# Module 3: An Introduction to Conservation Laws and Finite Volume Methods

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#### **Announcements**

- Assignment # 3 Posted this week (Hyperbolic Conservation Laws)
- Today and next class Finite Volume
- Finite Element Methods (FEM) starting next week (2 HW,  $1 \times 1D$ ,  $1 \times 2D$ )

# References and Acknowledgements

The following materials were used in the preparation of this lecture:

- Randall J. LeVeque Numerical Methods for Conservation Laws.
- 2 16.920, lecture 11,12 Notes
- Sethian, J.A., Level Set Methods Evolving interfaces in Geometry, Fluid Mechanics
- Versteeg and Malalasekera, An introduction to computational fluid dynamics – the finite volume method

The author of these slides wishes to thank these sources for making the current lecture.

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# Conservation of Mass Example

• Consider a simple conservation of mass representation:

#### Control Volume Mathematics

 We could recall from fluid dynamics that there is a control volume representation for this situation:

$$0 = \frac{\partial}{\partial t} \iiint_{\Omega} \rho dV + \iint_{\Gamma} \rho \vec{u} \cdot ndS$$
 (1)

 This expression relates the change in mass inside the element with the rate at which it is entering/leaving the element. We can impose the divergence theorem to transform the second integral (boundary integral):

$$0 = \frac{\partial}{\partial t} \iiint_{\Omega} \rho dV + \iiint_{\Omega} \nabla \cdot (\rho \vec{u}) dV$$
 (2)

• If we then combining the two integrals:

$$0 = \iiint_{\Omega} \left[ \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) \right] dV \tag{3}$$

#### Control Volume Mathematics

• The result is the familiar conservation of mass in differential form

$$0 = \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) \tag{4}$$

 Idea: What if we had the above conservation of mass equation, can we introduce a "finite volume" or control volume approach? If so, how do we do so?

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#### General Conservation Laws

- In general, many physical phenomena that change with respect to time are conserved.
  - Conservation of mass ( $\rho$  is mass per unit volume)
  - ullet Conservation of Momentum ( $ho ec{u}$  is momentum per unit volume ightarrow Newtons Law )
  - Conservation of Energy  $(\rho u \cdot u^T)$  is energy per unit volume  $\to$  Energy equation)
- The underlying conservation form is:

$$\frac{\partial u}{\partial t} + \frac{\partial (f(u))}{\partial x} = 0 \tag{5}$$

- Where:
  - u = the unknown property under consideration (in fluids, it is the per unit volume of the quantity)
  - f(u) =The flux of the quantity through the control volume

#### General Conservation Laws

• The basic conservation form:

$$\frac{\partial u}{\partial t} + \frac{\partial (f(u))}{\partial x} = 0 \tag{6}$$

• FYI, this can be re-written or expressed as:

$$\frac{\partial u}{\partial t} + \underbrace{\frac{\partial f}{\partial u}}_{a(u)} \frac{\partial u}{\partial x} = 0 \tag{7}$$

• or the (non-linear) advection equation. We saw the linear version of this last class (hyperbolic PDE).

- Let's define a 1-D finite volume geometry and discretization:
- We will need to define 1-D "volumes" and "boundaries":

 We are going to integrate the conservation law across a volume/area/ line element. Our original conservation law in 1-Dimension is:

$$\frac{\partial u}{\partial t} + \frac{\partial (f(u))}{\partial x} = 0 \tag{8}$$

• Let us take an integral across each of our finite line segments, and claim that our solution is the addition of all of the segments:

$$\sum_{i} \int_{x_{L}}^{x_{R}} \frac{\partial u_{i}}{\partial t} + \frac{\partial (f(u_{i}))}{\partial x} dx = 0$$
 (9)

 It turns out that each segment must satisfy the following integral expression:

$$0 = \frac{\partial}{\partial t} \int_{x_l}^{x_R} u dx + \int_{x_L}^{x_R} \frac{\partial f(u)}{\partial x} dx$$
 (10)

• Discussion: By taking this integral, have we changed the nature of the conservation law at all?

 The second integral simply becomes the flux evaluated at the left and right boundaries of the element/cell:

$$0 = \frac{\partial}{\partial t} \int_{x_L}^{x_R} u dx + \int_{x_L}^{x_R} \frac{\partial f(u)}{\partial x} dx = \frac{\partial}{\partial t} \int_{x_L}^{x_R} u dx + f(u)_R - f(u)_L$$
 (11)

We can re-arrange this a little as:

$$\frac{\partial}{\partial t} \int_{x_L}^{x_R} u dx = -[f(u)_R - f(u)_L]$$
 (12)

 This expression says: The change in the property integrated across our control volume is balanced by the flux in and out of the LHS and RHS boundaries of the element.

 Let's focus on the left hand side now. We may notice that the average value of the property u across the cell is:

$$\frac{1}{\Delta x} \int_{x_L}^{x_R} u dx = u_{avg} \tag{13}$$

Or:

$$\int_{x_l}^{x_R} u dx = \Delta x u_{avg} \tag{14}$$

• We can re-write our previous expression now as:

$$\frac{\partial}{\partial t}(\Delta x u_{\text{avg}}) = -[f(u)_R - f(u)_L] \tag{15}$$

 Pictorially, the average value vs. the actual value. What we have effectively done, is assumed a constant value function across each element (most crude approximation we could make, but lets go with it).

Only the time derivative is left:

$$\frac{\partial}{\partial t}(\Delta x u_{avg}) = -[f(u)_R - f(u)_L]$$
 (16)

Discretizing with a forward Euler equation:

$$\frac{(\Delta x u_{avg})^{k+1} - (\Delta x u_{avg})^k}{\Delta t} = -[f(u)_R - f(u)_L]$$
 (17)

• Rearranging to find the new *u*:

$$u^{k+1} = u^k - \frac{\Delta t}{\Delta x} [f(u)_R - f(u)_L]$$
 (18)

• Now we can find the updated *u* value at some future time.

• Let's Recap:

#### Traffic Flow Example (Leveque):

- $oldsymbol{
  ho}$  : Density of cars on the road
- u : velocity of the cars
- We are going to claim there is a relationship between the velocity of the cars and the density:

$$u(\rho) = u_{\text{max}} \left(1 - \frac{\rho}{\rho_{\text{max}}}\right) \tag{19}$$

• Let's take a look at this function (assuming that  $u_{max}=1$  and  $\rho_{max}=1$ , ie – normalized flow)

• The conservation of cars (mass) equation is:

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho u)}{\partial x} \tag{20}$$

• Based on the above equation, and the expression for the velocity as a function of density, the  $\mathbf{flux} = \rho u$  is:

$$f(\rho) = \rho u_{max} \left(1 - \frac{\rho}{\rho_{max}}\right) = \rho - \rho^2 \tag{21}$$

• Let's plot the flux as a function of  $\rho$  now:

Let's try to implement this for a particular problem:

- Let's choose  $\rho = a$  when x > 0
- Let's choose  $\rho = b$  when x < 0
- From before, we have:

$$u^{k+1} = u^k - \frac{\Delta t}{\Delta x} [f(u)_R - f(u)_L]$$
 (22)

- Let's try to put this together for a couple of control volumes.
- Notice, at the boundaries, the flux of cars from one element, into another could be different!

Let's try to implement this for a particular problem:

• Godunov came up with the following flux function:

$$F(u_l, u_r) = \begin{cases} \min_{(u_l \le u \le u_r)} f(u) & \text{if } u_l \le u_r \\ \max_{(u_r \le u \le u_l)} f(u) & \text{if } u_l > u_r \end{cases}$$
 (23)

• What does this mean?