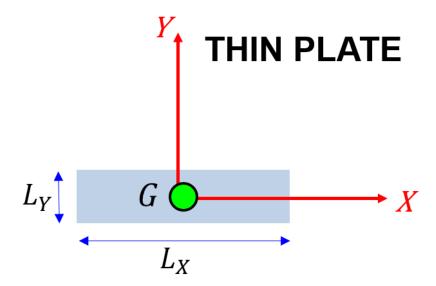
Inertia properties of a 2 blade propeller

What we're going to do:

In this FAQ, we're going to explore the inertia properties of a 2 bladed propeller. We'll approximate the propeller by a rectangular plate

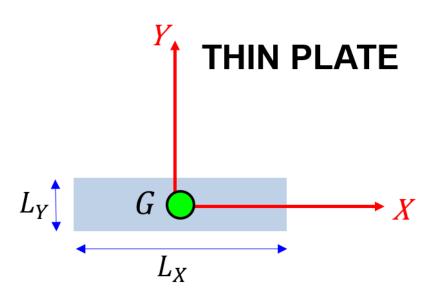


WHY are we doing this?

• explore how the inertia matrix (relative to the XY-frame) changes as the propeller spins

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Consider a thin Rectangular plate:

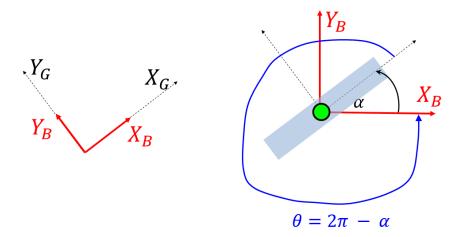


In this figure we have a G-frame attached to the Centre of mass of the plate, Let's calculate the inertia of the plate about this G-frame

I_LOCAL =
$$\begin{pmatrix} \frac{Ly^2 m}{12} & 0 & 0 \\ 0 & \frac{Lx^2 m}{12} & 0 \\ 0 & 0 & \frac{m (Lx^2 + Ly^2)}{12} \end{pmatrix}$$

Consider an arbitrarily orientated propeller:

Consider the following arbitrarily orientated propeller system:



```
% create a PASSIVE rotation object
syms alpha
BLUE_OBJ = bh_rot_passive_G2B_CLS({'D1Z'}, [ (2*pi - alpha) ], 'SYM');
% extract the PASIVE rotation matrix bRg
BLUE_bRg = BLUE_OBJ.get_R1
```

$$\begin{array}{cccc} \mathsf{BLUE_bRg} &= & \\ & \begin{pmatrix} \cos(\alpha) & -\sin(\alpha) & 0 \\ \sin(\alpha) & \cos(\alpha) & 0 \\ 0 & 0 & 1 \end{pmatrix} \end{array}$$

```
\% calculate the inertias relative to the XB,YB frame gI = I_LOCAL;
```

$$\begin{pmatrix} \frac{m \operatorname{Lx}^2 \sin(\alpha)^2}{12} + \frac{m \operatorname{Ly}^2 \cos(\alpha)^2}{12} & \sigma_1 & 0 \\ \sigma_1 & \frac{m \operatorname{Lx}^2 \cos(\alpha)^2}{12} + \frac{m \operatorname{Ly}^2 \sin(\alpha)^2}{12} & 0 \\ 0 & 0 & \frac{m (\operatorname{Lx}^2 + \operatorname{Ly}^2)}{12} \end{pmatrix}$$

where

$$\sigma_1 = \frac{\operatorname{Ly}^2 m \cos(\alpha) \sin(\alpha)}{12} - \frac{\operatorname{Lx}^2 m \cos(\alpha) \sin(\alpha)}{12}$$

Let's plot how the these terms vary with alpha.

substitute numeric values for Lx and Ly and mass

```
Lx_num = 1;
Ly_num = 0.1;
m_num = 1;
I_LOCAL_num = subs(I_LOCAL, [Lx, Ly, m], [Lx_num, Ly_num, m_num])
```

 $I_LOCAL_num =$

$$\begin{pmatrix} \frac{1}{1200} & 0 & 0 \\ 0 & \frac{1}{12} & 0 \\ 0 & 0 & \frac{101}{1200} \end{pmatrix}$$

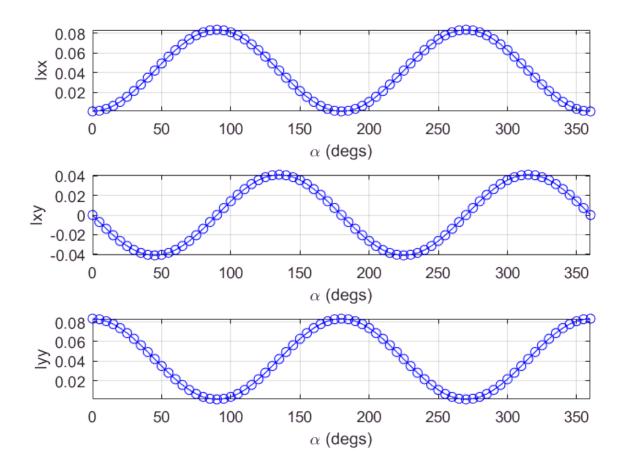
Ib_blade_num = subs(Ib_blade, [Lx, Ly, m], [Lx_num, Ly_num, m_num])

$$\begin{split} \text{Ib_blade_num} &= \\ & \left(\frac{\cos(\alpha)^2}{1200} + \frac{\sin(\alpha)^2}{12} - \frac{33\cos(\alpha)\sin(\alpha)}{400} & 0 \\ - \frac{33\cos(\alpha)\sin(\alpha)}{400} & \frac{\cos(\alpha)^2}{12} + \frac{\sin(\alpha)^2}{1200} & 0 \\ 0 & 0 & \frac{101}{1200} \\ \end{split} \right) \end{aligned}$$

OK: now let's calculate the inertia matrix for different values of α

```
alpha_deg_num = [0:5:360];
alpha_rad_num = (pi/180)*alpha_deg_num;
for kk=1:length(alpha_rad_num)
```

```
alpha num = alpha rad num(kk);
              = subs(Ib blade num, alpha, alpha num);
    bh.Ixx(kk) = tmp I(1,1);
    bh.Iyy(kk) = tmp I(2,2);
    bh.Ixy(kk) = tmp I(1,2);
end
% OK plot it
figure
subplot(3,1,1);
   plot(alpha deg num, bh.Ixx, 'ob-');
        axis('tight'); grid('on'); xlabel('\alpha (degs)'); ylabel('Ixx');
subplot(3,1,2);
   plot(alpha deg num, bh.Ixy, 'ob-');
        axis('tight'); grid('on'); xlabel('\alpha (degs)'); ylabel('Ixy');
subplot(3,1,3);
   plot(alpha deg num, bh.Iyy, 'ob-');
   axis('tight'); grid('on'); xlabel('\alpha (degs)'); ylabel('Iyy');
```



```
% OK plot the terms normalised by the local pose inertias figure subplot(2,1,1); plot(alpha_deg_num, bh.Ixx/I_LOCAL_num(1,1), 'or-'); axis('tight'); grid('on'); xlabel('\alpha (degs)'); ylabel('Ixx ./ Ixx'); subplot(2,1,2); plot(alpha_deg_num, bh.Iyy/I_LOCAL_num(2,2), 'or-'); axis('tight'); grid('on'); xlabel('\alpha (degs)'); ylabel('Iyy ./ Iyy');
```

