

Control of the DCDC converter connecting Super-caps to a DC bus

Tuning of two PI control loops to regulate the inductor current and the DC bus voltage

```
In [1]: import numpy as np
        pi = np.pi
```

Parameters of the system

```
In [2]: # Super-caps:
        C_sto = 20. #[F]
        # Inductance in series with the Super-caps
        L = 3e-3 # [H]
        # DC bus capacitor:
        C_dc = 50e-3 #[F]
```

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In [3]: # Set point for the DC bus voltage
        V_dc_set = 1300 # [V]
```

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In [4]: # Switching frequency
        Fs = 2000. # [Hz]
        # SEAREV production frequency:
        F_prod = 1./4 # [Hz]
```

Frequency spans for Bode diagram plotting:

```
In [5]: # frequency vectors:
        f = np.logspace(-1,4,500) # .1 Hz to 10 kHz
        w = f*2*pi
        # Laplace variable "s"
        s = 1j*w
```

1) Current loop

Objective: control the current i_L in the inductor to a reference value i_L^* .

The control is achieved by acting on the duty cycle d

PI controller :

$$d = (K_i + \frac{1}{T_i s}) \varepsilon$$

with $\varepsilon = i_L^* - i_L$ being the control error (in A).

Parameters: K_i (in A⁻¹) and T_i (in A.s)

Closed loop transfer i_L/i_L^* :

$$H_i = \frac{1 + K_i T_i s}{1 + K_i T_i s + L T_i / V_{dc} s^2}$$

```
In [6]: # 1) Choose the 2nd order parameters of the closed loop:
f0_i = 200. # natural frequency [Hz]
m_i = .7 # damping factor

# 2) Deduce the PI parameters (K,T)
V_dc = V_dc_set
T_i = V_dc/(L*(2*pi*f0_i)**2)
K_i = 2*m_i/(T_i*2*pi*f0_i)

## A set of good enough values:
#K_i=0.01
#T_i=0.1
#f0_i = sqrt(V_dc/(L*T_i))/(2*pi)
#m_i = K/2*sqrt(V_dc*T_i/L)

## 3) Display:
print('natural frequency f0 = %.1f Hz' % f0_i)
print('  1/f0 = %.2f ms' % (1e3/f0_i))
print('damping factor m = %.2f' % m_i)
print('PI params:\n  K={:.5f} \n  T={:.3f}'.format(K_i, T_i))

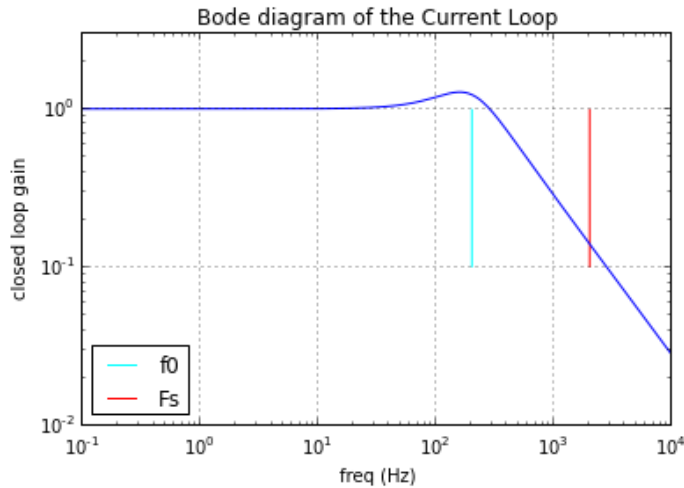
natural frequency f0 = 200.0 Hz
  1/f0 = 5.00 ms
damping factor m = 0.70
PI params:
  K=0.00406
  T=0.274
```

Bode diagram

```

In [7]: # Numerical eval of the transfer function:
Hi = (1 + K_i*T_i*s)/( 1 + K_i*T_i*s + L*T_i/V_dc*s**2 )
# Plot
loglog(f, abs(Hi))
vlines(f0_i, 0.1,1, color='cyan', label='f0')
vlines(Fs, 0.1,1, color='red', label='Fs')
ylim(ymax=3)
xlabel('freq (Hz)')
ylabel('closed loop gain')
title('Bode diagram of the Current Loop')
legend(loc='lower left')
grid(True, which='major'); grid(False, which='minor');

```



Rejection of the perturbation (V_{sto})

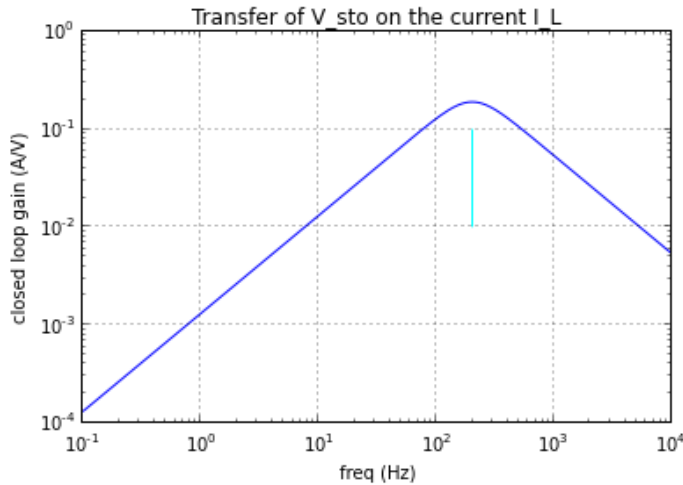
The voltage V_{sto} of the Super-caps acts as a perturbation in the current control loop.

Closed loop transfer is a 2nd order band pass:

$$\frac{1}{K_i V_{dc}} \frac{K_i T_i s}{1 + K_i T_i s + L T_i / V_{dc} s^2}$$

```
In [9]: Hi_perturb = (K_i*T_i*s)/( 1 + K_i*T_i*s + L*T_i/V_dc*s**2 ) / (K_i*V_dc)

# Plot
loglog(f, abs(Hi_perturb))
vlines(f0_i, 0.01,.1, color='cyan', label='f0')
xlabel('freq (Hz)')
ylabel('closed loop gain (A/V)')
title('Transfer of V_sto on the current I_L')
grid(True, which='major'); grid(False, which='minor');
```



Conclusion: since the variations of the super-caps voltage are below 1 Hz, it should have no influence on the current loop.

Voltage loop

Objective: control the voltage v_{dc} of the DC bus capacitor to a reference value v_{dc}^* .

The control is achieved by acting on the current reference i_L^*

PI controller :

$$i_L^* = -(K_v + \frac{1}{T_v s})\varepsilon$$

with $\varepsilon = v_{dc}^* - v_{dc}$ being the control error (in V). (the "-" sign compensates for the "-" in the transfer of the system)

Parameters: K_v (in A/V) and T_v (in V.s/A)

Closed loop transfer v_{dc}/v_{dc}^* :

$$H_v = \frac{1 + K_v T_v s}{1 + K_v T_v s + C_{dc} T_v / ds^2}$$

```

In [10]: # 1) Choose the 2nd order parameters of the closed loop:
f0_v = 10. # natural frequency [Hz]
m_v = 1 # damping factor

# 2) Deduce the PI parameters (K,T)
V_sto = 800. # half charge
V_dc = V_dc_set
alpha = V_sto/V_dc

T_v = alpha/(C_dc*(2*pi*f0_v)**2)
K_v = 2*m_v/(T_v*2*pi*f0_v)

## A set of good enough values:
#K_v = 10
#T_v = 0.001

## 3) Display:
print('natural frequency f0 = %.1f Hz' % f0_v)
print('  1/f0 = %.2f ms' % (1e3/f0_v))
print('damping factor m = %.2f' % m_v)
print('PI params:\n K={:.5f} \n T={:.3f}'.format(K_v, T_v))

natural frequency f0 = 10.0 Hz
  1/f0 = 100.00 ms
damping factor m = 1.00
PI params:
  K=10.21018
  T=0.003

```

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In [11]: # Compute the closed loop tranfer numerically:

# TF of the Controler
Cv = - K_v - 1/(T_v*s)

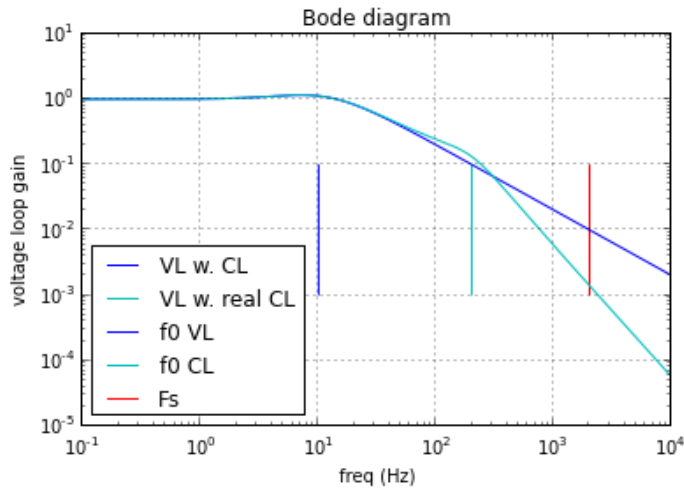
# Open-loop tranfer, with and without the current loop influence:
Hv_ol1 = Cv*1*-alpha/(C_dc*s)
Hv_oli = Cv*Hi*-alpha/(C_dc*s)

Hv1 = Hv_ol1/(1 + Hv_ol1)
Hvi = Hv_oli/(1 + Hv_oli)

```

```
In [12]: # Plot
loglog(f, abs(Hv1), color='blue', label='VL w. CL')
loglog(f, abs(Hvi), color='c', label='VL w. real CL')

vlines(f0_v, .001,.1, color='blue', label='f0 VL')
vlines(f0_i, .001,.1, color='c', label='f0 CL')
vlines(Fs, .001,.1, color='red', label='Fs')
#ylim(ymax=3)
legend(loc='lower left')
xlabel('freq (Hz)')
ylabel('voltage loop gain')
title('Bode diagram');
grid(True, which='major'); grid(False, which='minor');
```



TODO:

- plot the gain for several alpha (ie. V_{sto}) values -> smaller duty cycle implies higher resonance...
- see the effect of the inner current loop

Rejection of the perturbation ($I_{prod} - I_{grid}$)

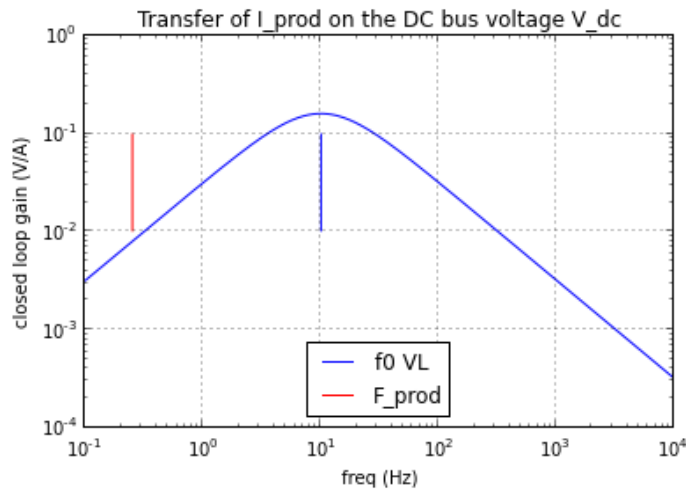
The currents I_{prod} and I_{grid} injected on the DC bus acts as a perturbation in the voltage control loop.

Closed loop transfer is a 2nd order band pass:

$$\frac{1}{K_v d} \frac{K_v T_v s}{1 + K_v T_v s + C_{dc} T_v / ds^2}$$

```
In [14]: Hv_perturb = (K_v*T_v*s)/( 1 + K_v*T_v*s + C_dc*T_v/alpha*s**2 ) / (K_v*alpha)

# Plot
loglog(f, abs(Hv_perturb), color='b')
vlines(f0_v, 0.01,.1, color='b', label='f0 VL')
vlines(F_prod, 0.01,.1, color='r', label='F_prod')
legend(loc='lower center')
xlabel('freq (Hz)')
ylabel('closed loop gain (V/A)')
title('Transfer of I_prod on the DC bus voltage V_dc')
grid(True, which='major'); grid(False, which='minor');
```



Analysis:

The pulsation of the current from the SEAREV production is about 1000 A peak-to-peak.

Located at about 0.3 Hz, it should therefore generate v_{dc} variations of less than $1000 \times 9.10^{-3} \approx 10$ V

Theses variations are small enough compared to the DC bus voltage reference (1300 V) : it is *acceptable*.

In []: