

## Lecture # 29 CHE331A

### Residence time distribution

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- ❑ Residence time distribution
  - ❑ Construction of  $C(t)$  and  $E(t)$
  - ❑ Convolution integral
  - ❑ Step-input
- ❑ Some more on RTD
  - ❑  $t_m$  and  $\tau$  and other moments
  - ❑ RTD of Ideal reactors
  - ❑ RTD of LFR

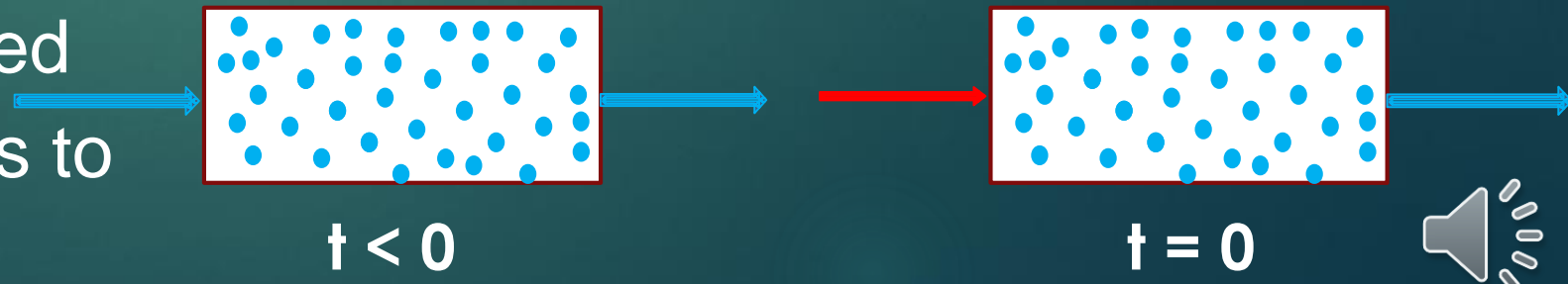


## Space time and mean residence time are related

- ▶ Space time ( $\tau$ ) was defined as  $V/v$  and it signified the average residence time the fluid spent in the reactor
- ▶ Based on the RTD function, the mean residence time is defined as:

$$t_m = \frac{\int_0^{\infty} tE(t)dt}{\int_0^{\infty} E(t)dt} = \int_0^{\infty} tE(t)dt$$

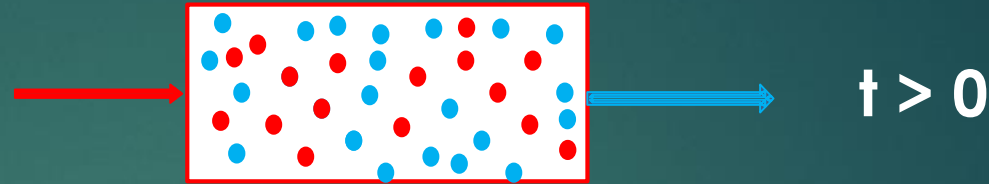
- ▶ This is the first moment of the RTD curve
- ▶ The total reactor volume can be determined from the cumulative distribution function  $F(t)$  of the reactor
  - At time  $t < 0$  the reactor is completely filled with blue fluid elements
  - At time  $t = 0$  red dye is injected
- ▶ Amount of blue dye corresponds to Reactor volume



# Calculation of reactor volume from cumulative distribution function

- ▶ At time  $t = t' (> 0)$
- ▶ Fraction of dye molecules in the effluent that have been in the reactor for  $t \geq t'$  is  $1-F(t')$
- ▶ Volume of molecules leaving in a time  $dt$  is  $vdt$
- ▶ Fraction of these molecules that have spent greater than equal to  $t$  is  $[1-F(t)]$  – only blue molecules have spent time more than  $t$  in the reactor
- ▶ Volume of blue molecules leaving the reactor in  $dt$  is  
 $dV = v[1 - F(t)]dt$ , which can be integrated from 0 to  $\infty$  to give  $V$
- ▶ Thus,  $V = \int_0^{\infty} v[1 - F(t)]dt$  and for constant volumetric flow rate

$$V = v \int_0^{\infty} [1 - F(t)]dt$$



# The relationship between the mean residence time and the space time

- ▶ Previously,  $V = v \int_0^\infty [1 - F(t)] dt$  integrating by parts
- ▶ Integrating by parts we have:  $\frac{V}{v} = \int_0^\infty [1 - F(t)] dt = [t(1 - F(t))]_0^\infty + \int_0^\infty t dF$
- ▶ At  $t = 0$ ,  $F(t) = 0$  and  $t \rightarrow \infty$ , then  $[1 - F(t)] = 0$ . Thus, first term is zero
- ▶ And,  $\frac{V}{v} = \int_0^\infty t dF = \tau$  However,  $dF = E(t) dt$
- ▶ Thus,  $\tau = \int_0^\infty t E(t) dt = t_m$  True when  $v = v_0$  and for isobaric and isothermal operations and no change in number of moles
- ▶ Further, this is true for a closed system, i.e., no dispersion across boundaries



# The RTD and its three moments

- ▶ First moment of the distribution is the mean residence time:

$$t_m = \int_0^{\infty} tE(t)dt$$

- ▶ Second moment is the variance,  $\sigma^2$  :

$$\sigma^2 = \int_0^{\infty} (t - t_m)^2 E(t)dt$$

- indicates the “spread” of the distribution

- ▶ Third moment is also taken about the mean and is related to “skewness”

$$s^3 = \frac{1}{\sigma^{3/2}} \int_0^{\infty} (t - t_m)^3 E(t)dt$$

- Magnitude indicates if the distribution is skewed in one direction or the other related to the mean

- ▶ Other moments exist too





# Dimensionless RTD function is used instead of function $E(t)$ , which depends on reactor size and flows

- ▶ Dimensionless time,  $\theta$ , defined as:  $\theta = \frac{t}{\tau}$
- ▶ Dimensionless RTD function,  $E(\theta)$ , is defined as:  $E(\theta) = \tau E(t)$
- ▶ Thus,  $E(\theta)$  vs  $\theta$  is identical for all ideal PFRs and CSTRs
  - $E(t)$  vs  $t$  would vary depending on the space-time, i.e., the value of  $\tau$
- ▶ By normalizing different reactors can be compared directly
  - Numerical values may be otherwise different
- ▶ It can be easily shown that  $\int_0^{\infty} E(\theta) d\theta = 1$
- ▶ Similar to  $E(t)$  (exit-age distribution function) the internal-age distribution,  $I(\alpha)$ , is also sometimes used:  $I(\alpha) = (1 - F(\alpha))/\tau$



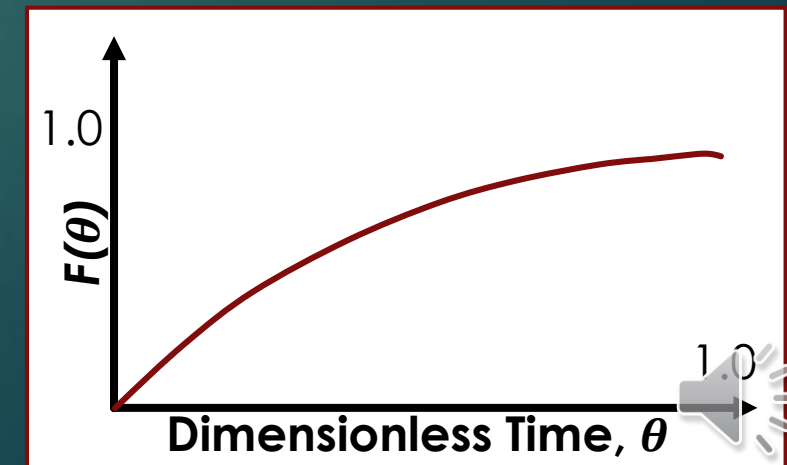
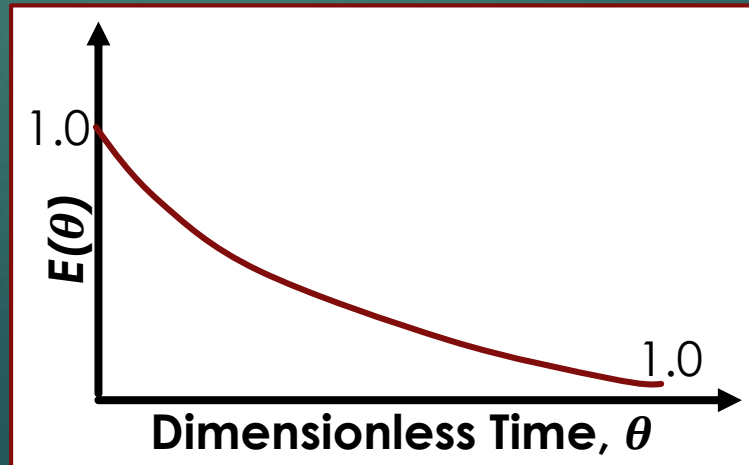
# RTD function can be defined for ideal reactors

- ▶ RTD function for PFR/PBR and Batch are simple
  - All atoms leaving the reactor (PFR/PBR) or in the reactor (Batch) have spent the same amount of time within the reactor
  - The RTD function is a spike of infinite height, zero width and area of 1
  - Spike occurs at  $t = \tau$  or  $\theta = 1 \rightarrow$  represented by the Dirac delta function
  - $E(t) = \delta(t - \tau)$  where  $\delta(x) = 0$  at  $x \neq 0$  and  $\delta(x) = \infty$  at  $x = 0$
  - Further,  $\int_{-\infty}^{\infty} \delta(x) dx = 1$  and  $\int_{-\infty}^{\infty} g(x) \delta(x - \tau) dx = g(\tau)$
- ▶ Mean residence time is:  $t_m = \int_0^{\infty} tE(t)dt = \int_0^{\infty} t\delta(t - \tau)dt = \tau$
- ▶ Variance  $\sigma^2 = \int_0^{\infty} (t - \tau)^2 \delta(t - \tau)dt = 0 \rightarrow$  No variance!
- ▶ Cumulative distribution function  $F(t)$  is:  $F(t) = \int_0^t E(t)dt = \int_0^t \delta(t - \tau)dt$



# RTD function for the CSTR is not the same

- ▶ In a CSTR the conc. inside is the same as the conc at the exit
- ▶ For an inert tracer pulsed at  $t = 0$  into a CSTR then at  $t > 0$  we can do a material balance for the tracer, i.e., in – out = accumulation (no reaction)
- ▶  $0 - v.C = V \frac{dC}{dt}$  Further,  $C = C_0$  at  $t = 0$ . Then  $C(t) = C_0 \exp(-t/\tau)$
- ▶ The  $C(t)$  for the CSTR can be used to determine  $E(t)$
- ▶ Thus,  $E(t) = \frac{C(t)}{\int_0^\infty C(t) dt} = \frac{C_0 \exp(-t/\tau)}{\int_0^\infty C_0 \exp(-t/\tau) dt}$  and  $E(t) = \frac{\exp(-t/\tau)}{\tau}$
- ▶ Further,  $E(\theta) = \exp(-\theta)$  and
- ▶  $F(\theta) = \int_0^\theta E(\theta) d\theta$   
 $F(\theta) = 1 - \exp(-\theta)$





# The moments of the RTD for a CSTR

- ▶ The first moment, the mean residence time, is given by:  $t_m = \int_0^\infty tE(t)dt$
- ▶ Thus,  $t_m = \int_0^\infty \frac{t}{\tau} \exp(-t/\tau) dt = \tau$  and
- ▶ The mean residence time is the space time,  $\tau = V/v$
- ▶ The second moment, which is a measure of spread:  $\sigma^2 = \int_0^\infty (t - t_m)^2 E(t) dt$
- ▶  $\sigma^2 = \int_0^\infty \frac{(t-\tau)^2}{\tau} \exp(-t/\tau) dt = \tau^2$ 
  - Standard deviation is the square root of variance, and
  - For a CSTR, the standard deviation of the RTD function is as large as the mean



# Laminar flow tubular reactor is an non-ideal reactor

- ▶ Before applying the RTD function to estimate conversions we can look into the flow behavior for a tubular reactor where there is laminar flow
- ▶ For laminar flow the velocity profile is parabolic,  $U(r)$  – not ideal
- ▶ Velocity profile: 
$$U(r) = U_{max} \left[ 1 - \left( \frac{r}{R} \right)^2 \right] = 2 \left( \frac{v_0}{\pi R^2} \right) \left[ 1 - \left( \frac{r}{R} \right)^2 \right]$$
  - Where  $\frac{v_0}{\pi R^2}$  is the average fluid velocity through the tube
- ▶ The time required for a fluid element,  $t(r)$ , to flow through the tube of length  $L$

$$t(r) = \frac{L}{U(r)} = \frac{\pi R^2 L}{v_0} \frac{1}{2 \left[ 1 - \left( \frac{r}{R} \right)^2 \right]} = \frac{\tau}{2 \left[ 1 - \left( \frac{r}{R} \right)^2 \right]}$$

- ▶ The volumetric flow rate of fluid element between  $r$  and  $r+dr$ ,  $dv$ , is
- ▶  $dv = U(r)2\pi r dr$  and the fraction of fluid passing is:  $\frac{dv}{v_0} = \frac{U(r)2\pi r dr}{v_0}$



# The $E(t)$ curve for a laminar flow reactor

- ▶ The fraction of fluid between  $r$  and  $r + dr$  is  $dv/v_0$ , which is  $\frac{dv}{v_0} = \frac{U(r)2\pi r dr}{v_0}$
- ▶ This fraction of fluid between  $r$  and  $r + dr$  has a flow between  $v$  and  $v + dv$  spends time between  $t$  and  $t + dt$  in the reactor
- ▶ Thus,  $E(t)dt = \frac{dv}{v_0} = \frac{U(r)2\pi r dr}{v_0}$
- ▶ This fluid fraction between  $r$  and  $r + dr$  is to be related to the fluid spending between  $t$  and  $t + dt$  in the reactor
  - The time required to flow through the reactor of length  $L$ :  $t(r) = \frac{\tau}{2\left[1 - \left(\frac{r}{R}\right)^2\right]}$
  - Thus,  $\frac{dt}{dr} = \frac{d}{dr} \left[ \frac{\tau}{2\left[1 - \left(\frac{r}{R}\right)^2\right]} \right] = \frac{4t^2}{\tau R^2} r$  Thus,  $rdr = \frac{\tau R^2}{4t^2} dt$



## The E(t) curve for the Laminar flow reactor ... contd

► Previously,  $E(t)dt = \frac{dv}{v_0} = \frac{U(r)2\pi r dr}{v_0} = \frac{L}{t} \left( \frac{2\pi}{v_0} \right) r dr = \frac{L}{t} \left( \frac{2\pi}{v_0} \right) \left( \frac{\tau R^2}{4t^2} \right) dt = \frac{\pi R^2 L \tau}{v_0 2t^3} dt$

$$E(t) = \frac{\tau^2}{2t^3}$$

► Minimum time ( $t_{\min}$ ) the fluid spend in the reactor is:  $t_{\min} = \frac{L}{U_{\max}} = \frac{L}{2U_{\text{avg}}} = \frac{\tau}{2}$

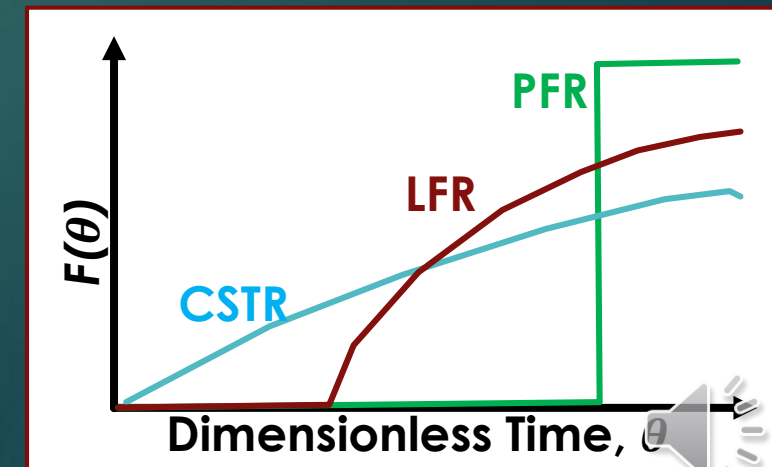
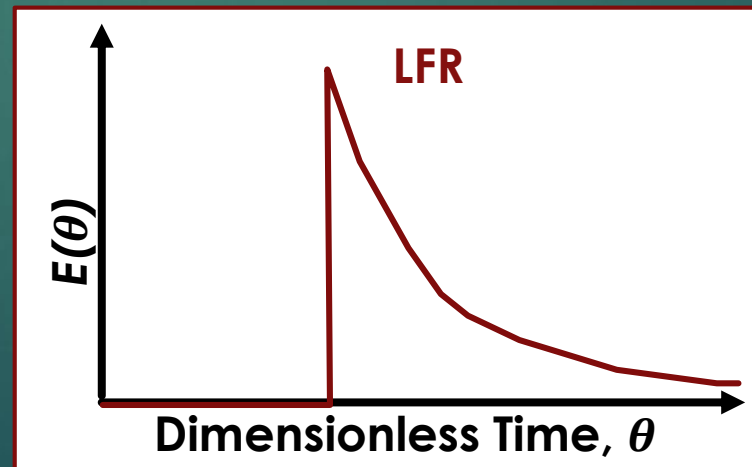
► Thus, the RTD function is given by:  $E(t) = 0 \text{ for } t < \frac{\tau}{2}$

$$E(t) = \frac{\tau^2}{2t^3} \text{ for } t \geq \frac{\tau}{2}$$

► Based on this above  $E(t)$   
it can be shown:

$$t_m = \tau \text{ and } F(t) = 1 - \frac{\tau^2}{4t^2}$$

► Further,  $E(\theta)$  and  $F(\theta)$  can be derived



# Summary

- ▶ Determination of volume of reactor from  $F(t)$  curve:  $V = v \int_0^\infty [1 - F(t)] dt$
- ▶ Equivalence of space-time and mean residence time:  $\tau = t_m$
- ▶ Three moments of the RTD:  $t_m, \sigma^2, s^3$
- ▶ Dimensionless time and RTD function:  $\theta, E(\theta)$  and  $F(\theta)$
- ▶ RTD functions for PFR/PBR and CSTR:  $E(t) = \delta(t - \tau)$       $E(t) = \frac{\exp(-t/\tau)}{\tau}$
- ▶ Laminar flow reactor as an ideal reactor:  $E(t) = 0$  for  $t < \frac{\tau}{2}$   
 $E(t) = \frac{\tau^2}{2t^3}$  for  $t \geq \frac{\tau}{2}$

