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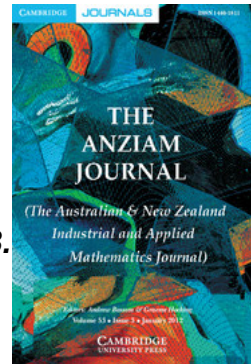
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OPTIMAL DRIVING STRATEGIES FOR A TRAIN JOURNEY WITH SPEED LIMITS

PETER PUDNEY and PHIL HOWLETT¹

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Abstract

How should a vehicle be driven to minimise fuel consumption? In this paper we consider the case where a train is to be driven along a straight, level track, but where speed limits may apply over parts of the track. The journey is to be completed within a specified time using as little fuel as possible.

For a journey without speed limits, the optimal driving strategy typically requires full power, speed holding, coasting and full braking, in that order. The holding speed and braking speed can be determined from the vehicle characteristics and the time available to complete the journey. If the vehicle has discrete control settings, the holding phase should be approximated by alternate coast and power phases between two critical speeds.

For a journey with speed limits, a similar strategy applies. For each given journey time there is a unique holding speed. On intervals of track where the speed limit is below the desired holding speed, the speed must be held at the limit. If braking is necessary on an interval, the speed at which braking commences is determined in part by the holding speed for the interval. For vehicles with discrete control, speed-holding is approximated by alternate coast and power phases between two critical speeds, or between a lower critical speed and the speed limit.

1. Introduction

Systems for calculating efficient driving advice during a journey are particularly applicable to timetabled suburban and long-haul railway journeys. The Metromiser [2] is an example of a system that displays efficient driving advice to the driver of a suburban train. It is easy to use, and has achieved fuel savings in excess of 20% and significant improvements in timekeeping. It does not, however, generate optimal advice for long journey segments, journey segments with many changes of gradient, or journey segments with multiple restrictive speed limits.

In this paper we will consider the case where a train is to be driven along a straight,

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level track of fixed length, but where speed limits apply over various track intervals. The journey is to be completed within a specified time, using as little fuel as possible.

The train control problem has been considered by various authors. Milroy [9] used an heuristic application of the Pontryagin Principle to obtain conditions for a journey that minimised the mechanical energy supplied during tractive acceleration. His results were confirmed independently by Kraft and Schnieder [8], Asnis *et al.* [1] and by Howlett [4].

We will approach the problem by considering a vehicle with discrete control settings, and by considering journeys with a prescribed control sequence. The problem then becomes one of determining where the control should be changed. Once we determine necessary conditions on the optimal switching locations for a given sequence, we can then consider the problem of determining which sequence is optimal.

A similar approach has been used by Cheng and Howlett [7, 6] for the case where the vehicle is to be driven over level track without speed limits. Recently this work has been extended to the case of an undulating track [5, 3]. The extended procedure may also be applicable to curved tracks. By combining this work, we hope to develop a method for calculating optimal driving strategies for curved, undulating tracks with speed limits. Ultimately we wish to develop a vehicle-borne system, suited to a variety of vehicles, that can monitor the progress of a journey and recalculate the appropriate optimal driving strategy from any given point on the journey. Such a device would be able to compensate for the inevitable departures from any pre-planned optimal strategy.

2. Vehicle model

Assume that the vehicle has a number of discrete control settings denoted by

$$u \in U = \{-q, \dots, -2, -1, 0, 1, 2, \dots, Q\},$$

where q is the number of brake control settings,
 Q is the number of traction control settings,
 $u = 0$ represents coasting.

On straight, level track the acceleration of the vehicle is given by

$$v \frac{dv}{dx} = \phi_u(v) - r(v), \quad (1)$$

where v is the speed of the vehicle,
 x is the distance travelled,
 $\phi_u(v)$ is the tractive or braking acceleration developed by the vehicle for control setting u at speed v ,
 $r(v)$ is the deceleration of the vehicle due to resistance at speed v .

We assume a constant cost rate c_u for each control setting, and that $c_u = 0$ for $u \leq 0$. We also assume that $\phi_u(v)$ decreases as v increases, and that $r(v)$ increases as v increases.

3. Journey model

Consider a journey with n distinct phases. The control setting is specified for each phase. The distances at which the control must be changed are to be determined. These distances are denoted by $0 = x_0 < x_1 < \dots < x_n = X$. The journey starts at distance $x = 0$ and finishes at distance $x = X$.

The track speed limit changes at distances $0 = X_0 < X_1 < \dots < X_p = X$. The speed limit for the interval (X_j, X_{j+1}) is M_{j+1} .

It is necessary to determine the locations of the points $\{x_k\}$ for $k = 1, 2, \dots, n-1$ in relation to the fixed points $\{X_j\}$ for $j = 0, 1, \dots, p$. We use the notation $\{r(j)\}$ to denote the sequence with $r(0) = 0$ and $r(p) = n$ and with

$$x_{r(j)} \leq X_j < x_{r(j)+1} \quad j = 1, 2, \dots, p-1.$$

Let $\xi_{k+1} = x_{k+1} - x_k$ denote the length of the interval $[x_k, x_{k+1}]$. The control setting in this interval is $u(k+1)$. If the time taken to traverse the interval $[x_k, x_{k+1}]$ is τ_{k+1} then the cost of the journey is

$$J = \sum_{k=0}^{n-1} c_{u(k+1)} \tau_{k+1}. \quad (2)$$

If the time allowed for the journey is T , we require

$$\sum_{k=0}^{n-1} \tau_{k+1} \leq T. \quad (3)$$

The speed of the vehicle at the beginning of the journey is V_0 . The speed of the vehicle at the end of the journey is V_f . Both speeds are given. The speed V_k at location x_k must be determined for $k = 1, 2, \dots, n-1$. It can be shown that V_k depends only on ξ_1, \dots, ξ_k .

4. Fundamental speed profiles

Following Howlett [4], we can define distance as a function of speed by

$$\hat{x}_K(V) = \begin{cases} \int_0^v \frac{w}{\phi_{u(k+1)}(w) - r(w)} dw & v \in [0, W_{u(k+1)}) & u(k+1) > 0 \\ \int_v^{W_Q} \frac{w}{r(w) - \phi_{u(k+1)}(w)} dw & \begin{cases} v \in (W_{u(k+1)}, W_Q] & u(k+1) > 0 \\ v \in [0, W_Q] & u(k+1) \leq 0 \end{cases} \end{cases} \quad (4)$$

where W_u is the limiting speed for control setting u .

If $\phi_u(0) \geq r(0)$, the limiting speed W_u is the unique number given by $\phi_u(W_u) = r(W_u)$. If we assume that $d\phi_u(v) < 0$ when $dv < 0$ then we can use (4) to show that $\hat{x}_k(v) \rightarrow \infty$ as $v \rightarrow W_u(k+1)$. In this case we have $V_k < W_{u(k+1)} \Rightarrow V_{k+1} < W_{u(k+1)}$ and $V_k > W_{u(k+1)} \Rightarrow V_{k+1} > W_{u(k+1)}$. The monotonic nature of the speed on $[x_k, x_{k+1}]$ means that speed limits can be imposed on the entire interval by constraining V_k and V_{k+1} .

If $\phi_u(0) < r(0)$ then we define $W_u = 0$.

The function \hat{v}_k is the inverse of \hat{x}_k . The actual speed on the interval $[x_k, x_{k+1}]$ is given by

$$v(x) = \hat{v}_k(x - x_k + \hat{x}_k(V_k)) \quad (5)$$

provided that $V_k \neq W_{u(k+1)}$.

The speed U_j at location X_j for $j = 1, 2, \dots, p-1$ is

$$U_j = \hat{v}_{r(j)}(X_j - x_{r(j)} + \hat{x}_{r(j)}(V_{r(j)})). \quad (6)$$

The time required to traverse the interval $[x_k, x_{k+1}]$ is given by

$$\tau_{k+1} = \int_0^{\xi_{k+1}} \frac{1}{\hat{v}_k(\xi + \hat{x}_k(V_k))} d\xi. \quad (7)$$

5. Optimal driving strategies

Since $V_k = V_k(\xi_1, \xi_2, \dots, \xi_k)$, we have $\tau_k = \tau_k(\xi_1, \xi_2, \dots, \xi_k)$. If we write $\xi = (\xi_1, \xi_2, \dots, \xi_n) \in \mathcal{R}^n$ then the key variables can be written as functions of ξ .

The cost of the journey is

$$J(\xi) = \sum_{k=0}^{n-1} c_{u(k+1)} \tau_{k+1}, \quad (8)$$

the total distance travelled is

$$\Theta(\xi) = \sum_{k=0}^{n-1} \xi_k,$$

and the time taken for the journey is

$$T(\xi) = \sum_{k=0}^{n-1} \tau_{k+1}. \quad (9)$$

We wish to minimise the cost of the journey $J(\xi)$. We require that the total distance travelled and the total time taken satisfy the constraints

$$\Theta(\xi) = X, \quad T(\xi) \leq T.$$

Note that the constraint $\Theta(\xi) = X$ can be weakened to read $\Theta(\xi) \geq X$ with no change to the solution.

In addition to the distance and time constraints, we must also satisfy the speed constraints

$$\begin{aligned} V_{k+1} &\leq M_j & \text{where } r(j-1) < k+1 < r(j) & \quad k = 0, 1, \dots, n-2, \\ U_j &\leq N_j & \text{where } j = 1, 2, \dots, p-1, & \quad \cdot \end{aligned}$$

where N_j is the most restrictive of the speed limits at $x = X_j$, i.e. $N_j = \min\{M_j, M_{j+1}\}$. The first of these constraints ensures that the switching speeds do not exceed the speed limit on any interval (X_j, X_{j+1}) . This is sufficient to ensure that the vehicle speed will not exceed the speed limit, since the speed of the vehicle will always lie between the switching speeds. The second ensures that speed limits are not exceeded at any point X_j where the speed limit changes. We ensure that the journey finishes at the correct speed by adding the constraint $V_n = V_f$. We define a Lagrangean function

$$\begin{aligned} \mathcal{J}(\xi) = & J(\xi) + \lambda[X - \Theta(\xi)] + \mu[t(\xi) - T] + \sum_{j=1}^{p-1} \sum_{k=r(j-1)}^{r(j)-1} \rho_{k+1}[V_{k+1} - M_j] \\ & + \sum_{k=r(p-1)}^{r(p)-2} \rho_{k+1}[V_{k+1} - M_p] + \sigma[V_n - V_f] + \sum_{j=1}^{p-1} \eta_j[U_j - N_j] \end{aligned} \quad (10)$$

where $\lambda, \mu \in \mathbb{R}^n$, $\rho = (\rho_1, \rho_2, \dots, \rho_{n-1}) \in \mathbb{R}^{n-1}$, $\sigma \in \mathbb{R}$ and $\eta = (\eta_1, \eta_2, \dots, \eta_{p-1}) \in \mathbb{R}^{p-1}$.

We then apply the Kuhn-Tucker conditions

$$\frac{\partial \mathcal{J}}{\partial \xi_{k+1}} = 0 \quad k = 0, 1, \dots, n-1,$$

and the complementary slackness conditions

$$\begin{aligned} \lambda[X - \Theta(\xi)] &= 0 & \lambda &\geq 0 \\ \mu[t(\xi) - T] &= 0 & \mu &\geq 0 \\ \rho_{k+1}[V_{k+1} - M_j] &= 0 & \rho_{k+1} &\geq 0 \quad r(j-1) < k+1 \leq r(j+1) \\ & & & j = 1, 2, \dots, p-1 \\ \sigma[V_n - V_f] &= 0 \\ \eta_j[U_j - N_j] &= 0 & \eta_j &\geq 0 \quad j = 1, 2, \dots, p-1, \end{aligned}$$

and assume that ξ lies in an open set such that $V_k(\xi) \neq W_{u(k)}$ for all k .

For $k = 0, 1, \dots, n-1$ and j such that $r(j-1) < k+1 \leq r(j)$

$$\begin{aligned} \frac{\partial \mathcal{J}}{\partial \xi_{k+1}} = & \sum_{h=k}^{n-1} c_{u(h+1)} \frac{\partial \tau_{h+1}}{\partial \xi_{k+1}} - \lambda + \mu \sum_{h=k}^{n-1} \frac{\partial \tau_{h+1}}{\partial \xi_{k+1}} + \sum_{h=k+1}^{n-2} \rho_{h+1} \frac{\partial V_{h+1}}{\partial \xi_{k+1}} \\ & + \sigma \frac{\partial V_n}{\partial \xi_{k+1}} + \sum_{l=j}^{p-1} \eta_l \frac{\partial U_l}{\partial \xi_{k+1}}. \end{aligned} \quad (11)$$

The calculation of these derivatives is similar to the calculation of the corresponding derivatives in Cheng and Howlett [7, 6].

At the end of the journey, the equation $V_n \partial \mathcal{J} / \partial \xi_n = 0$ gives

$$\lambda V_n - \mu = c_{u(n)} - \sigma [\phi_{u(n)}(V_n) - r(V_n)]. \quad (12)$$

Since $V_n = V_f$ is known, equation (12) simply relates the three Lagrange multipliers λ , μ and σ .

For $k = 1, 2, \dots, n-1$, the equation

$$V_k \left(\frac{\partial \mathcal{J}}{\partial \xi_k} - R_k(V_k) \frac{\partial \mathcal{J}}{\partial \xi_{k+1}} \right) = 0$$

gives, for j such that $r(j-1) < k \leq r(j)$,

$$\begin{aligned} \left(\sum_{l=j}^{p-1} \eta_l \frac{\phi_{u(r(l)+1)}(U_l) - r(U_l)}{U_l} + \lambda \right) V_k - \mu \\ = \frac{c_{u(k)} - R_k(V_k) c_{u(k+1)}}{1 - R_k(V_k)} + \frac{\rho_k \phi_{u(k)}(V_k) - r(V_k)}{1 - R_k(V_k)}, \end{aligned}$$

where

$$R_s(V) = \frac{\phi_{u(s)}(V) - r(V)}{\phi_{u(s+1)}(V) - r(V)}.$$

If we let

$$\lambda_j = \begin{cases} \lambda & j = p \\ \sum_{l=j}^{p-1} \eta_l \frac{\phi_{u(r(l)+1)}(U_l) - r(U_l)}{U_l} + \lambda & j < p, \end{cases}$$

then we have $V_k = M_j$ or $\rho_k = 0$. In the case $\rho_k = 0$ we have

$$\lambda_j V_k - \mu = \frac{c_{u(k)} - R_k(V_k) c_{u(k+1)}}{1 - R_k(V_k)}. \quad (13)$$

If $\eta_j \neq 0$, the complementary slackness conditions require that $U_j = N_j$. If, on the other hand, $\eta_j = 0$ and $U_j < N_j$, then $\lambda_j = \lambda_{j+1}$. If $U_j < N_j$ for all j then $\lambda_j = \lambda$ and the conditions are identical to the conditions obtained by Cheng and Howlett for the case where there are no speed limits.

6. Critical speeds

Consider a vehicle with three control settings: *power*, *coast* and *brake*. Acceleration due to the vehicle is given by

$$\phi_u(v) = \begin{cases} \phi(v) & u = 1 & (\text{power}) \\ 0 & u = 0 & (\text{coast}) \\ -B & u = -1 & (\text{brake}), \end{cases} \quad (14)$$

where ϕ is the acceleration corresponding to full tractive effort,

B is the deceleration corresponding to full braking effort.

We can assume that the cost rate $c_1 = 1$ for *power*, and that c_u is zero for *coast* and *brake*.

By alternating between *coast* and *power*, and by *braking* when necessary, the three control modes can be used to follow any possible speed profile. We will further assume that the control is never changed between *power* and *brake* without an intermediate *coast* phase.

When changing between *coast* and *power*, the conditions for an optimal journey require $V_k = M_j$ or $\rho_k = 0$. In the case $\rho_k = 0$ we get

$$\lambda_j V_k - \mu = \frac{r(V_k)}{\phi(V_k)}. \quad (15)$$

The function $F(v) = r(v)/\phi(v)$ is often strictly convex with $F(0) \geq 0$. Suburban and long-haul trains typically have $\Psi(v) = H/v$, where H is the tractive power per unit mass, and $r(v) = r_0 + r_1 v + r_2 V^2$. In such cases, (15) will generally have two solutions, $V_k = \mathcal{V}_j$ and $V_k = \mathcal{W}_j$, where $0 \leq \mathcal{V}_j \leq \mathcal{W}_j$. Furthermore, for $\lambda_j > \lambda_k$ we have $0 \leq \mathcal{V}_j < \mathcal{V}_k \leq \mathcal{W}_k < \mathcal{W}_j$. When changing between *coast* and *brake*, the conditions for an optimal journey require $V_k = M_j$ or $\rho_k = 0$. In the case $\rho_k = 0$, we get

$$\lambda_j V_k - \mu = 0. \quad (16)$$

Equation (16) will have one solution, $V_k = \mathcal{U}_j$, where $0 \leq \mathcal{U}_j \leq \mathcal{V}_j \leq \mathcal{W}_j$. The speeds \mathcal{U}_j , \mathcal{V}_j and \mathcal{W}_j are *critical speeds* for the interval (X_{j-1}, X_j) .

In an interval (X_{j-1}, X_j) with speed limit M_j , the control may be changed from *coast* to *power* only when $V_k = \mathcal{V}_j$, and requires $\mathcal{V}_j < M_j$. Similarly, the control may be changed from *power* to *coast* only when $V_k = \min\{\mathcal{W}_j, M_j\}$. A change from *coast* to *brake* may occur when $V_k = \mathcal{U}_j$. Once braking has commenced, the speed of the vehicle will remain below the critical speeds for the interval, and so the control cannot be changed again within the interval.

At a boundary X_j between two intervals, a change from *power* to *coast* may occur if $V_k = \mathcal{W}_j = \mathcal{W}_{j+1} \leq N_j$ or if $V_k = N_j \leq \min\{\mathcal{W}_j, \mathcal{W}_{j+1}\}$. A change from *coast* to

power can occur at this point only if $V_k = \mathcal{V}_j = \mathcal{V}_{j+1} < N_j$. A change from *brake* to *coast* can occur if $N_j < \mathcal{U}_j$. These changes allow us to maintain a feasible strategy.

Thus the possible control changes are:

in the interval (X_{j-1}, X_j) power to coast if $V_k = \min\{\mathcal{W}_j, M_j\}$

coast to power if $V_k = \mathcal{V}_j$

coast to brake if $V_k = \mathcal{U}_j$

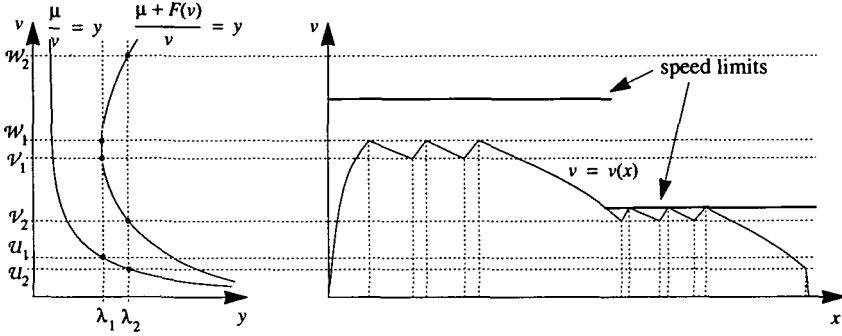
at X_j

power to coast if $V_k = \mathcal{W}_j = \mathcal{W}_{j+1} \leq N_j$
or $V_k = N_j \leq \min\{\mathcal{W}_j, \mathcal{W}_{j+1}\}$

coast to power if $V_k = \mathcal{V}_j = \mathcal{V}_{j+1} < N_j$

brake to coast if $V_k = N_j \leq \mathcal{U}_j$.

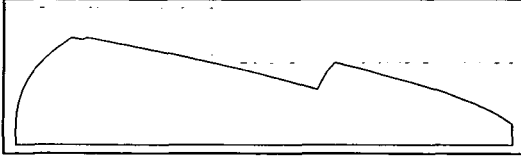
The construction of an optimal journey is illustrated in the diagram below.



If $F(v)$ is strictly convex and if $F(v)/v \rightarrow \infty$ as $v \rightarrow \infty$, then for μ such that $\mu + F(0) > 0$ it can be shown that the function $[\mu + F(v)]/v$ has a unique minimum turning point in the region $v > 0$. For values of λ above the minimum there are precisely two solutions to the equation $\lambda = [\mu + F(v)]/v$ in the region $v > 0$.

The Lagrange multipliers μ and λ_j determine critical speeds \mathcal{U}_j , \mathcal{V}_j and \mathcal{W}_j for each track interval (X_j, X_{j+1}) . We can construct an approximate speed-holding phase on a track interval using *coast-power* pairs, with the speed of the vehicle oscillating between $\mathcal{V}_j < M_j$ and $V = \min\{\mathcal{W}_j, M_j\}$. If the number of *coast-power* pairs is given for each track interval, then for each μ we can adjust the Lagrange multipliers $\lambda_j = \lambda_j(\mu)$ so that the distance and speed constraints are satisfied for each interval. We can then adjust μ to satisfy the time constraint for the journey.

As we increase the number of *coast-power* pairs, either $\mathcal{V}_j, \mathcal{W}_j \rightarrow \mathcal{V}$ where \mathcal{V} is a unique holding speed for the journey, or $\mathcal{V}_j \rightarrow M_j$. Thus there is a unique holding speed for the journey. On track intervals where this holding speed is above the limit, the speed of the vehicle must be held at the limit.



time	distance	speed	control
0.00	0.00	0.0000	Power
148.89	1978.96	19.4932	Coast
170.83	2402.48	19.1022	Power
177.36	2528.40	19.4932	Coast
436.98	7000.00	15.0000	Coast
742.00	10809.10	10.0212	Power
790.22	11421.73	15.0000	Coast
1496.25	17992.88	3.8013	Brake
1500.00	18000.00	0.0000	

EXAMPLE 1. 2 intervals, 7 phases

7. Examples

In the following examples, the vehicle acceleration is given by

$$\phi_u(v) = \begin{cases} 1.5/v & u = \text{power} \\ 0 & u = \text{coast} \\ -1 & u = \text{brake} \end{cases}$$

and resistance is given by

$$r(v) = 0.015 + 0.00003v + 0.000006v^2.$$

In all examples we use *coast-power* pairs to approximate speed holding. The number of pairs in each speed limit interval is specified.

In examples 1-3 the track is of length $X = 18000$ metres and the required journey time is $T = 1500$ seconds. The speed limit for the track is

$$M(x) = \begin{cases} 25 & x < 7000 \\ 15 & x \leq 7000. \end{cases}$$

For Example 1, there is one *coast-power* pair in the first interval and one in the second. The optimal journey has Lagrange multipliers $\mu = 0.097400$, $\lambda_1 = 0.022861$ and $\lambda_2 = 0.025623$. The cost of the journey is $\mathcal{J} = 203.63$.

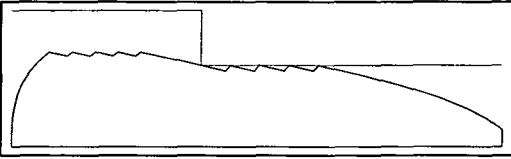
For Example 2, there are no *coast-power* pairs in the first interval and two in the second. The optimal journey has Lagrange multipliers $\mu = 0.065715$, $\lambda_1 = 0.0212728$ and $\lambda_2 = 0.0214888$. The cost of the journey is $\mathcal{J} = 202.52$. Note that this journey has the same number of phases as the journey in Example 1, but is less expensive.

Without speed limits, the minimum cost for a journey with seven phases is $\mathcal{J} = 201.98$.



time	distance	speed	control
0.00	0.00	0.0000	Power
155.45	2108.15	19.8757	Coast
436.42	7000.00	15.0000	Coast
565.66	8799.52	12.8568	Power
589.20	9128.13	15.0000	Coast
718.44	10927.65	12.8568	Power
741.97	11256.26	15.0000	Coast
1496.98	17995.39	3.0581	Brake
1500.00	18000.00	0.0000	

EXAMPLE 2. 2 intervals, 7 phases



time	distance	speed	control
0.00	0.00	0.0000	Power
115.57	1364.00	17.3692	Coast
155.59	2045.34	16.6788	Power
165.34	2211.25	17.3692	Coast
205.36	2892.60	16.6788	Power
215.11	3058.50	17.3692	Coast
255.13	3739.85	16.6788	Power
264.87	3905.76	17.3692	Coast
304.90	4587.10	16.6788	Power
314.64	4753.01	17.3692	Coast
453.53	7000.00	15.0000	Coast
515.47	7896.96	13.9661	Power
527.37	8069.44	15.0000	Coast
589.30	8966.40	13.9661	Power
601.21	9138.88	15.0000	Coast
663.14	10035.84	13.9661	Power
675.05	10208.31	15.0000	Coast
736.98	11105.27	13.9661	Power
748.89	11277.75	15.0000	Coast
1496.88	17995.07	3.1644	Brake
1500.00	18000.00	0.0000	

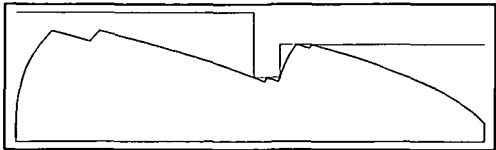
EXAMPLE 3. 2 intervals, 19 phases

For Example 3, there are four *coast-power* pairs in each track interval. The optimal journey has Lagrange multipliers $\mu = 0.067873$, $\lambda_1 = 0.021239$ and $\lambda_2 = 0.021449$. The cost of the journey is $\mathcal{J} = 202.16$. Without speed limits, the journey cost is $\mathcal{J} = 201.89$.

In Examples 4 and 5 the track is also of length $X = 18000$ metres, but therequired journey time is $T = 1620$ seconds. The speed limit for the track is

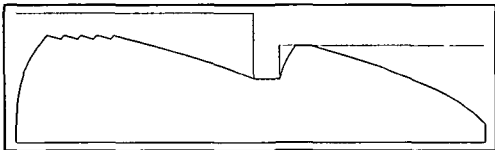
$$M(x) = \begin{cases} 20 & x < 9000 \\ 10 & 9000 \leq x \leq 10000 \\ 15 & x > 10000. \end{cases}$$

For Example 4, there is one *coast-power* pair in the first interval, two in the second, and one in the third. The optimal journey has Lagrange multipliers $\mu = 0.060353$, $\lambda_1 = 0.020798$, $\lambda_2 = 0.022309$ and $\lambda_3 = 0.020866$. The cost of the journey is $\mathcal{J} = 199.14$. Without speed limits, the cost of the journey is $\mathcal{J} = 198.01$.



time	distance	speed	control
0.00	0.00	0.0000	Power
112.28	1307.18	17.1400	Coast
204.42	2813.64	15.5648	Power
225.53	3159.21	17.1400	Coast
657.52	9000.00	10.0000	Coast
704.16	9449.10	9.2610	Power
709.44	9500.00	10.0000	Coast
756.08	9949.10	9.2610	Power
761.36	10000.00	10.0000	Power
809.74	10614.22	15.0000	Coast
844.40	11124.04	14.4198	Power
851.20	11224.20	15.0000	Coast
1617.15	17995.88	2.8925	Brake
1620.00	18000.00	0.0000	

EXAMPLE 4. 3 intervals, 11 phases



time	distance	speed	control
0.00	0.00	0.0000	Power
104.14	1170.07	16.5555	Coast
136.18	1691.67	16.0084	Power
143.47	1810.39	16.5555	Coast
175.50	2331.98	16.0084	Power
182.79	2450.71	16.5555	Coast
214.83	2972.30	16.0084	Power
222.12	3091.02	16.5555	Coast
254.16	3612.62	16.0084	Power
261.45	3731.34	16.5555	Coast
659.48	9000.00	10.0000	Coast
677.66	9179.13	9.7114	Power
679.77	9200.00	10.0000	Coast
697.95	9379.13	9.7114	Power
700.07	9400.00	10.0000	Coast
718.24	9579.13	9.7114	Power
720.36	9600.00	10.0000	Coast
738.53	9779.13	9.7114	Power
740.65	9800.00	10.0000	Coast
758.83	9979.13	9.7114	Power
760.94	10000.00	10.0000	Power
809.32	10614.22	15.0000	Coast
817.78	10740.48	14.8580	Power
819.48	10765.80	15.0000	Coast
827.93	10892.06	14.8580	Power
829.63	10917.39	15.0000	Coast
838.09	11043.65	14.8580	Power
839.78	11068.97	15.0000	Coast
848.24	11195.24	14.8580	Power
849.94	11220.56	15.0000	Coast
1617.17	17995.93	2.8731	Brake
1620.00	18000.00	0.0000	

EXAMPLE 5. 3 intervals, 29 phases

For Example 5, there are four *coast-power* pair in the first interval, five in the second, and four in the third. The optimal journey has Lagrange multipliers $\mu = 0.059733$, $\lambda_1 = 0.020749$, $\lambda_2 = 0.022008$ and $\lambda_3 = 0.020791$. The cost of the journey is $\mathcal{J} = 199.05$. Without speed limits, the cost of the journey is $\mathcal{J} = 197.95$.

8. Conclusions

For a train with three control levels (*power*, *coast* and *brake*) on a straight level track, we can construct an optimal journey. For each given journey time there is a unique holding speed. Speed holding can be approximated by a sequence of *coast-power* pairs. On intervals of track where the speed limit is below the desired holding speed, the speed must be held at the limit. If braking is necessary on an interval, the speed at which braking commences is determined in part by the holding speed for the interval. We have used the examples to show that the key equations (12) and (13) can be used to determine optimal driving strategies.

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