### Reactor 1 $C_2H_6$ C2H6 - C2H6 + H2 Separato O2, C2H4, N2, C2H4O V = 81 ft3 X = 0.8Reactor 2 Cyt, + 102 Ag CH2 CH2 W = 45,440 lb C2H4O Reactor 3 C<sub>2</sub>H<sub>4</sub>O(aq) V = 197 ft<sup>3</sup> OH-CH<sub>2</sub>-CH<sub>2</sub>-OH

**Process Flowsheet for Ethylene Glycol Manufacture** 

From "Elements of Chemical Reaction Engineering", 4<sup>th</sup> Editions, H.S. Fogler, For teaching purposes only.

### Lecture #2.1

- Chemical industries involve at least one chemical reaction
- Chemical reactions take place in a REACTOR
- Reaction, Reactors and more Reactors!

GOUTAM DEO

CHEMICAL ENGINEERING DEPARTMENT

IIT KANPUR



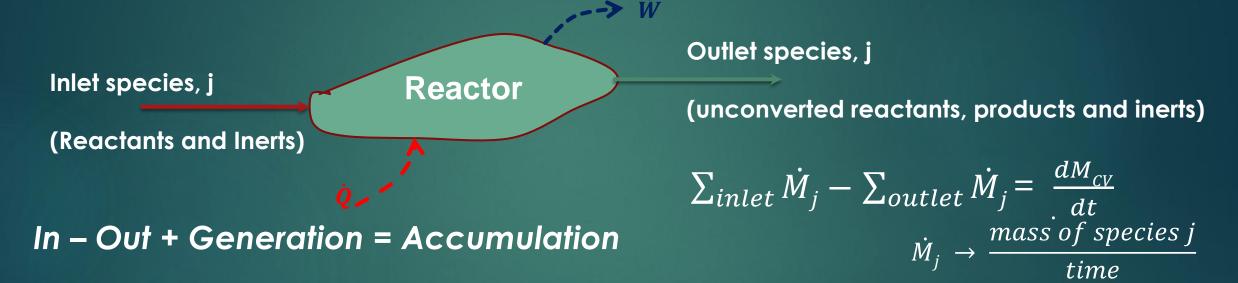
## **Briefly**

- ► Course policy
- Course content
- Reactions occur in primarily three ways
- ► Importance of Chemical Engineering Thermodynamics
- Reaction rate is independent of the reactor and is an algebraic function



# ESO201A & CHE251A intro. us to mass, species, & energy balances in chemical processes

▶ For a control volume (Reactor) the three balances can be applied



$$(F_{j})_{inlet} _{-}(F_{j})_{outlet} + G_{j} = \frac{d(Nj)_{cV}}{dt} \quad F_{j} \rightarrow \frac{moles\ of\ species\ 'j'}{time} \quad G_{j} \rightarrow \frac{moles\ of\ 'j'\ generated}{time}$$

$$\sum_{inlet} \dot{E} - \sum_{outlet} \dot{E} + \dot{Q} - \dot{W} = \frac{dE_{cV}}{dt} \quad \dot{E} \rightarrow \frac{Energy\ (Enthalpy)}{time} \quad (Nj)_{cV} \rightarrow moles\ of\ 'j'\ in\ CV_{outlet}$$

## From simple to complex for understanding

Balance for species A (not showing heat and work)



**Reactants and Inerts** 

Reactor

Outlet species

Unconverted reactants, products and Inerts

$$(F_A)_{inlet}$$
  $(F_A)_{outlet}$  +  $G_A$  =  $\frac{d(N_A)_{CV}}{dt}$  = 0 for steady state

$$F_A \rightarrow \frac{moles\ of\ A}{time}$$

$$G_A 
ightarrow rac{moles\ of\ A\ generated}{time}$$

$$(N_A)_{CV} \rightarrow moles\ of\ A\ in\ CV$$

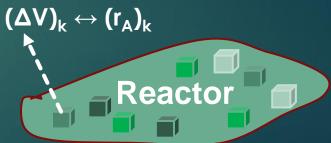
$$(\Delta V)_k \leftrightarrow (r_A)_k$$
Reactor

Rate of Generation,  $G_A$ , is  $G_A = \sum_{k=1}^n g_A = \sum_{k=1}^n (r_A)_k \cdot (\Delta V)_k$  summed over all volume Rate of Generation,  $G_A$ , is elements  $(\Delta V)_k$ 

$$\longrightarrow G_A = \sum_{k=1}^n g_A = \sum_{k=1}^n (r_A)_k \cdot (\Delta V)_k$$

## Ideal reactors are defined based on variations of rates in Reactor

- ► For a well-mixed reactor, all  $(r_A)_k$  are the same (rate of reaction is the same through out the reactor  $\rightarrow$  T, P, Conc., Cat same throughout)
  - "Ideal" BATCH REACTOR and "Ideal" Continuous Stirred Tank Reactor (CSTR)
  - BATCH Reactor does not have any inlet or outlet flow and a CSTR is a ideal flow reactor
  - Then,  $G_A = \sum_{k=1}^{\infty} (r_A)_k \cdot (\Delta V)_k = r_A \cdot V$
- Else,  $G_A = \sum_{k=1}^n (r_A)_k \cdot (\Delta V)_k = \int r_A \cdot dV$





# A general mole balance equation for species *j* in a reactor is useful for analysis

$$F_{j0} - F_j + \int r_j \, dV = \frac{dN_j}{dt}$$

In – Out + Generation = Accumulation ← for species j

- where,  $F_{j0}$   $\rightarrow$  inlet molar flow rate of j,  $\frac{moles\ of\ j}{time}$   $F_{j} \rightarrow \text{outlet molar flow rate of}\ j$ ,  $\frac{moles\ of\ j}{time}$ 
  - $r_j \rightarrow \text{rate of formation of } j \text{ (applicable if } j \text{ is reactant or product), } \frac{moles\ of\ j\ formed}{volume.time}$
  - $N_j \rightarrow \text{moles of A in Reactor at time 't', moles of } j$

▶ The general mole balance eq<sup>n</sup> can be applied to different Reactors



## Batch Reactor (BR) is a closed system

#### **Batch Reactors used for**

- Testing new process that are under R&D
- Manufacture of expensive products
- Processes difficult to make continuous (Biochemical reactions, pharmaceuticals, paints, some polymerization reactions)
- Disadvantages
  - High labor
  - Variability of product
  - Difficulty for large scale operation
- Semi-batch used for gas-liquid reactions

Mole balance for species j



$$F_{j0} - F_j + \int r_j dV = \frac{dN_j}{dt}$$
$$F_{j0} = 0 = F_j$$

Well-mixed  $\rightarrow \int r_j . dV = r_j . V$ 

**V** is the volume of the **BR**, which may or may not change with **t** 

Thus, the **design eq**<sup>n</sup> is

$$\frac{dN_j}{dt} = r_j.V$$

For semi batch reactor

$$F_{j0}$$
 or  $F_j \neq 0$ 



# Time taken to achieve a certain amount of product can be determined

Design equation can be integrated

$$\frac{dN_j}{dt} = r_j.V$$

lacksquare With  $N_j=N_{j0}$  at t=0 and  $N_j=N_{j\_required}$  at  $t=t_{required}$ 

$$t_{required} = \int_{N_{j0}}^{N_{j-required}} \frac{dN_{j}}{r_{j}.V}$$

- This is the time required to change the number of moles of j from  $N_{j0}$  to  $N_{j\_required}$
- ▶ NOTE: we have assumed  $V \neq f(t)$

