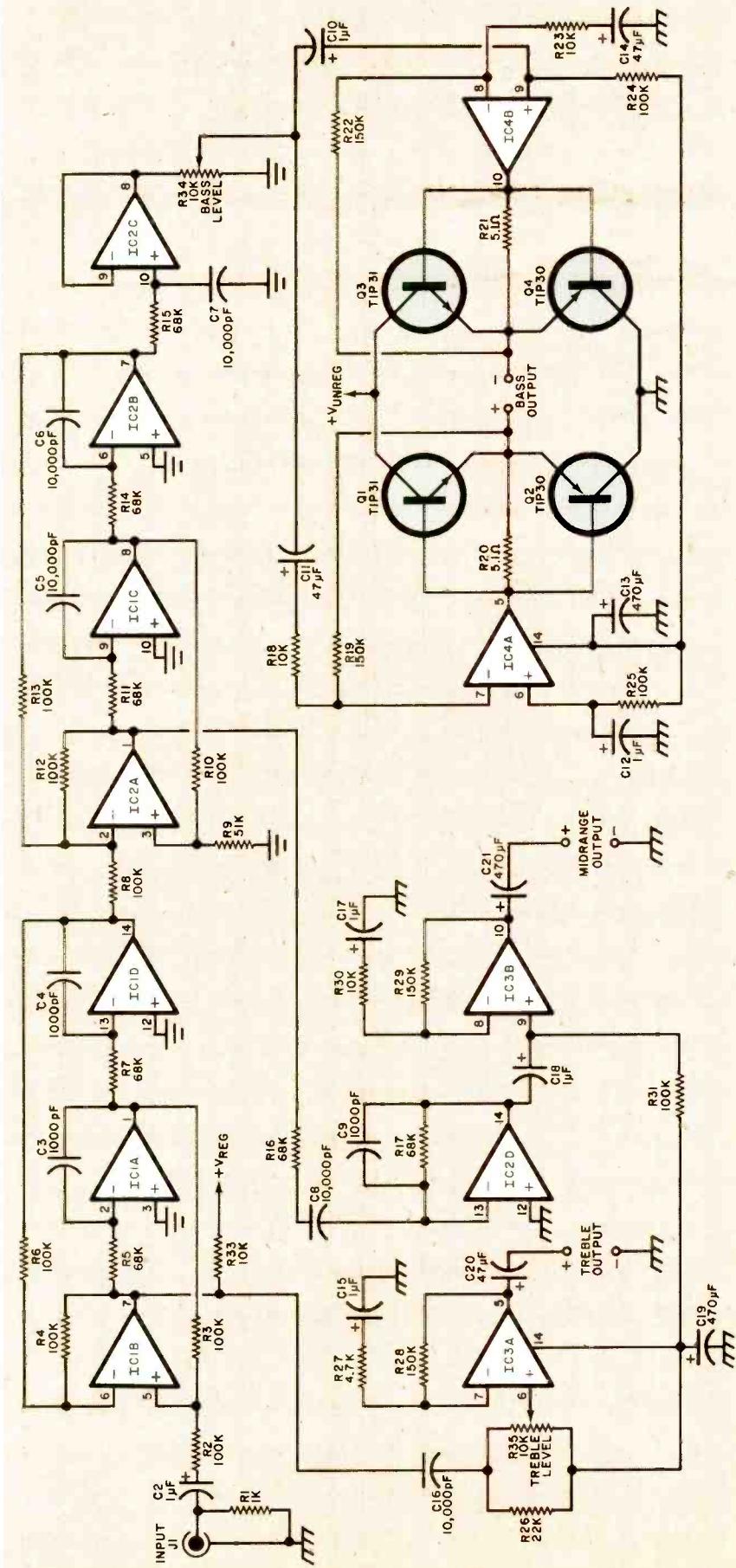
Quad operational amplifiers *IC1* and *IC2* are the central elements of the filters. Integrated circuits *IC1A*, *IC1B*, *IC1D*, and their associated components and *IC1C*, *IC2A*, *IC2B*, and their associated components comprise two active filters with ultimate slopes of 12 dB/octave. The first filter separates the high frequencies from the low and middle frequencies. The second

(Continued on page 48)

PARTS LIST

C1—13,000- μ F, 50-volt electrolytic
 C2,C10,C12*,C15*,C17*,C18—1- μ F,
 50-volt radial-lead electrolytic
 C3,C4,C9—1000-pF, 5% polystyrene
 C5,C6,C7,C8,C16—10,000-pF, 5% poly-
 styrene
 C11,C14*,C20*—47- μ F, 50-volt radial-
 lead electrolytic
 C13*,C19,C21*—470- μ F, 25-volt radial-
 lead electrolytic
 C22 through C28—0.1- μ F disc ceramic
 D1,D2—6.8-volt, 1-watt zener diode
 F1—1-ampere fast-blow fuse
 IC1,IC2—LM324N, T1.074CN, or simi-
 lar quad operational amplifier
 IC3*,IC4*—LM379S dual six-watt au-
 dio amplifier
 J1—RCA phono jack
 Q1*,Q3*—TIP31 npn power transistor
 Q2*,Q4*—TIP30 pnp power transistor
 The following, unless otherwise specified,
 are 1/2-watt, 5%, carbon-film resistors.
 R1,R32—1000 ohms
 R2,R3,R4,R6,R8,R10,R12,R13,R24*,
 R25*,R31*—100,000 ohms
 R5,R7,R11,R14,R15,R16,R17—68,000
 ohms
 R9—51,000 ohms
 R18,R23*,R30*,R33—10,000 ohms
 R19*,R22*,R28*,R29*—150,000 ohms
 R20*,R21*—5.1 ohms, 1/2-watt, carbon-
 composition
 R26—22,000 ohms
 R27*—4700 ohms
 R34,R35—10,000-ohm, pc-mount, lin-
 ear-taper potentiometer
 RECT1—6-ampere, 100-PIV modular
 bridge rectifier
 S1—Spst toggle switch
 T1—24-volt, 2-ampere transformer
 (Stancor No. P-8617 or equivalent)
 Misc—Printed circuit board, heat sinks
 (four Thermalloy No. 6070 or equiva-
 lent, two Thermally No. 6072 or equiva-
 lent), line cord and strain relief, fuse-
 holder, circuit board standoffs, hard-
 ware, hookup wire, shielded cable, etc.
 Note—An etched and drilled glass-epoxy
 printed circuit board is available for
 \$15.00 from Marchand Electronics,
 Inc., 1334 Robin Hood Lane, Webster,
 NY 14580. New York residents, please
 add 7% state sales tax.

Fig. 1. Schematic diagram
 of the active crossover
 for one audio channel.
 Further power amplification
 may be added if desired.



then divides the low and middle frequencies. The high, middle, and low frequencies, which appear at the outputs of $IC1B$, $IC2A$, and $IC2B$, respectively, are fed to passive high-pass and low-pass filters $C16$, $R26$, and $R35$ and $C7$, $R15$ and to active band-pass filter $C8$, $R16$, $C9$, $R17$, and $IC2D$.

These last circuits are first-order filters having ultimate slopes of 6 dB/octave. Because the second- and first-order filters are cascaded, the resulting ultimate slope is 18 dB/octave.

The values of capacitance and resistance which determine the low and high crossover frequencies have the following relationships:

$$C_{high} = C3 = C4 = C16 / 10$$

$$C_{low} = C5 = C6 = C7$$

$$R_{high} = R5 = R7 = 10 \text{ } (R26 \parallel R35)$$

$$R_{low} = R11 = R14 = R15$$

The values of R_{high} and R_{low} in kilohms and of C_{high} and C_{low} in picofarads are determined from the equations: $R = 10^9 / 6.28fC$ and $C = 10^9 / 6.28fR$. Choose a convenient value of capacitance, say 100,000 pF for a low crossover, 10,000 pF for a high one. Then calculate the necessary resistor values. A negative value for $R26$ means that $R35$ is too low to allow it and $R26$ in parallel to reach the desired resistance. Repeat the calculation with a larger value for C .

The specified op amps are sufficiently fast to give good performance. However, anyone concerned about transient intermodulation (TIM) distortion may substitute a pin-compatible IC, such as type TL074CN, which has a higher slew limit.

To use the project with two-way systems, make f_{high} and f_{low} equal. The bandpass output should be left floating as there is no midrange driver.

Power Amplifiers. The choice of power amplifiers for a triamped system depends on the efficiency and power-handling capabilities of the drivers, the crossover frequencies and how loud you want the music to be. Generally, you will want to use the best quality amplifiers you can afford; but, as noted earlier, factors that influence the high-frequency performance of the bass amp are unimportant. Similarly, damping factor, dc coupling, and other parameters or features that relate to low-frequency performance are not critical in the treble and midrange amps.

To decide how much power each of the amplifiers

must have, start with the reasonably conservative assumption that music has equal power in each of the 10 audible octaves. With your chosen crossover frequencies in mind, determine how many octaves each driver will handle. The number of octaves is given by the relation $N = \log_{10}(f_2/f_1) / \log_{10} 2$, where f_1 and f_2 are the lower and upper limits, respectively, of the passband allocated to a particular driver. (This is a formidable looking calculation, but it can be performed easily on most scientific calculators.) A driver handling five octaves would get 50% of the system power; one handling three octaves would get 30%, etc.

If an appropriate calculator is not available, draw a chart, marking octave boundaries at 20, 40, 80, 160 Hz etc., and note which bands contain your crossover frequencies. Then you can get an approximate idea of how many octaves are reproduced by each driver. Obviously, this method is not exact, but you are not likely to find power amplifiers in exactly the sizes you need anyway.

A constructor who can be satisfied with a modest amount of power at distortion levels that are adequate but not state-of-the-art can build the power amplifiers included in Fig. 1. These are built around two National LM379s, dual 6-watt integrated power amplifiers, which require few additional components and have built-in thermal protection. Integrated circuits $IC3A$ and $IC3B$ are the amplifiers for the high and middle frequencies. They are connected as standard noninverting operational amplifiers and the outputs are capacitively coupled to the loudspeakers via $C20$ and $C21$.

To satisfy the higher power requirement of the low-frequency channel, $IC4$ is arranged as a balanced amplifier with booster transistors $Q1$, $Q2$, $Q3$ and $Q4$. The op amps are arranged as an inverting and a noninverting amplifier, differentially driving the bass loudspeaker. This doubles the maximum voltage across the loudspeaker, yielding four times the power. The booster transistors handle the doubled output current. All three amplifiers are designed for 8-ohm drivers.

Power Supply. Power for the filters and power amplifiers can be provided by the supply shown schematically in Fig. 2. A simple bridge rectifier and filter capacitor provide 35 volts dc at no load. As the LM 379 is relatively insensitive to power-supply ripple, no additional filtering is required.

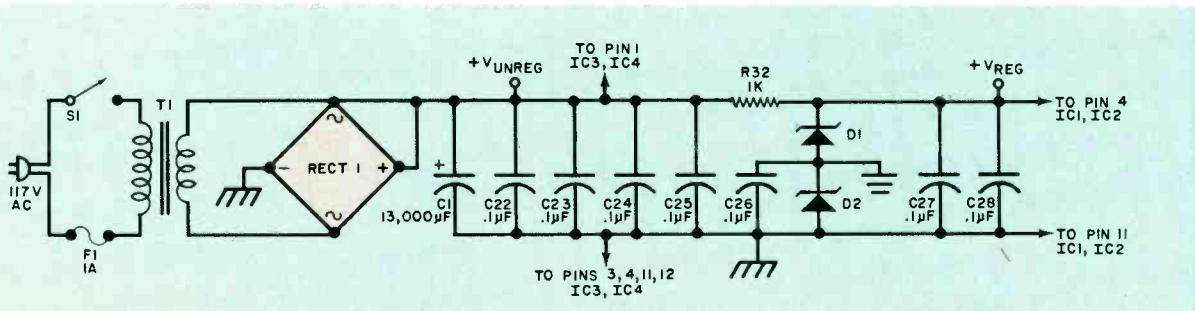


Fig. 2. Schematic diagram of a power supply for the filters and amplifiers. Capacitors supply filtering and zener diodes regulation for various voltages.

Supply voltages for IC_1 and IC_2 are provided by the 6.8-volt zener diodes, D_1 and D_2 . Capacitors C_{22} through C_{28} provide power-supply decoupling. Power amplifiers IC_3 and IC_4 require high-frequency power-supply decoupling to prevent ultrasonic oscillation. This decoupling is provided by C_{22} through C_{25} . These disc ceramic capacitors are mounted in pairs close to the LM379 integrated circuits.

Note that two distinct ground symbols are employed in the two schematic diagrams. This is so because the power supply is single-ended. The "earth ground" symbol is employed as the input and output signal ground and the negative supply line for the ICs. The "chassis ground" symbol signifies an artificial ground for operational amplifiers IC_1 and IC_2 that is at a dc level equal to one half the regulated supply voltage. It is derived by means of the voltage-dropping action of zener diodes D_1 and D_2 .

The gains of the low and high channels can be adjusted with potentiometers R_{34} and R_{35} . With the wipers of these controls at the center of their travel, the gains of all amplifiers are approximately 15. An input sine wave of 460 mV rms will then result in full power output.

Construction. The assembly of the project is relatively straightforward. All parts except the 24-volt power transformer are mounted on a single $5\frac{1}{2} \times 6\frac{1}{2}$ -inch printed circuit board. The full-size etching and drilling guide for this board appears in Fig. 3. A complementary parts placement guide is reproduced in Fig. 4. When inserting electrolytic capacitors, diodes, transistors and integrated circuits, be sure to observe proper polarity.

Resistors R_2 through R_{17} and R_{26} and capacitors C_3 through C_9 and C_{16} determine the crossover frequencies. For best performance, these components should have a tolerance of no more than $\pm 5\%$. Polystyrene capacitors are specified but other low-loss precision types, can be substituted.

Transistors Q_1 through Q_4 are mounted on Thermalloy No. 6070 or similar heatsinks with suitable mounting hardware. Cooling for the LM379 ICs is accomplished by mounting them directly on Thermalloy No. 6072 or similar heatsinks with two No. 4-40 machine screws. The holes in these heatsinks do not line up with the threads in the ICs, so two holes spaced 1 inch (2.54 cm) apart must be drilled in the heatsinks. Pin 1 of the power ICs is marked with a small white dot on the

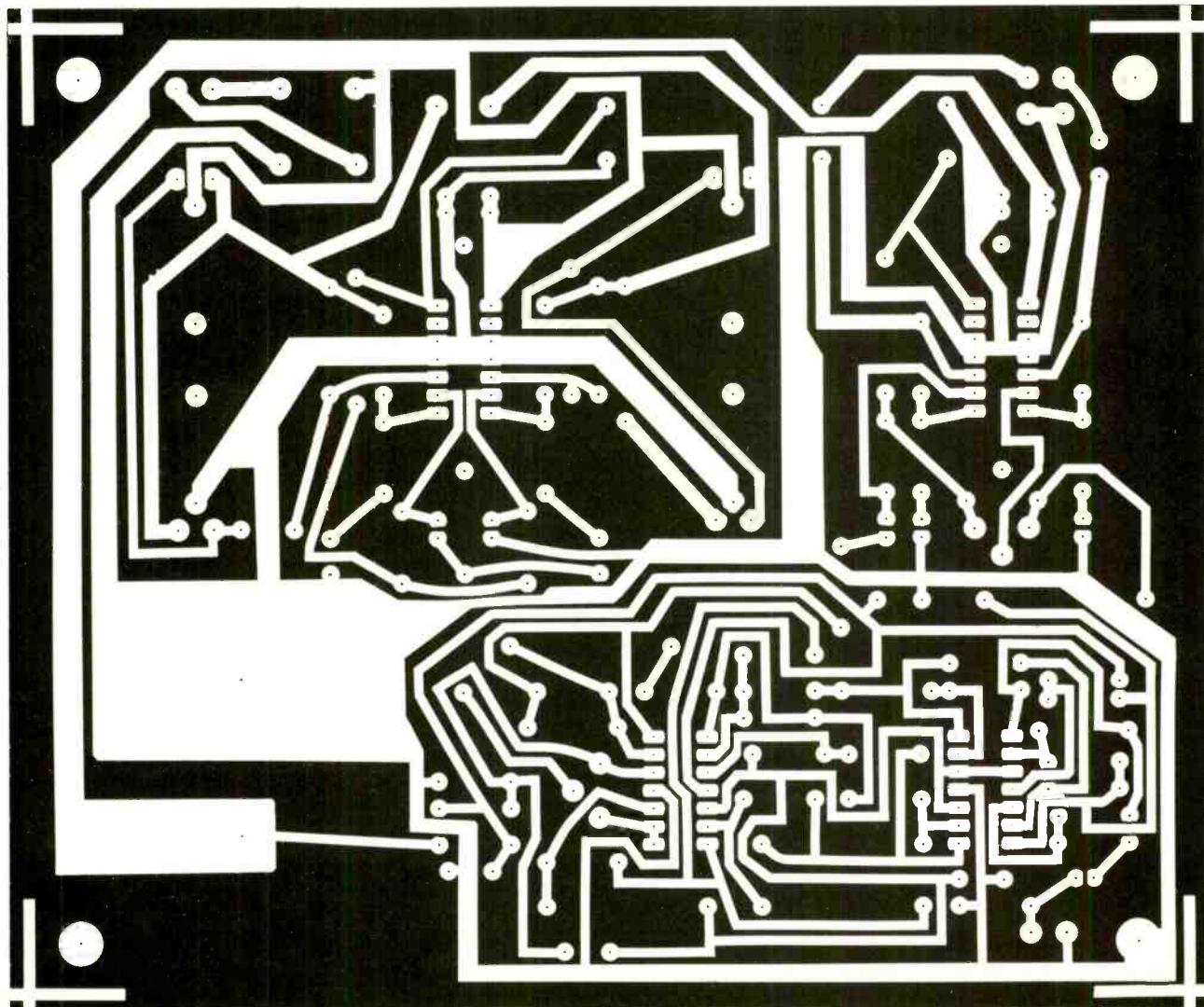


Fig. 3. Actual-size etching and drilling guide for printed circuit board.

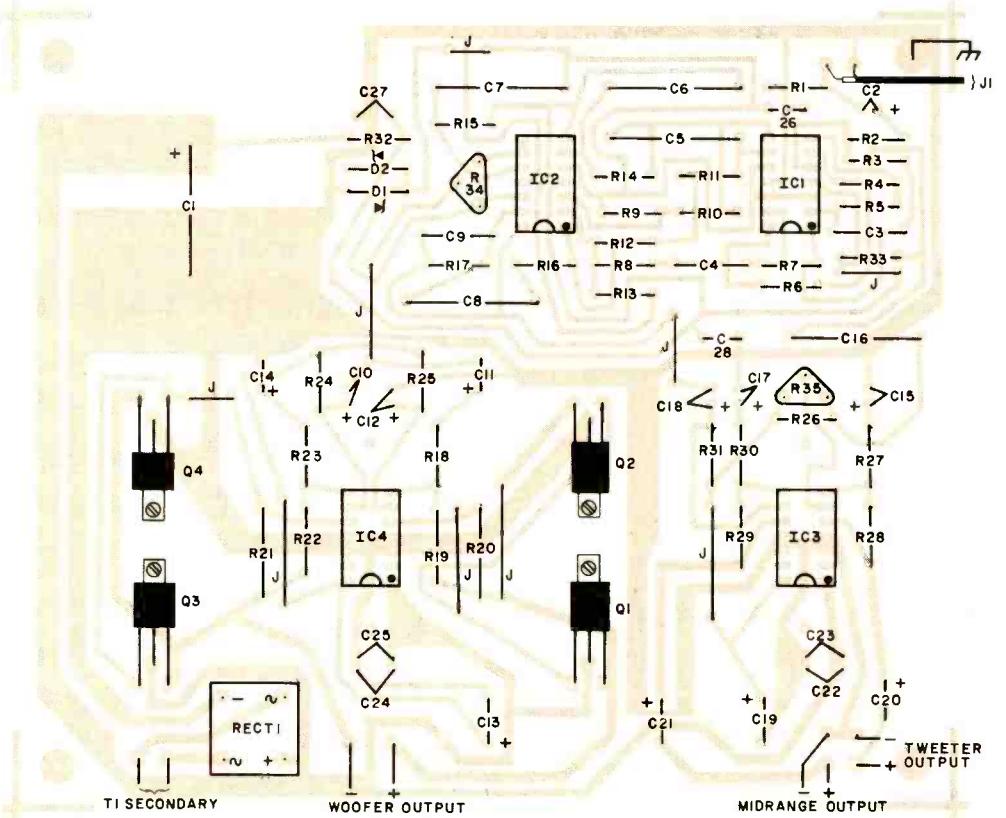


Fig. 4. Component layout diagram for the printed circuit board. Transistors Q1 through Q4 are mounted on heat sinks.

underside of the package. The large filter capacitor, C_1 , is mounted on the board with standard hardware.

Should you decide to use other power amplifiers, IC_3 and IC_4 , Q_1 through Q_4 , and their associated components (see parts list) can be omitted. Outputs for the external amplifiers can be taken from the solder pads intended to accommodate pins 6 and 9 of IC_3 (high and mid frequencies) and pin 7 or 9 of IC_4 (low frequencies). Use shielded cable with phono jacks and the shield grounded only at the jacks. Keep cables short, adding 100-ohm buffer resistors if needed to prevent oscillation.

If you use the on-board power amps, it will be convenient to mount the entire project inside the loudspeaker enclosure. Potentiometers R_{34} and R_{35} can be mounted in place of the original crossover controls, and the fuse holder, input connector, and on-off switch can be installed on the rear of the enclosure. To allow adequate ventilation, mount the circuit board as low in the box as possible, positioning it so that damping material does not interfere with air circulation. Leads to the pots and speakers should be twisted together.

To use the project with external power amps, it will be necessary to fabricate some form of enclosure. The controls, input and output connectors, fuse holder, and on-off switch can be mounted on one of its panels.

Power-supply components T_1 , B_1 , C_1 are more than adequate for two stereo channels of filtration. Decoupling capacitors C_{22} through C_{25} can be omitted, but a

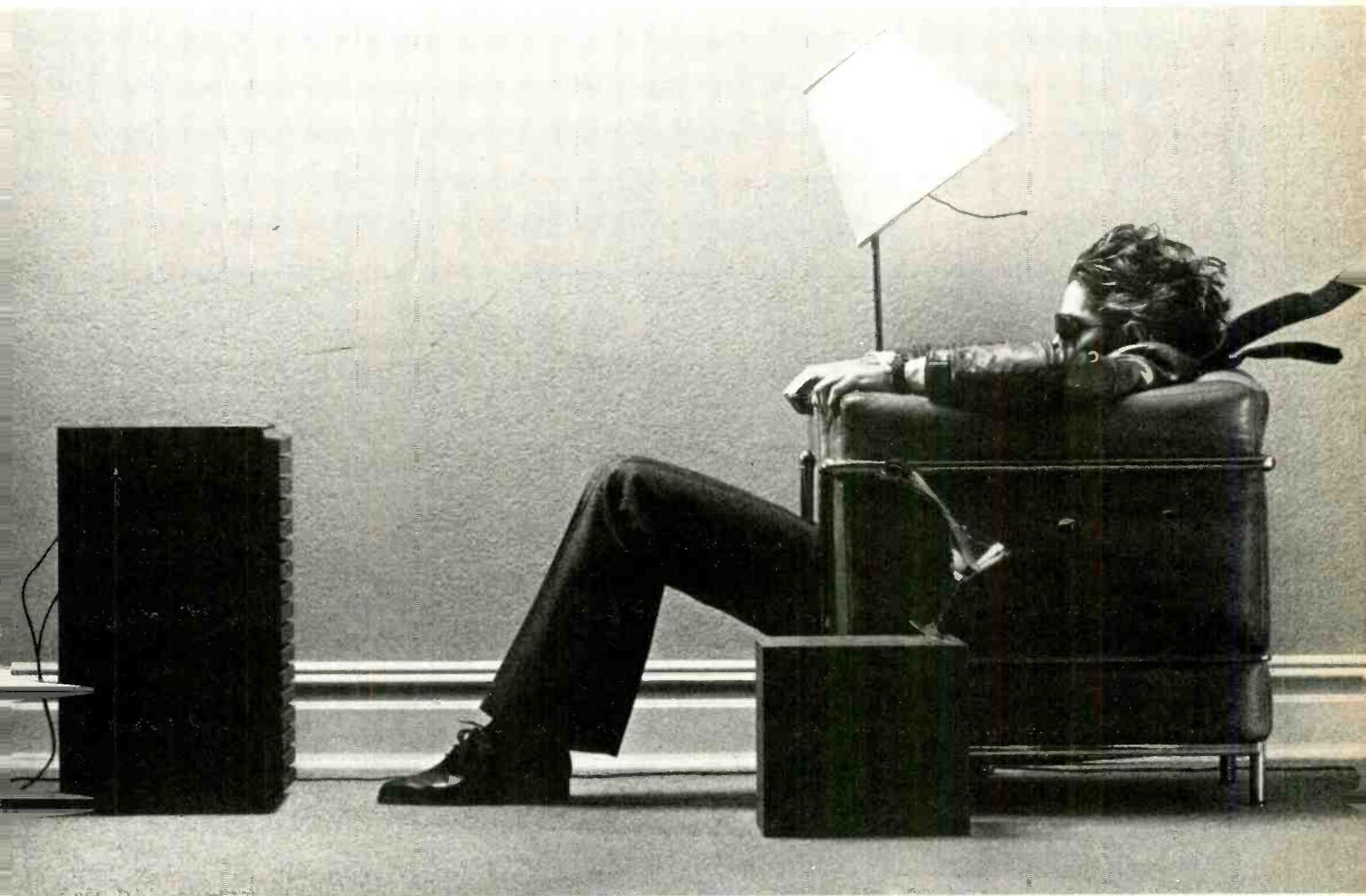
separate zener-diode regulator section should be used for each channel. The loudspeaker system will have to be fitted with a separate set of connectors for each driver. If desired, the drivers can be protected by individual fuses of appropriate ratings.

Setting it Up. Whichever arrangement you use, pay careful attention to the polarity of the drivers, sometimes indicated with a red dot meaning "plus" (+). Some authorities feel that, with 18-dB/octave crossovers, the best phase response near the crossover frequencies is achieved by connecting adjacent drivers out of phase. You may want to experiment to see which arrangement gives you the best results.

In some cases, coupling the amplifier directly to a woofer will increase damping to the point where a small amount of bass response is lost. This can be cured by connecting a small resistor, generally 1 ohm or less, in series with the driver. To protect the speaker drivers from transients, be sure that the power amps are turned on *after* the crossover is powered and turned off *before* crossover power is removed.

Once you are certain that the project is operating correctly, make all necessary corrections and set the level controls for flattest frequency response. The improvement in the sound of your speakers will not be earth-shaking but should be clearly audible. Many listeners who use tri-amping report clearer, tighter sound with reduced distortion.

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Extra Keyboards for Microcomputers

BY ADOLPH A. MANGIERI

A keyboard can be connected directly in tandem with the main board of most computers to expand operating versatility.

AN ADDITIONAL keypad or keyboard in tandem with the main keyboard of a computer can have a myriad of uses. A small numeric keypad can be convenient for entering arithmetic data and allows players to enter game moves easily. A full typewriter keyboard duplicating the main one makes one computer setup almost as useful as two for group use and instruction. In any case, a second keyboard, can be used for remote data entry.

The tandem keyboard connects directly to the computer keyboard matrix lines and requires no additional components. Once the warranty on your computer expires, there is no reason why you should not open the cabinet and bring out the keyboard matrix lines. It's both safe and simple. Details are given here for the Radio Shack TRS-80 com-

puter, but the modification can be applied to many other makes.

Circuit Operation. Most computer keyboards employ normally-open spst keyswitches wired with keyboard characters assigned to row and column lines of a matrix. As shown in the diagram, the TRS-80 keyboard is arranged as an 8 X 8 matrix. The eight D0 through D7 column lines connect to column line output buffers (not shown) that, in turn, connect to the data bus. The eight A0 through A7 row lines are driven by row-line buffers connected to the address bus. Each intersection of the matrix has an spst keyswitch, as shown for column lines D0 and D7. When the A key is pressed, row line A0 and column line D1 are connected to each other to generate an output on column line D1 and the

appearance of character A on the monitor screen.

To add a remote keypad or a full keyboard in tandem, you merely carry out the required row and column lines to the switches of the remote keyboard. Just how the computer encodes key closure is not material. In the TRS-80, encoding of the keyboard is accomplished with a program in ROM. (See the TRS-80 Microcomputer Technical Reference Manual for details.) Many computers employ a chip encoded keyboard.

The only consideration to be taken into account when connecting a tandem keyboard into an existing microcomputer system is whether cable capacitance and stray pickup will affect computer operation. Fortunately, almost any keyboard can tolerate several feet of connecting cable to the tandem keyboard.

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(Level "A" makes a perfect OEM controller for industrial applications and is available in a special Hex Version which can be programmed using the Netronics Hex Keypad/Display.)

PC Board: glass epoxy, plated through holes with solder mask

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... provision for 24-pin DIP socket for hex keyboard/display... cassette tape recorder input... cassette tape control output... speaker output... LED output indicator on SOD (serial output) line... printer interface (less drivers)... total of four 8-bit plus one 6-bit I/O ports.

• Crystal Frequency: 6.144 MHz

• Control Switches: reset and user (RST, 7.5) interrupt... additional provisions for RST 5.5, 6.5 and TRAP interrupts onboard.

• Counter/Timer: programmable, 14-bit binary

• System RAM: 256 bytes located at F800, ideal for smaller systems and for use as an isolated stack area in expanded systems... RAM expandable to 64k via S-100 bus or 4K on motherboard.

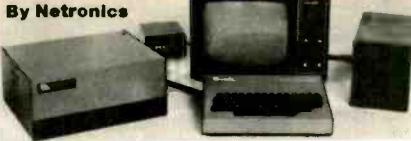
System Monitor (Terminal Version): 2k bytes of deluxe system monitor ROM located at F000 leaving 0000 free for user RAM/ROM. Features include tape load with labeling... tape dump with labeling... examine/change contents of memory... insert data... warm start... examine and change all registers... single step with register display at each break point, a debugging/training feature... go to execution address... move blocks of memory from one location to another... fill blocks of memory with a constant... display blocks of memory... automatic baud rate selection... variable display line length control (1-255 characters/line)... channelized I/O monitor routine with 8-bit parallel output for high speed printer... serial console in and console out channel so that monitor can communicate with I/O ports.

System Monitor (Hex Version): Tape load with labeling... tape dump with labeling... examine/change contents of memory... insert data... warm start... examine and change all

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Hex Keypad/Display

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Explorer/85 with L card cage

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Level "E" Specifications

Level "E" adds sockets for 8k of EPROM to use the popular Intel 2716 or the TI 2516. It includes all sockets, power supply regulator, heat sink, filtering and decoupling components. Sockets may also be used for soon to be available RAM IC's (allowing for up to 12k of onboard RAM).

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The keyboard follows the standard typewriter configuration and generates the entire 128 character ASCII upper/lower case set with 96 printable characters. Features include onboard regulators, selectable parity, shift lock key, alpha lock jumper, a drive capability of one TTY load, and the ability to mate directly with almost any computer, including the new Explorer/85 and ELF products by Netronics.

The Computer Terminal requires no I/O mapping and includes 1k of memory, character generator, 2 key rollover, processor controlled cursor control, parallel ASCII/BAUDOT to serial conversion and serial to video processing—fully crystal controlled for superb accuracy. PC boards are the highest quality glass epoxy for the ultimate in reliability and long life.

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When connected to a computer, the computer must echo the character received. This data is received by the VID which processes the information, converting to data to video suitable to be displayed on a TV set (using an RF modulator) or on a video monitor. The VID generates the cursor, horizontal and vertical sync pulses and performs the housekeeping relative to which character and where it is to be displayed on the screen.

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!@#\$%^&*()+=,-./0123456789;:<=>?
ABCDEFGHIJKLMNOPQRSTUVWXYZ
abcdefghijklmnopqrstuvwxyz

BAUDOT Character Set: ABCDEFGHIJKLMNOPQ
RSTUVWXYZ - : ? \$ # () , 9 0 1 4 5 7 ; 2 1 6 8 •

Cursor Modes: Home, Backspace, Horizontal Tab, Line Feed, Vertical Tab, Carriage Return. Two special cursor sequences are provided for absolute and relative X-Y cursor addressing •

Cursor Control: Erase, End of Line, Erase of Screen, Form Feed, Delete • Monitor Operation: 50 or 60Hz (jumper selectable).

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EXTRA KEYBOARDS *continued*

Before you install the connecting socket on the computer, make temporary connections to a row and column line to determine whether this method is suitable for your keyboard. Once you have determined that your computer can, indeed, tolerate a tandem keyboard, you can proceed to modify it.

Cable Connections. Open the TRS-80's cabinet, following instructions detailed in the Technical Reference Manual. Carefully raise the keyboard to avoid any strain on the short ribbon cable that connects the two boards. Pull off the board spacers and set the keyboard on its keytops in front of the cabinet with the main circuit board riding loosely in the bottom half of the cabinet. Although the CPU and several other MOS devices wired into the circuit are largely protected from static discharge, it still pays to observe standard handling precautions when working with MOS circuits.

Locate the eight column line resistors, which are clearly identified on the keyboard. Mark the solder pad at the lower end of each resistor with its associated column line. You may or may not be able to locate row lines at row-line buffers because some buffers were interchanged in some keyboard models. A better approach would be to identify row lines directly at the key terminals.

For the TRS-80, touch the negative (com) lead of an ohmmeter set to a medium range, to limit current, to column line D1 at the lower end of resistor R5 and the other test lead to either terminal of keyswitch A (see board labelling). If you obtain a zero resistance reading, the remaining terminal is row line A0; but if resistance is infinite, the terminal being tested is row line A0. Label the solder pad as A0. Similarly, select other keys and locate all row lines. Keyboard ground is line 19 on the board's interconnect cable. Line 1 is at the extreme edge of the keyboard. Trace ground to a convenient solder pad location.

Decide how you wish to route a cable from the computer's or terminal's cabinet. There is ample unused space at the edges of the keyboard in the TRS-80 for installation of an internal disconnect. For a clean cable exit away from heat sinks and main-board adjustment pots, locate the disconnect at the front edge and pass the cable through the front.

A 16-pin DIP socket that mates with a DIP patchcord is very easy to install. When not in use, the exposed male pins at the other end of the patchcord can be protected with a DIP socket. Less easily

installed is a male IDC (insulation displacement connector) made up of Wire Wrap posts inserted on the keyboard to allow use of female IDC patchcords. Also, IDC cables are more rugged, easy to assemble and patch end-to-end with homemade adapters.

Cover the main circuit board to exclude debris and solder splatter. With a wood-block backup, drill the keyboard to accept the 16-pin socket, using pattern board retained with double-stick tape as a drilling template. For the male IDC, drill 0.042" (1.1-mm) holes to accept 20 Vector No. T46-5-9 wrap posts. For front exit, position the disconnect as far from the edge as possible, but do not drill into board traces! Normally, the male IDC is formed using the No. MB45-20 perforated alignment block to back up the board and maintain the installed pins perpendicular. However, to use this block, you must remove both boards from the cabinet to obtain clearance. Lacking the alignment block, use a hardwood block for board backup, keeping it very close to the pin. If you remove the main board from the cabinet, do not disturb trimpots on it.

Use a Vector No. P205 board-pin insertion tool to install No. T46-5-9 wrap posts for the male IDC. This tool eases installation of pins with cross bars in alignment as required to accept a female IDC plug. Lacking this tool, over-drill board holes slightly to ease pin

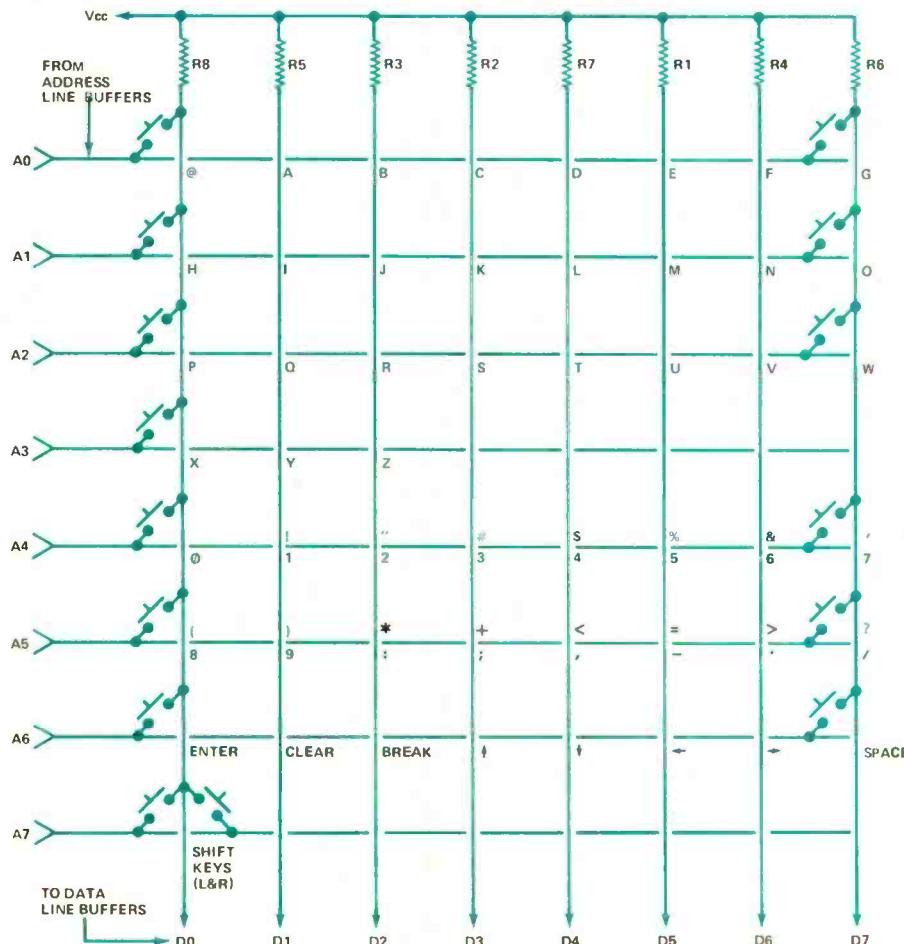
insertion and install using longnose pliers. Wire the connections to the marked row and column lines. Use the four extra wires on the 20-conductor IDC cable as a ground screen. Assign the outermost and two intermediate conductors to ground. Check soldered connections for presence of solder splatter and excessive solder. Install the keyboard into the cabinet and straighten any misaligned wrap posts on the top with longnose pliers.

Install a 12" (305-mm) cable for front exit. Fabricate the IDC cable using Vector No. KS2-20 20-pin female IDC plugs and mating cable No. KW2-20-10. Press the IDC plug onto the end of the cable using a smooth-acting vise or use the P187 IDC fixture. For a longer cable run, make a second 24" (610-mm) cable and fabricate a male IDC adaptor to join IDC cables end to end. Cut the top half or long end of the No. T46-5-9 wrap post down to 1/4" (6.4 mm), round off the burr and install posts on a small piece of perforated board. Note: you can face IDC plugs the same way or one up and one down on a cable. If you use a cable-splice adaptor in lieu of changing the entire cable, you must use the adaptor in every setup because cable line transpositions occur at the splice.

Keyboard Assembly. Inexpensive surplus desktop calculator keyboards as shown in the photos are suitable for tan-



Desktop calculator keyboard can be cut apart to make smaller keypads. The pencil at right points to removed top part of keyswitch. Topsides brass stampings form part of switch and key strings.



Schematic shows 8×8 matrix layout of the TRS-80 keyboard, which is typical of boards of this type. A keyswitch is located at each intersection of the matrix to generate an output for a specific character.

dem hookups and require only slight alterations. The key bodies are thermally staked to the phenolic board, and one terminal of each switch is available on the bottom. A top-side circuit made up of thin brass stampings serves as switch contacts and interconnecting lines to form key strings that have a common connection. The top portion of each switch is removable to reveal the working parts and snap-action disc.

Let us implement a numeric keypad for the TRS-80. From the keyboard matrix diagram, keys 0 through 7 require a 1×7 matrix or key string, with the common side of the switches connected to row line A4 and the isolated side of the switches connected to the column lines. Keys 8, 9, and decimal point require a 1×3 key string, with the common side of the switches connected to row line A4 and the isolated side of the switches connected to the column lines. Keys 8, 9, and decimal point require a 1×3 key string, with the

common side of the switches connected to row line A5 and remaining switch terminals connected to column lines D0, D1, and D6. The numeric set of this keyboard was a 1×10 key string, with keys 8, 9, and decimal point at one end of the string.

To separate the required 1×3 key string, cut off four plastic nubs on the bottom and remove the number 7 key body. Use a fine-toothed, broken-off hacksaw blade to cut the metal band alongside key 8 and remove the top part of the switch body. Sparingly, apply epoxy cement to the plastic pegs of the key body and install using a clamp for a tight fit. Clean switch parts with alcohol and reassemble the switch.

Trim and install the keypad in a small case. The numeric keypad shown is housed in a Vector No. W20-46-31B Multi-Mod case. The trimmed keypad slides into case-card grooves. Punch holes in the panel using a Greenlee chassis punch to pass the key shanks.

Using the full keyboard, install in the Vector No. 51X-1 aluminum frame. Trim the keyboard to length to fit frame grooves and cut a top panel to size. Secure the keyboard to the punched panel using four machine screws and extra nuts for spacing. Finally, mark key-switch terminals with the required row and column lines and wire to an IDC male connector or DIP socket. The aluminum frame accepts the M6088-3-1 perforated bottom plate; otherwise, cut a plate to size and install.

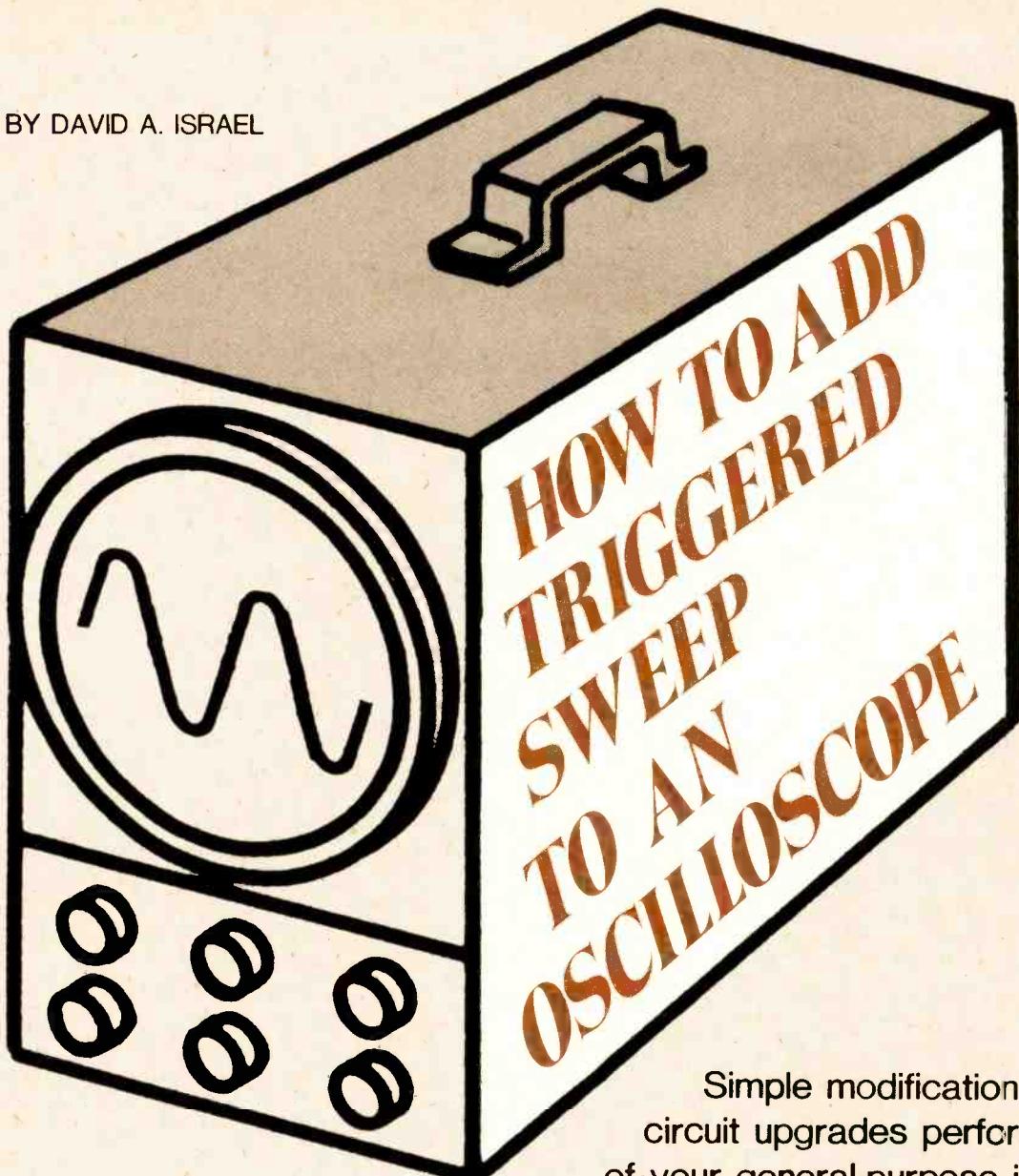
Assign extra keys to any desired matrix character or command. Six keys already wired in a 1 x 6 key string provide hex letters A through F. With some trace cutting, remaining keys can be assigned to the TRS-80 T-Bug monitor commands. Two keys on this keyboard were latching on/off switches. We removed the top part and snap disk from two switches of a spare keyboard and installed them in the on/off switch bodies. Then we relabelled keytops.

Keystrokes on a full typewriter keyboard are usually fully isolated, normally open spst types, but check before you buy. The surplus typewriter keyboard may differ in some respects and may contain extra keys and keytop label variations. With some relabelling of keys, these make excellent tandem keyboards that allow a student and instructor to operate the same computer from different locations.

The possibility of connecting several additional keyboards in tandem may occur to some readers. However, you cannot run long lengths of ribbon cable with wild abandon. Our tandem keyboard was tested using 10' (about 3 meters) of KW2-20 ribbon cable with four lines assigned as a ground screen. This is not good practice because the lengthy cable is not adequately buffered and is not fully ground-planed. Also, its lines are not terminated. The TRS-80 performed satisfactorily but in all likelihood with a reduction in noise margin. It is recommended that cable length be limited to 4' or 5' (1.2 to 1.5 m) and no more than required in any case.

Conclusion. From the foregoing, you can readily see that adding a keyboard in tandem with one in an existing computer system or terminal is a relatively simple matter. Although we used a Radio Shack TRS-80 computer to demonstrate how to perform the modification, the procedure is readily adaptable to most other types of personal computer systems.

BY DAVID A. ISRAEL



Simple modification
circuit upgrades performance
of your general-purpose instrument

IF YOU ARE still struggling along with an old, service-type recurrent-sweep oscilloscope, your instrument is woefully inadequate for modern needs. However, one can upgrade such a general-purpose scope's performance at relatively little cost simply by adding the high-performance triggered-sweep circuit described here. In comparison with an earlier triggered-sweep add-on (POPULAR ELECTRONICS, May 1978), the new circuit is much faster and triggering sensitivity does not interact with output amplitude among other benefits.

This circuit can be added to most scopes to produce calibrated triggered sweeps at speeds from 0.5 s to 0.5 μ s/division in the standard 1-2-5 format. In addition to manual trigger-level selec-

tion, it features free-run capability with automatic triggering, and adjustable input-stage gain and frequency response for easy triggering on low-level and noisy signals. A LED tells you when a sweep is being generated. Cost is about \$35.

About the Circuit. The heart of the circuit, shown in Fig. 1, is field-effect current regulator CR1. This device adjusts its resistance to provide a constant current with only slight regard (within limits) to the voltage applied across it.

Since the rate of change in voltage across timing capacitor C_T is directly proportional to the current flow, keeping the charging current constant causes the capacitor voltage to rise linearly. Applying this linear ramp waveform to

the horizontal axis of the scope makes the electronic beam move equal distances across the CRT screen in equal time increments. The sweep rate is also inversely proportional to the value of C_T . Therefore, to obtain varying sweep rates, the charging current is kept constant, while the value of C_T is changed.

The input of IC1 is isolated from dc by C1, while D1 and D2 clamp excessive-amplitude signals. Resistors R4 and R5 provide biasing for IC1 so that the output can symmetrically vary within the supply range. Stage gain for IC1 is either $\times 10$ through R2 or $\times 1$ through R3. When S2 switches in C3, stage bandwidth is limited to allow reliable triggering on slow input signals on which high-frequency noise is superimposed.

(continued on page 62)

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FACTS YOU NEED TO KNOW The Ion Fountain™—System Five

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<i>Warranty:</i>	1 year
<i>Output voltage:</i>	15KV
<i>Ozone:</i>	Less than 2 parts per billion
<i>Dimensions:</i>	5 $\frac{3}{8}$ " x 4 $\frac{1}{4}$ " x 2 $\frac{3}{8}$ "

Executive System Four™

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<i>Output voltage:</i>	15KV
<i>Ozone:</i>	Less than 2 parts per billion
<i>Dimensions:</i>	11" x 5" x 4"
<i>Use:</i>	Large room or office 10,000 cu. ft.
<i>Warranty:</i>	1 year

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Comparator *IC2* determines the actual trigger point on the input waveform. Two modes of operation are selectable via *S4*. In NORM, the *IC1* signal is compared with a dc voltage set by TRIG LEVEL control *R7*. When the voltage at the + input of *IC2* exceeds that at its - input, *IC2*'s output swings positive, and vice versa. Resistor *R10* adds positive feedback to the circuit, and the approximately 0.5-volt hysteresis prevents generation of multiple outputs with noisy input signals.

In AUTO, $R7$ is switched out of the circuit and is replaced by $R11$ and $C4$. Now, $IC2$ operates as an astable multivibrator at approximately 50 Hz in the absence of an input signal. This provides a constant scope trace base line for operator convenience and allows dc input levels to be measured.

When a greater than 50-Hz signal is

applied to the input, $I/C2$ automatically synchronizes to the input signal. With $S4$ set to NORM, $S3$ selects triggering on either the positive or the negative slope of the input waveform. When $S4$ is set to AUTO, $S3$ has no effect.

The remainder of the circuit controls the charging and discharging of C_T to produce the sweep waveform. When the circuit is quiescent (not triggered), the not-Q output of $IC3$ is high and $Q1$ conducts to discharge C_T and prevent recharging as long as not-Q is high. Note that not-Q also sets the J input of $IC3$ to high. Since the K input is tied to ground, the flip-flop must change states on the next clock input.

When the positive-going edge of the trigger pulse is applied to the CK input of IC3, the flip-flop changes states. Now, Q1 cuts off and allows C_T to charge through CR1 to produce a linear sweep.

When not-Q goes low, Q goes high and TRIGGERED LED1 comes on to signal that triggering has occurred. The J and K inputs of IC3 are now both low, and the flip-flop is immune to any trigger pulses that might occur in the sweep.

The selected C_T capacitor charges until the voltage across it just exceeds the voltage at the $R15/R16$ junction. When this occurs, comparator $IC4$, whose output has been at near ground potential, generates a positive reset pulse for $IC3$. This forces $IC3$ back into quiescence, turning off $LED1$ and turning on $Q1$ to rapidly discharge C_T . As C_T rapidly discharges, the scope's electron beam rapidly retraces to the starting position on the left side of the scope CRT screen.

Construction. With the exception of *S1* through *S5*, *R7*, and *LED1*, which mount

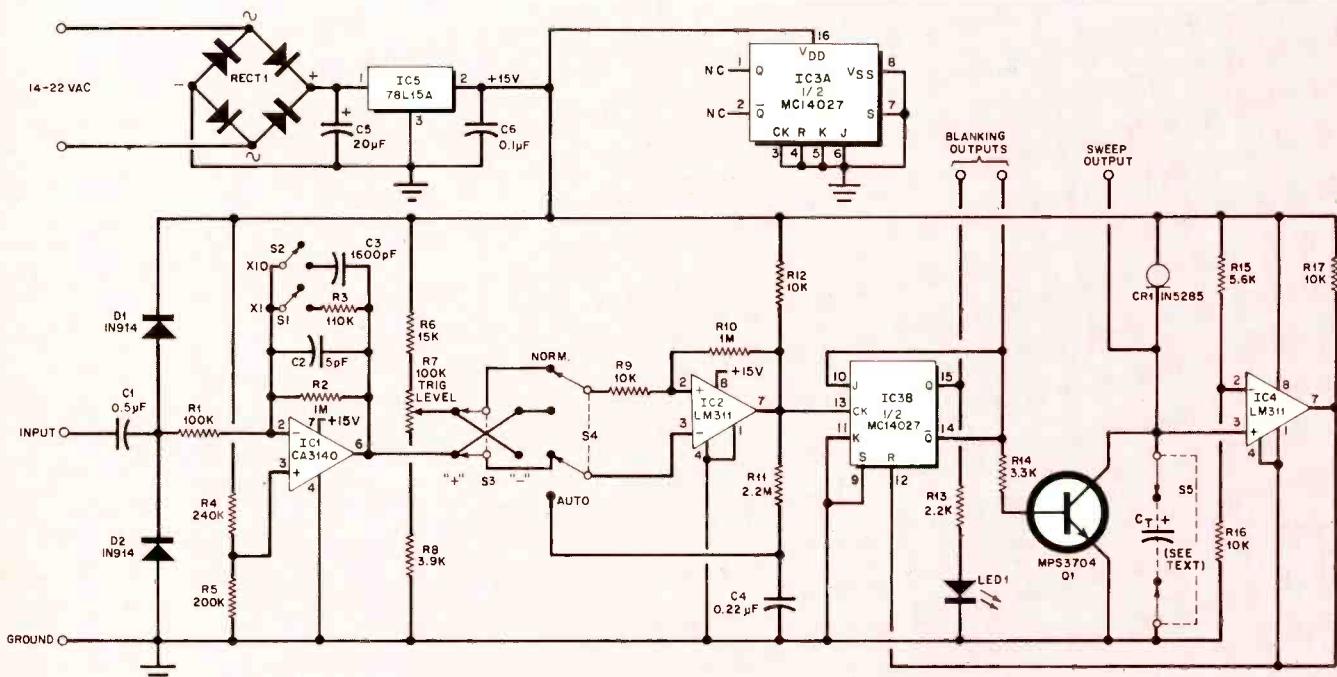


Fig. 1. A linear ramp is generated across the timing capacitor by the current regulator CR1.

PARTS LIST

- C1—0.5- μ F, 600-V
 C2—5-pF ceramic
 C3—1600-pF ceramic
 C4—0.22- μ F, 50-V miniature monolithic
 C5—20- μ F, 35-V electrolytic
 C6—0.1- μ F, 50-V miniature monolithic
 C_T—Timing capacitor (see text)
 CR1—1N5285 field-effect current-regulating diode, 0.27 mA (Motorola)
 D1,D2—1N914
 IC1—CA3140S MOS bipolar op amp
 IC2,IC4—LM311N comparator
 IC3—MC14027CP dual J-K flip-flop
 IC5—78L15A 15-V voltage regulator
 LED1—Discrete LED
 Q1—MPS3704 general-purpose npn small-signal transistor (or similar)
 RECT1—50-PIV, 1-ampere modular bridge rectifier
 The following are 1/4-watt, 5% fixed resistors unless otherwise noted:
 R1—100,000 ohms
 R2,R10—1 megohm
 R3—110,000 ohms
 R4—240,000 ohms
 R5—200,000 ohms
 R6—15,000 ohms
 R7—100,000-ohm linear-taper potentiometer
 R8—3900 ohms
 R9,R12,R16,R17—10,000 ohms
 R11—2.2 megohms
 R13—2200 ohms
 R14—3300 ohms
 R15—5600 ohms
 S1,S2—Miniature spst switch
 S3,S4—Miniature dpdt switch
 S5—2-pole, 2-23 position rotary selector switch (Centralab PA-4003 or similar)
 Misc.—Pc board, mounting hardware, knobs, LED panel-mount adapter.

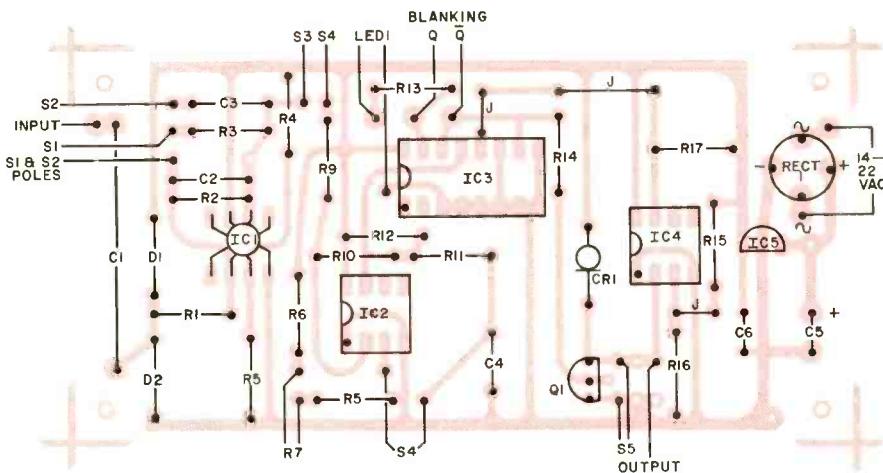
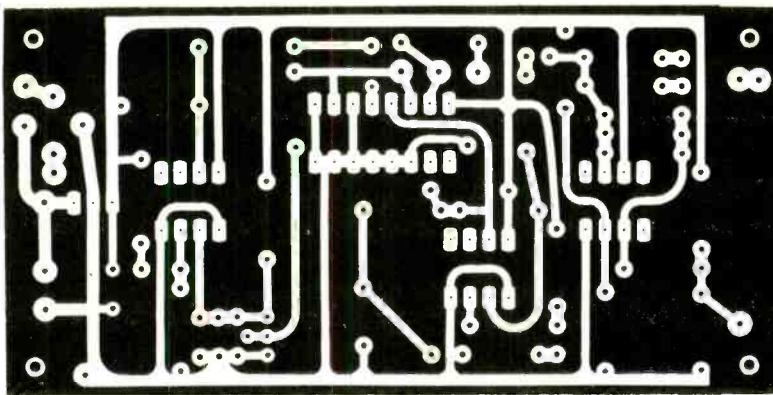


Fig. 2. An actual-size etching and drilling guide for a printed-circuit board is shown at top. Below it is guide for component placement.

on the scope's front panel, all components mount on a small printed-circuit board. An actual-size etching and drilling guide for the board is shown in Fig. 2. During installation of the components on the board, be sure to observe the proper polarities and orientations of the diodes, CR1, and ICs. Also, be sure to observe the safe handling procedures for IC1 and IC3, which are MOS devices.

The C_T timing capacitors mount directly on SWEEP SPEED switch S5. No values are given for these capacitors in the Parts List since they are hand selected to minimize cost while providing the necessary accuracy. More about this under Calibration.

The circuit board is best mounted inside the scope, although a separate case can be used if desired. Inside the scope, try to locate the board as far as possible from heat-producing components. Unless you wish to retain the recurrent-sweep generator in the scope, disable this circuit and remove the associated controls from the front panel. When mounting the TRIG LEVEL control, switches, and LED1 on the panel, it may

be necessary to drill additional holes to accommodate them.

You may wish to use a rotary switch on TRIG LEVEL control R7 for S4 instead of a miniature toggle switch. This will allow you to turn R7 to one end of its travel to switch the circuit to AUTO. Also, if you wish to avoid drilling holes in your scope, S1 and S2 can be replaced by a double-pole, four-position rotary switch.

If your scope has a +18- to +30-volt power supply, you can omit RECT1 and connect the dc supply to the input of IC5. Alternatively, you can use a small filament transformer rated at 14 to 22 volts rms to supply power. The circuit draws typically 20 to 25 mA.

The pickoff point for the trigger signal depends on the scope being modified. Ideally, it should be at a point in the scope's vertical amplifier after the input attenuator and any gain controls so that the input voltage varies over a limited range, in the region of 0.5 to 20 volts peak-peak. (Refer to the schematic diagram of your scope.) In some cases, the scope manufacturer will make this easy for you by using such a point as a source

of sync signal to the recurrent sweep.

Your scope may have a horizontal mode selector that provides sync from + and - slopes of input signals, as well as from the 60-Hz line and external sources. This type of selector is an ideal trigger pickoff point and provides switch-selectable trigger signals. If such a switch is present, S3 in the project is redundant and can be eliminated. It is very useful to have the capability to connect the input of the trigger circuit directly to the external input jack because in some cases the poor response of the scope's vertical amplifier will severely limit trigger generator performance at high frequencies.

Connect the sweep output to the input of the scope's horizontal amplifier. Direct coupling works best. With capacitive coupling, you will have to keep recentering the trace as the average dc level of the sweep waveform varies with changing proportions of sweep period and repetition rate for different signals. In some cases, the coupling capacitor at the input of the scope's horizontal amplifier can be removed if it is not blocking a dc bias level that will be fed into the sweep circuit. The sweep output of the trigger circuit is designed to be connected to a typical horizontal amplifier that has a 1-megohm or greater input impedance. Lower impedances will shunt charging current from C_T and generate a nonlinear sweep waveform.

If the circuit you are driving has less than 1-megohm input impedance, use a buffer amplifier between it and the trigger sweep. A CA3130 op amp connected in a standard voltage-follower configuration, powered from the existing single 15-volt supply, will do.

The Q and not-Q outputs of IC3 should go to pads for connection to the Z-axis circuit of the scope to provide retrace blanking. The not-Q output is at 0 volt during the sweep and switches to +15 volts during retrace, while the Q output is complementary to this. Choose the output that is correct for your scope. Again, dc coupling is preferred if available in your scope. Capacitive coupling will differentiate the blanking pulse. While you may get satisfactory retrace blanking, the beam can recover its brightness before beginning the next sweep, resulting in a vertical line at the left side of the trace. Also, when sweep begins, the blanking signal switches state rapidly, causing the coupling capacitor to charge in the opposite direction and resulting in undesirable intensification of the trace.

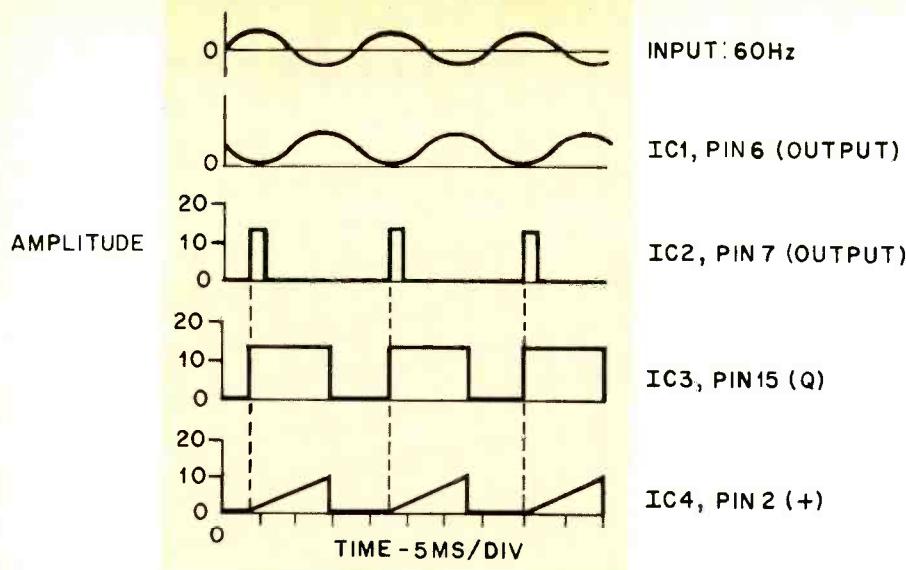


Fig. 3. Representative waveforms to be used in troubleshooting, with S1 on X1, S2 open, S3 on +, S4 on NORMAL, R7 three-quarters CCW and the timing capacitor selected for 1 ms/div.

The last problem can be reduced by first passing the blanking signal through one coupling capacitor to differentiate it and then diode clipping the unwanted half of the resulting waveform and finally connecting this signal to the Z-axis coupling capacitor.

A word of caution: In many scopes, the coupling capacitor is connected directly to the grid or cathode circuit of the CRT, which may be operating at 1000 or more volts. Do NOT attempt to bypass this capacitor or serious damage will result. A coupling capacitor can be removed from the circuit *only* if it is not blocking a dc bias voltage.

Test and Calibration. Temporarily connect a 1- μ F tantalum capacitor across the C_T terminals, observing polarity. Turn on the scope and adjust for a moderate-intensity dot in the middle of the screen. Apply power to the sweep circuit. Set S4 to AUTO; a horizontal baseline trace should appear on the CRT and the TRIGGERED LED should come on. With this value of capacitor, the trace and LED indicator should flicker rapidly at the same rate.

If a trace does not appear, check the scope's BRIGHTNESS control and for +15 volts on the trigger-sweep bus. Representative waveforms for trouble-shooting are shown in Fig. 3. In this test, S1 is set to $\times 1$, S2 is open, S3 is at +, S4 is set to NORMAL, R7 is three-quarters CCW, and C_T is selected for 1 ms/division.

Using this setup, apply a 1-volt, 60-Hz sine-wave signal to the scope's vertical input. The sweep should automatically lock onto this signal and a steady display of three to four cycles should be seen on-screen. Check for any obvious nonlinearities. Rotate TRIG LEVEL control R7; the trace should disappear and reappear and the trigger level should vary up and down one side of the sine wave. Also note the change in the sensitivity of R7 when ATTENUATOR S1 is switched from $\times 1$ to $\times 10$.

Center the scope trace and note its length. Before you can calibrate the sweep for a given time per unit length, overall length of the sweep must be set to a given repeatable value. (To ensure that the sweep is not inadvertently adjusted after calibration, the horizontal-gain control can be mounted inside the scope, or it can be replaced with a pair of fixed resistors.)

Adjust the length of the trace to fill the screen. In some cases, the frequency response of the scope's horizontal amplifier may roll off at a lower frequency than those generated by this circuit at the highest sweep speeds, resulting in a shorter trace. You can compensate for this by setting the horizontal gain so that the trace is longer than the width of the screen at slow speeds. This will not affect accuracy at any speed, since each range is individually calibrated.

To calibrate the sweep, you need a source of reasonable-accuracy (1% will

do) square waves. A crystal-controlled timebase is ideal. You can also use a signal generator and frequency counter.

Before starting, wire the pc board terminals to the rotor connections of SWEEP SPEED selector S5, using a length of two-conductor cable that will be appropriate for the physical layout of your scope. It is important that you do this before calibration because the capacitance of the cable will be in parallel with the selected timing capacitors and at the highest sweep speeds will comprise a large portion of the timing capacitance.

Begin calibration at the highest sweep speed and work down. With the capacitance of the cable serving as the timing capacitor, feed a 1-MHz square wave to the scope's input. Adjust the trigger and scope controls for a stable, centered display. To obtain a stable display with low-bandwidth scopes, the vertical amplifier may have to be bypassed with the sweep circuit input connected directly to the signal source. Experiment with several different capacitors connected to the switch until you find the value that produces a sweep speed closest to the desired 0.5 μ s/division but not slower than this. That is, one cycle should occupy two divisions or slightly more. Unless you have a large number of capacitors on hand, you will find that the best way to obtain the exact capacitance value needed will be to parallel one capacitor with a lower-value capacitor until you obtain the desired display. Do your measuring between corresponding points in different cycles of the waveform. Do not, for example, measure between a rising and a falling edge of one cycle or of consecutive cycles. By following this rule, you will avoid errors introduced by asymmetry in the signal source and splaying or overshoot of the trace itself. For best results, choose two points separated by about six or eight divisions and equally spaced from the center line of the scope screen.

In the same manner, select the remaining timing capacitors, soldering them to the lugs of S5 as you proceed. The next value should produce a 1- μ s/division sweep speed, then 2 μ s/division, 5 μ s/division, etc., in the 1-2-5 format. For values larger than 0.5 μ F or so, use high-quality tantalum capacitors and take care to observe polarity.

Operating Hints. The triggered-sweep circuit is very easy to use. For most applications, leave the input amplifier selector set to $\times 10$ and set the mode

switch to AUTO. Then set the number of cycles of the waveform you wish to view with SPEED selector S5. The period of any waveform can be obtained directly from the screen as the time it takes the beam to "write" one cycle, while the frequency is the reciprocal of this time.

Obtaining a stable display of a fraction of a repetitive waveform cycle is also easy. First, adjust the scope's vertical-gain, brightness, and centering controls for a stable display of several cycles. Set S4 to NORM and adjust R7 until the beginning of the portion of interest is at the left side of the screen.

Large-amplitude signals may drive IC1 into saturation, causing clipping and an apparent reduction in the range of the TRIG LEVEL control. If you cannot position the waveform properly, close S1 to reduce the gain of the input op amp stage to unity.

Once the waveform is positioned, increase sweep speed until desired magnification is reached. Advance the brightness as necessary. When using very high-speed sweeps with relatively low-repetition-rate triggers, the scope beam and TRIGGERED LED will be very dim or appear to be off even when a sweep

is present. This is due to the very low duty cycles in these situations.

As mentioned previously, bandwidth and/or noise limitations of the vertical amplifiers of some low-cost scopes may make triggering on high-frequency signals jittery at best or even impossible. In some of these cases (CMOS or TTL logic running in the low megahertz-range, for example), where signal amplitudes are in the 1-to-20-volt range and circuit loading tolerance is not too critical, the trigger signal can be routed directly to the input of the scope sweep circuit.

Another situation in which the best choice of trigger source is not immediately obvious occurs when you are looking for 60-Hz line noise. For example, if you are checking the output of a dc power supply with 1 or 2 mV of ripple, there will often be insufficient gain in the scope's vertical amplifier to yield a clean trigger pulse and the sweep will run free. However, since the ripple will occur exactly at the power-line frequency or a whole-number multiple thereof, syncing the sweep to the 60-Hz line will provide a rock-steady trace.

Providing a trigger-source selector

switch that can disconnect the input of the sweep circuit from the vertical amplifier and connect it to an internal line-voltage source simplifies sweep syncing. The pickoff point can be the secondary of any low-voltage transformer in your scope.

If you wish to gate an external device, such as an oscillator, in sync with the sweep generator, a CMOS-compatible signal is available at the Q output of IC3, which is at 0 volt during retrace and +15 volts during sweep. The inverse of this is present at not-Q. In some applications, you may wish to sweep an external oscillator directly, using the sweep output of the circuit. Use a buffer amplifier if necessary to prevent excessive loading by low-impedance inputs.

Summing Up. By substituting the high-performance triggered sweep described here for the recurrent sweep in an older scope, you can upgrade the instrument to permit better waveform analysis as needed for examining modern circuits. Cost is modest and installation is fairly simple. It will also enable you to hold off on purchase of a costly modern scope for a while longer. ◇

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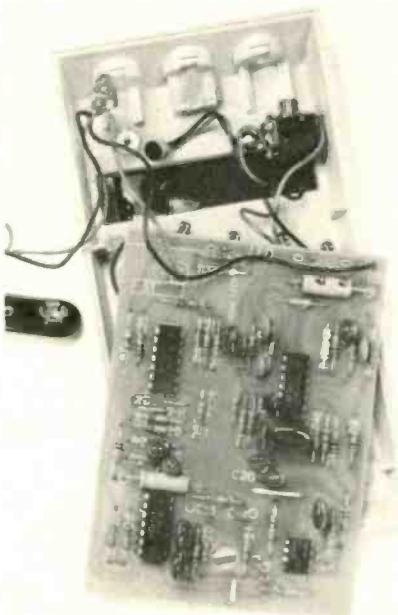
SO-CALLED “electronic lie detectors” have become controversial items. Some workers in the fields of security and law-enforcement swear by them, while others (including some psychologists) hold that the principles on which the devices are based are ill-founded and unscientific. Still other individuals denounce the application of lie detectors as an invasion of privacy.

Actually, the best that these detectors can do is measure psychological

stress. Even then, the measurement is indirect. Basically, the device makes its determination by sensing an effect of one type or another that many researchers believe is an accurate indicator of stress. Validation studies have been used to compile an impressive record of successes, but it should be remembered that a high degree of interpretational skill is required and there is always an appreciable probability for error in using such an instrument.

One popular indicator of stress has been the relative amplitude of certain vocal modulations in a person's speech. The Voice Stress Analyzer described here is a small, readily portable unit. It is designed to operate on the principles pioneered by Dektor and other companies in the field whose products have received wide acceptance.

Basic Theory. Extensive military research and wartime counterintelligence work have yielded several theories and devices that have been used during interrogation in an attempt to separate truth from falsehood. One of these theories is that human voices, which have fundamental frequencies ranging from about 90 to 200 Hz, are normally modulated by an 8-to-12-Hz “microtremor” signal. The latter's effect is usually masked by other voice components; but, according to these researchers, reasonably simple electronic circuitry can detect and measure the microtremors.



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VOCAL ANALYZER *continued*

When a person is under stress, says the theory, normal vocal microtremors diminish greatly in amplitude. The autonomic nervous system, preparing the body for emergency reactions, causes the pupils to dilate, blood to rush away from the limbs, and the muscles to tense. Since the vocal chords are principally muscular tissue, they, too, tighten and decrease the amplitude of microtremors. Thus, it is claimed, measuring the relative amplitude of vocal microtremors gives an indication of stress. The waveform of a human voice with microtremor, indicating no or very little stress, is shown in Fig. 1A, its spectral content in Fig. 1B.

System Operation. Basic operation of the Voice Stress Analyzer is shown in Fig. 2, while Fig. 3 illustrates typical waveforms (not drawn to scale) that occur in the circuit.

The input voice signal in Fig. 3A illustrates the somewhat closer peak spacing attributed to microtremors as compared with the "normal" spacing of the peaks in the voice signal. After amplification, the composite voice signal goes to a voice-frequency bandpass filter to remove extraneous noise. Then the signal input is half-wave rectified. In a 150-Hz low-pass filter, the higher voice frequencies are attenuated, leaving only the lower frequencies, including those of the microtremors (Fig. 3B). The positive-going output then toggles a Schmitt trigger (Fig. 3C) to produce a squared-off waveform. The latter is suitable for toggling a one-shot multivibrator that then

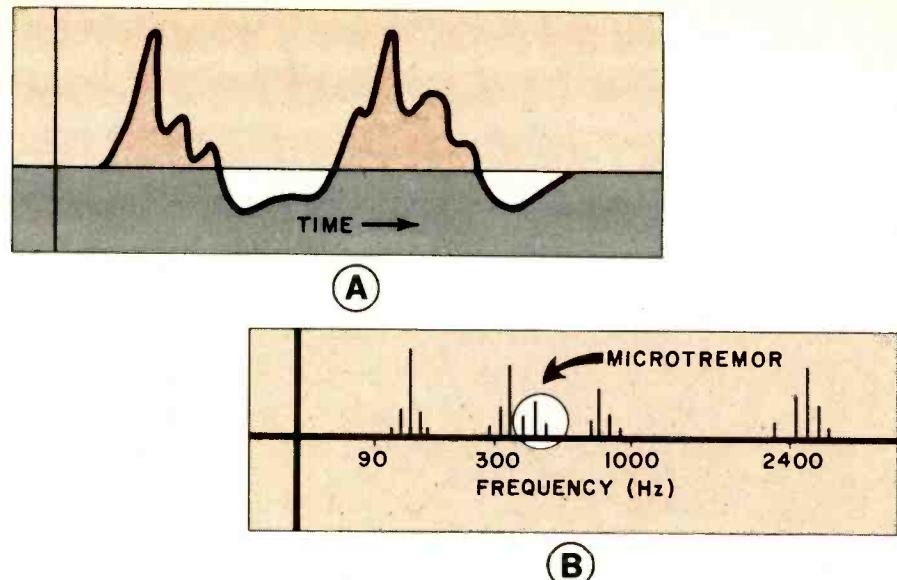


Fig. 1. Waveform of the human voice with microtremors is shown at (A), spectral content of voice is at (B).

produces the 1.5-ms pulses shown in Fig. 3D.

As the 8-to-12-Hz microtremor modulates the fundamental, spacing between pulses changes. Pulses from the one-shot then pass through a 20-Hz low-pass filter and an 8-to-12-Hz filter, after which it is rectified and integrated to form a smooth voltage. This signal may rise above a preset threshold when the microtremors are closely spaced, in a manner similar to that of the vertical-sync scheme used in a TV receiver. When the integrated output is above the threshold, it causes the LEDs to come on in a particular sequence (Fig. 3E).

The Circuit. Figures 4 and 5 illustrate the complete schematic diagram of the Voice Stress Analyzer. The IC2D circuit (Fig. 5) supplies the ground tap required by the op amps. Resistors R_1 and R_2 and capacitor C_1 provide power from battery B_1 for the condenser microphone. Jack J_1 is a transfer type that disconnects MIC when an external audio source is plugged into it. (The external source can be a telephone pickup, dynamic microphone, or output from a tape recorder.)

Audio amplifier IC_{1A} operates close to its open-loop gain whose output goes to the IC_{1B} bandpass-filter circuit. Recti-

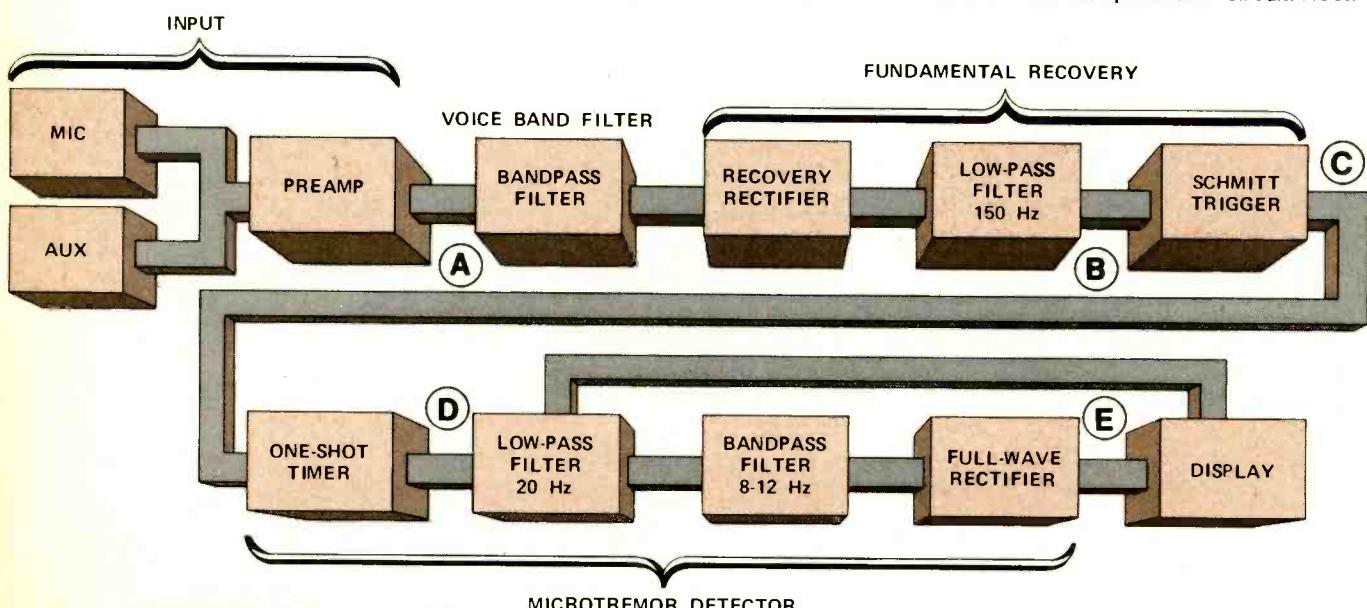


Fig. 2. The analyzer circuit is designed to extract the 8-to-12-Hz microtremor from the voice input and use the resultant signal to turn on a LED display.

fier *D*₁ half-wave rectifies the signal to recover the fundamental modulating frequency. Higher harmonics are removed by *IC*_{1C}, an 18-dB/octave filter that passes only those frequency components below 150 Hz.

Schmitt-trigger circuit *IC1D* converts the recovered fundamental into steep rising and falling edges that are suitable for driving timer *IC4*. As shown in Fig. 3C and D, the Schmitt trigger's sharp rise time toggles the timer, which produces a 1.5-ms pulse.

The generated pulse train goes through low-pass filter IC2A to remove the waveform's sharp edges and amplify any frequencies below 20 Hz. Bandpass filter IC2B is "tuned" to the 8-to-12-Hz microtremor frequency and amplifies any signal within this range.

Full-wave rectifier IC3A/IC3B accepts this signal and produces a dc output voltage that is proportional to the amplitude of the microtremor (Fig. 3E). This voltage is developed across C19, which is constantly being discharged by time-constant resistor R32.

Display drivers *IC3C* and *IC3D* are

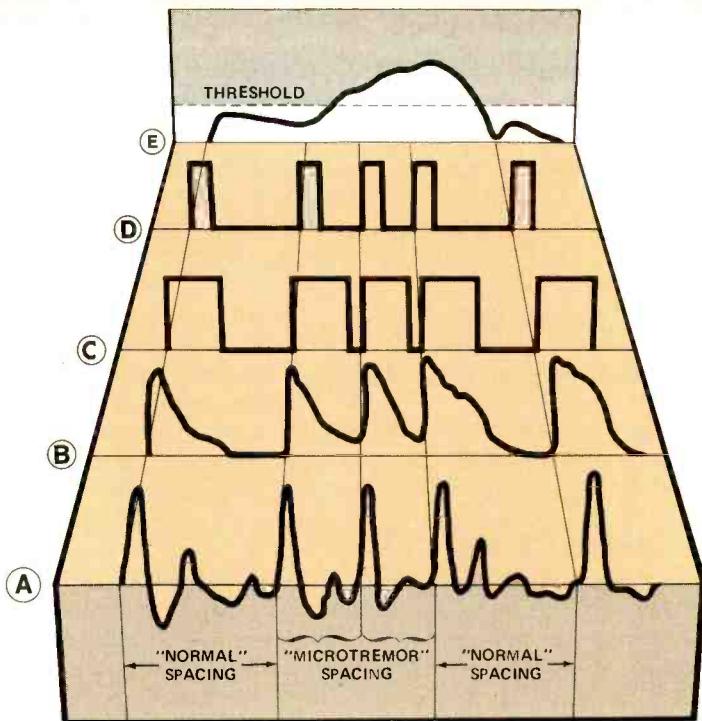


Fig. 3. Typical waveforms within the analyzer. According to the authors, the "trick" lies in detecting the presence of the narrower microtremor peak spacing within the voice frequencies. Integrated one-shot pulses derived from these signals are used to toggle the readouts.

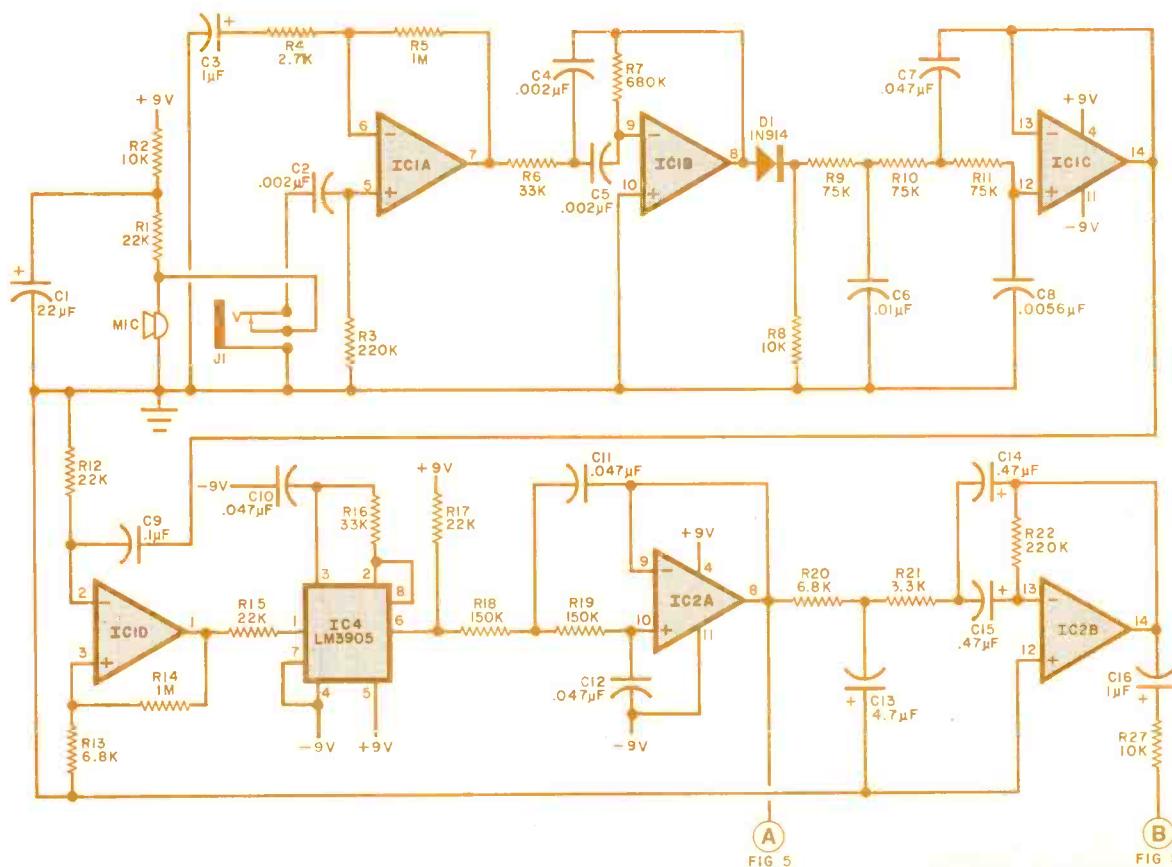


Fig. 4. The voice processing circuits of the analyzer result in 20-Hz signals from IC2A and 8-to-12-Hz signals from IC2B. These signals drive the rectifier/display section shown in Fig. 5.

connected as comparators, using the voltage generated across R33, R34, and R35 as the reference. The comparators then drive the LEDs. When LED1 comes on, presence of microtremors is indicated, meaning no stress. When these frequencies are missing, LED4 comes on to indicate high stress. As microtremors come and go, LED2 and LED3 come on.

The display also receives a control signal from the 20-Hz filter that turns off the LEDs when no input signal is present, conserving battery life.

Construction. Using the actual-size etching and drilling guide shown in Fig. 6, the Analyzer was designed to fit in a calculator-type case. Referring to the component-placement guide in Fig. 6, mount the components in their respective locations, taking care to properly orient the diodes, polarized capacitors, ICs, and LEDs. When installing compo-

nents on pc board, be sure to properly orient diodes, LEDs, ICs, and electrolytic capacitors, as shown in the component placement guide.

With exception of the microphone, auxiliary input jack, power switch, and battery, all components mount directly on the circuit board. The microphone and auxiliary jacks mount in holes at the top of the plastic case. (Make certain that the pickup end of the microphone points outward.) Mount the power switch on the upper surface of the case, below the display window and label its on position with a dry-transfer lettering kit. Connect and solder the positive lead of B1's battery connector to the hole A-pad on the circuit board, the negative lead to the hole B-pad.

Examine the jack and schematic diagram and connect and solder lengths of hookup wire from the jack's lugs to the appropriate E, F, and G pads on the circuit board. If you choose a recharge-

able battery for B1, mount a suitable power jack on the plastic case and wire it to the battery.

Now, use a dry-transfer lettering kit to label the LEDs in the display. Label LED1 NORMAL and LED4 STRESS. Leave transitional LED2 and LED3 without legends. This completes construction.

Construction. Using the actual-size controls, it should be operational as soon as power is turned on. As you speak into the microphone, you should note that the LEDs flicker, with the NORMAL LED on most of the time.

A number of tests were performed on the Voice Stress Analyzer by one of the authors. Using the audio from a TV-network news broadcast, it was noted that when the newscaster spoke, the NORMAL LED was on most of the time. When actors and actresses were speaking their roles, basically the same results were observed. However, when

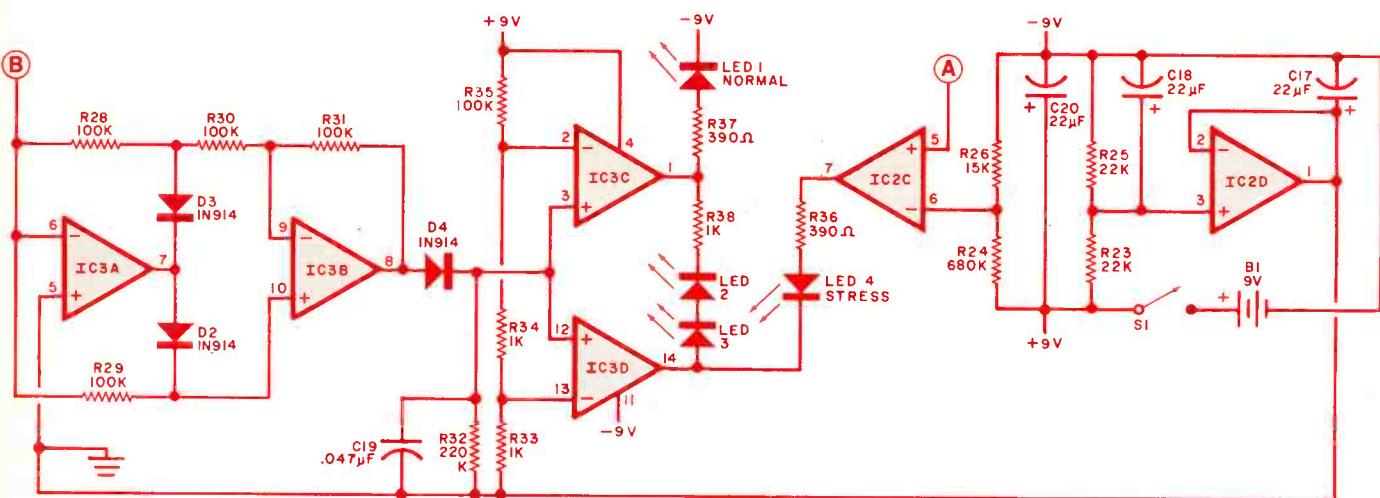


Fig. 5. The 8-to-12-Hz signals are rectified in IC3A and IC3B, integrated in C19 and used to turn on a comparator (IC3C, IC3D) that causes the LED(s) to glow. IC2C shuts down the LEDs when there is no 20-Hz signal, while IC2D creates a bipolar supply from a single 9-volt battery.

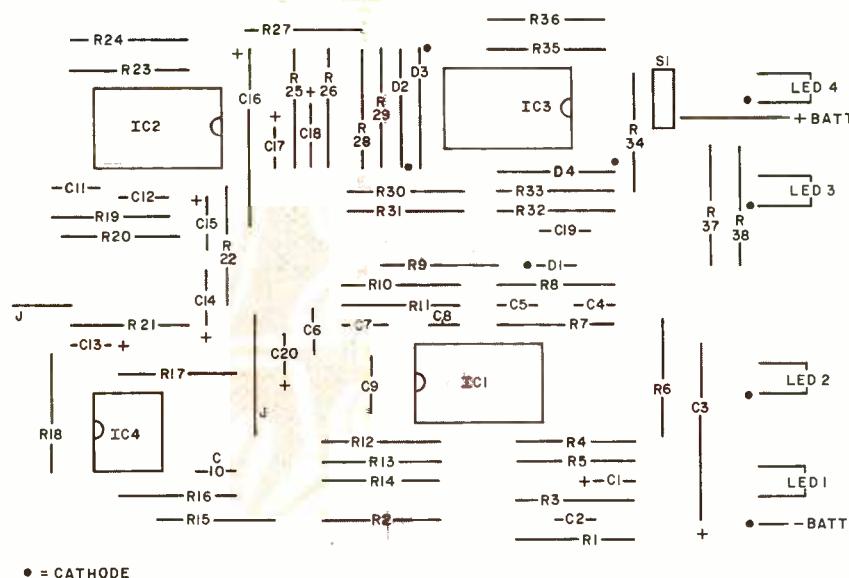
PARTS LIST

- B1—9-volt battery
- C1,C17,C18,C20—22- μ F, 16-volt tantalum
- C2,C4,C5—0.002- μ F, 100-volt Mylar
- C3,C16—1- μ F, 100-volt electrolytic
- C6—0.01- μ F, 100-volt Mylar
- C7,C10,C11,C12,C19—0.047- μ F, 100-volt Mylar
- C8—0.0056- μ F, 100-volt Mylar
- C9—0.1- μ F, 100-volt Mylar
- C13—4.7- μ F, 35-volt tantalum
- C14,C15—0.47- μ F, 35-volt tantalum
- D1 through D4—1N914
- IC1,IC2,IC3—LM324 quad op amp
- IC4—LM3905 precision timer
- J1—subminiature phone jack with switch

- LED1 through LED4—red LED
- The following are 1/4-watt 5% resistors:
- R1,R12,R15,R17,R23,R25—22,000 ohms
- R2,R8,R27—10,000 ohms
- R3,R22,R32—220,000 ohms
- R4—2700 ohms
- R5,R14—1 megohm
- R6,R16—33,000 ohms
- R7,R24—680,000 ohms
- R9,R10,R11—75,000 ohms
- R13,R20—6800 ohms
- R18,R19—150,000 ohms
- R21—3300 ohms
- R26—15,000 ohms
- R28 through R31,R35—100,000 ohms
- R33,R34,R38—1000 ohms

- R36,R37—390 ohms
- Misc.—suitable enclosure, battery clip, hook up wire, mounting hardware, etc.

Note: The following is available from Logical Systems, 3314 H St., Vancouver, WA 98663 (Tel: 206-694-7905): complete kit including microphone, battery clip, pc board, case, and manual for \$79.00. Also available separately: etched and drilled pc board at \$9.00; hand-held case, battery clip with power jack and condenser microphone at \$18.00. Please add \$3.50 for postage/handling. Washington state residents, please add 5.1% sales tax. Allow four weeks for delivery.



• = CATHODE

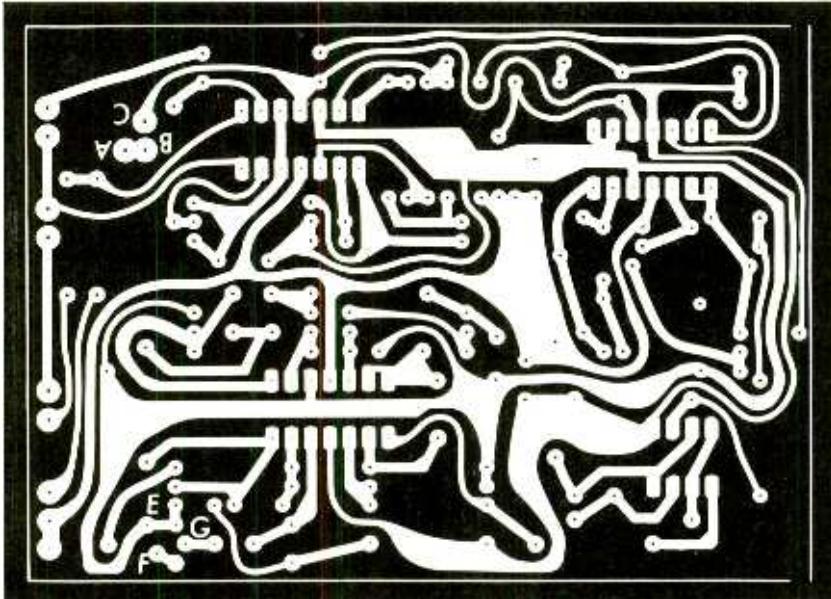


Fig. 6. Actual-size foil pattern and component placement guide for the voice analyzer. Be sure to observe polarities of electrolytic capacitors and diodes and orientation of ICs.

various advertising announcers' voices were monitored, it was interesting to note that the other LEDs had a tendency to flicker on, with the STRESS LED coming on quite often. The same was true when monitoring a number of phone-in radio programs. Finally, a number of situations were rigged, using various people as test subjects, all instructed to lie in answer to certain questions. The results were inconclusive. The results might have been pointedly different if the subjects being monitored were not aware that vocal stress tests were being conducted. Too, it should be kept in mind that voice characteristics differ among different people and even with the same

person over a short period of time.

Psychologists at one U.S. university have stated that there is no conclusive evidence that microtremors actually exist in the vocal chords. One report, prepared by a psychologist on behalf of the U.S. Army's Land Warfare Laboratory at Aberdeen Proving Ground, concluded that results obtained with voice stress devices are "no better than chance." Moreover, American Civil Liberties Union suits have been presented alleging such devices constitute invasion of privacy.

Whether or not voice stress analyzers do what is claimed of them is a debatable point. However, they are interesting devices with which to experiment. ◇

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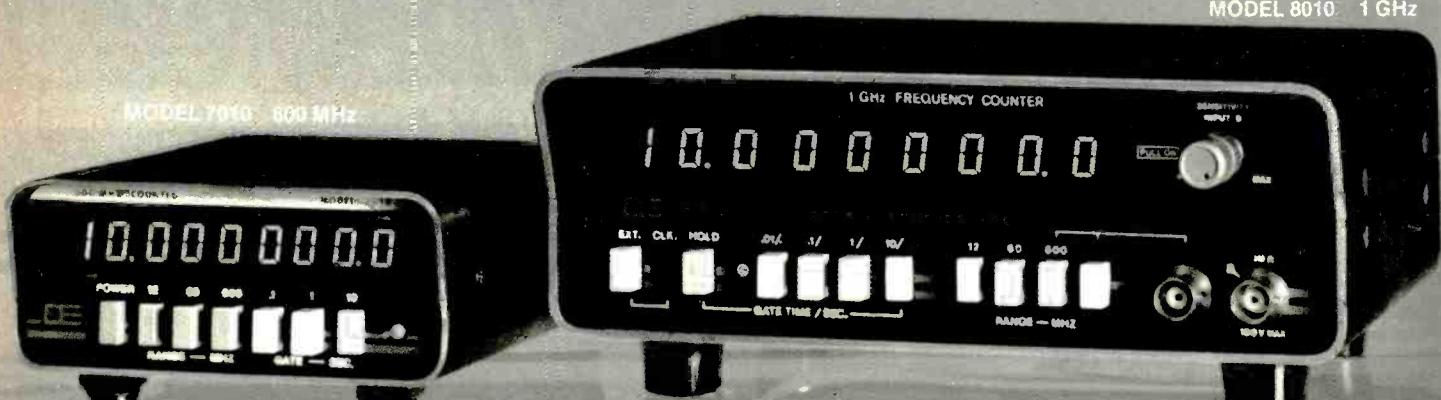
For improved resolution there are 3 gate times on the 7010 and 8 gate times on the 8010 with rapid display update. For example, the 10 second gate time on either model will update the continuous display every 10.2 seconds. Some competitive counters offering a 10 second gate time may require 20 seconds between display updates.

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7010	145.00	600 MHz	9	5-20 mV	10-30 mV	20-40 mV to 600 MHz	1-50 nsec	.1Hz	1Hz	10 Hz 500 MHz	1 PPM	10 MHz	YES OPTION \$25.	
*7010.1	225.00									0.1 PPM	0.1 PPM		YES OPTION \$15.	
8010	325.00	1 GHz	9	1-10 mV	5-20 mV	10-25 mV	1-50 nsec	10.01-20 SEC	.1 Hz	1 Hz	10 Hz 1 GHz	1 PPM	10 MHz	YES STD
*8010.1	405.00									0.1 PPM	0.1 PPM		YES OPTION \$30.	

* Has precision 0.1 PPM TCXO time base.

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TRUTH TABLE QUIZ

BY ROBERT P. BALIN

A TRUTH Table indicates how a gate or combination of gates, responds when level 0 and level 1 signals are applied to its inputs. The table present the kind of concise picture of a circuit's characteristics that we need to apply it to solving logic problems.

To test your ability for making a truth table, determine if the output at D on each of the circuits (1-10) below is a 1 or a 0 for each of the seven arrangements shown in the table at top left. The answers are in the truth table at bottom of page.

ANSWERS:

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
2	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
3	1	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
4	1	1	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
5	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
6	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7	1	0	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	
8	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0	1	
9	1	0	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
10	0	1	0	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1
11	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1
12	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1	0	1	1
13	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1
14	0	1	1	1	1	0	1	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0
15	1	0	1	1	1	1	0	1	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1
16	0	1	1	1	1	1	0	1	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1	0	1	1	1
17	1	0	1	1	1	1	1	0	1	1	1	1	0	1	1	1	1	0	1	1	1	1	0	1	1	1	1
18	0	1	1	1	1	1	1	0	1	1	1	1	1	0	1	1	1	1	0	1	1	1	1	0	1	1	1
19	1	0	1	1	1	1	1	1	0	1	1	1	1	1	0	1	1	1	1	0	1	1	1	1	0	1	1
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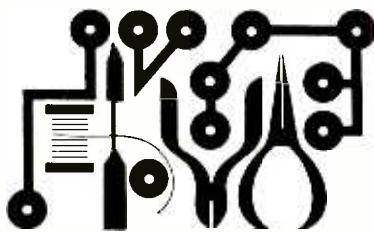
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Experimenter's Corner



By Forrest M. Mims

THE PHOTOPHONE CENTENNIAL: 1880-1980

HAVE YOU ever talked over a sunbeam? I hope every reader of this column will do just that during 1980, for this is the centennial year of the invention of light-wave communications.

On February 19, 1880, Alexander Graham Bell and Sumner Tainter, Bell's lab assistant, became the first men to transmit voice over a beam of reflected sunlight. One kind of transmitter they developed, shown in Fig. 1, was a thin, silvered mirror attached to one end of a hollow cylinder. Sound waves were directed against the mirror through a speaking tube. The resulting vibrations of the mirror caused a reflected beam of sunlight to become more or less divergent. The net result was an amplitude-modulated light beam.

Bell's receiver consisted of a series of selenium cells mounted in the focus of a parabolic reflector and connected in series with a telephone receiver and a battery. Figure 2 shows one of Bell's early optical receivers.

Bell called his invention the *photophone*. In June of 1880, he and Tainter transmitted intelligible voice from the top of the Franklin School in Washington, D.C. to Bell's laboratory at 1325 L Street, a distance of 213 meters. Later Bell and Tainter were granted several patents covering the photophone and its variations. Until his death in 1922, Bell considered the photophone to be his most important invention, more important even than the telephone.

If you would like more information about the photophone, I've written a detailed paper on the subject which appears in the Spring edition of *Optics News*, a publication of the Optical Society of America (available at well-stocked libraries). Also, if you happen to be in Washington, D.C. this spring or summer, stop by Explorer's Hall, the museum of the National Geographic Society at 17th and M Streets, N.W., to see their excellent photophone centennial exhibit. It was constructed by Bell Telephone Laboratories, and traces the history of light-wave communications from the photophone to today's glass-fiber communication links.

Alexander Graham Bell played a pioneering role in the early history of the National Geographic Society. His grandson, Dr. Melville Bell Grosvenor, is Editor Emeritus of the *National Geographic*. Several

years ago, when I met with Dr. Grosvenor to propose a photophone centennial exhibit, his interest perked up considerably when I pulled a homemade photophone from my briefcase. He scurried out onto the balcony to catch a few rays of sunlight, and we were soon communicating over his grandfather's invention.

That was a very exciting moment for me, and one I hope to share with you by means of this column. You can be "on the air" in a matter of minutes with an aluminum-foil-and-cardboard transmitter and a receiver made from a solar cell and a portable amplifier! With your own photophone, you'll never be without an entertaining and educational gadget to demonstrate for friends, neighbors, scout troops and school classes. Indoors, at night, or when clouds obscure the sun, you can use light from an artificial source. I've used many kinds of flashlights, a helium-neon laser, infrared LEDs and a continuously operating (CW) injection laser with good results. Interested? Here are some details.

Photophone Transmitters. Bell and Tainter devised many ways to modulate a light beam, but the simplest is the use of a flexible mirror. My favorite photophone transmitter, shown in Fig. 3, is a 25-mm diameter, ultra-thin glass mirror cemented to one end of a 1" (25.4 mm) diameter aluminum tube. The mirror is catalog number 30,626, available from Edmund Scientific Company (300 Edscorp Bldg., Barrington, NJ 08007).

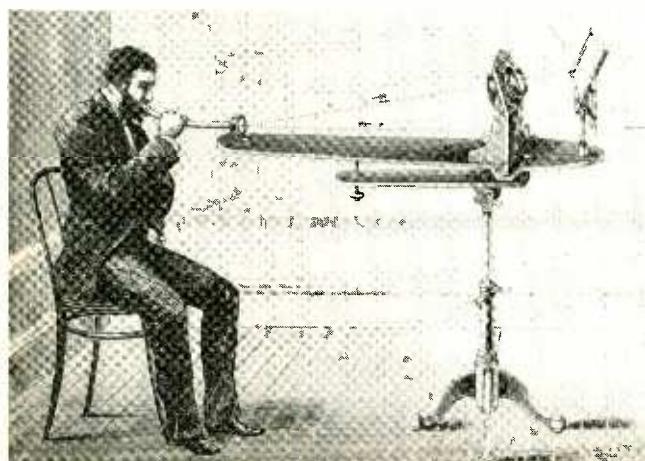
A larger mirror will give more range, but suitable glass mirrors are hard to find and are very fragile. Bell solved this problem by using a system of lenses to collect more light than would otherwise be intercepted by the mirror alone (see Fig. 1). You can take this approach also, but a suitable alternative is the use of a mirror fabricated from aluminum foil or aluminized Mylar.

A powerful transmitter can be made by taping a sheet of foil or Mylar over one end of a metal can from which both ends have been removed. The Mylar is easier to attach and forms a highly desirable flat, drum-like surface. Unfortunately, aluminized Mylar, at least the type which I've used, is not quite as reflective as aluminum foil. A simple test shows that about 5% of incident sunlight passes through the thin film of aluminum deposited on the Mylar and is therefore not available for reflection.

Aluminum foil is almost perfectly reflective, but it tears easily. Another problem with foil is the difficulty of obtaining a perfectly flat surface. Both of these problems can be partially alleviated by crossing strips of masking tape across the dull side of a sheet of foil (use four strips) and centering the shiny side of the foil out over the end of the can. The tape reduces tearing, keeps the foil reasonably flat and improves the sound quality by damping out resonances.

Instead of a metal can, the Mylar or foil can be taped over a 4" to 6" (10-cm to 15.25-cm) diameter hole cut in a square of corrugated cardboard. This method works well with foil because it results in less chance of tearing.

You can experiment with other kinds of transmitters. Several years ago, at a hot-air balloon competition in New Mexico, Otis Imboden, a *National Geographic* photographer, and I experimented with a large foil-covered board he was using to reflect sunlight at balloon crews that were shadowed by the huge bags of hot air rising above them.



Photos courtesy Bell Labs.

Fig. 1. The photophone transmitter used by Bell and Tainter in their historic experiment of 1880.

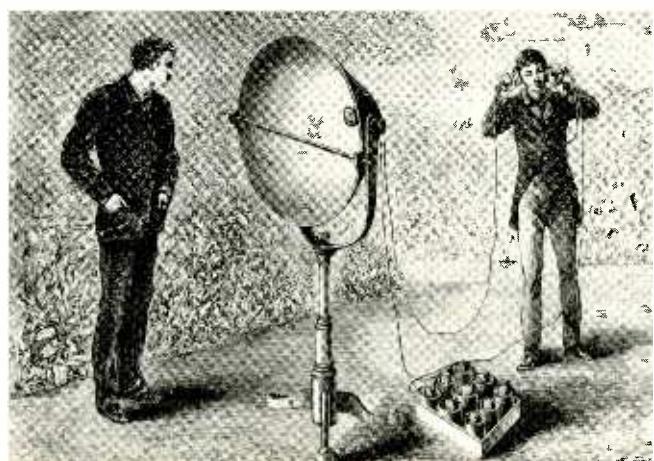


Fig. 2. A photophone receiver of 1880. The detector is the cylindrical object in the reflector.

We found that we were able to send voice messages to a nearby receiver simply by talking near the reflector. Later, we gave a receiver to a balloon crew. Otis spoke to the pilot with the help of his reflector while the balloon was in tethered flight.

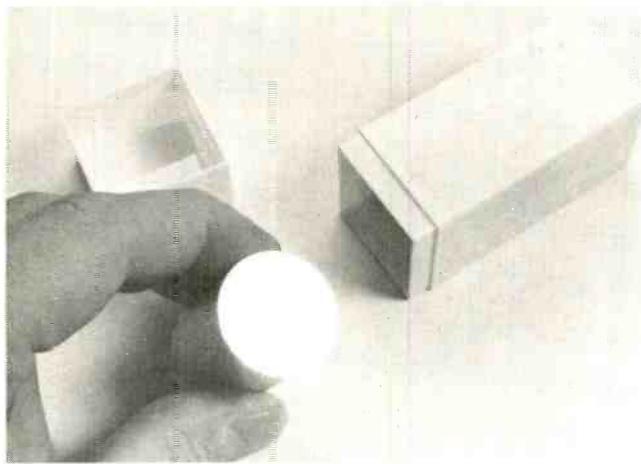


Fig. 3. A photophone transmitter is easily made using a 25-mm diam. mirror cemented to an aluminum tube.

Passive transmitters like those described thus far work fine, but you can make an electronic photophone transmitter by cementing a thin glass mirror to the rim of the cone of a miniature speaker. Refer to the Edmund Scientific catalog for suitable mirrors. This technique results in very high quality voice transmission and allows one person to conduct photophone tests unassisted because the transmitter can be driven by signals from the earphone or external speaker jack of a portable radio or tape player.

Photophone Receivers. Bell and Tainter experienced considerable difficulty making selenium detectors for their photophone experiments, but today you can purchase for a few dollars a silicon solar cell that's considerably more sensitive and easier to use. I prefer silicon solar cells for photophone receivers because their large surface area (the larger the better) reduces or eliminates entirely the need for collecting lenses or reflectors for short-range experiments. When a lens or reflector is used to increase communications range, the greater area of the detector does away in large part with the alignment difficulties associated with the use of small detectors such as phototransistors.

An ultra-simple receiver can be made by connecting a silicon solar cell directly to the microphone input of an audio amplifier. Figure 4 is the schematic of a circuit with plenty of gain that works quite well. Rather than building an amplifier, you can salvage one from a discarded cassette recorder or purchase a factory-assembled amplifier module from one of the dealers who advertise in this magazine.

Silicon solar cells are very thin and are easily broken. One way to protect a cell is to install it in a clear plastic box or container like that

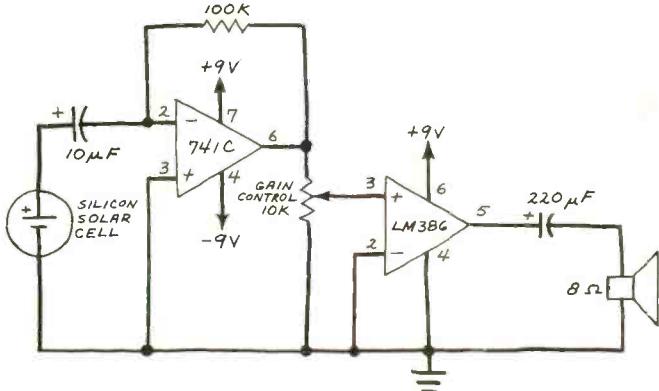
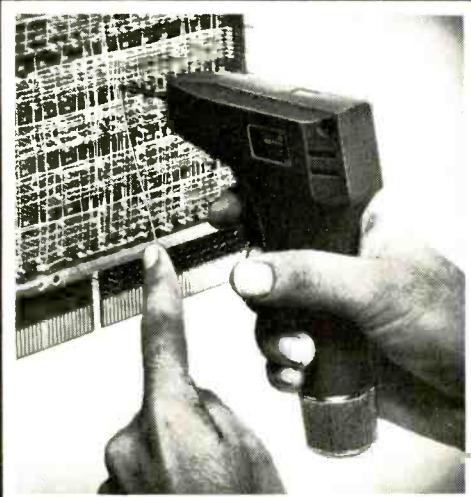


Fig. 4. Schematic of a high-gain photophone receiver.

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in which a typical cell is packaged when sold. A layer of plastic foam behind the cell will cushion it from shock, and a small notch or hole can be easily formed for the leads.

Some solar cells are supplied with wire leads. Others are not. If you must attach your own leads, use a small, low-wattage iron with a well-tinned tip. For best results, use tinned wrapping wire for leads. Most silicon cells have electrodes on the front and back surfaces. Solder the back electrode first by forming a small puddle of solder near an edge of the cell and then holding the stripped end of a wire lead in the solder until it cools.

The front electrode is usually in the form of a thin strip and requires more care. Touch the tip of the iron to the electrode and, after a second or two, apply enough solder to form a small bump or ridge. Then reheat the solder and position the second wire lead along the electrode. Hold the lead in place until the solder cools.

The leads, particularly the one soldered to the front electrode, must be protected from excessive strain. One way to do this is to attach the leads directly to the cell's protective housing with glue or miniature solder lugs. A shielded cable can then be connected to the leads or lugs.

Your mounting problems will be simplified if you install the cell in a reflector or behind a lens. Alignment of the receiver will be much easier if you use the reflector rather than a lens. Various types of reflectors are available from Edmund Scientific, but I prefer to modify ordinary flashlights. For example, the reflector in a typical 6-volt lantern has plenty of room for two solar cells connected in series and mounted back-to-back. The battery compartment has more than enough space for a modular amplifier, miniature speaker, battery, switch, gain control and phone jack.

Figure 5 shows a photophone receiver and a LED voice transmitter installed in 6-volt lanterns (Burgess "Dolphin" brand). I made the receiver in 1966, and it's worked fine ever since. The solar cells are secured in place, perpendicular to the axis of the reflector, by wrapping their leads around the protruding shoulder at the small opening in the reflector. While this mounting method might appear to be very flimsy, my cells have survived a trip around the world (including a one-year stint in Vietnam) and numerous field tests of various

light-wave communications devices. The cells simply bounce upon their leads when the receiver is dropped or jostled.

I recommend one or more silicon solar cells for your photophone receiver, but you can use selenium cells, phototransistors or photodiodes instead. Keep in mind that small detectors will require external optics for best results and might be difficult to align.

Range Testing. For initial photophone tests, leave the receiver with a friend and walk 25 paces in the direction of your shadow. Then,



Fig. 5. Photophone receiver (left) and LED voice transmitter installed in 6-volt lantern lights. Note the position of the two back-to-back solar cells in the receiver's reflector.

while facing the receiver, point the transmitter toward the ground in front of you until the sun's reflection is visible as a bright spot. It's a simple procedure to slowly move the spot toward the receiver by following the spot of light along the ground.

It's helpful to place the receiver in a shaded location so the reflected spot will be easier to see. A trick I usually employ is to place a large red bicycle reflector next to the receiver. When the reflector lights up, the transmitter is on target. Here's another tip: placing the receiver *inside* a building and directing the transmitter beam through a window makes for an impressive demonstration because the voice of the person at the transmitter can be heard only via the light beam and *not* by the propagation of sound waves through the air.

While testing a photophone, you'll soon discover some difficulty in keeping the reflected spot of sunlight trained on the receiver. One way to stay on target is to rest the transmitter against a fixed object like a tree, fence post, or building. A better way is to mount the transmitter on a photographer's tripod. Of course, the receiver must be kept in a fixed location. You'll also need to make frequent adjustments to compensate for the earth's rotation, which manifests itself as the apparent continuous motion of the sun.

Once you have an operational photophone, you'll probably want to determine its maximum transmitting range. For long-range tests, a tripod is essential. An electronic transmitter (i.e., a speaker with attached mirror) is very helpful also, because one person can perform the test unaided. It's very easy to achieve a range of 100 meters or more. For ranges of one kilometer or more, the photophone receiver I described in the February 1976 issue of POPULAR ELECTRONICS is ideal. This receiver uses a large glass reflector installed in a special cabinet complete with amplifier and solar cell. Though very difficult to align, the receiver has exceptional sensitivity. If you don't have this article in your back issues, you can find it at a library. It's also in the 1980 ELECTRONIC EXPERIMENTER'S HANDBOOK.

In Conclusion. The photophone will allow you to explore the fascinating world of light-beam communications. However, remember one word of caution. Always avoid staring at the bright reflection of sunlight from photophone transmitters! Protect your eyes by wearing sunglasses with optical-quality glass lenses and by looking away from the transmitter mirror.

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Hobby Scene



By John McVeigh,
Technical Editor

DEGAUSSING

Q. A while ago, a friend showed me some interesting visual effects that he could create by placing a magnet near the screen of his black-and-white television. Unfortunately, I tried the same thing with my color receiver, and now I am stuck with a pink-purple splotch on my screen. Why was the effect of the magnet permanent on my receiver, and what can be done to correct the problem (short of replacing the picture tube)?—Fred Martin, Woodstock, NY.

A. The effects that your friend created on his monochrome picture tube were due to the deflection of electrons streaming from the cathode of the CRT to the screen. This deflection was caused by the external magnetic field generated by the bar magnet. The patterns which appeared on the screen are similar to those created when a magnet is slipped under a sheet of paper upon which iron filings have been sprinkled.

The reason why the monochrome CRT was not permanently affected and the color tube

was lies in the fundamental difference between the two devices. A monochrome tube employs only one electron beam and one set of phosphor dots, all of which glow the same color. In a color tube, however, there are three sets of dots, each glowing a different color, and each excited by a separate beam of electrons.

It is essential for proper image reproduction that each electron beam in a color tube strike only its respective color dots. There are two separate means employed in color picture tubes to achieve this end. First, each individual beam is adjusted so that it converges at each of the shadow mask holes at the proper angle. A convergence network is charged with this responsibility. Second, a purity adjustment ensures that all three beams pass through the exact deflection center of the yoke so that they are equally deflected and line up with the array of holes spaced across the screen. Essentially, the convergence network bundles the electron beams together and the purity network centers the bundle on the triads of dot holes.

Extreme accuracy in the deflection of the electron beams is required. Unfortunately, any extraneous magnetic field in the neighborhood of the color picture tube can affect the electron beams and prevent them from reaching their appropriate color phosphor dots. In operation, residual magnetization of the metallic structure around the color tube that causes color splotches can build up. (That's what the problem is with your picture tube.) The cure for this is *degaussing*. When this is done, an alternating magnetic field derived from the 60-Hz ac line is set up in the vicinity of the picture tube. It demagnetizes the tube in much the same manner that the heads of tape decks are demagnetized for optimal performance.

In most color televisions of recent vintage, there is an automatic degaussing circuit which functions in the following manner. When power is first applied to the receiver, alternating current flows through a thermistor and a coil wound around the periphery of the screen. An alternating magnetic field is set up around the coil which neutralizes any residual magnetization in the vicinity of the picture tube. The current causes self-heating of the thermistor, whose coefficient is positive. As the temperature of the thermistor increases, its resistance increases to the point that practically no current flows through the coil. The alternating magnetic field collapses as the current through the coil decreases. Thus, a brief degaussing process occurs each time the receiver is turned on from a cold start.

If your receiver has such a degaussing circuit, it obviously is not functioning properly. Otherwise the color splotches would have disappeared the first time that power was removed from the receiver and reapplied a few minutes later. The most likely cause of a malfunctioning automatic degausser is a failed thermistor.

If your receiver lacks such a circuit, you can either build or buy a degaussing coil. Commercial degaussers are relatively inexpensive (about \$8.00) and are available from most electronic supply stores. Also, most television repairmen keep one on hand and will gladly perform degaussing for you. A degaussing coil can be fashioned by winding approximately 400 turns of No. 20 or No. 22 enameled copper wire on a circular form 12 inches (30.4 cm) in diameter. The coil should be soldered to an ac line cord and the connections insulated with heat-shrink tubing or PVC electrical tape. Degaussing is performed by plugging the line cord into an ac power socket, bringing the coil near the front of the picture tube, and moving the coil around the screen. The coil should then be slowly withdrawn from the screen to a distance of perhaps ten feet. Power should then—and only then—be removed from the degaussing coil.

This procedure should clear up your pink-purple splotch without any need for replacing the picture tube, and allow you to continue experimenting with the magnetic deflection of electron beams without permanently affecting color reception.

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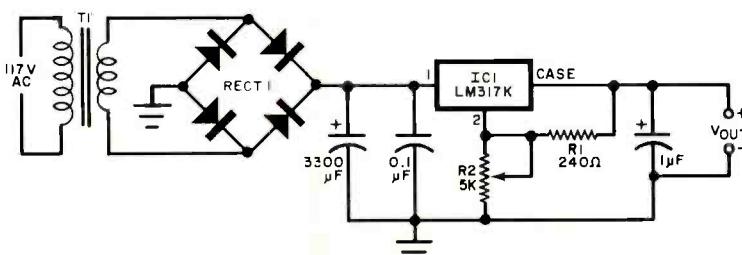
Q. I have an HO power pack that's not being used on my layout. Is it possible to use it as a variable-voltage power supply as is? If not, can it be modified for such an application? The power pack is rated at 12 volts dc output at 1 ampere maximum.—Robert Grisson, Dothan, AL.

A. Most HO power packs consist of a transformer, a rectifier, a rheostat and a circuit breaker. No filter capacitors are employed because pulsating dc is applied across the track rails. To use this type of power pack as a variable-voltage supply for electronic projects, it must be modified to include filtering and some efficient method of varying the output voltage.

Shown in the figure is a circuit that can be constructed using a portion of the original power pack and some additional components. The stepdown transformer is that

included in the stock power pack. If the pack's rectifiers are silicon diodes, they can be used as is. If not, replace them with a modular bridge rectifier. Voltage regulator IC1 and R1 and R2 take the place of the power pack's rheostat. Together they form a source of variable, regulated voltage whose amplitude is determined by the setting of R2.

The LM317K is housed in a TO-3 package that must be heat sunk but electrically isolated from the chassis. Employ a mica washer and silicone thermal compound to accomplish this. If adequately heat sunk, the regulator will be able to deliver the rated current of your transformer (1 ampere) on a continuous basis. Assuming the transformer secondary is rated at 12.6 volts rms, the maximum voltage available at the output terminal will exceed 12 volts. It might reassure you to know that the LM317 includes current limiting, thermal-overload and safe-area protection.



Have a problem or question in circuitry, components, parts availability, etc.? Send it to the Hobby Scene Editor, POPULAR ELECTRONICS, One Park Ave., New York, N.Y. 10016. Though all letters can't be answered individually, those with wide interest will be published.

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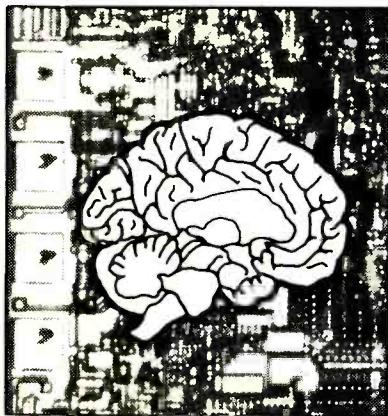


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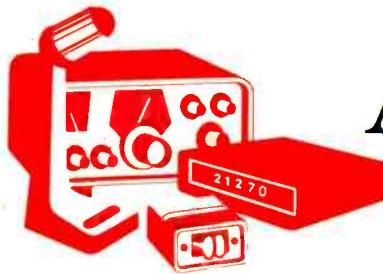
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Amateur Radio

By Karl T. Thurber, Jr., W8FX/4

SPECIAL CLUBS FOR SPECIAL FOLKS

AMATEUR radio is a many-faceted hobby whose aspects include DXing, ragchewing, QRP (low-power) operation, certificate-chasing, vhf experimentation, two-way television communications, and radioteletype, among many others. Dozens of clubs cater to these special ham interests. Let's take a look at some of them.

The 10-10 Net. The current increase in sunspot activity (Solar Cycle No. 21 is now peaking) has been accompanied by a dramatic surge in interest in the 10-meter band. Many newcomers to ham radio have only recently discovered the band's potential, but oldtimers have known about the potential of 10 meters for many years. Interest in 10 has been kept alive between cycle peaks by members of the Ten-Ten International Net, a far-flung organization of dedicated 10-meter operators whose motto is "Use and Enjoy Ten Meters." The club originated in Southern California during the early sixties. At that time, the group was a traffic-handling net in the San Dimas area. As conditions on 10 meters deteriorated following cycle 19's decay, the group decided that there was little need for a traffic net on the band. Still, the little group wanted to stay in touch and convened its net every night at 10 p.m. PST on

28.8 MHz. Thus, the name "Ten-Ten" was born ("on 10 at 10").

The net has grown immensely and has become a worldwide club with a membership in five digits. The members have one thing in common. That is their goal of keeping the band active even in years of low sunspot activity when other services might be tempted to convert portions of the band's wide-open spaces to their own uses. Ten-Ten members also consider the club a fraternal organization whose emphasis is assistance to fellow hams and service to the public.

To become a member, one must be active on 10 meters. The prospective member contacts 10 club members, obtaining from each his distinctive "10-10" identification number and other details of the contact. The list of contacts, along with a small service fee, is submitted to a district manager who issues a membership certificate and an ID number for use in future exchanges with other members and prospective members.

The club also publishes a news bulletin and has a far-reaching awards program conducted in cooperation with its more than 100 active local chapters. The program, which is very popular among "certificate hunters," includes a series of 10-10 net contests, Bar and Plaque awards (for specific numbers of

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A membership certificate for ARRL's Old Times Club.

QSOs with fellow members), and Worked-All-States (WAS) certificates. Members who contact 500 qualifying 10-10 stations can become honorary Vice Presidents in the exclusive "International 500 Club."

Ten-Ten International has a national organization, but its main activities are decentralized to the district managers who run the membership and activity programs for their districts (broken down by U.S. call area), and to the independent chapters, most of which have their own unique awards programs. To join in the fun, simply get on 10, work the required 10 contacts, and inquire as to the name and address of your district manager. Send in your contact list and fee, and you're in business with this highly popular group.

QRP Amateur Radio Club International.

This club caters to the large segment of the ham fraternity that enjoys running low power. The QRP-ARC-I, as it is called, was formed in 1961 to further the interests of QRP operators—those who limit their input power levels to 100 watts CW or 200 watts PEP on SSB. You can join the club as a full member if you run QRP power levels or as an associate if you regularly run higher power levels but also have a serious interest in low-power or even QRP_p (low-low-power) operations using 5 watts or less. Dues in the club are a modest \$3 per year and include a subscription to a quarterly newsletter. Membership details can be obtained by writing to the Secretary/Treasurer, Joseph C. Szempias, W8JKB, 2359 Woodford Ave., Toledo, OH 43605.

The group very actively promotes low-power operations by on-the-air contests and awards. The QRP-ARC-I sponsors a very large operating awards program, the objective of which is to demonstrate that the use of limited power levels reduces QRM (interference) on the ham bands, yet still allows full enjoyment of the hobby. As a result, the club issues a number of interesting awards, many of which parallel regular ARRL (American Radio Relay League) operating awards. The QRP members chase such certificates as the WAC-QRP (worked all continents, low-power), WAS-QRP (worked all states), DXCC-QRP (worked 100 countries), and several other very specialized awards. The latter include QRP-25 (working 25 club members) and the WAS-QRP_p (working all states using 5 watts or less). Besides the challenging awards program, the club also holds informal "QSO parties" each month, an annual formal contest, and other activities of special interest to the low-power operator.

The SWL (shortwave listener) isn't forgotten in the QRP-ARC-I's plans. SWLs can qualify for any of the club's awards on a stations-heard basis. Also, hams can use SWL reception reports in lieu of two-way QSL card confirmations in applying for the various achievement awards and certificates.

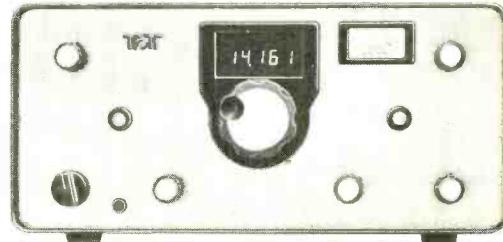
The Quarter Century Wireless Association. This one's for you if you've been involved in amateur radio for longer than you might otherwise care to remember. The club limits its membership to amateurs who were first licensed at least 25 years ago, though not necessarily continuously licensed for the whole period. The Quarter Century Wireless Association or QCWA was formed in the New York area in 1947 by 54 charter members. It quickly spread and enlarged its membership

to form chapters across the country. The QCWA is based on the fellowship and respect of one "old timer" for another, and tries to keep its membership on a very personal, fraternal basis through its many local chapters. The chapters are active, holding meetings, luncheons and brunches at which local problems and interests are discussed. These are often held in conjunction with local hamfests, swap meets and conventions. QCWA also conducts a weekly on-the-air

QCWA provides, you'll find that membership dues are reasonable (\$14 for a 3-year period plus a one-time \$3 initial registration fee). More information can be obtained by writing to the Quarter Century Wireless Association, 1409 Cooper Dr., Irving, TX 75061.

International Fox-Tango Club. This is a really unusual amateur club—a sort of "mutual aid society" of individuals who have bought or have an interest in amateur gear

This 70-watt Ten-Tec transceiver is popular with Novices and is also good for low-power operation. It has a built-in vfo and instant band change.



get-together for the exchange of club activity information among the chapters. A national meeting is held once a year, as is the QCWA "QSO party" which brings together on the air several hundred members who compete for the greatest number of contacts with fellow old-timers. The club also publishes a well-written, interesting and often nostalgic journal, *QCWA News*, which keeps members informed on national and chapter activities and provides a vehicle for keeping old on-the-air friends in touch with each other.

If you're interested in the kind of fellowship

manufactured by the Yaesu Musen Co. The club's sole purpose is to enhance the effectiveness of its members' use of Yaesu Equipment by providing a medium for the exchange of information. It was founded in 1971 primarily to trade information on the popular Yaesu FT-101 (hence the name Fox-Tango). Its members are scattered throughout the world, so a conventional club organization isn't practical. The club therefore holds no meetings and elects no officers.

Members trade information about their gear mainly by means of the *FT Newsletter*.

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the club bulletin that is published ten times each year. The bulletin deals with a variety of equipment-related issues such as modifications, improvements, manufacturers service notes, schematic and pictorial diagrams, troubleshooting and servicing techniques, and reviews of new gear. Recently, the Fox-Tango Net was established to expedite the timely exchange of information between club members. Of course, one doesn't have to be a member or an owner of Yaesu gear to participate in the on-the-air net.

The club also operates a technical committee to respond to members' requests for

with whoever responds to the call.

Another popular ARRL group is the *Old Timers Club*, which issues a handsome membership certificate to any amateur radio operator who held an amateur license 20 or more years ago. One applies for membership by certifying to the ARRL the year he held his first license and the callsign he had then. As with RCCers, OTC members may sign "OTC" after their calls to indicate their seniority and membership in the club. The OTC is different from the QCWA; the former is a casual, honorary group, while the latter holds regular meetings and social events.



The Fox-Tango Club was originally started to exchange information on the popular Yaesu FT-101 transceiver. Shown here are members of Yaesu's more contemporary 301 equipment series.

data and assistance in servicing their gear. In addition, the Fox-Tango group operates a purchasing service which enables members to buy communications equipment and accessories at a discount. The purchasing service also tries to make available hard-to-find Japanese replacement transistors, parts kits, and small items necessary to making the many modifications and improvements suggested by members. The club publishes a catalog of these components known as a "green sheet" for its members.

Dues in the Fox-Tango organization are \$6 on a calendar-year basis. For more information, write to the club c/o Milton Lowens, N4ML, 248 Lake Dora Dr., W. Palm Beach, FL 33411. For the record, the club welcomes Citizens Band members who are seriously interested in amateur radio, but won't provide any information about the illegal conversion or use of Yaesu ham gear on CB frequencies. There is no relationship to the CB group having a similar name.

ARRL Operating Clubs. To make amateur radio more challenging, to improve public service contributions, and to enhance operating skills, the American Radio Relay League sponsors a number of operating "clubs." Although several of these bestow an honorary club membership on the applicant, the clubs are not regular organizations in the sense that they don't elect officers or hold meetings.

One of the groups most easily joined is the *Rag Chewers Club*. It's an especially easy one for the beginner. All one has to do is converse with another ham for 30 minutes or more and report this fact to ARRL headquarters (211 W. Main St., Newington, CT 06111). The League will promptly issue a membership certificate. The RCC, of course, is designed to promote interesting, meaningful contacts, something beyond the "hello-goodbye" QSO too often occurring on amateur frequencies. Many club members "tail-end" their CQ calls with the letters "RCC" to indicate that they'd like to "chew the rag" a bit

One has to handle a substantial amount of message traffic to qualify for the *Brass Pounders League*. To achieve BPL status, an amateur must pass a certain amount of radio traffic each month on the ham bands and report his totals to the ARRL Section Communications Manager (SCM). The SCM keeps score and in turn reports traffic totals for his section to headquarters, making a list of those who qualify for BPL. Results are published in the League's monthly magazine, *QST*. Each time an amateur qualifies, he is awarded a BPL certificate. A special medallion is issued the third time. The certificate can be earned by club and multi-operator stations handling traffic, but the medallion is available only to individual amateurs who must personally handle the traffic to qualify. This award goes a long way in promoting the public-service capabilities of ham radio.

A real honor is to be nominated for membership in the *A-1 Operator's Club*. An amateur cannot apply for this one. Rather, his skills as a first-class operator are spontaneously identified by any two operators who already hold A-1 membership. Starting as a CW operators' group in the 1930's, the membership of the A-1 Operator's Club now includes people in many different phases of amateur radio. Some of the nomination criteria include on-the-air procedures, judgement and courtesy, code-copying ability, and general operating considerations. These four factors encompass one's entire posture as an amateur radio operator and include both technical skills and "radio personality."

Besides these club activities, the ARRL also sponsors a number of operating awards and certificates, such as Worked-All-States, Worked-All-Continents, the Satellite DX Achievement, 6-Meter 600 Club, and the DX Century Club awards, to mention but a few. The League also promotes a number of contests and other activities during the year.

No matter what a particular amateur's interests are, there's almost certainly a specialty group or achievement club that's just right for him.

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9:30 a.m.-5:00 p.m.	1430-2200	UN Radio	A	21670, 15410, 26020 (when in session)
9:35-10:20 a.m.	1435-1520	R. Nepal	D	3425 or 7105 or 9590
10:00-10:15 a.m.	1500-1515	R. Japan	C	9505
10:00-11:00 a.m.	1500-1600	V. of Rev. Ethiopia	D	9560
10:00-11:00 a.m.	1500-1600	BBC	B	17830, 15260 (Sat, Sun)
10:00-11:00 a.m.	1500-1600	R. Moscow	B	12070, 12010, 11570, 11790, 9790, 9580, 7170
10:00-12:30 a.m.	1500-1730	BSHKJ, Jordan	D	9560
10:15-10:30 a.m.	1515-1530	V. of Greece	B	17830, 15125, 11730 (first & last not Tues.)
10:30-11:00 a.m.	1530-1600	R. Afghanistan	D	4775
10:30-11:00 a.m.	1530-1600	R. Yugoslavia	C	15300, 15240
10:30-11:00 a.m.	1530-1600	Swiss R. International	B	21570
10:30-11:15 a.m.	1530-1615	NSB, Tokyo	C	9595, 6055 (exc. Sun)
10:30-11:30 a.m.	1530-1630	V. of Vietnam	C	12033, 10040
10:30 a.m.-5:00 p.m.	1530-2200	R. Moscow (via Cuba)	A	11880
10:45-11:00 a.m.	1545-1600	R. Canada International	A	21695, 17820, 15325
11:00-11:15 a.m.	1600-1615	R. Japan	C	9505
11:00-11:15 a.m.	1600-1615	R. Pakistan	C	21755, 21635, 21486, 17910, 17660
11:00-11:30 a.m.	1600-1630	R. Korea	B	11830, 9720
11:00-11:30 a.m.	1600-1630	R. Norway	B	15345 (Sun only)
11:00-12:00 a.m.	1600-1700	R. Moscow	B	15210, 12070, 12010, 11870, 11790, 9790, 9580, 7170
11:00 a.m.-12:09 p.m.	1600-1709	BBC	B	21710, 21550, 17885
11:00 a.m.-1:00 p.m.	1600-1800	AFRS-Washington	A	17765, 15430, 15330, 11805
11:00 a.m.-6:00 p.m.	1600-2300	VOA	A	26040, 21485, 17870, 17710, 15445, (15410 to 2200)
	1630	R. Singapore	C	11940 (fade-in time varies)
11:45-12:00 a.m.	1645-1700	R. Canada International	A	21695, 17820, 15325
12:00-12:15 p.m.	1700-1715	R. Japan	C	9505
12:00-12:15 p.m.	1700-1715	Vatican R.	B	17900
12:00-12:30 p.m.	1700-1730	R. Pakistan	C	15470, 11675
12:00-1:00 p.m.	1700-1800	HCB, Ecuador	B	26020, 21480, 17790 (frequent changes)
12:00-1:00 p.m.	1700-1800	WYFR, Family Radio	A	21615, 15160
12:00-1:00 p.m.	1700-1800	R. Moscow	B	15210, 12070, 12010, 11870, 11790, 9790, 9580, 9500, 7170
12:00 p.m.-12:30 a.m.	1700-0530	R. New Zealand	C	17860, 15345
12:05-12:55 p.m.	1705-1755	R. France International	B	21620, 21580, 21515 (from April 1605-1655)
12:05-12:50 p.m.	1705-1750	BRT, Belgium	C	17730 (from April, 1605-1650)
12:09-12:45 p.m.	1709-1745	BBC	B	17830, 15260 (Sat & Sun only)
12:45-3:00 p.m.	1745-2000	BBC	C	15400, 15070, 12095 (11820 from 1800)
12:45-5:30 p.m.	1745-2230	All India R.	C	11620
1:00-1:15 p.m.	1800-1815	R. Japan	B	9505
1:00-1:30 p.m.	1800-1830	R. Canada International	B	17820, 15260
1:00-1:30 p.m.	1800-1830	R. Norway	C	17755 (Sun only)
1:00-1:45 p.m.	1800-1845	R. Korea	C	15255, 11830
1:00-2:00 p.m.	1800-1900	R. Moscow	B	15210, 12070, 12050, 12010, 11870, 11790, 9790, 9500, 7170
1:00-2:00 p.m.	1800-1900	WYFR, Family Radio	A	21615, 15425
1:00-2:00 p.m.	1800-1900	V. of Nigeria	C	15119, 15185
1:00-2:00 p.m.	1800-1900	R. Uganda	C	15250
1:00-3:00 p.m.	1800-2000	R. Australia	C	11800, 9580, 9505
1:00-4:00 p.m.	1800-2100	R. Kuwait	C	11665 (frequent changes)
1:00-5:00 p.m.	1800-2200	B.S.K. Saudi Arabia	C	11854
1:00-5:00 p.m.	1800-2200	AFRS Washington	A	21570, 17765, 15430, 15345, 15330
1:15-1:45 p.m.	1815-1845	Swiss R. International	C	21585, 17830, 17760, 15125
1:15-2:15 p.m.	1815-1915	R. Bangladesh	D	15285, 11765 (both vary, freq. changes)
1:30-1:35 p.m.	1830-1835	UN Radio	A	21670, 19505-SSB, 15410 (Fri)
1:30-2:00 p.m.	1830-1900	V. of Revolution, Guinea	B	15308 (varies) (Mon and Fri)
1:45-2:15 p.m.	1845-1915	Sri Lanka Br. Corp.	C	17850, 15120, 15115, 11870
2:00-2:10 p.m.	1900-1910	R. Tahiti	C	15170, 11825 (exc. Sun)
2:00-2:15 p.m.	1900-1915	R. Japan	C	15270
2:00-2:30 p.m.	1900-1930	R. Canada International	A	17760, 15325, 11905
2:00-2:30 p.m.	1900-1930	R. Afghanistan	B	17820, 15260
2:00-3:00 p.m.	1900-2000	HCB, Ecuador	C	15075 (frequent changes)
2:00-3:00 p.m.	1900-2000	R. Moscow	B	26020, 21480, 17885, 15295 (freq. changes)
2:00-5:00 p.m.	1900-2200	WYFR, Family Radio	B	15210, 12050, 12010, 11870, 11790, 9790, 9500, 7170
2:30-3:30 p.m.	1930-2030	V. of Iran	A	21615, 21525, 15130
3:00-3:15 p.m.	2000-2015	R. Japan	C	9022 (frequent changes)
3:00-3:30 p.m.	2000-2030	R. Algiers	B	15270
3:00-3:30 p.m.	2000-2030	R. Canada International	C	11810, 11646 or 11615, 9610 (frequent changes)
3:00-3:30 p.m.	2000-2030	Kol Israel	A	17820, 17760, 15325, 11905
3:00-4:00 p.m.	2000-2100	R. Moscow	B	21675, 17645, 11655
3:00-4:00 p.m.	2000-2115	BBC	B	15210, 15180, 12050, 12010, 11870, 11790, 9500, 7170
3:10-4:40 p.m.	2010-2140	R. Havana Cuba	A	21710, 17840, 15260, 15070, 6175
3:30-4:20 p.m.	2030-2120	R. Nederland	A	11920
3:30-4:30 p.m.	2030-2130	V. of Vietnam	B	21640, 17695, 17605, 15220, 11730
3:30-4:30 p.m.	2030-2130	V. Turkey	C	12033, 10040
3:50-4:40 p.m.	2050-2140	R. Havana Cuba	C	11955, 9550
4:00-4:15 p.m.	2100-2115	R. Japan	C	17750, 9770
4:00-4:45 p.m.	2100-2145	R. Nacional, Venezuela	B	15270
4:00-4:50 p.m.	2100-2150	R. RSA	C	15400 (var; time + freq. vary)
4:00-5:00 p.m.	2100-2200	V. of Nigeria	B	21535, 17780, 15155
4:00-5:00 p.m.	2100-2200	R. Moscow	C	15185, 15119
4:00-5:00 p.m.	2100-2200	R. Moscow	B	17720, 15180, 12050, 12010, 9500

4:15-5:00 p.m.	2115-2200	BBC
4:15-7:00 p.m.	2115-2400	R. Free Grenada
4:30-5:00 p.m.	2130-2200	R. Canada International
4:30-5:00 p.m.	2130-2200	KGEI, San Francisco
4:30-5:00 p.m.	2130-2200	HCJB Ecuador
4:30-5:00 p.m.	2130-2200	R. Sofia
4:30-5:30 p.m.	2130-2230	R. Baghdad
4:40-5:40 p.m.	2140-2240	V. of Free China
4:50-5:00 p.m.	2150-2200	R. Free Europe
5:00-5:15 p.m.	2200-2215	R. Yugoslavia
5:00-5:15 p.m.	2200-2215	R. Japan
5:00-5:30 p.m.	2200-2230	V. Chile
5:00-5:30 p.m.	2200-2230	R. Norway
5:00-5:45 p.m.	2200-2245	BBC
5:00-6:00 p.m.	2200-2300	WYFR, Family Radio
5:00-6:00 p.m.	2200-2300	R. Moscow
5:00-6:00 p.m.	2200-2300	V. of Turkey
5:00-6:00 p.m.	2200-2300	CBC Radio
5:00-7:00 p.m.	2200-2400	AFRTS-Washington
5:00-8:00 p.m.	2200-0100	VOA
5:30-6:00 p.m.	2230-2300	Kol Israel
5:45-6:00 p.m.	2245-2300	BBC
5:45-6:00 p.m.	2245-2300	SODRE, Uruguay
5:45-6:00 p.m.	2245-2300	UN Radio
6:00-6:30 p.m.	2300-2330	R. Japan
6:00-6:30 p.m.	2300-2330	R. Korea
6:00-6:30 p.m.	2300-2330	R. Sweden
6:00-6:30 p.m.	2300-2330	R. Vilnius
6:00-6:50 p.m.	2300-2350	Rdif. Argentina
6:00-7:00 p.m.	2300-2400	AVEH, Haiti
6:00-7:30 p.m.	2300-2430	BBC
6:00-7:50 p.m.	2300-2450	R. Pyongyang
6:00-8:00 p.m.	2300-0100	CBC Southern Service
6:00-8:00 p.m.	2300-0200	R. Moscow
6:05-6:20 p.m.	2305-2320	Austrian R.
6:35-6:55 p.m.	2335-2355	SODRE, Uruguay
6:45-7:45 p.m.	2345-2445	R. Japan
7:00-7:15 p.m.	0000-0015	R. Japan
7:00-7:25 p.m.	0000-0025	R. Tirana
7:00-7:30 p.m.	0000-0030	Kol Israel
7:00-7:30 p.m.	0000-0030	R. Norway
7:00-7:55 p.m.	0000-0055	R. Peking
7:00-8:00 p.m.	0000-0100	R. Sofia
7:00-8:00 p.m.	0000-0100	AFRTS-Washington
7:00-9:00 p.m.	0000-0200	R. Luxembourg
7:00-9:00 p.m.	0000-0200	VDA
7:00-12:00 p.m.	0000-0500	FEBC Philippines
7:00-12:00 p.m.	0000-0500	R. Moscow (via Cuba)
7:00 p.m.-1:06 a.m.	0000-0606	CBC Northern Service
7:00 p.m.-4:00 a.m.	0000-0900	UN Radio
7:05-8:55 p.m.	0005-0155	Spanish Foreign R.
7:15-7:30 p.m.	0015-0030	V. of Greece
7:15-8:00 p.m.	0015-0100	BRT, Belgium
7:30-7:50 p.m.	0030-0050	SODRE, Uruguay
7:30-8:00 p.m.	0030-0100	R. Sweden
7:30-8:00 p.m.	0030-0100	R. Prague
7:30-8:00 p.m.	0030-0100	R. Kiev
7:30-8:00 p.m.	0030-0100	La Cruz del Sur, Bolivia
7:30-9:00 p.m.	0030-0200	HCJB, Ecuador
7:30-9:30 p.m.	0030-0230	BBC
7:30-9:30 p.m.	0030-0230	HCJB, Ecuador
7:50-8:35 p.m.	0050-0135	TWR-Bonaire
8:00-8:15 p.m.	0100-0115	R. Japan
8:00-8:15 p.m.	0100-0115	Vatican R.
8:00-8:20 p.m.	0100-0120	RAI, Italy
8:00-8:25 p.m.	0100-0125	Kol Israel
8:00-8:30 p.m.	0100-0130	R. Canada International
8:00-8:45 p.m.	0100-0145	R. Berlin International
8:00-8:55 p.m.	0100-0155	R. Prague
8:00-8:55 p.m.	0100-0155	R. Peking
8:00-9:00 p.m.	0100-0200	V. of Free China
8:00-11:30 p.m.	0100-0200	AFRTS-Washington
8:00-10:30 p.m.	0100-0330	R. Australia
8:00-11:50 p.m.	0100-0450	R. Habana Cuba
8:00-12:00 p.m.	0100-0500	WYFR, Family Radio
8:30-8:50 p.m.	0130-0150	V. of Germany
8:30-8:55 p.m.	0130-0155	Austrian Radio
8:30-8:55 p.m.	0130-0155	R. Tirana
8:30-9:00 p.m.	0130-0200	R. Budapest

A 21710, 15420, 15260, 15070, 6175
B 15045 (time varies)
A 17820, 15325, 15150, 11945
C 15280
C 26020, 21480, 17885, 15295
(frequent changes)
B 9665, 9530 (frequent changes)
C 9745
C 17890, 15345, 11745
C 11770 (frequent changes)
C 9620
C 17755, 11735
B 17798, 17791, 15150
(frequent changes)
C 17795, 15175, 11850 (Sun only)
A 21710, 15420, 15260, 15070, 6175
A 21525, 15130, 11855
B 17720, 15455, 15180, 15140, 12050,
9710, 9530, 9500
C 11955, 9550, 9515, 7215
A 15325, 11925 (Mon-Fri.)
A 25615, 21570, 15430, 15330
A 21460
A 17815, 15585, 11637, 11610, 9815
A 15420, 15260, 15070, 9410, 6175
C 11885, 9515 (time varies)
A 15225, 11830 (Fri)
C 17755
C 15570, 15385, 11840 (frequent changes)
C 15275, 11705
B 17870, 15405, 15180, 12060,
11790, 11735
C 11710 (Mon-Fri)
B 11835, 9770
A 15420, 15260, 15070, 9590,
9580, 9410, 7325, 6175,
6120, 5975
C 9977
A 11850, 5960 (Mon-Fri)
A 17720, 15455, 15180, 15140, 12050,
11860, 11780, 11735, 9710, 9610,
9530, 9505, 9490
C 12015, 9770, 5945 (Sun only)
C 11885, 9515
C 17825, 15270
C 17755
B 9750, 7065
A 15585, 11637, 9815
C 15135, 11850 (Mon only)
B 17855, 17680, 15520, 15120
B 9705 or 15330
A 25615, 21570, 15330, 11790
C 6090
A 17730, 15205, 11740, 9640, 6130
C 17810
A 6115 or 9600
B 9625, 6195 (not all English)
A 6055 (when in session)
B 11880, 9630
B 11730, 9655, 9515
C 15175
C 11885, 9515 (time varies)
C 11905 (dropped after April 5)
C 6055
B 17870, 15405, 15100, 11790, 11770
D 4875 (Mon only)
A 15115
A 15260, 15070, 11750, 9580,
9410, 7325, 6175, 6120, 5975
B 11910, 9745
B 11925
C 17755
B 11845, 9605, 6015
B 11800, 9575
A 15585, 11637, 9815
A 11940, 11830, 5960
C 11975, 9730
B 11990, 9740, 9540, 7345, 5930
B 17855, 17680, 15520, 15120
C 17890, 15345, 15270
A 25615, 21570, 15330, 11790, 6030
B 21740, 17795
A 11930, 11725
A 11740
A 11865, 9605, 9565, 9545, 6145,
6100, 6085, 6040
B 9770, 5945
B 9750, 7120
B 17710, 15225, 11910, 9835, 9585,
6105 (Wed, Fri only)

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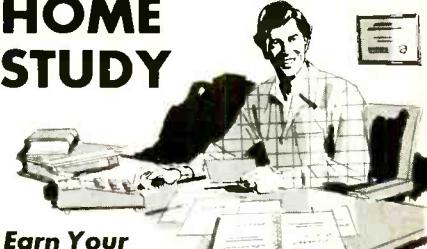
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8:30-9:25 p.m.	0130-0225	R. Bucharest	C	11940, 11840, 11735, 9690, 9570, 5990
8:30-9:30 p.m.	0130-0230	R. Japan	C	21640, 17825, 17725, 15270
8:45-9:15 p.m.	0145-0215	Swiss R. International	B	15305, 11715, 9725, 6135
9:00-9:15 p.m.	0200-0215	R. Japan	C	17755
9:00-9:25 p.m.	0000-0225	Kol Israel	A	15585, 11637, 9815
9:00-9:25 p.m.	0200-0225	R. Warsaw	C	15120, 11815, 9525, 7270, 7145, 6135, 6095
9:00-9:30 p.m.	0200-0230	R. Canada International	A	11940, 11845, 5960
9:00-9:30 p.m.	0200-0230	R. Norway	B	9645, 9550, 6185 (Mon only)
9:00-9:30 p.m.	0200-0230	R. Budapest	B	17710, 15225, 11910, 9835, 9585, 6105 (not Mon)
9:00-9:50 p.m.	0200-0250	R. RSA	B	17770, 15220, 15155, 11900
9:00-9:55 p.m.	0200-0255	R. Peking	C	17680, 15600, 15120
9:00-10:05 p.m.	0200-0305	TIFC, Costa Rica	C	9645, 5055
9:00-10:30 p.m.	0200-0330	R. Cairo	B	12050, 9475
9:00-11:00 p.m.	0200-0400	R. Moscow	A	17720, 15455, 15180, 15140, 12050, 12010, 11860, 11780, 11735, 9710, 9700, 9610, 9530, 9490
9:00-11:30 p.m.	0200-0430	AFRTS-Washington	A	21570, 17765, 11790, 6030
9:15-9:30 p.m.	0215-0230	V. of Greece	B	11730, 9650, 9515
9:30-9:45 p.m.	0230-0245	R. Pakistan	C	21590, 17830
9:30-9:55 p.m.	0230-0255	R. Tirana	B	9750, 7120
9:30-10:00 p.m.	0230-0300	R. Lebanon	D	11785 (frequent changes)
9:30-10:00 p.m.	0230-0300	R. Sweden	C	11705, 9695
9:30-10:15 p.m.	0230-0315	R. Berlin International	C	11975, 9730
9:30-10:25 p.m.	0230-0325	R. Nederland	A	9590, 6165
9:30-10:30 p.m.	0230-0330	BBC	A	11750, 9580, 9410, 7325, 6175, 6120, 5975
9:30-12:00 p.m.	0230-0500	HCJB, Ecuador	A	15115, 11910, 9745
9:37-9:45 p.m.	0237-0245	UN Radio	A	15240, 10869-55 B, 7768.5 558, 6035
10:00-10:15 p.m.	0300-0315	R. Japan	C	17755
10:00-10:25 p.m.	0300-0325	R. Warsaw	C	15120, 11815, 9525, 7270, 7145, 6135, 6095
10:00-10:30 p.m.	0300-0330	R. Canada International	A	11940, 11845, 11770, 9535, 5960
10:00-10:30 p.m.	0300-0330	R. Portugal	B	11925, 6025 (Mon-0320)
10:00-10:30 p.m.	0300-0330	R. Budapest	B	17710, 15225, 11910, 9835, 9585, 6105
10:00-10:30 p.m.	0300-0330	R. Kiev	B	17870, 15100, 11965, 11790, 11770, 9580
10:00-10:50 p.m.	0300-0350	V. of Free China	C	17890, 15345, 15270
10:00-10:55 p.m.	0300-0355	R. Prague	B	11990, 9740, 9540, 7345, 5930
10:00-10:55 p.m.	0300-0355	R. Peking	B	17680, 15300, 12055, 11685
10:00-11:00 p.m.	0300-0400	RAE, Argentina	C	9690 (Tue-Sat)
10:00-11:00 p.m.	0300-0400	Radiobras, Brazil	A	15290
10:00-11:00 p.m.	0300-0400	R. Baghdad	C	11935
10:00-11:15 p.m.	0300-0415	R. Uganda	B	(irregular)
10:00-11:26 p.m.	0300-0426	R. RSA	B	11900, 9585, 7270, 5980, 4990
10:00-11:30 p.m.	0300-0430	R. Cultural, Guatemala	B	3300
10:00 p.m.-1:00 a.m.	0300-0600	HIRVO, Honduras	B	4820
10:00 p.m.-2:30 a.m.	0300-0730	VOA	A	17865, 15240, 9670, 5995
10:30-10:55 p.m.	0330-0355	R. Tirana	B	7300, 6200
10:30-10:55 p.m.	0330-0355	Austrian Radio	C	9770, 5945
10:30-11:00 p.m.	0330-0400	R. Australia	B	17795
10:30-11:15 p.m.	0330-0415	R. Berlin International	B	11975, 11890, 5955
10:30-11:45 p.m.	0330-0445	BBC	A	9410, 6175, 5975
10:30-11:00 p.m.	0330-0400	R. Finland	C	9645, 11755
10:30-12:00 p.m.	0330-0500	R. Tanzania	D	15435
10:30 p.m.-1:00 a.m.	0330-0600	R. Habana Cuba	A	11760, 11725
10:51-10:58 p.m.	0351-0358	V. of Yerevan	C	15265, 11690, 9735, 9505 (Sun, Wed, Thu, Sat)
11:00-11:15 p.m.	0400-0415	R. Japan	C	17755
11:00-11:15 p.m.	0400-0415	R. Budapest	B	17710, 15225, 11910, 9835, 9585, 6105 (Wed & Sat) (Mon-0430)
11:00-11:30 p.m.	0400-0430	R. Bucharest	C	11940, 11840, 11735, 9690, 9570, 5990
11:00-11:30 p.m.	0400-0430	R. Canada International	A	11845, 11770, 5960
11:00-11:30 p.m.	0400-0430	R. Norway	B	9550, 6185 (Mon only)
11:00-11:45 p.m.	0400-0445	R. Korea	C	15570, 11820
11:00-11:55 p.m.	0400-0455	R. Peking	B	17680, 15300, 12055, 11685
11:00-12:00 p.m.	0400-0500	R. Moscow	B	17870, 15455, 15180, 15140, 12050, 11960, 9580
11:00-12:00 p.m.	0400-0500	R. Australia	B	17795, 15320
11:00 p.m.-1:00 a.m.	0400-0600	R. Moscow	B	11790, 11770, 9610, 9530, 9490
11:30-11:55 p.m.	0430-0455	Austrian R.	B	15260
11:30-12:00 p.m.	0430-0500	Swiss R. International	B	15305, 9725
11:30-12:00 p.m.	0430-0500	R. Sofia	B	9530 (frequent changes)
11:30 p.m.-2:00 a.m.	0430-0700	AFRTS-Washington	A	15330, 11790, 6030
11:45 p.m.-12:45 a.m.	0445-0545	BBC	A	9510, 6175, 5975
11:55 p.m.-1:00 a.m.	0455-0600	V. of Nigeria	B	7255
12:00-12:15 a.m.	0500-0515	Kol Israel	B	17815, 15585, 15105, 11638
12:00-12:15 a.m.	0500-0515	R. Japan	C	15270
12:00-12:30 a.m.	0500-0530	R. Portugal	B	11925, 6025 (Mon-0520)
12:00-1:00 a.m.	0500-0600	R. Australia	C	21680, 17890, 17870, 17725
12:00-1:00 a.m.	0500-0600	HCJB, Ecuador	B	15115, 11910, 9745, 6095
12:00-3:00 a.m.	0500-0800	R. Moscow	B	15470, 15455, 12050, 12010, 11960, 9790, 9580
12:00-6:00 a.m.	0500-1100	V. of Cuba	B	600
12:15-1:15 a.m.	0515-0615	Spanish Foreign R.	B	11880, 9630
12:22-12:30 a.m.	0522-0530	UN Radio	A	9540, 6055 (Sat)

12:30-12:50 a.m.	0530-0550	V. of Germany
12:30-1:25 a.m.	0530-0625	R. Nederland
12:30-2:30 a.m.	0530-0730	R. New Zealand
12:45-1:00 a.m.	0545-0600	UN Radio
12:45-2:30 a.m.	0545-0730	BBC
1:00-1:15 a.m.	0600-0615	R. Japan
1:00-1:30 a.m.	0600-0630	R. Norway
1:00-1:30 a.m.	0600-0630	R. Australia
1:00-2:00 a.m.	0600-0700	RAE, Argentina
1:00-2:00 a.m.	0600-0700	HCB, Ecuador
1:00-2:00 a.m.	0600-0700	R. RSA
1:15-1:30 a.m.	0615-0630	R. Canada International
1:25-3:55 a.m.	0625-0855	V. of Malaysia
1:30-2:00 a.m.	0630-0700	R. Australia
1:45-2:00 a.m.	0645-0700	R. Canada International
1:57-4:55 a.m.	0657-0955	V. of Philippines
2:00-2:15 a.m.	0700-0715	R. Japan
2:00-3:00 a.m.	0700-0800	Xandir Malta
2:00-3:00 a.m.	0700-0800	V. of Vietnam
2:00-4:00 a.m.	0700-0900	R. Australia
2:07-2:15 a.m.	0707-0715	UN Radio
2:30-2:45 a.m.	0730-0745	UN Radio
2:30-3:25 a.m.	0730-0825	R. Nederland
2:30-4:00 a.m.	0730-0900	BBC
2:30-6:30 a.m.	0730-1130	R. New Zealand
2:55 a.m. (ade)	0755-	Action Radio, Guyana
3:00-3:15 a.m.	0800-0815	R. Japan
3:30-4:25 a.m.	0830-0925	R. Nederland
3:30-5:00 a.m.	0830-1000	FEBC, Philippines

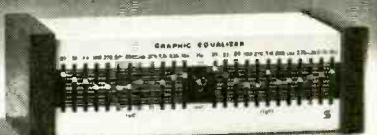
A	11905, 11785, 9650, 9545, 6185, 5960
A	9715, 6165
C	17860, 6105
A	9540, 6055 (Sat)
B	15070, 11955, 11860, 9640, 9510, 6175
C	15270
B	9645 (Mon only)
C	21680, 21525, 17725, 17755, 15240
C	9690 (Tue-Sat.)
A	11910, 9745, 6095
C	21535, 17780, 15220
B	11735, 9730, 9655, 6140 (Mon-Fri)
C	15295, 12350, 9750
B	21680, 17725, 15240, 9670
B	11735, 9730, 9655, 6140 (Mon-Fri)
C	11950, 9579
C	15270
D	9670 (Sat only) (frequent changes)
C	10010, 9840, 7512
B	21680, 17725, 11740, 9670, 9570
A	11840, 6135 (Sat)
A	11840, 6135 (Sat)
B	9770, 9715
B	15070, 11955, 9640, 9510
C	11945, 6105
C	5950
B	9505
B	9715
C	11765 or 11890

Explanatory Notes.

1. Times in first column are EST. For AST, add 1 hour. CST, subtract 1 hour. MST, subtract 2 hours. PST, subtract 3 hours. Days of week are in GMT.
2. Quality. A—strong signal and very reliable reception. B—regular reception. C—occasional reception under favorable conditions. D—rarely audible. These ratings are for locations in the central USA. European and African stations are in general, more reliably received in eastern North America. Asian and Pacific stations are more reliably received in western North America. North American stations are received well except in areas too close to the transmitter site.
3. The information in this listing is correct to press time. However, frequencies and schedules are constantly changing. Listen to "WX Digest" on R. Canada International for date changes, Sunday at 1807; 1915 (to Europe), GMT Mondays at 0117 and 0317, and Wednesdays at 2140.
4. R.—Radio; V.—Voice

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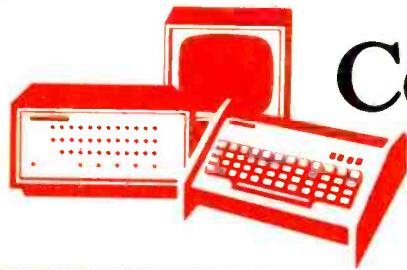
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By Leslie Solomon
Technical Director

3D GRAPHICS

TWO-DIMENSIONAL graphics at various levels of resolution are quite common. Some computers, especially the newer ones, come with built-in graphics capability, while older machines (especially the S-100 variety) rely on plug-in boards. In either case, reasonably high-resolution graphics, even in color, present no problem.

Now there is a new approach: user-controlled, full three-dimensional graphics. Designed for the Apple II, the graphics are provided by the A2-3D1 Animation Package from SubLogic, Box V, Savoy, IL 61874. This software package is available on cassette for \$45, and the diskette version is \$55. Although it has limited use with 16K of RAM, 24K is required for optimum utility.

After a 10K machine-language program is placed in memory, for an introduction, some simple BASIC commands allow you to maneuver a three-dimensional cube around the screen. The cube can be rotated on any of its axes, can be moved closer to or farther away from the viewer's "eye", and can even be made to move off the screen to either side, then apparently pass around (or over) the viewer and return to the screen. The perspective of the figure changes with rotation and movement.

The manuals explain how to create various shapes, or groups of shapes, and move them about. On the Apple, the viewed objects use the 140 X 192 high-resolution mode and can move at 150 lines per second, with a 20-line drawing presented at 5 frames per second. The variable field of view also allows camera-like zooming.

Besides a 32-page Load and Go manual that guides the user through an orientation session, there is also an 84-page booklet that completely covers the machine language and BASIC programs. Special features include array generation of line start and end points so that the program can be used with future graphic output devices; a zero-page restore that leaves all zero-page variables intact after subroutine exit; a page control that allows selective page erase, display and draw to permit smooth animation; and a selective erase feature that allows movement of viewed objects without erasing the full screen.

Another package, Load and Go 3D Graphics in BASIC for the Apple II with Applesoft, is also available. This package contains a 60-page BASIC 3D graphics manual and a 22-page preliminary manual. The BASIC version on cassette is \$30 (\$10 extra for diskette) and generates its own trig functions. There-

fore, the listing may be adapted for other BASIC-using computers from a Level II TRS-80 to more complex models.

Tarbell Disk. The VDS-II Vertical Disk Subsystem includes two Siemens 8" disk drives, Tarbell Floppy Disk Interface, CP/M Disk Operating System, and Tarbell BASIC. It is assembled, tested and packaged, with fan and power supply. It includes all cables and complete documentation. The system uses standard IBM-compatible soft-sectored 8" diskettes. Capacity per drive is 256K bytes with a 250-kHz transfer rate. The interface is S-100. Four extra slots allow four more drives. \$1888 from Tarbell Electronics, 950 Dovlen Place, Suite B, Carson, CA 90746 (Tel: 213-538-4251 or 2254).

Reserve Power. The APPLEJUICE reserve power supply protects against program interruption and data loss due to power flickers and brownouts. It provides a visual, audible and electronic signal output to alert the user when a power failure is occurring. Designed for the Apple computer line, the power supply back-up time is approximately 15 minutes. \$249 from High Technology, Inc., 1611 N.W. 23rd St., Oklahoma City, OK 73106 (Tel: 405-528-8012).

S-100 Mainframe. This 12-slot actively terminated S-100 mainframe measures 11⁵/8 inches high, 7 inches wide and 18 inches deep and comes complete with fan and circuit breaker. It supports +8 volts at 20 amps and ± 16 volts at 4 amps. Input may be 105,

115 or 125 volts ac. It features a flip-top cover and comes in various colors. \$399.95 assembled and tested from California Computer Systems, 309 Laurelwood Dr., Santa Clara, CA 95050 (Tel: 408-988-1620).

Apple Lower Case. The Keyboard Expander is a hardware-software modification to an Apple II that allows it to use both upper and lower case. The shift keys can be used conventionally. The hardware change is a one-wire modification. The software modification is a transparent machine-language routine that augments the capabilities of the monitor while avoiding its upper case conversion code. All Apple II characters and editing functions are permitted as well as cap and shift lock. It requires 1/4K of memory. \$20 from C&H Micro, P.O. Box 249, Clifton Park, NY 12065.

S-100 Accessories. A catalog of various S-100 plug-ins such as memories, disk systems, motherboards, multi-I/O ports, and software is available from Thinker Toys, 5221 Central Ave., Richmond, CA 94804.

Apple Graphics. The Versa-Writer is a digitizer and software package for the Apple II. Sixteen commands permit fill-in coloring using six colors and control cursor movement, horizontal and vertical scaling, centering on screen, and storing and recalling to and from disk, etc. The drawing board plugs into the game I/O, and requires 32K of RAM, Applesoft in ROM and Disk II. \$199 from Rainbow Computing Inc., 9719 Reseda Blvd., Northridge, CA 91324 (Tel: 213-349-5560).

KIM I/O. This RS-232 interface is designed for the AIM/KIM/SYM microcomputers, to allow these devices to connect to any RS-232 terminal, printer or modem. The I/O features 15 baud rates, programmable word length, a choice of stop bits, odd/even parity, serial echo mode, interrupt and status register, half/full duplex operation, parity/framing/overrun error detection, expansion connector and a DB25 connector. Kit is \$69.95, wired/tested is \$84.95. Fobel Enterprises, 552 E. El Morado, Ontario, CA 91764 (Tel: 714-984-8871).

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The SubLogic A2-3D1 Apple II Animation Package provides full three-dimensional graphics which can be easily maneuvered on the screen.



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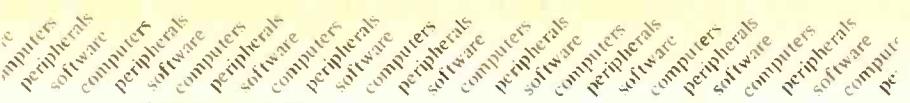
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Software Sources

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Technical Director

TRS-80 Dialer/Timer. This TRS-80 Level-II BASIC program holds up to 500 names and telephone numbers in 16K, or 30 names and numbers in 4K. The cable that normally goes to the cassette remote jack is used to pulse the interface relay. The computer displays the name, number and area code of the party selected, then displays each digit as it is dialed. After contacting the remote party, hitting ENTER starts timing and displaying the call by the second. At the end of the call, the user inserts rate and computer displays time and charge. \$10 from Blechman Enterprises, 7217 Bernadine Ave., Canoga Park, CA 91307 (Tel: 213-346-7024).

Text Processor. The Master Text Processor, for the Apple II and Apple Plus systems contains a mailing list and programmable form letter writer. It requires 32K of RAM and one or two disk drives. It features user-defined formatting, automatic line length adjust, and text merging, and includes change, insert, delete, text formatting, sentence merger, string location and word/phrase replacement. \$139.95 from CMA dealers. Charles Mann and Assoc., Micro Software Div., 7594 San Remo Trail, Yucca Valley, CA 92284 (Tel: 714-365-9718).

CP/M SBASIC. SBASIC (structured BASIC) is a pre-compiler offering the power of structured programming for conventional BASIC. SBASIC provides additional statements for program control. These include IF . . FIN, UNLESS . . FIN, WHEN . . FIN, ELSE . . FIN, FOR . . FIN, REPEAT UNTIL . . FIN, REPEAT WHILE . . FIN, UNTIL . . FIN, WHILE . . FIN, SELECT . . FIN, CONDITIONAL . . FIN, PROCEDURE . . FIN, and PERFORM. Thus, SBASIC allows the user to write exactly what is meant without GOTO's or THEN's. CP/M diskette is \$50, BASIC source listing is \$35. Ultimate Computer Systems, 313 Meadow Lane, Hastings, MI 49058 (Tel: 616-945-5334).

TRS-80 Pencil Pal. If you use the Electric Pencil on your TRS-80, then the addition of Pencil Pal allows automatic merging of letters with an address file. It is entirely compatible with lower-case modifications. One or two fields within the address file may be used to select letters to be printed. \$35 on cassette with documentation, or \$5 for documentation alone. MicroComputer Specialists, P.O. Box 11295, Elkins Park, PA 19117, (Tel: 215-635-2473).

Z8000 FP Package. This package provides a unified set of floating-point support subroutines for any Z8002. 32-bit binary floating-point format is used to provide fast arithmetic operations, integer-float and float-integer conversions, float-ASCII string representation, and ASCII string-float conversions. Precision is between 6 and 7 digits and exponent range is $1E-20$ to $1E+20$. The package is ROMable, and requires 1412 bytes and 50 bytes of stack RAM. \$99.95 from Hemenway Associates, Inc., 101 Tremont St., Suite 208, Boston, MA 02108 (Tel: 617-426-1931).

Fantasy Software. The game called "Morloc's Tower" was designed for a PET with 20K, TRS-80 Level II with 16K, and Apple II with 32K and Applesoft in ROM. The game features a maze of 30 rooms, all displayed on screen, in the search for the elusive wizard, Morloc the Mad. It has full graphics and 18 real-time commands. All forms of "magic" things appear on the screen—monsters, rings, swords, amulets, etc. There are three levels of difficulty that can be played. \$14.95 from Byte Shops or Automated Simulations, P.O. Box 4232, Mountain View, CA 94040 (Tel: 415-964-8021).

Medical Package. This program handles all details of billing, insurance forms, treatment records, and many reports including charge and payment entry, patient statements, Blue Cross billings, Medicare submittals and remittances, commercial insurance billing, collection accounting and dunning, patient processing, numeric or alphabetic patient listing, CPT-4 procedure and ICDA-9 diagnostic code reports, aged accounts receivables, third party accounting and reconciliation, and transaction reporting. Program is available on 8" or various mini-floppies. Storage capacity of two-disk (8") single-density system: on Disk B, 1200 patient records and 2100 treatment/payment records; on Disk A, 1000 CPT codes and charges, 1000 diagnostic codes, and 2000 third-party billing records. Graham-Dorian Software Systems, Inc., 211 N. Broadway, Wichita, KS 67202.

Atari and TI 99/4 Games. New line of software includes: for the Atari, All Star Baseball 6401, Wall Street Challenge 6402, Mind Master 6403, Strategy Packs I 6404 and II 6405, and Skill Builder 6406; and for the TI system, Tournament Brick Bat 9401, Wall Street Challenge 9402, Wildcatting 9403, Strategy Pack I 9404, Mind Master 9405 and Skill Builder I 9406. Image Computer Products, Inc., 615 Academy Drive, Northbrook, IL 60062 (Tel: 312-564-5060).

Apple Circuit Design. This electronic design package for the Apple II with Applesoft in ROM and 48K of RAM features 84 different formulas for use in circuit analysis. There are 11 formulas for dc, 30 for ac, 20 for designing filters, 4 for vacuum tubes and 8 for transistors. The set of 84 is completed with 11 formulas covering miscellaneous areas. High-resolution graphics of the filters are shown. All programs are self-promting. In diskette form for \$99.95. Korsmeyer Electronic Design, 9612 Chevy Chase, Huntington Beach, CA 92646 (Tel: 714-964-4346).

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PROJECT OF THE MONTH

BY FORREST M. MIMS

THE Project of the Month in the December 1979 issue of POPULAR ELECTRONICS was a random number generator made from an LM331 voltage-to-frequency converter and a 4017 decade counter/decoder. After describing the circuit, I presented results of 100 trials and concluded "If the results were perfectly random, each of the ten LEDs would be selected an equal number of times or ten times each for a sample of 100 trials."

Readers Warner Clements and Thomas D. Martin were quick to catch the error in this conclusion. Quoting from Mr. Clements's letter, "Suppose the device were an absolutely perfect random number generator, in accord with theory. Then, what would be the probability that, in a run of 100 generated numbers, you'd get ten of each digit? Mims's statement sets the probability at unity. But in reality the probability is 1/42,423,000. Mims thus overestimates the probability by more than four billion percent."

Fortunately the operation of the circuit was unaffected by my statistical misconception. Both Messrs. Clements and Martin observed that the results given in the column are, in Mr. Clements' words, "...random enough for any practical purpose."

Mr. Martin explained some statistical concepts and plotted the results given in the December column on a probability chart. The results tend to indicate the lack of any statistical bias on the part of the original circuit, but, as Mr. Martin said, "This fact does not indicate an absence of bias either, only that your sample is not much different from some other samples taken from data that has been previously tested."

I very much appreciate the help these readers have provided. Since random number generation is so important, this encore column gives some additional circuits.

Coin Tosser. Figure 1 is a CMOS coin tosser which lights, with virtually the same probability, either of two LEDs. The oscillator, which is made from the two gates, operates at a frequency of about 1 MHz. Pressing S1 for a second or two allows the oscillator to run, which in turn toggles the flip-flop at a rate far too fast to second guess which LED will glow when switch S1 is released.

If you use red LEDs, label one heads and the other tails (or label one left and the other right). You can avoid labels by using a red LED and a green LED. Furthermore, you can add an additional element of chance by inserting a cadmium sulfide photoresistor between R1 and point "x".

More on Pseudorandom Number Generators

Subtle variations in the light striking the cell will alter the oscillator frequency.

Pseudorandom Number Generator. If you can't find an LM331 for use in the December 1979 Project of the Month, try the circuit shown in Fig. 2. Although this circuit won't exhibit wheel-of-fortune operation (that is, press the button and all LEDs glow; release the button and the LED cycle gradually slows until only one remains on), it produces results that are just as random.

The oscillator portion of Fig. 2 is identical to the oscillator shown in Fig. 1. The remainder of the circuit is identical to the

decade counter/decoder section of the December circuit.

Label the LEDs 0 through 9 (or 1 through 10). To operate the pseudorandom number generator, press S1 for a second or two to activate the oscillator. All the LEDs will glow as they are scanned sequentially by the decoder. When S1 is released, one of the LEDs remains on.

You can modify this circuit for digital readout by substituting a BCD counter/decoder and a seven-segment LED or liquid crystal display for the 4017 and its string of LEDs. Current consumption is low, so the circuit will operate for a long time when powered by a 9-volt alkaline cell. ◇

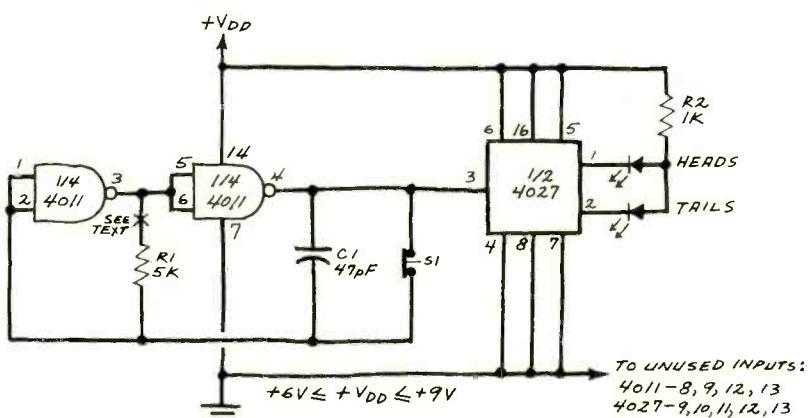


Fig. 1. Schematic diagram for a coin tosser using CMOS circuitry.

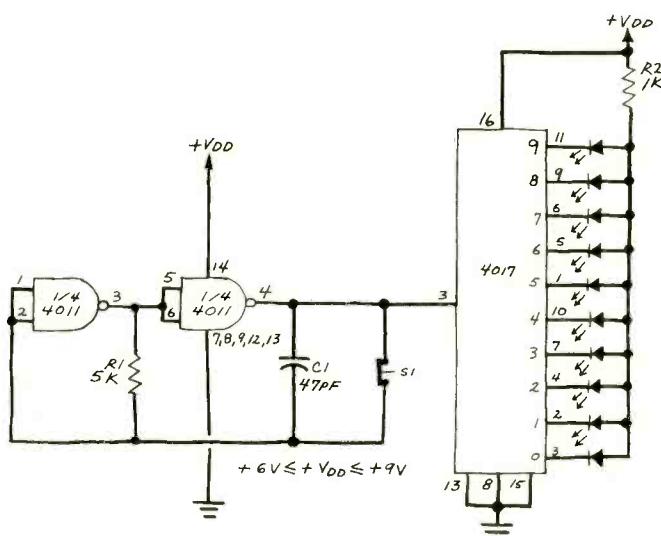
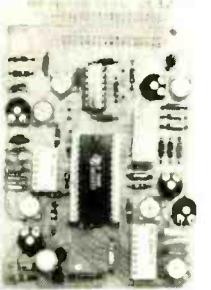


Fig. 2. Circuit for a pseudorandom number generator.

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Published by Reston Publishing Co., Inc. Reston, Va. Hard cover. 246 pages. **\$16.95.**

THE A TO Z BOOK OF COMPUTER GAMES

By Thomas C. McIntyre

This collection of 26 BASIC programs for playing video games was designed to teach the reader how a program is developed, culminating in listings one can copy. Thus, it is not merely a technical book or a listing of programs. The best of both are illustrated for learning and fun. Programs include information on what the challenge is, how to approach developing the program, how the game works, what the program contains, how to alter or modify the existing program, and how the program relates to other programs. Among the games presented are poker, blackjack, solitaire, battleship, golf, roulette, etc. Some games can be played against the computer, some against one opponent, and some against more than one opponent.

Published by Tab Books, Blue Ridge Summit, PA 17214. 308 pages. **\$12.95 hard cover, \$7.95 soft cover.**

HANDBOOK OF ELECTRONIC FORMULAS, SYMBOLS AND DEFINITIONS

by John R. Brand

Contained in this book are thousands of electronic formulas, symbols, and definitions for modern passive and active analog circuits. Its alphabetical format permits one to locate information quickly without first having to look it up in an index. For even easier location of desired information, the book is divided into three main sections: passive circuits (Section 1), transistor circuits (Section 2), and operational-amplifier circuits (Section 3). Separate appendices list 5% component-value ratios that give maximum and minimum values for a desired mean value.

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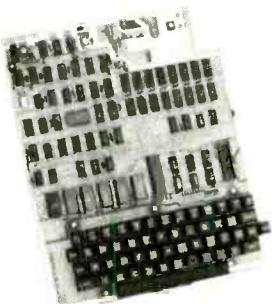
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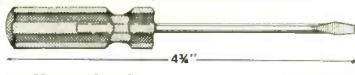
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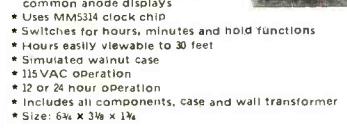
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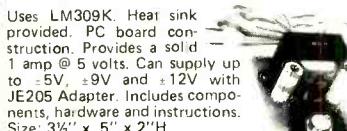
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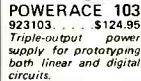
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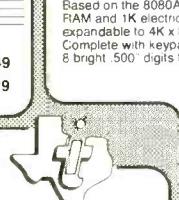
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4680-pin edge

4700-pin edge

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Crosley model 9-419M-1LD TV and model T-3R3 radio. Need schematics and parts list. Raymond Friend, 236 W. Pearl St., Butler, PA 16001.

Rauland model W-861 audio power amplifier. Need schematic and parts list. Neville Mair, 741 E. 213 St., Apt. #1, Bronx, NY 10467.

Lambda model LYD-5-062 power supply. Need operating instructions. R. Davy, 7816 No. 47th Ave., Glendale, AZ 85301.

Bozen model DB-230 amplifier. Need schematic and operation manual. P. Terezakis, Box 340, New York, NY 10036.

Marconiphone model T26AG radio and **Seeburg model 3W-1** wall box jukebox. Need service manuals and schematics. Edward H. Joseph, 20701 Reef Lane, Huntington Beach, CA 92646.

Solar Manufacturing Corp., models CE and CB-1-60 testers. Need schematics and user information. Jeff Lucas, 2253 Coral Sea Dr., Youngstown, OH 44511.

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Knight model KG-200 dc oscilloscope. Need schematic and owner's manual. Nguyen D. Hoan, 6021 Factor Ave., Azusa, CA 91702.

Contex model 6706, 25-40-MHz linear amplifier. Need parts list and schematic. Robert Sweerus, 251 McCosh Road, Upper Montclair, NJ 07043.

Heathkit IM12 harmonic distortion meter. Need schematic and manual. Ernest Koenderink, 9 Begonia Straat, 2565 SP, The Hague, Netherlands.

General Radio Co., model 650A impedance bridge. Need operation manual and schematic. James B. Powell, 300 Cellier Blvd., Napa, CA 94558.

Winston Electronic Inc., model 820 dynamic sweep circuit analyzer. Need operation manual and schematic. Luther Mayberry, 3112 5th St., Union Gap, WA 98903.

Calibration Standards Corp., model DC-200B precision dc voltmeter. Need manual and/or schematic. José E. Cordero, Box 4522, San Juan, PR 00936.

General Electric model 4ST2A02 oscilloscope. Need operating manual and schematic. Doug McDermott, 24 Tuxedo Dr., Rome, NY 13440.

Johnson Viking Valiant-I transmitter kit. Need assembly instructions. John S. Anderson, 4267 Coronado Ave., San Diego, CA 92107.

Eico model 425 oscilloscope, RCA WV-97A Senior Voltphymyst and **Hallcrafters S120** receiver. Need schematics and/or operating instructions. Kenneth W. Hillis, BTC K-9, Eleison AFB, AK 99702.

Knight KG-50 AM-FM stereo tuner and KG-250 stereo amplifier. Need schematic, alignment and service manuals. Gregory P. Widin, 1644 Eldridge Ave. W., St. Paul, MN 55113.

Dumont model 185-A electronic switch. Need schematic and operation manual. **Solar model CB-1** capacitor analyzer. Schematic needed. Mark D. Pickering, 80 Desmond Rd., Salinas, CA 93907.

Symphonic model 235001 AM/FM stereo. Need schematic and part number of replacement PWR transformer. Leon Weston, Box 13, Winthrop, ME 04364.

Craig Corp., model 6403 video tape recorder. Need service manual and schematic. Fred W. Keylor, Box 400, 1250 Turner St., Auburn, ME 04210.

Knight KG-790 AM/FM tuner, JVC model CHR-250 UB 8-track recorder, Dual/BSR model 1219 turntable. Need service/maintenance manuals. Charles T. Huth, 146 Schonardt St., Tiffin, OH 44883.

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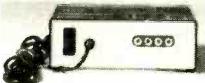
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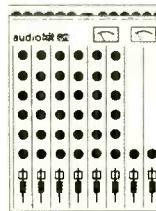
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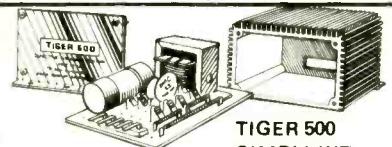
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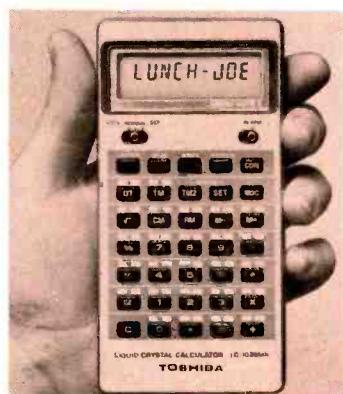
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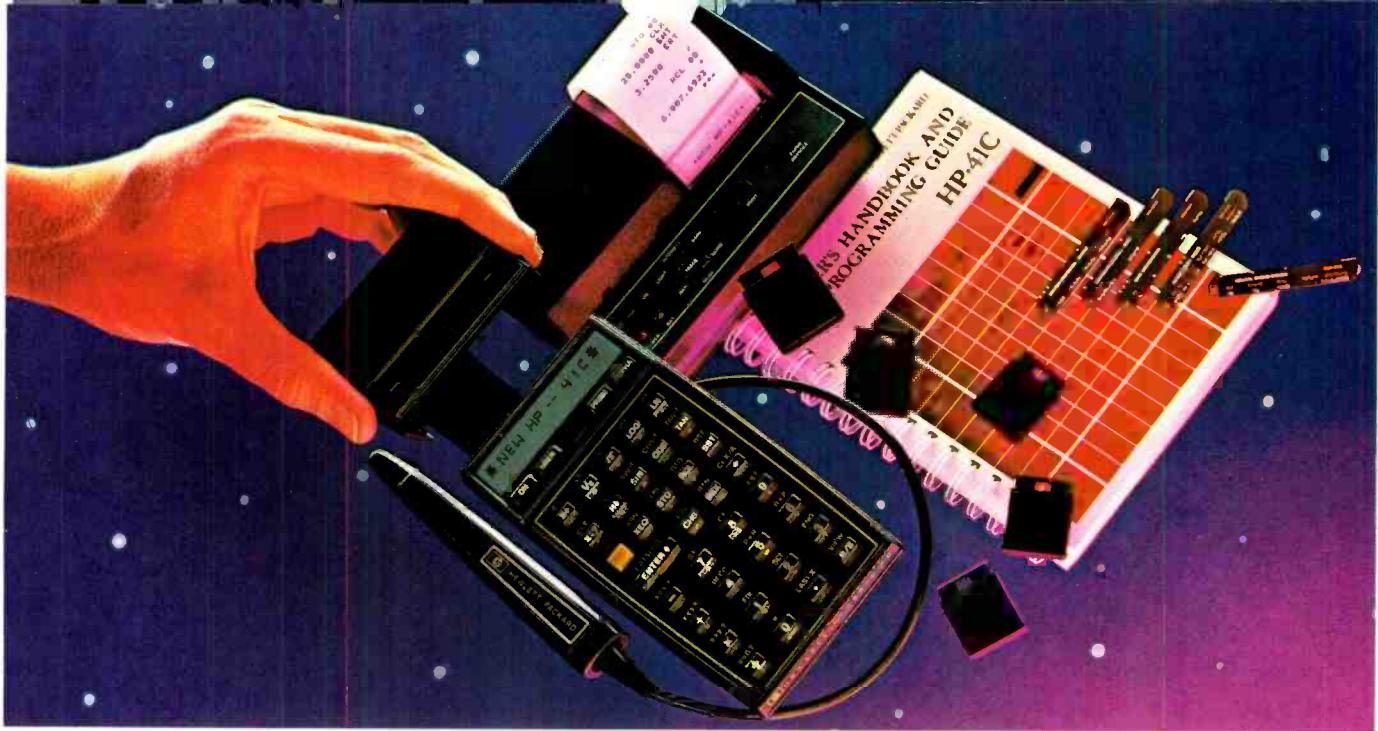
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Toshiba's Memo Note II is an alphanumeric pocket calculator with alarm that stores messages for recall up to a year later. With 30 alphanumeric memories, the device stores reminder messages for alarm alert on a desired date and time. Thus, at a specific time on a certain day, the calculator might announce (with an alarm) the message: DADS-BIRTH; the telephone: 326-0383; the date/time: 10-30/3:30 PM. In addition to scheduling appointments, anniversaries, and notes for a year's time, the Memo Note II has stored in its preprogrammed memory the equivalent time in 26 cities in different time zones around the world. It is also possible to link up to four alarm times to one message for, say, taking pills during the course of a day. P. S. It can also be used as a calculator.

TOTALLY AUTOMATED FACSIMILE SERVICE which resolves incompatibility of machines and offers rate categories not affected by distance is the promise of FAXPAK, the new nationwide facsimile transmission service of ITT Domestic Transmission Systems. ITT's front-end processors perform speed code and protocol translation necessary to let any facsimile machine talk to any other machine. FAXPAK's computer also allows a user to "broadcast" one document to several different terminals with a single transmission. Business day-time, per-minute terminal connection charges are 16 cents for delivery within 15 minutes and 10 cents for delivery within two hours. Night and weekend rates are lower.

VIDEOTAPE CASSETTE COPY PIRATES face a tougher future if Composite Video, Oklahoma City, OK, has its way. The company's Videoguard VG-350 encoder, available in PAL and NTSC standards, is reported to protect all 1/2" and 3/4" video cassette tapes. Its color process amplifier and sync generator strip all blanking, sync, and burst signals from the master VTR playback and replaces them with new signals. The sync generator restores incoming signal amplitude and level to proper standards. Moreover, it's claimed to defeat the latest VTR sync circuits without causing vertical roll. Attempts at pirating will result in a muted blank picture with no audio (Sony Beta 1/2" and 3/4" formats); loss of sync and tracking control (4-hour mode 1/2" VHS-type VCRs); and loss of tracking control with head switching (2-hour mode VHS-type VCRs and 3/4" Panasonic and JVC models).

NEW STANDARDS ON MICROPHONE POLARITY or phase have been issued by the Electronic Industries Association. Including an up-to-date scheme for marking polarity on three-terminal microphone connectors and new procedures in verifying polarity and establishing the polarity of an existing dynamic or moving microphone, "Polarity or Phase of Microphones for Broadcasting, Recording and Sound Reinforcement" (RS-221-A) is available from EIA, 2001 Eye Street, N.W., Washington, D.C. 20006 at \$3.00 per copy. One can also request a free Catalog of EIA and JEDEC Standards and Engineering Publications at the same time.



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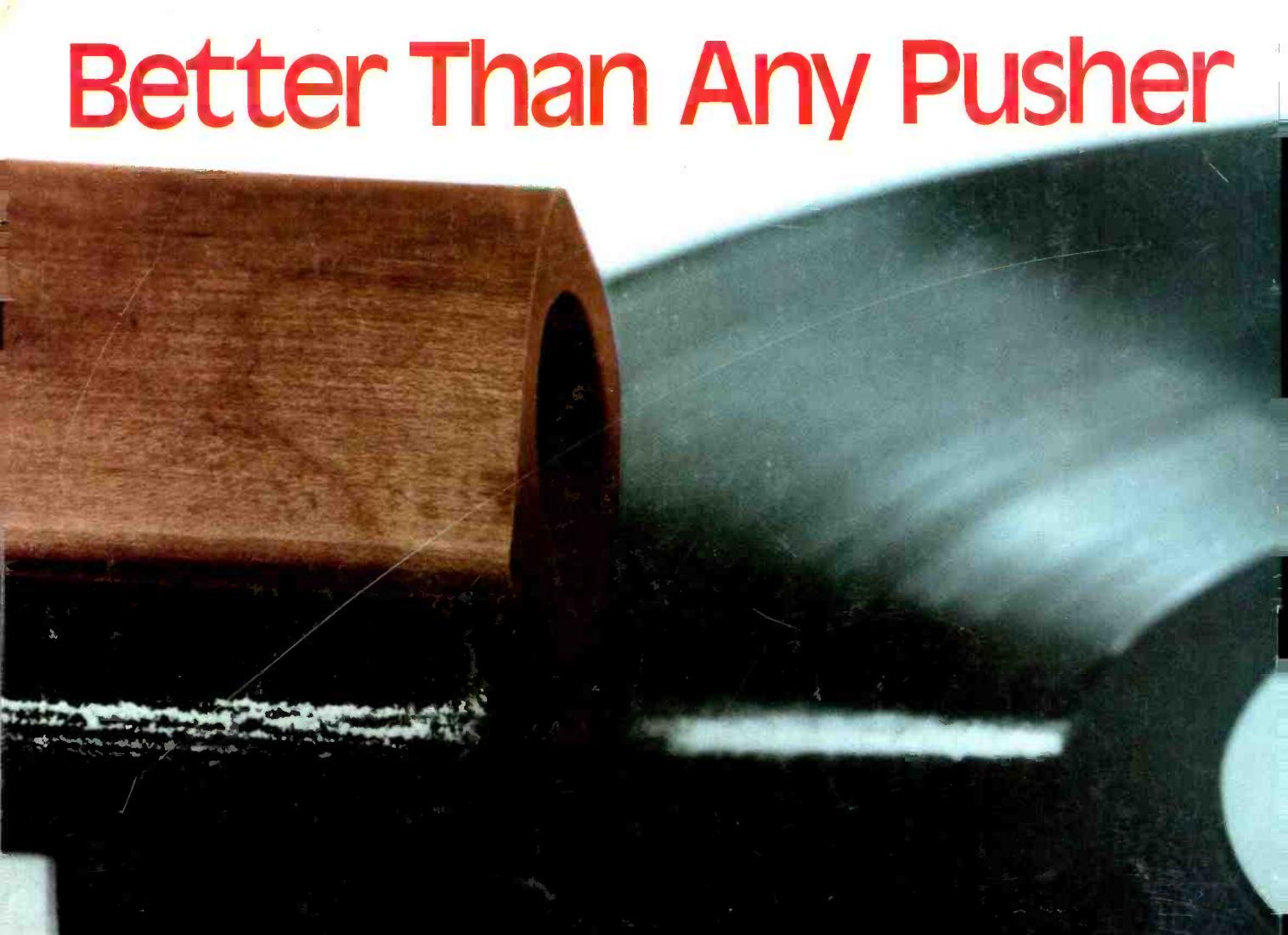
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