

## Lecture # 7.2 CHE331A

- Design of ideal reactors - Basics
- Reaction kinetics and Rate law as a function of conversion
- Design/Analysis of a PFR with variable volume
- Cracking of Ethane in a PFR as an example of variable volume flow

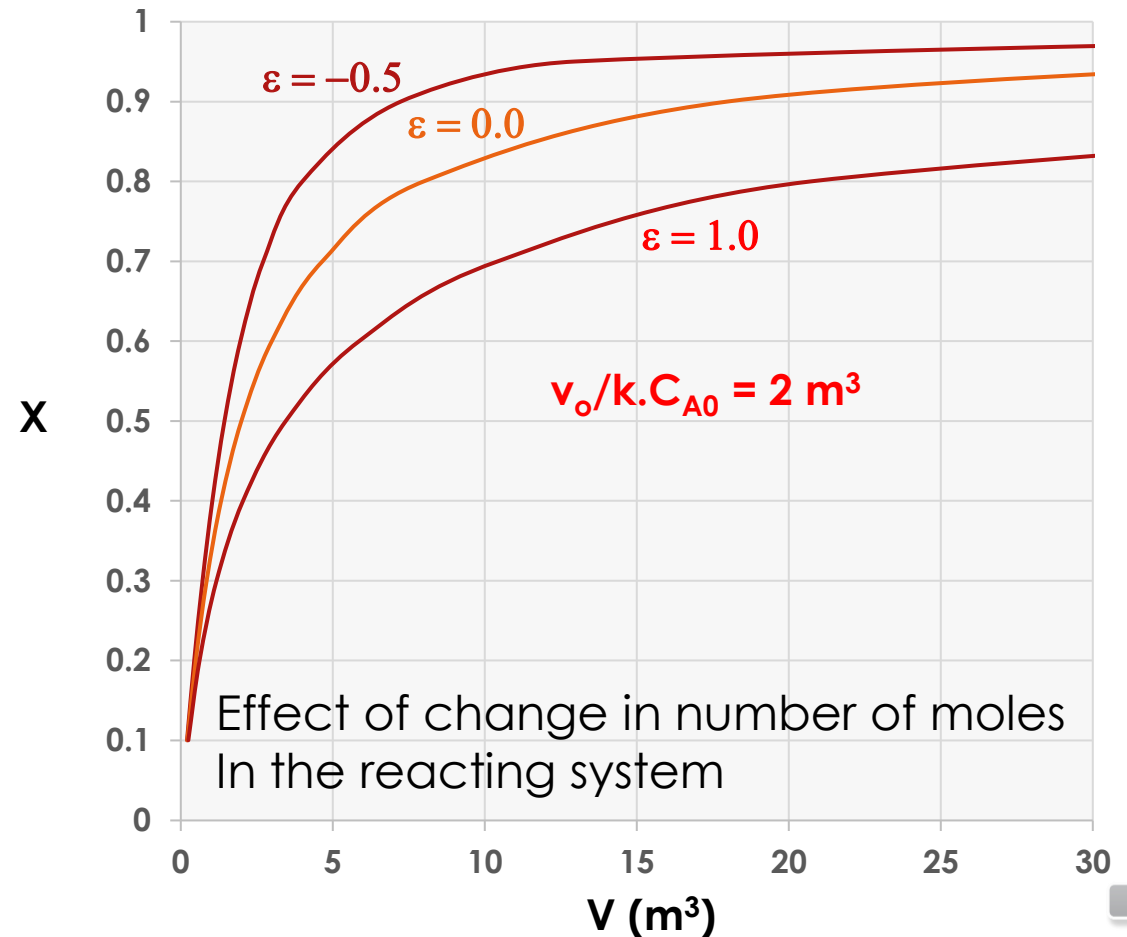
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$$V = \frac{\dot{v}_0}{k \cdot C_{A0}} \left[ 2\varepsilon(1 + \varepsilon) \ln(1 - X) + \varepsilon^2 X + \frac{(1 + \varepsilon)^2 \cdot X}{(1 - X)} \right]$$



# Tubular reactor design for Ethane Cracking to Ethylene

- ▶ Required to produce 300 million lbs per year of ethylene in a PFR at 6 atm and 1100 K (isothermal and isobaric) with 0.80 conversion
- ▶ Gas phase reaction:  $C_2H_6(A) \rightarrow C_2H_4(B) + H_2(C)$
- ▶  $F_B = 300 \text{ million} \frac{\text{lb}}{\text{year}} = 0.340 \frac{\text{lbmol}}{\text{s}}$  and  $F_{A0} = \frac{0.340}{0.8} = 0.425 \frac{\text{lbmol}}{\text{s}}$
- ▶  $C_{A0} = y_{A0} C_{T0} = \frac{y_{A0} P_0}{RT_0} = \frac{1 \cdot 6 \text{ atm}}{0.73 \frac{\text{ft}^3 \cdot \text{atm}}{\text{lbmol} \cdot \text{R}} \cdot 1980 \text{ R}} = 0.00415 \frac{\text{lbmol}}{\text{ft}^3}$  and
- ▶ For pure ethane feed:  $y_{A0} = 1$ , and for the reaction:  $\delta = 1 + 1 - 1 = 1$
- ▶ Thus,  $\varepsilon = y_{A0} \delta = 1$



# In Ethane Cracking the number of moles change and concentration is affected

- Mole balance for PFR in terms of conversion:

$$F_{A0} \frac{dX}{dV} = -r_A$$

- Rate law:  $-r_A = k \cdot C_A$  with  $k = 3.07 \text{ s}^{-1}$

$$V = F_{A0} \int_0^X \frac{dX}{-r_A} = F_{A0} \int_0^X \frac{dX}{k C_A}$$

- Stoichiometry:  $\dot{v} = \dot{v}_0(1 + \varepsilon X)$   $P = P_0, T = T_0, Z = Z_0$

$$C_A = \frac{F_A}{\dot{v}} = \frac{F_{A0}(1-X)}{\dot{v}_0(1+\varepsilon X)} \quad \text{and} \quad -r_A = k \cdot C_A = k \cdot \frac{F_{A0}(1-X)}{\dot{v}_0(1+\varepsilon X)}$$



# Number of moles change affects the volume of PFR

► With  $C_A = \frac{F_A}{\dot{v}} = \frac{F_{A0}(1-X)}{\dot{v}_0(1+\varepsilon.X)} = C_{A0} \frac{(1-X)}{(1+\varepsilon.X)}$  then

$$-r_A = k \cdot C_A = k \cdot C_{A0} \frac{(1-X)}{(1+\varepsilon.X)}$$

► And,

$$V = F_{A0} \int_0^X \frac{dX}{k C_A} = \frac{F_{A0}}{k \cdot C_{A0}} \int_0^X \frac{(1+\varepsilon X)}{(1-X)} dX$$

$$V = \frac{F_{A0}}{k \cdot C_{A0}} \left[ (1+\varepsilon) \ln \left[ \frac{1}{1-X} \right] - \varepsilon X \right]$$



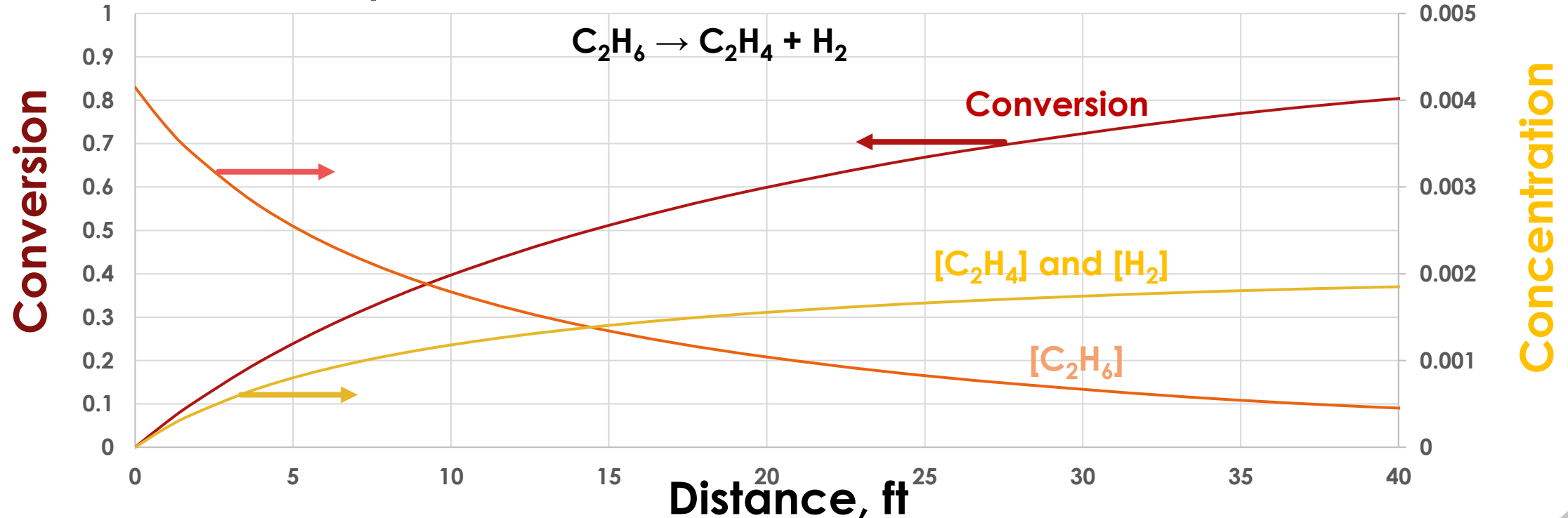
# Calculation for volume continued

- ▶  $V = \frac{F_{A0}}{k.C_{A0}} \left[ (1 + \varepsilon) \ln \left[ \frac{1}{1-X} \right] - \varepsilon X \right] = \frac{0.425}{3.07 * 0.0045} \left[ (1 + 1) \ln \left[ \frac{1}{1-0.8} \right] - 1 * 0.8 \right]$
- ▶  $V = 80.7 \text{ ft}^3$  (about 2.28 m<sup>3</sup>)
- ▶ PFRs are usually in the form of tubes/pipes.
  - Pipes are available with definite diameter as per pipe schedule
  - Pipe schedule 80 gives a cross-sectional area = 0.0205 ft<sup>2</sup>
  - For a length of 40 ft the number of tubes can be found out
  - Number of tubes:  $n = \frac{80.7}{0.0205 * 40} \approx 100$
- ▶ Thus, using 100 tubes of schedule 80 one has the reactor volume necessary to produce 300 million lbs of ethylene from ethane



# Conversion and concentration profile along the length can be calculated with distance, Z

Conversion/Concentration versus distance for each tube



$$V = \frac{F_{A0}}{k \cdot C_{A0}} \left[ (1 + \varepsilon) \ln \left[ \frac{1}{1 - X} \right] - \varepsilon X \right]$$

