

Module 4.6.2

Laplace Domain Analysis

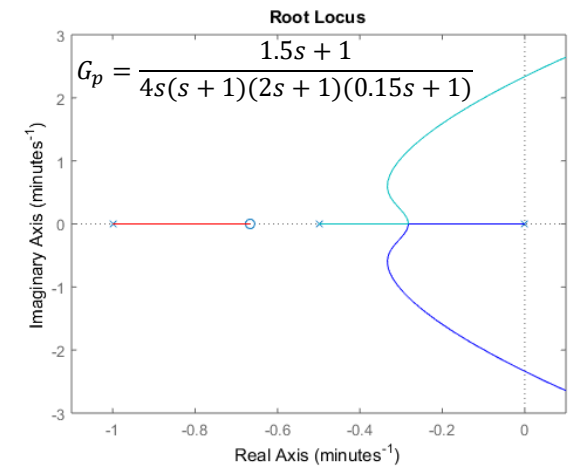
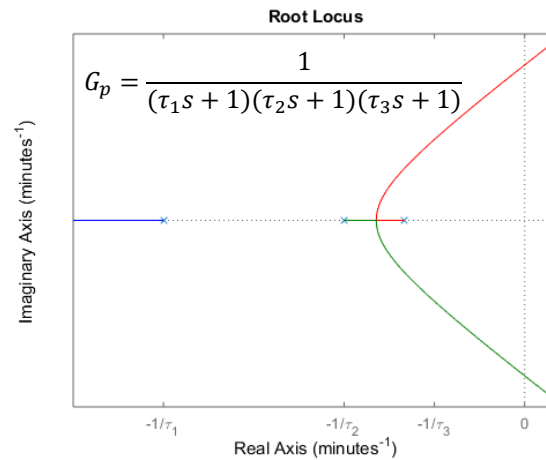
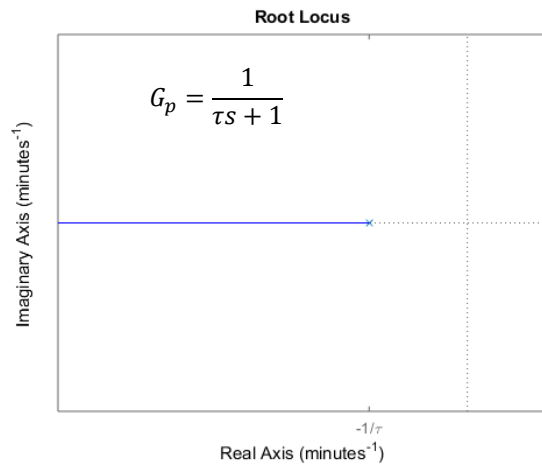
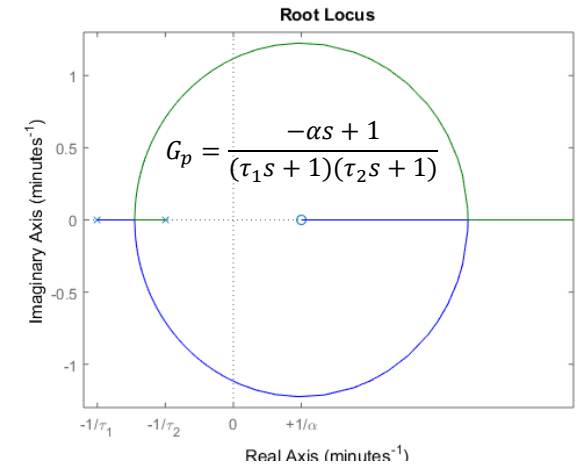
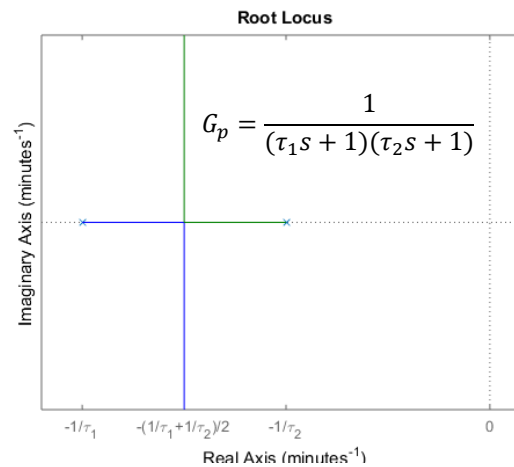
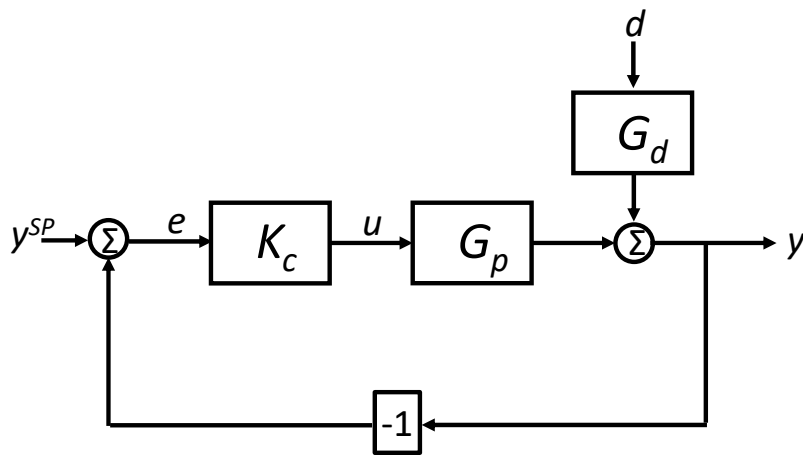
Root Locus

Controller Design

Lectures on

CHEMICAL PROCESS CONTROL
Theory and Practice

Example Root Loci



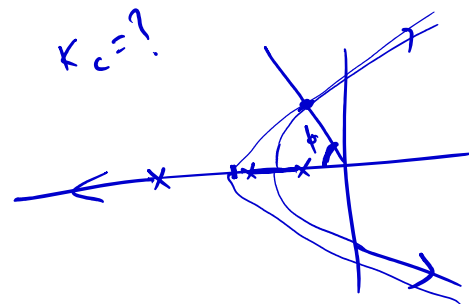
P Controller Design Using Root Locus

$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)}$$

$$G_c = K_c$$

OL poles $s = -1, -\frac{1}{2}, -\frac{1}{4}$

$$\sigma = \frac{1 \frac{3}{4}}{3} = \frac{7}{12}$$



$K_c = ?$

$$1 + K_c G_p = 0 \Rightarrow K_c = -\frac{1}{G_p}$$

$$K_c = \frac{1}{|G_p|_{s=\text{dom. pole}}}$$

$$[-a + j\sqrt{3}a] = -a^3 + 3\sqrt{3}a^2j + 3a^3 - \sqrt{3}a^3j = 8a^3$$

$$[-a + j\sqrt{3}a]^2 = a^2 - 3a^2 - 2\sqrt{3}aj = -2a^2 - 2\sqrt{3}aj$$

$$\text{Im} = 0 \Rightarrow a = \frac{1}{4}$$

$$s = -\frac{1}{4} \pm \frac{\sqrt{3}}{4}j \text{ dominant pole pair}$$

$$\xi = 0.5$$

$$\cos \beta = 0.5$$

$$\Rightarrow \beta = 60^\circ$$

$$s = -a + j\sqrt{3}aj \text{ lies on CLCE}$$

$$(s+1)(2s+1)(4s+1) + K_c = 0$$

$$[2s^2 + 3s + 1][4s + 1] + K_c = 0$$

$$\text{CLCE} \rightarrow 8s^3 + 14s^2 + 7s + 1 + K_c = 0$$

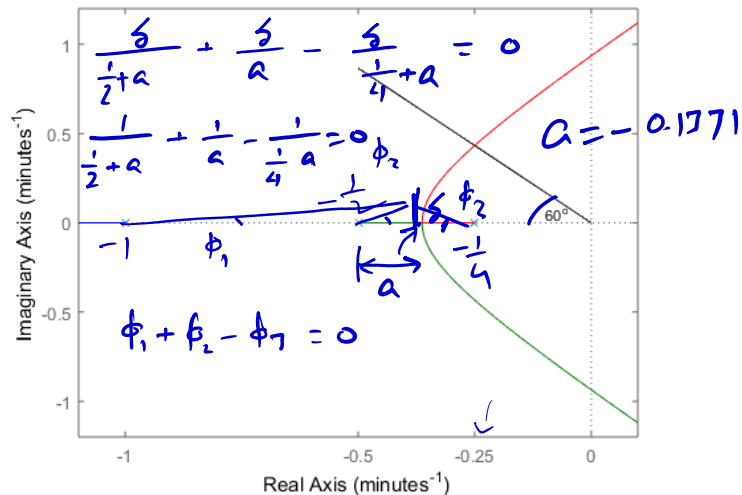
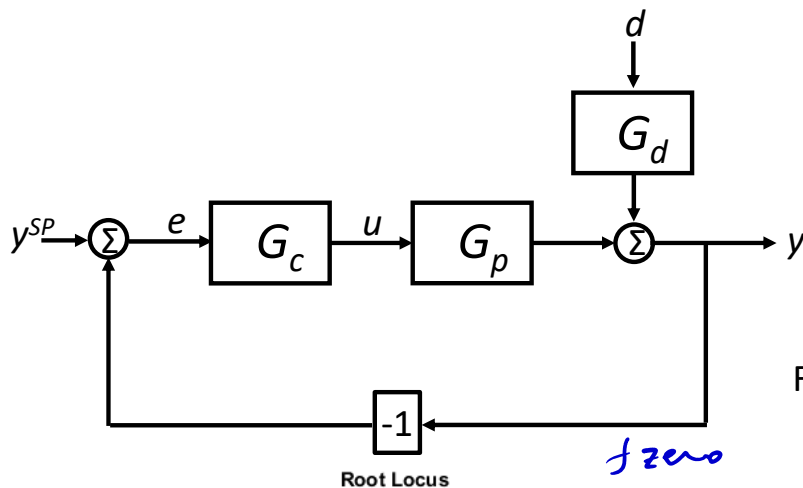
$$8 - 8a^3 + 14[-2a^2 - 2\sqrt{3}a^2j] + 7[-a + j\sqrt{3}aj] + 1 + K_c = 0$$

$$64a^3 - 28a^2 - 28\sqrt{3}a^2j - 7a + 7\sqrt{3}aj + 1 + K_c = 0$$

$$[64a^3 - 28a^2 - 7a + 1 + K_c] + aj[7\sqrt{3} - 28\sqrt{3}a] = 0$$

$$\frac{K_c = 1.5}{\xi = 0.5} \quad \left[K_c = \frac{1}{|G_p|_{s=-\frac{1}{4} + \frac{\sqrt{3}}{4}j}} \right]$$

P Controller Design Using Root Locus



$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)} \quad G_c = K_c$$

Obtain K_c such that $\xi = 0.5$ for CLCE dominant roots

Breakpts $\sigma = -0.5 + 0.1371j$

$s = -0.3619$ $K_c = \frac{1}{|G|_{s=-0.3619}} =$

For $\xi = 0.5$, $s = -a + \sqrt{3}aj$ satisfies CLCE $\equiv 8s^3 + 14s^2 + 7s + 1 + K_c = 0$

Substituting and collecting real and imaginary terms

$$[64a^3 - 28a^2 - 7a + 1 + K_c] + aj[-28\sqrt{3}a + 7\sqrt{3}] = 0$$

$\therefore a = \frac{1}{4}$ and $s = -\frac{1}{4} \pm \frac{\sqrt{3}}{4}j$ are CLCE dominant poles

$$K_c = \left| \frac{1}{G} \right|_{s=-\frac{1}{4} + \frac{\sqrt{3}}{4}j} = 1.5$$

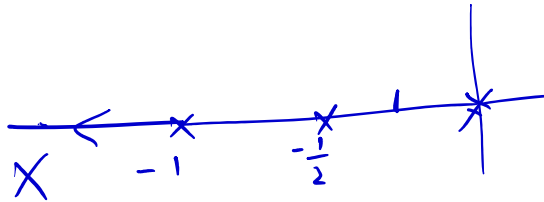
PI Controller Design Using Root Locus

$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)}$$

$$\tau_T = 1 \quad K_c \quad \xi = 0.5$$

$$\sigma = -\alpha + \sqrt{3}\alpha j$$

$$\phi = 60^\circ$$



$G_p G_c$

$$\tau_T = 4 \text{ min}$$

Dominant CLCE
pole pair

$$s = -\frac{1}{6} \pm \frac{\sqrt{3}}{6}j$$

$$K_c^{PI} = 1.04$$

$$K_c^P = 1.5$$

$$G_c = K_c \frac{\tau_T s + 1}{\tau_I s}$$

$$G_{OL} = \frac{K_c}{4s(s+1)(2s+1)}$$

$$4s(s+1)(2s+1) + K_c = 0$$

$$4s(2s^2 + 3s + 1) + K_c = 0$$

$$\text{CLCE } 8s^3 + 12s^2 + 4s + K_c = 0$$

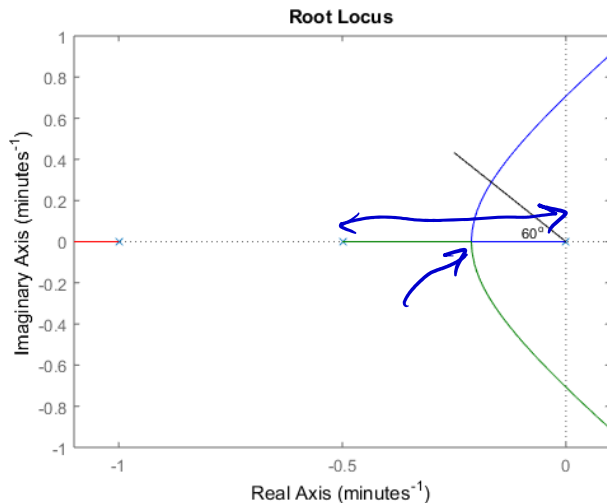
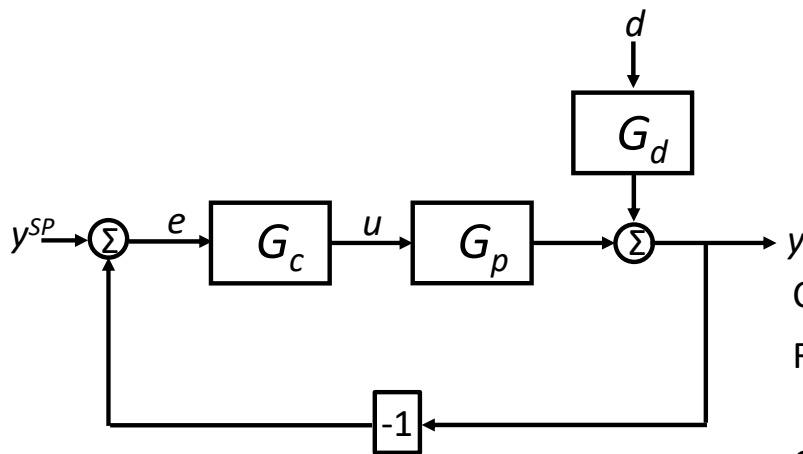
$$64\alpha^3 + 12[-2 - 2\sqrt{3}j]\alpha^2 + 4[-\alpha + \sqrt{3}\alpha j] + K_c = 0$$

$$[64\alpha^3 - 24\alpha^2 - 4\alpha + K_c] + j[4\sqrt{3} - 24\sqrt{3}\alpha] = 0$$

$$\alpha = \frac{1}{6}$$

$$K_c = \frac{1}{|G_{OL}|_{s = -\frac{1}{6} + \frac{\sqrt{3}}{6}j}} = 1.037 \approx \underline{\underline{1.04}}$$

PI Controller Design Using Root Locus



$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)} \quad G_c = K_c \frac{\tau_I s + 1}{\tau_I s}$$

Obtain K_c such that $\xi = 0.5$ for CLCE dominant roots

Choose reasonable value for τ_I

RULE OF THUMB: Set τ_I to largest open loop time constant. Controller zero then cancels open loop pole closest to RHP.

CLCE then becomes $8s^3 + 12s^2 + 4s + K_c = 0$

For $\xi = 0.5$, $s = -a + \sqrt{3}aj$ satisfies CLCE

$$3s^2 + 3s + \frac{1}{2} = 0 \quad s = -\frac{3}{6} \pm \frac{\sqrt{9-6}}{6}$$

$$(s+a)^2(s+b) = 0$$

$$s = -\frac{1}{2} \pm \frac{\sqrt{3}}{2}j$$

Substituting and collecting real and imaginary terms

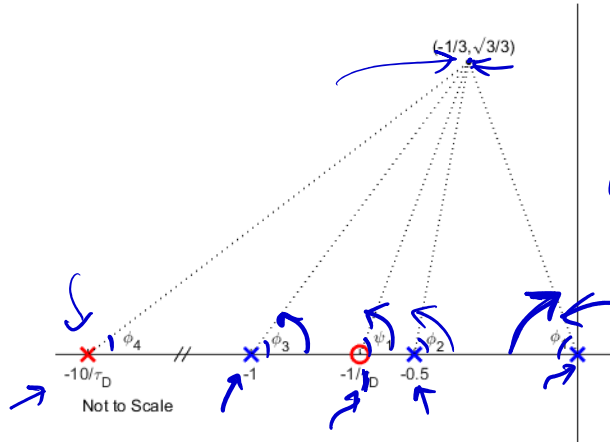
$$[64a^3 - 24a^2 - 4a + K_c] + aj[-24\sqrt{3}a + 4\sqrt{3}] = 0$$

$\therefore a = \frac{1}{6}$ and $s = -\frac{1}{6} \pm \frac{\sqrt{3}}{6}j$ are CLCE dominant poles

$$K_c = \left| \frac{1}{G} \right|_{s=-\frac{1}{6} + \frac{\sqrt{3}}{6}j} = 1.037$$

PID Controller Design Using Root Locus

Forcing Angle Condition at Desired Closed Loop Pole



$$-\phi_1 - \phi_2 - \phi_3 - \phi_4 + \psi_1 = -180^\circ$$

$$|\phi_1| = \tan^{-1} \frac{\sqrt{3}/3}{1/3} = 60^\circ \sim -120^\circ$$

$$\phi_2 = \tan^{-1} \frac{\sqrt{3}/3}{1/6} = 73.9^\circ$$

$$\phi_3 = \tan^{-1} \sqrt{3}/3 / 2/3 = 40.9^\circ$$

$$G_c = \frac{K_c (\tau_D s + 1)}{4s(n+1)(2s+1)(0.1\tau_D s + 1)}$$

$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)}$$

$$G_c = K_c \frac{(\tau_D s + 1)}{4s(0.1\tau_D s + 1)}$$

$$\tau_D = 1 \quad K_c \quad \xi = 0.5$$

$S = 2 \times \text{PI dominant pole must lie on root locus}$

$S = -\frac{1}{3} + \frac{\sqrt{3}}{2}j \text{ must lie on root locus}$

Condition must be satisfied

$$+ \tan^{-1} \frac{\sqrt{3}/3}{\frac{1}{\tau_D} - \frac{1}{2}} - \tan^{-1} \frac{\sqrt{3}/3}{\frac{10}{\tau_D} - \frac{1}{2}} = -180^\circ$$

$$-234.8^\circ = -180^\circ$$

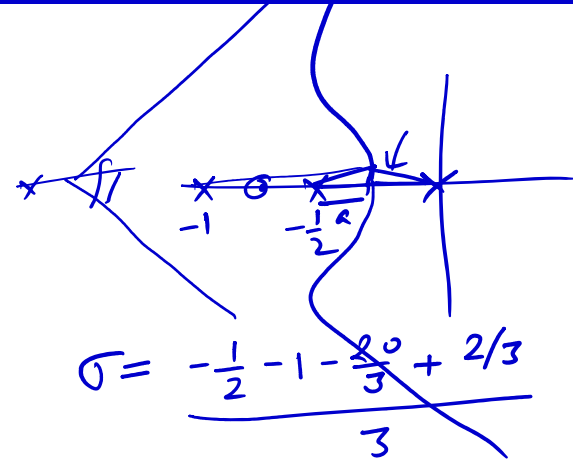
$$K_c = \frac{1}{|G_{ol}|_{s=-\frac{1}{3} + \frac{\sqrt{3}}{2}j}}$$

$$K_c \approx 2.70$$

$$\tau_D = 1.5 \text{ min}$$

$$\tan^{-1} \frac{\sqrt{3}/3}{\frac{1}{\tau_D} - \frac{1}{2}} - \tan^{-1} \frac{\sqrt{3}/3}{\frac{10}{\tau_D} - \frac{1}{2}} = 54.8^\circ$$

PID Controller Design Using Root Locus



$$\sigma = -2.5$$

$$\frac{s}{a} - \frac{s}{\frac{1}{2} - a} - \frac{s}{\frac{1}{6} + a} + \frac{s}{\frac{1}{2} + a} + \frac{s}{\frac{20}{3} - \frac{1}{2} + a} = 0$$

$$\frac{1}{a} - \frac{1}{\frac{1}{2} - a} - \frac{1}{\frac{1}{6} + a} + \frac{1}{\frac{1}{2} + a} + \frac{1}{\frac{37}{6} + a} = 0$$

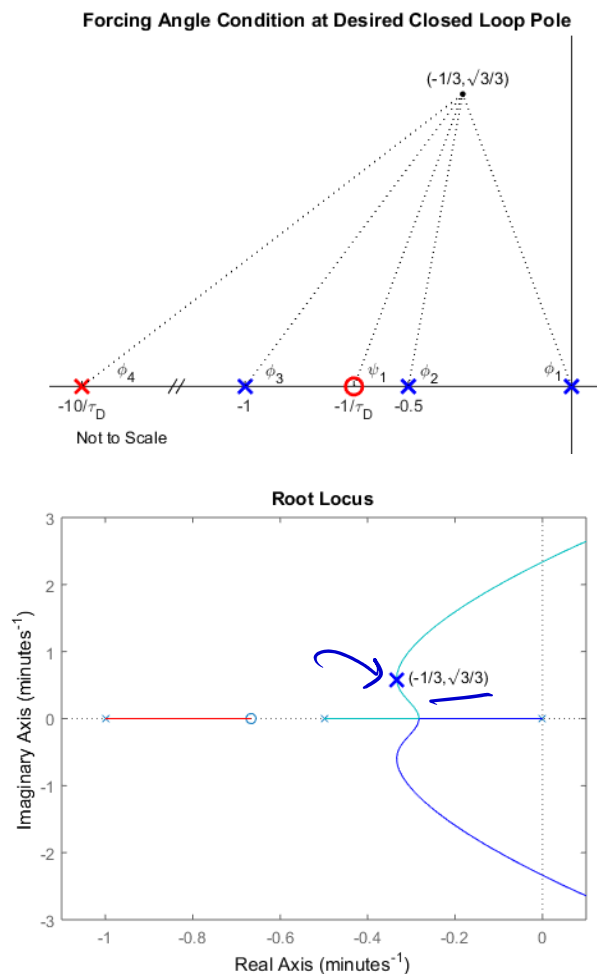
$$a = 0.2177$$

$$\rho = -0.5 + 0.2177j$$

$$s = -0.2823 \text{ break pt}$$

$$G = \frac{1}{(s+1)(2s+1)4s(s+0.15)} \bigg|_{K_c^{\text{breakpt}}} = \frac{1}{|G|_{s=-0.2823}} \Rightarrow K_c^{\text{bp}} = 0.5861$$

PID Controller Design Using Root Locus



$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)} \quad G_c = K_c \frac{(\tau_I s + 1)}{\tau_I s} \frac{(\tau_D s + 1)}{(0.1\tau_D s + 1)}$$

Want CLCE $\xi = 0.5$ and response speed twice that of PI controller

Set $\tau_I = 4$ mins as before. For twice the response speed of a PI controller, the dominant pole pair should be twice in magnitude of PI dominant pair.

Dominant pole pair is $s = 2 \left[-\frac{1}{6} \pm \frac{\sqrt{3}}{6} j \right] = -\frac{1}{3} \pm \frac{\sqrt{3}}{3} j$

$s = -\frac{1}{3} \pm \frac{\sqrt{3}}{3} j$ must satisfy angle condition to be on root locus

Choose τ_D to ensure angle condition is indeed satisfied.

From figure,

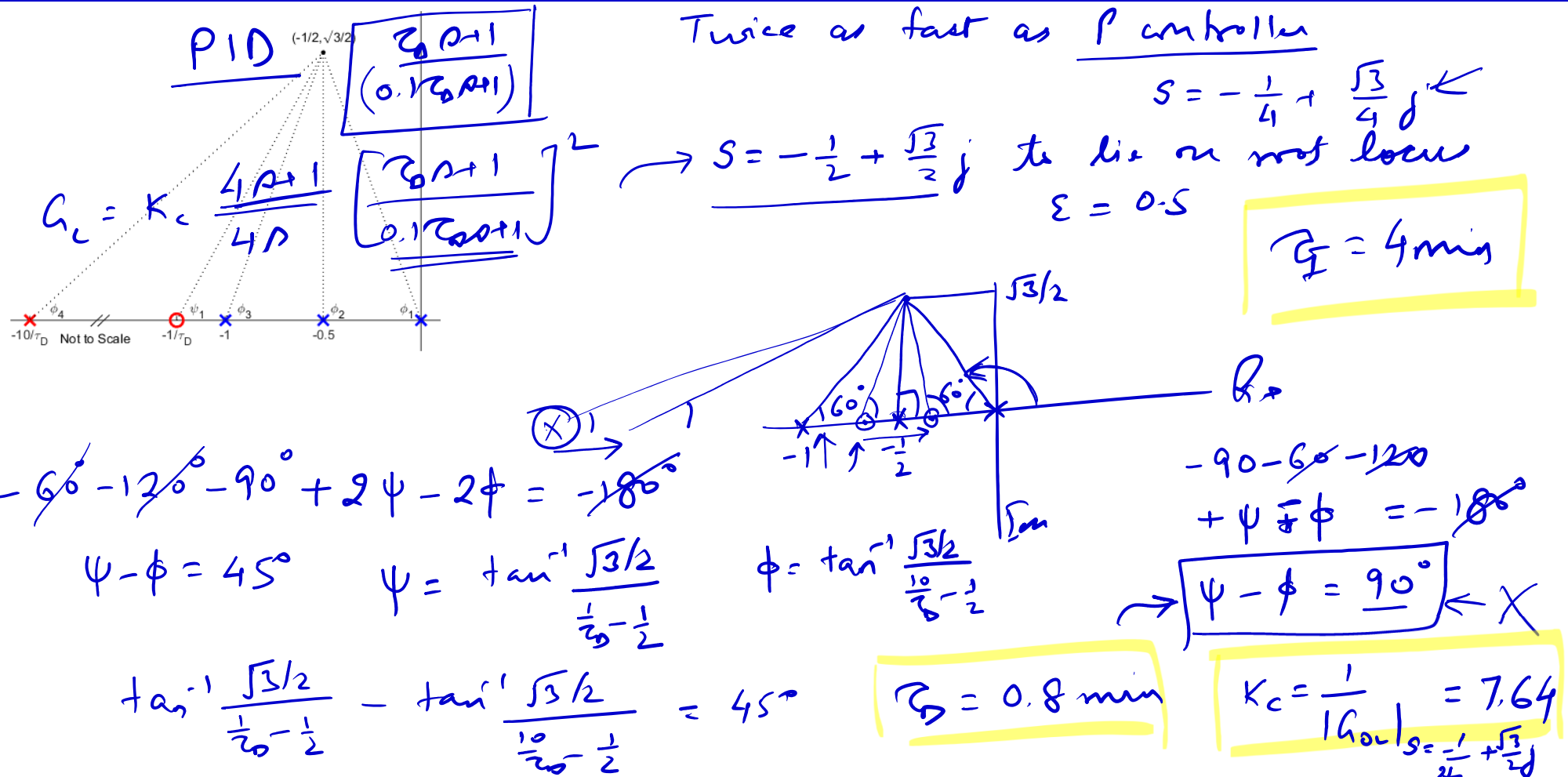
$$\phi_1 = \tan^{-1} \frac{\sqrt{3}/3}{1/3} = 60^\circ \quad \phi_2 = \tan^{-1} \frac{\sqrt{3}/3}{1/6} = 73.90^\circ \quad \phi_3 = \tan^{-1} \frac{\sqrt{3}/3}{2/3} = 40.89^\circ$$

$$\psi_1 + \phi_1 - \phi_2 - \phi_3 - \phi_4 = 180^\circ$$

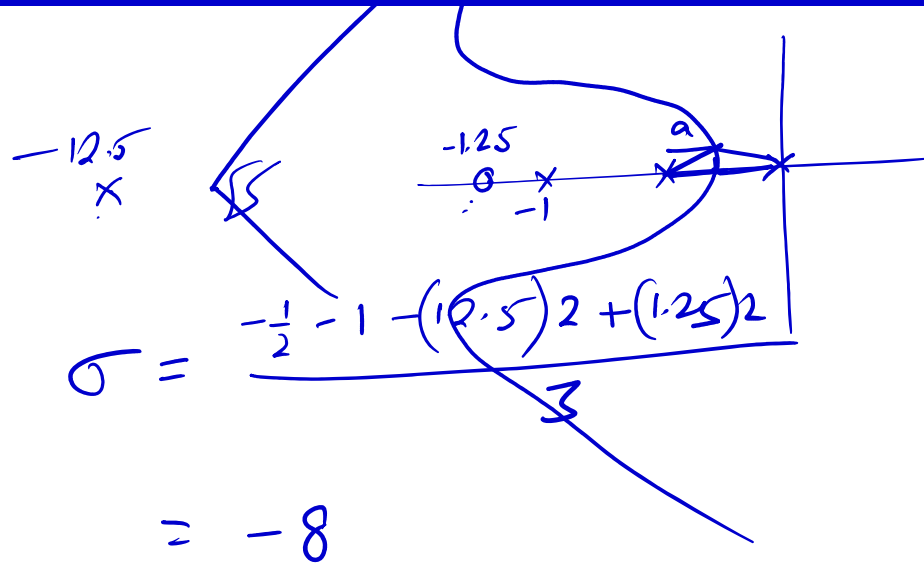
$$\Rightarrow \tan^{-1} \frac{\sqrt{3}/3}{1/\tau_D - 1/3} - \tan^{-1} \frac{\sqrt{3}/3}{10/\tau_D - 1/3} = 54.79^\circ \Rightarrow \tau_D = 1.5 \text{ min}$$

magnitude condition $\rightarrow K_c = \left| \frac{1}{G} \right|_{s=-\frac{1}{3} + \frac{\sqrt{3}}{3} j} = 2.70$

PIDD Controller Design Using Root Locus



PID Controller Design Using Root Locus



$$\frac{s}{a} - \frac{s}{\frac{1}{2} - a} + \frac{s}{\frac{1}{2} + a} - \frac{2s}{0.75 + a} + \frac{2s}{12 + a} = 0$$

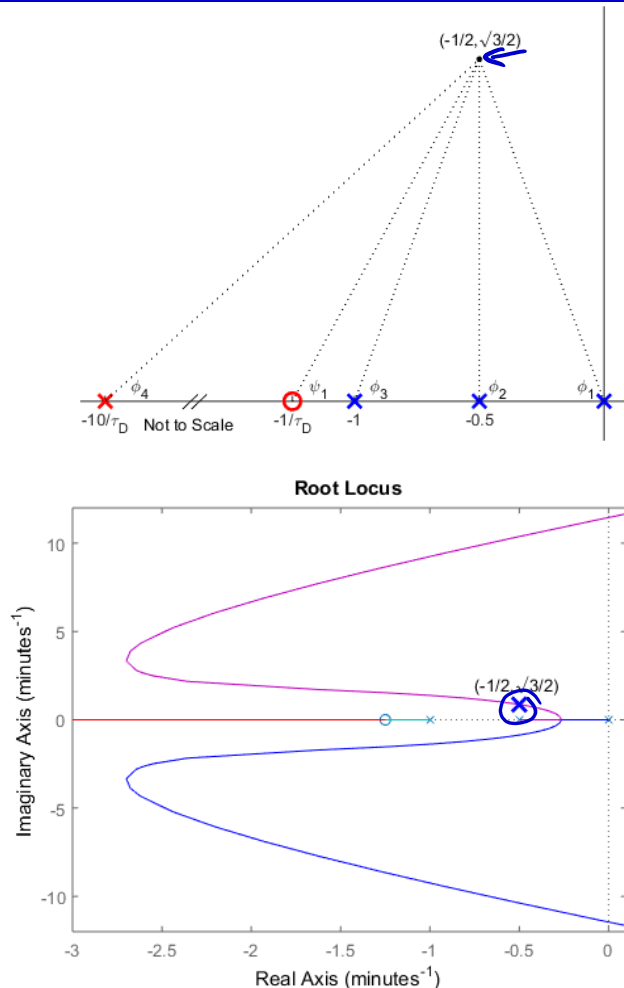
Solve for $a = 0.2342$

$$D = -\frac{1}{2} + 0.2342$$

$$s = -0.2658 \text{ break pt}$$

$$K_c^{bp} = \frac{1}{|G_{ol}|_{s=-0.2658}} = 0.5650$$

PIDD Controller Design Using Root Locus



$$G_p = \frac{1}{(s+1)(2s+1)(4s+1)} \quad \checkmark$$

Want CLCE $\xi = 0.5$ and response speed twice that of P controller

Set $\tau_I = 4$ mins. Dominant pole pair should be twice P dominant pair.

$$\text{Dominant pole pair is } s = 2 \left[-\frac{1}{4} \pm \frac{\sqrt{3}}{4} j \right] = -\frac{1}{2} \pm \frac{\sqrt{3}}{2} j$$

$s = -\frac{1}{2} \pm \frac{\sqrt{3}}{2} j$ must satisfy angle condition to be on root locus

Single τ_D lead-lag $\frac{(\tau_D s + 1)}{(0.1\tau_D s + 1)}$ cannot cause angle condition to be satisfied.

So put 2 identical lead-lags $G_c = K_c \frac{(\tau_I s + 1)}{\tau_I s} \left[\frac{(\tau_D s + 1)}{(0.1\tau_D s + 1)} \right]^2$

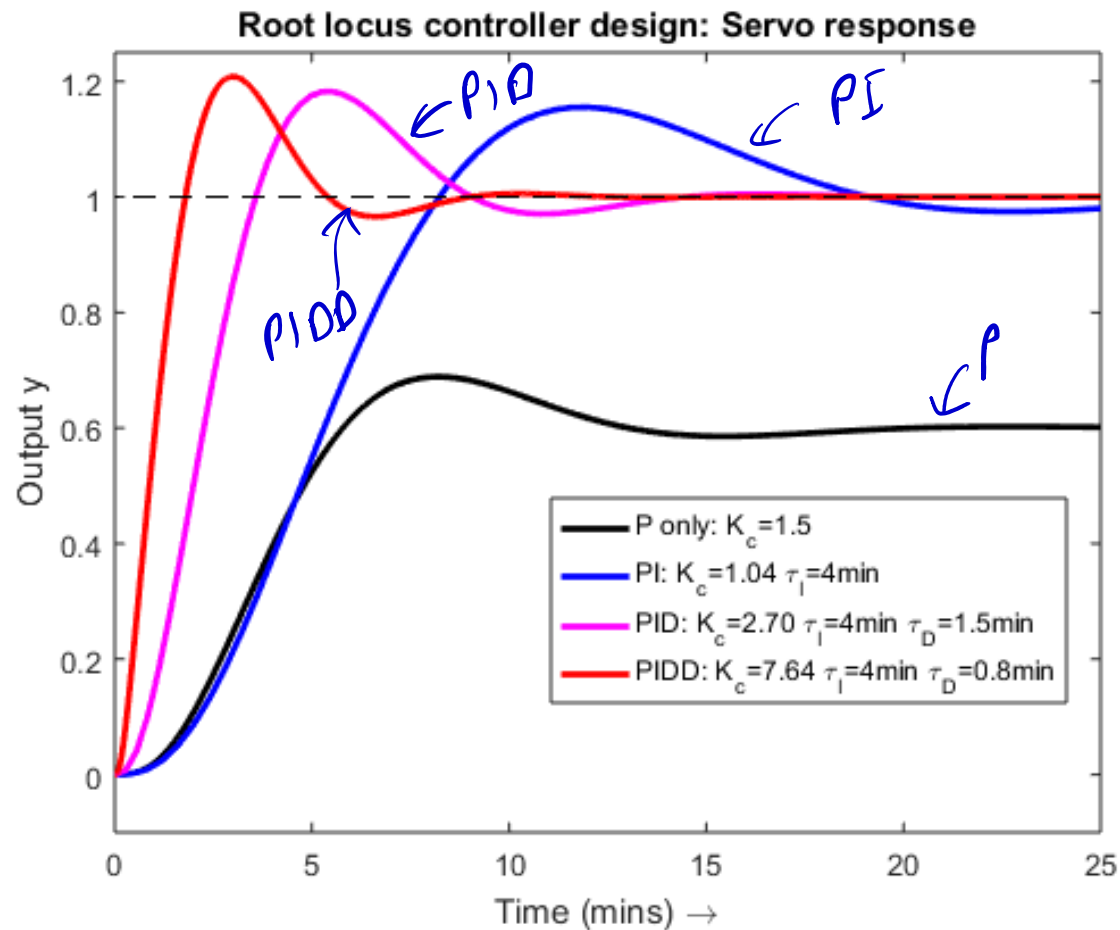
From figure, $\phi_1 = \tan^{-1} \frac{\sqrt{3}/2}{1/2} = 60^\circ$ $\phi_2 = 90^\circ$ $\phi_2 = \tan^{-1} \frac{\sqrt{3}/2}{1/2} = 60^\circ$

$$2\psi_1 + \phi_1 - \phi_2 - \phi_3 - 2\phi_4 = 180^\circ$$

$$\Rightarrow \tan^{-1} \frac{\sqrt{3}/2}{1/\tau_D - 1/2} - \tan^{-1} \frac{\sqrt{3}/2}{10/\tau_D - 1/2} = 45^\circ \Rightarrow \tau_D = 0.80 \text{ min}$$

$$K_c = \left| \frac{1}{G_p G_c} \right|_{s = -\frac{1}{2} + \frac{\sqrt{3}}{2} j} = 7.64$$

Closed Loop Servo Response



Root Locus Design Procedure Summary

- Obtain desired closed loop pole location (region)
 - Degree of oscillatoriness (damping coefficient ξ)
 - Speed of response
- For zero offset, set τ_i to cancel slowest (closest to RHP) open loop pole
- Choose τ_D lead-lag to force locus to pass through desired closed loop pole
 - Angle condition gives necessary τ_D
 - Magnitude condition gives necessary K_C
 - Use only if simple PI control does not give fast enough closed loop response
 - Derivative lead-lag is used to pull root locus sufficiently to the left for faster response
 - May require double derivative for very fast closed loop response
 - Amplifies noise
- Root locus construction rules allow easy visualization of reshaped root locus