## The MOSFET Amplifier (1)

Lecture 7 October 4<sup>th</sup>, 2018

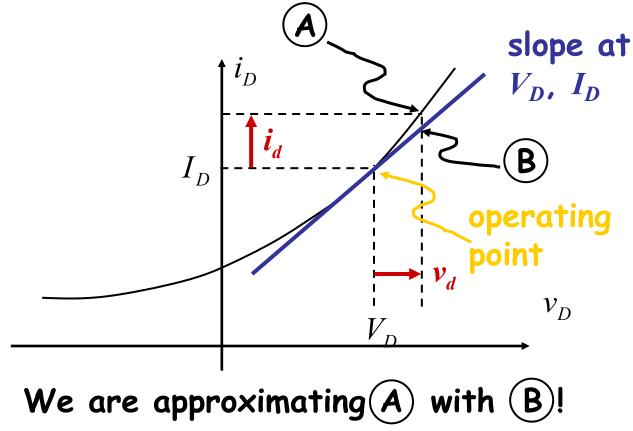
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Seoul National University

Slide credits: Prof. Anant Agarwal at MIT

#### Review

#### Nonlinear circuits

- We can use the node method (or others) with nonlinear equations.
- Incremental analysis "linearizes" the circuit for small signals.



#### **Outline**

Textbook: 7.1, 7.2, 7.3, 7.4

- (Review of) Dependent Sources
- Why Amplify?
- Signal Amplification
- Actual MOSFET Characteristics
- MOSFET SCS Model

Independent source

#### Seen previously

Resistor

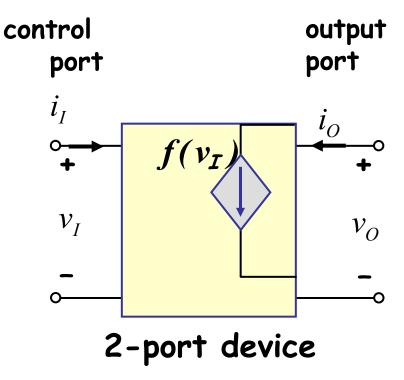
$$\begin{array}{ccc}
\bullet & V & - \\
\hline
i & R & \\
\hline
i & R
\end{array}$$

Independent Current source

$$\begin{array}{cccc}
\bullet & v & - \\
\hline
i & I & I
\end{array}$$

2-terminal 1-port devices

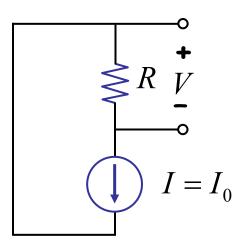
#### Dependent source



e.g., Voltage Ctrl'd Current Source Current at output port is a function of voltage at the input port

Example 1 (independent source): Find V

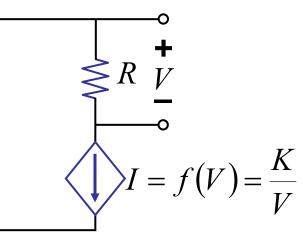
independent current source

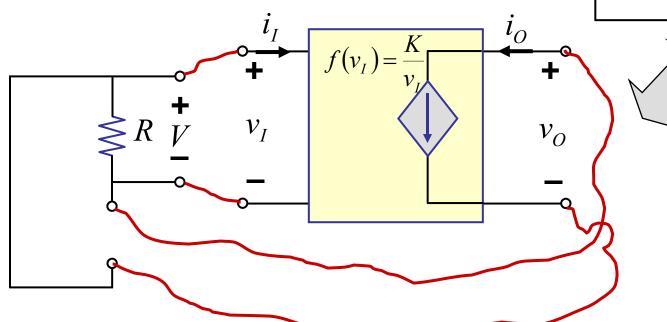


$$V =$$

Example 2 (dependent source): Find V

voltage controlled current source

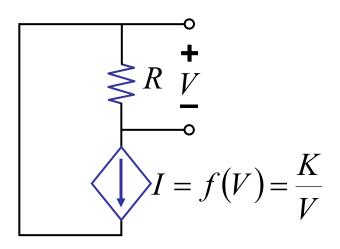




Example 2 (dependent source): Find V

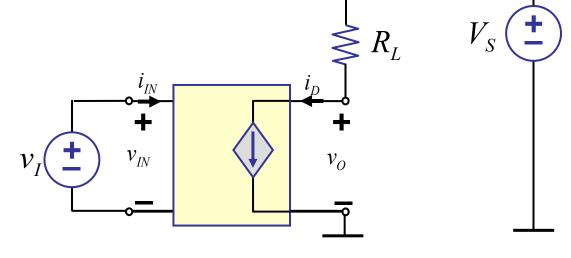
voltage controlled current source

$$V = IR = \frac{K}{V}R$$
 or  $V^2 = KR$  or  $V = \sqrt{KR}$   $= \sqrt{10^{-3} \cdot 10^3}$   $= 1 \, Volt$ 



e.g. 
$$K = 10^{-3} Amp \cdot Volt$$
  
 $R = 1k\Omega$ 

Example 3



$$i_D = f(v_{IN})$$

(This is MOSFET Switch-Current Source (SCS) model with 
$$V_T=1V...$$
)

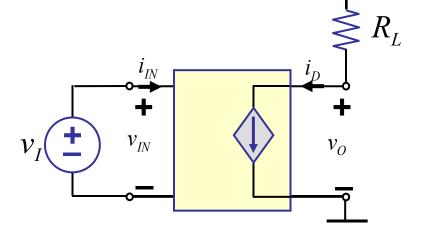
e.g. 
$$i_D = f(v_{IN})$$

$$= \frac{K}{2}(v_{IN} - 1)^2 \quad \text{for} \quad v_{IN} \ge 1$$

$$i_D = 0 \quad \text{otherwise}$$

Find  $v_O$  as a function of  $v_I$ .

Example 3



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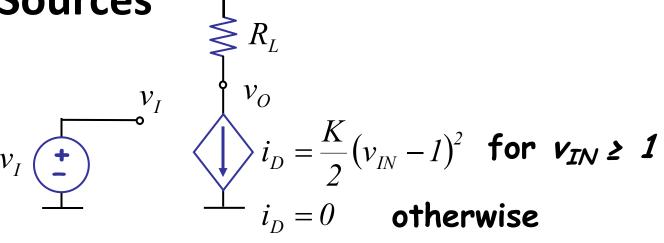
(This is MOSFET Switch-Current Source (SCS) model with  $V_T=1V...$ )

Find  $v_O$  as a function of  $v_I$ .

10

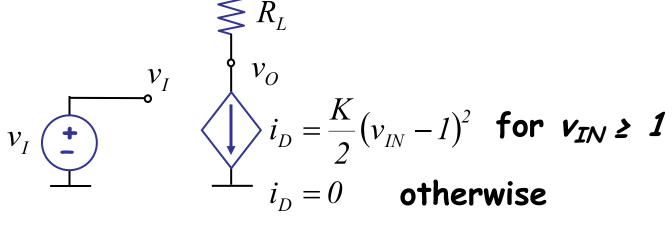
# **Dependent Sources**

Example 3



Find  $v_O$  as a function of  $v_I$ .

**Example 3** 



 $v_{\mathcal{O}}$  as a function of  $v_{\mathcal{I}}$ .

**KVL** 

$$-V_S + i_D R_L + v_O = 0$$
$$v_O = V_S - i_D R_L$$



$$v_O = V_S - \frac{K}{2}(v_I - 1)^2 R_L$$
 for  $v_I \ge 1$ 

Hold that thought  $v_0 = V_s$ 

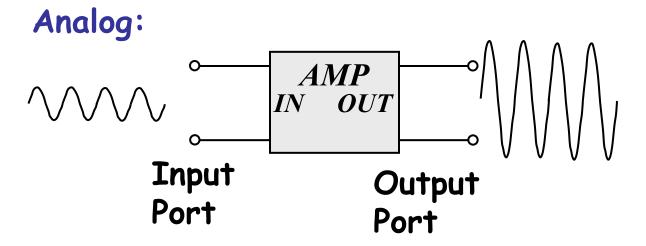
$$v_O = V_S$$

#### **Outline**

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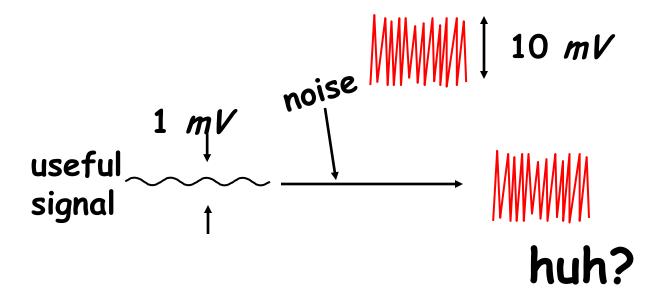
Signal amplification key to both analog and digital processing.



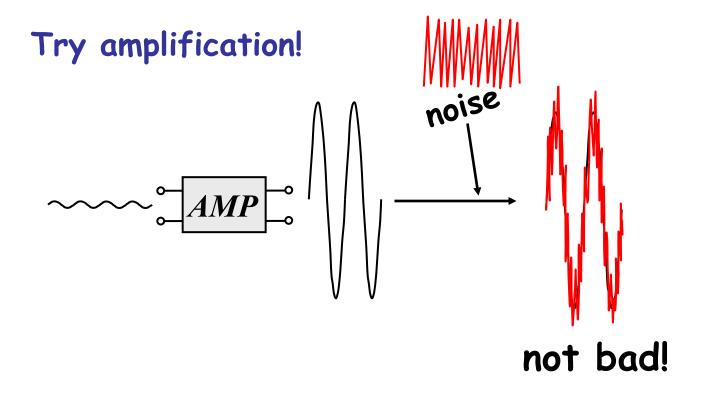
Besides the obvious advantages of being heard farther away, amplification is key to noise tolerance during communication

Amplification is key to noise tolerance during communcation

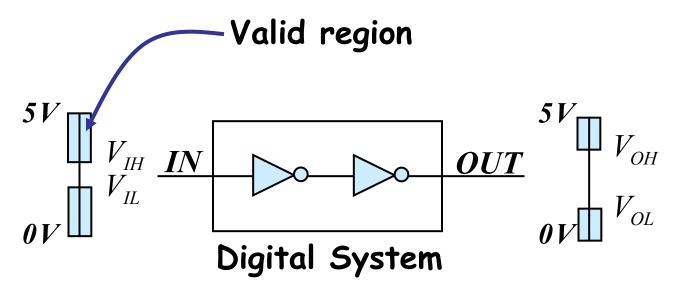
#### No amplification

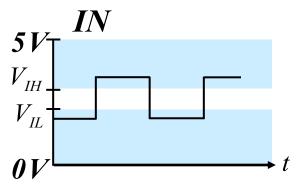


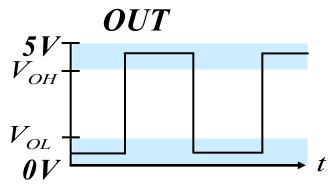
Amplification is key to noise tolerance during communcation



### Digital:

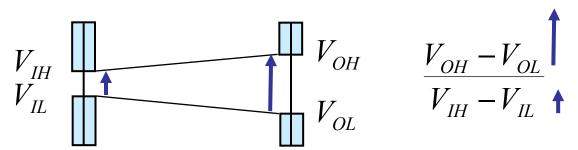




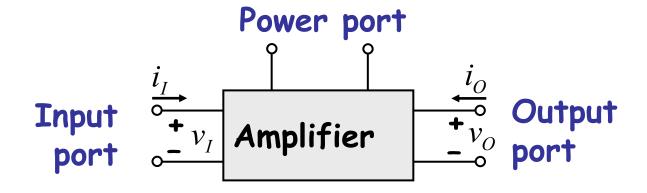


## Digital:

Static discipline requires amplification! Minimum amplification (gain) needed:

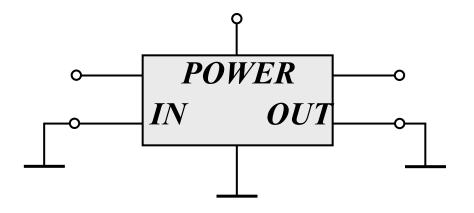


An amplifier is a 3-ported device, actually



We often don't show the power port.

An amplifier is a 3-ported device, actually



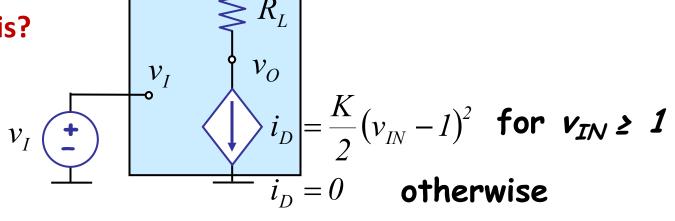
Also, for convenience we commonly observe "the common ground discipline."

In other words, all ports often share a common reference point called "ground."

How do we build one?



Remember this?



Find  $v_{\mathcal{O}}$  as a function of  $v_{\mathcal{T}}$ .

**KVL** 

#### Claim:

This is an amplifier!

$$-V_S + i_D R_L + v_O = 0$$
$$v_O = V_S - i_D R_L$$



$$v_O = V_S - \frac{K}{2} (v_I - 1)^2 R_L$$
 for  $v_I \ge 1$ 

$$v_O = V_S$$

### So, where's the amplification?

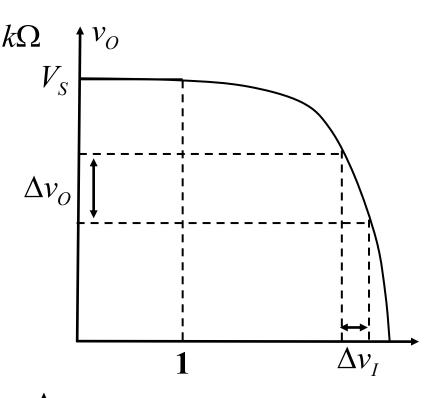
Let's look at the  $v_O$  versus  $v_I$  curve.

**e.g.** 
$$V_S = 10V$$
,  $K = 2\frac{mA}{V^2}$ ,  $R_L = 5k\Omega$ 

$$v_O = V_S - \frac{K}{2}R_L(v_I - 1)^2$$

$$= 10 - \frac{2}{2} \cdot 10^{-3} \cdot 5 \cdot 10^3 (v_I - 1)^2$$

$$v_O = 10 - 5(v_I - 1)^2$$

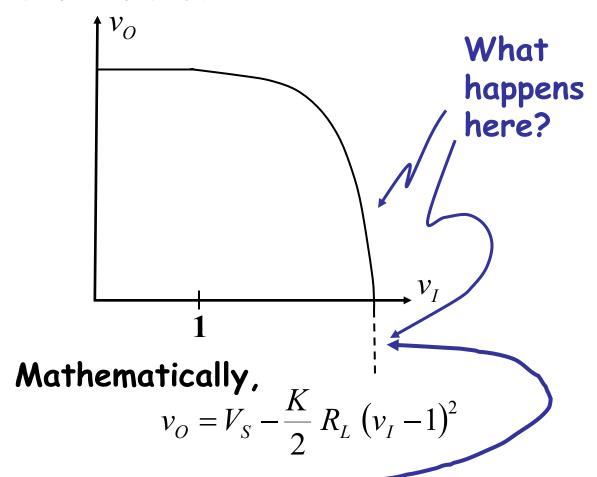


### So, where's the amplification?

Plot  $v_O$  versus  $v_I$ 

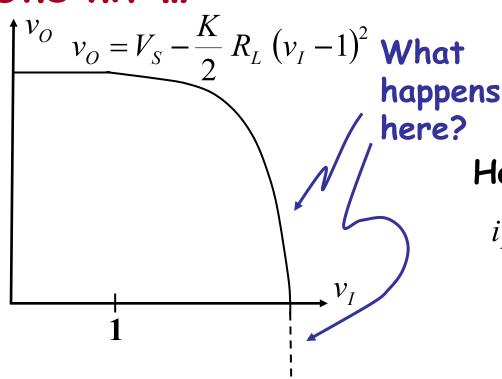
$v_O = 10 - 5(v_I - 1)^2$	$v_I$	$v_O$	
	0.0	10.00	
	1.0	10.00	
	1.5	8.75	
0.1 change	2.0	5.00	1V change
$in v_I$	2.1	4.00	in $v_0$
	2.2	2.80	
	2.3	1.50	
	2.4	~ 0.00	Gain!
•			_

One nit ...



50 is mathematically predicted behavior

#### One nit ...



However, from

$$i_{D} = \frac{K}{2} (v_{I} - 1)^{2} \text{ for } v_{I} \ge 1$$

$$V_{S}$$

$$R_{L}$$

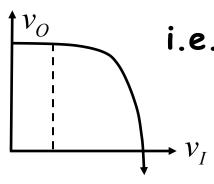
$$v_{O}$$

$$VCCS \longleftrightarrow i_{D}$$

For  $v_0>0$ , VCCS consumes power:  $v_0 i_D$  $v_{o}<0$ , VCC5 must supply power!

### One nit ...

If VCCS were a device that can source power, then the mathematically predicted behavior could be observed —



i.e. 
$$v_O = V_S - \frac{K}{2} R_L (v_I - 1)^2$$

where  $v_0$  goes negative

### One nit ...

If VCCS is a passive device,

then it cannot source power, so  $v_o$  cannot go negative.

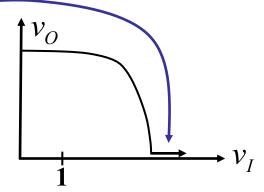
Turns out, our model breaks down.

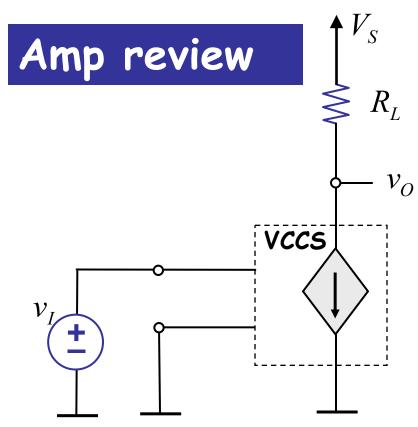
Commonly 
$$i_D = \frac{K}{2} (v_I - 1)^2$$

will no longer be valid when  $v_0 \le 0$ .

e.g.  $i_D$  saturates (stops increasing)

and we observe:





$$i_D = \frac{K}{2} (v_I - 1)^2 \quad \text{for } v_I \ge 1V$$
$$= 0 \quad \text{otherwise}$$

$$v_O = V_S - i_D R_L$$

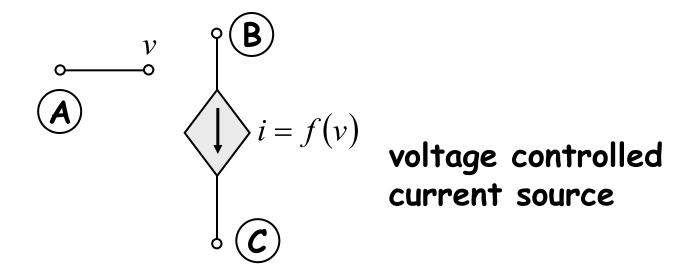
$$\frac{K}{2} (v_I - 1)^2$$

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### Key device Needed:

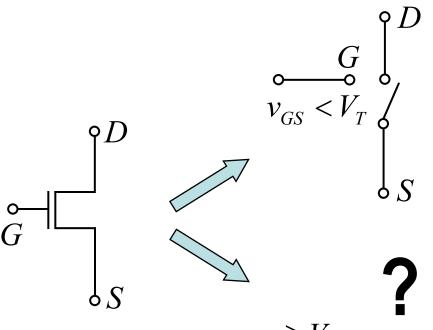


Let's look at our old friend, the MOSFET ...

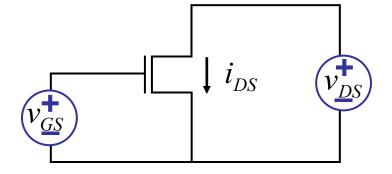
### Key device Needed:

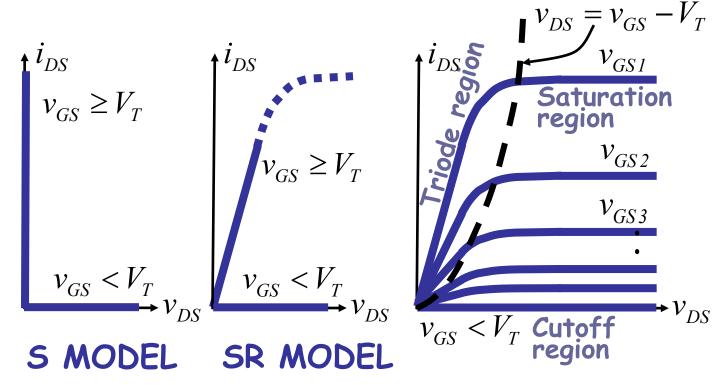
Our old friend, the MOSFET ...

First, we sort of lied. The on-state behavior of the MOSFET is quite a bit more complex than either the ideal switch (S) or the resistor (SR) model.

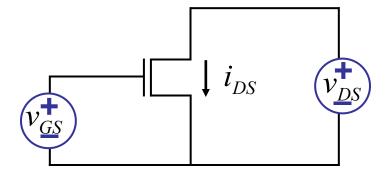


Graphically





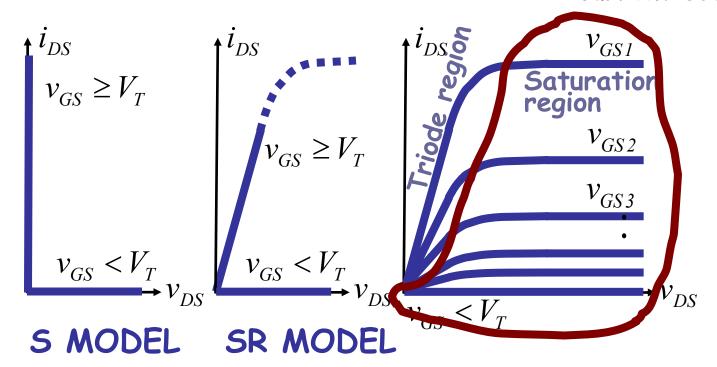
Graphically



#### when

$$v_{DS} \ge v_{GS} - V_T$$

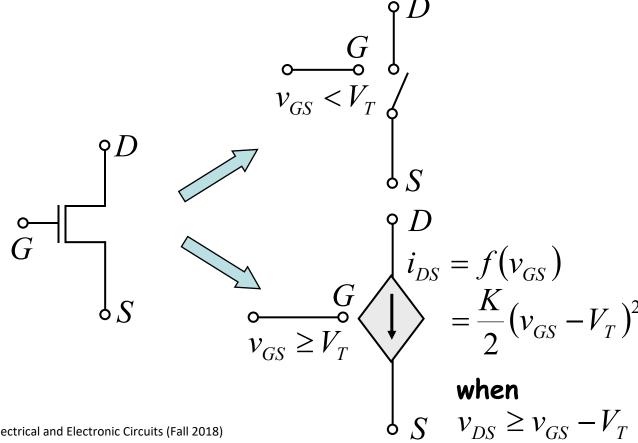
Notice that MOSFET behaves like a current source



#### **MOSFET SCS Model**

- **SCS Model: Switched Current Source Model** 
  - Saturation region of operation: "saturation principle"

When 
$$v_{DS} \ge v_{GS} - V_T$$



#### **MOSFET SCS Model**

Reconciling the models

