

BJT Transistor Modeling

Transistor Modeling

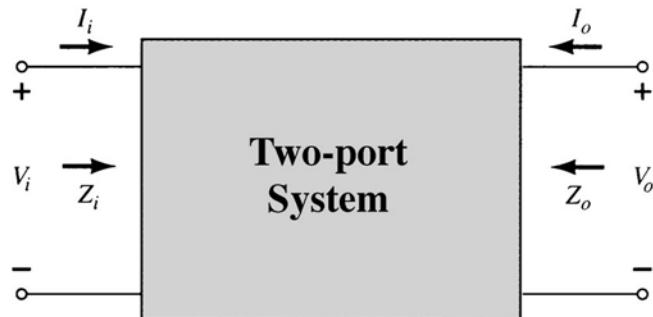
A model is an equivalent circuit that represents the AC characteristics of the transistor. It uses circuit elements that approximate the behavior of the transistor.

There are 2 models commonly used in small signal AC analysis of a transistor:

- hybrid equivalent model

Important Parameters

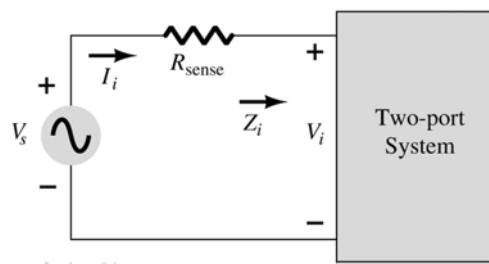
Z_i , Z_o , A_v , A_i are important parameters for the analysis of the AC characteristics of a transistor circuit.



Input Impedance, Z_i

To determine I_i : insert a “sensing resistor”

$$Z_i = \frac{V_i}{I_i}$$



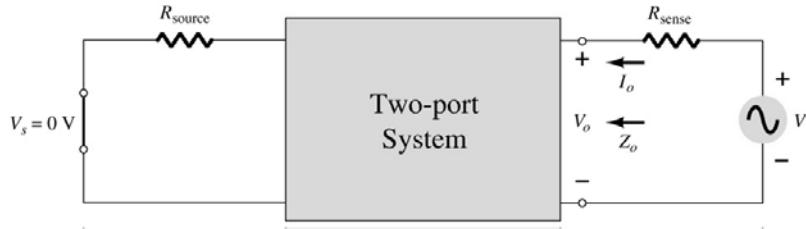
then calculate I_i :

$$I_i = \frac{V_s - V_i}{R_{\text{sense}}}$$

Output Impedance, Z_o

To determine I_o : insert a “sensing resistor”

$$Z_o = \frac{V_o}{I_o}$$



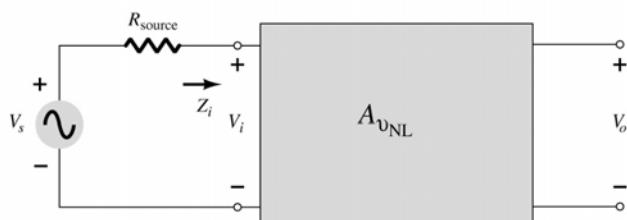
then calculate I_o :

$$I_o = \frac{V - V_o}{R_{\text{sense}}}$$

Voltage Gain, A_v

$$A_v = \frac{V_o}{V_i}$$

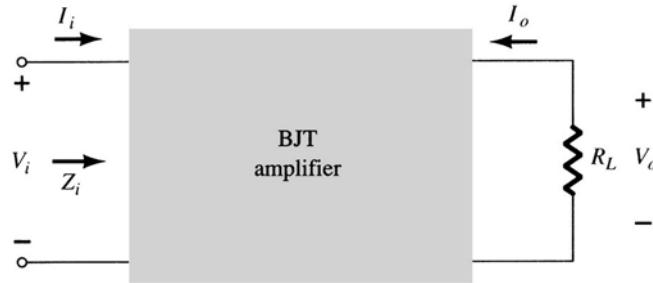
For an amplifier with no load: $A_{vNL} = \left. \frac{V_o}{V_i} \right|_{R_L = \infty \Omega (\text{opencircuit})}$



Note: the no-load voltage gain (A_{vNL}) is always greater than the loaded voltage gain (A_v).

Current Gain, A_i

$$A_i = \frac{I_o}{I_i}$$



The current gain (A_i) can also be calculated using the voltage gain (A_v):

$$A_i = -A_v \frac{Z_i}{R_L}$$

Phase Relationship

The phase relationship between input and output depends on the amplifier configuration circuit.

Common – Emitter : 180 degrees

Common - Base : 0 degrees

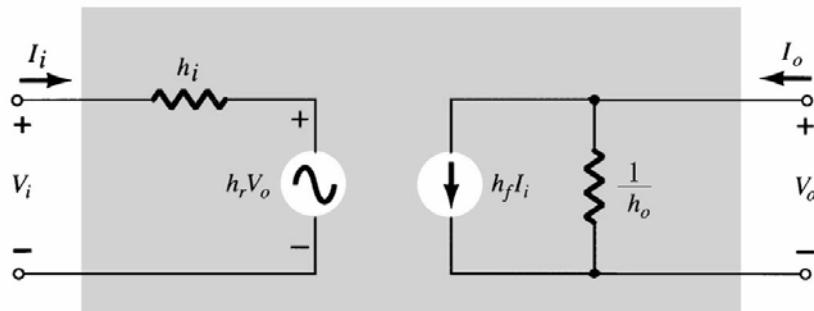
Common – Collector: 0 degrees

Hybrid Equivalent Model

The hybrid parameters: h_{ie} , h_{re} , h_{fe} , h_{oe} are developed and used to model the transistor. These parameters can be found in a specification sheet for a transistor.

- h_i = input resistance
- h_r = reverse transfer voltage ratio (V_i/V_o)
- h_f = forward transfer current ratio (I_o/I_i)
- h_o = output conductance

General h-Parameters for any Transistor Configuration

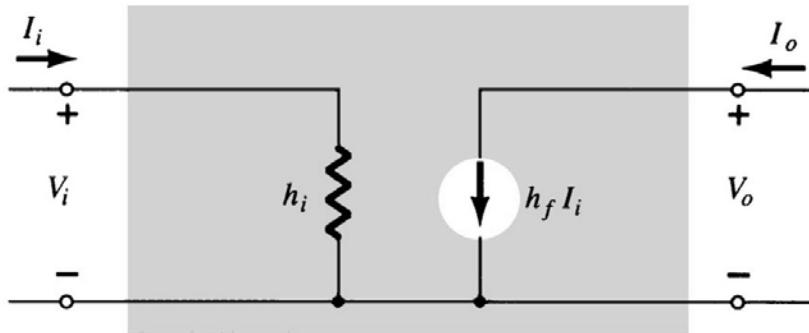


- h_i = input resistance
- h_r = reverse transfer voltage ratio (V_i/V_o)
- h_f = forward transfer current ratio (I_o/I_i)
- h_o = output conductance

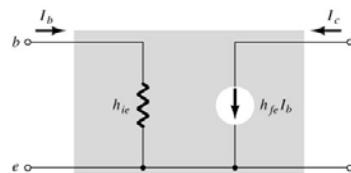
Simplified General h-Parameter Model

The above model can be simplified based on these approximations:

$$h_r \approx 0 \text{ therefore } h_r V_o = 0 \text{ and } h_o \approx \infty$$



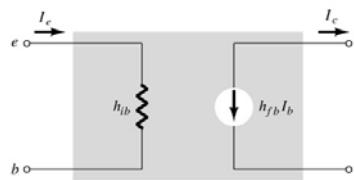
Common-Emitter h-Parameters



$$h_{ie} = \frac{25\text{mV}}{I_{BQ}} \cong \frac{h_{fe} 25\text{mV}}{I_{EQ}}$$

$$h_{fe} = \beta_{ac}$$

Common-Base h-Parameters

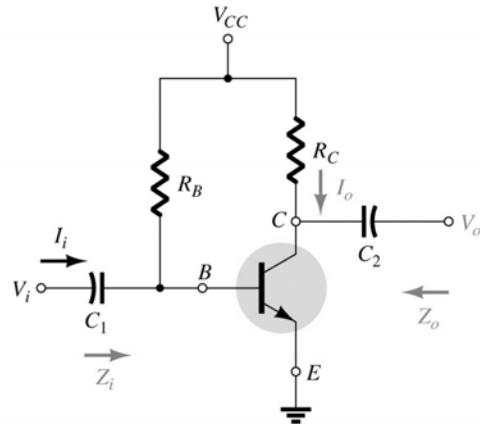


$$h_{ib} = \frac{25\text{mV}}{I_{EQ}}$$

$$h_{fb} = -\alpha_{ac} \cong -1$$

BJT Small-Signal Analysis

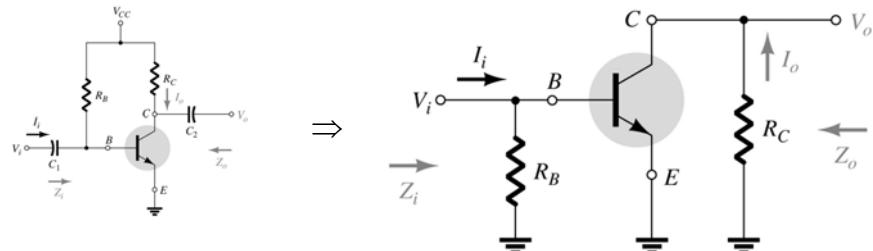
Common-Emitter (CE) Fixed-Bias Configuration



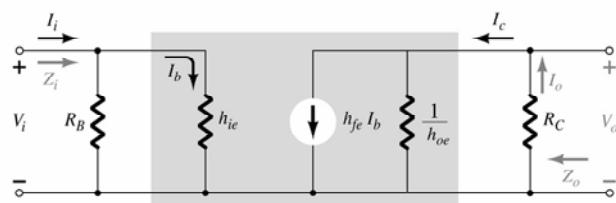
The input (V_i) is applied to the base and the output (V_o) is from the collector.

The Common-Emitter is characterized as having high input impedance and low output impedance with a high voltage and current gain.

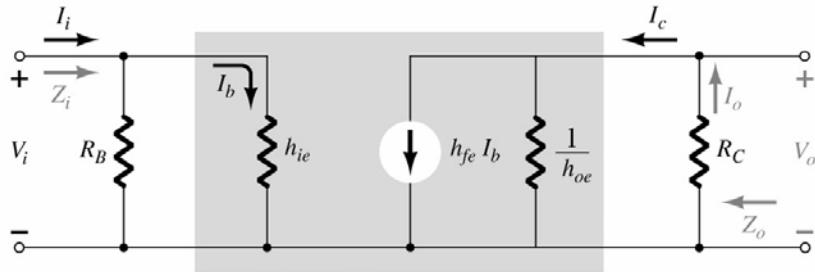
Removing DC effects of V_{CC} and Capacitors



Hybrid Equivalent Circuit



Hybrid Equivalent Circuit

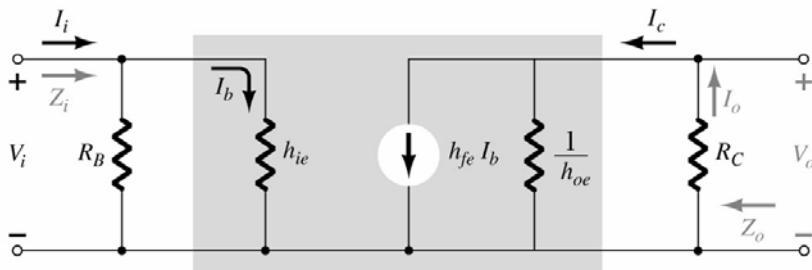


Determine h_{fe} , h_{ie} , and h_{oe} :

h_{fe} and h_{oe} : look in the specification sheet for the transistor or test the transistor using a curve tracer.

h_{ie} : calculate h_{ie} using DC analysis:
$$h_{ie} = \frac{25\text{mV}}{I_{BQ}} \approx h_{fe} \frac{25\text{mV}}{I_{EQ}}$$

Impedance Calculations

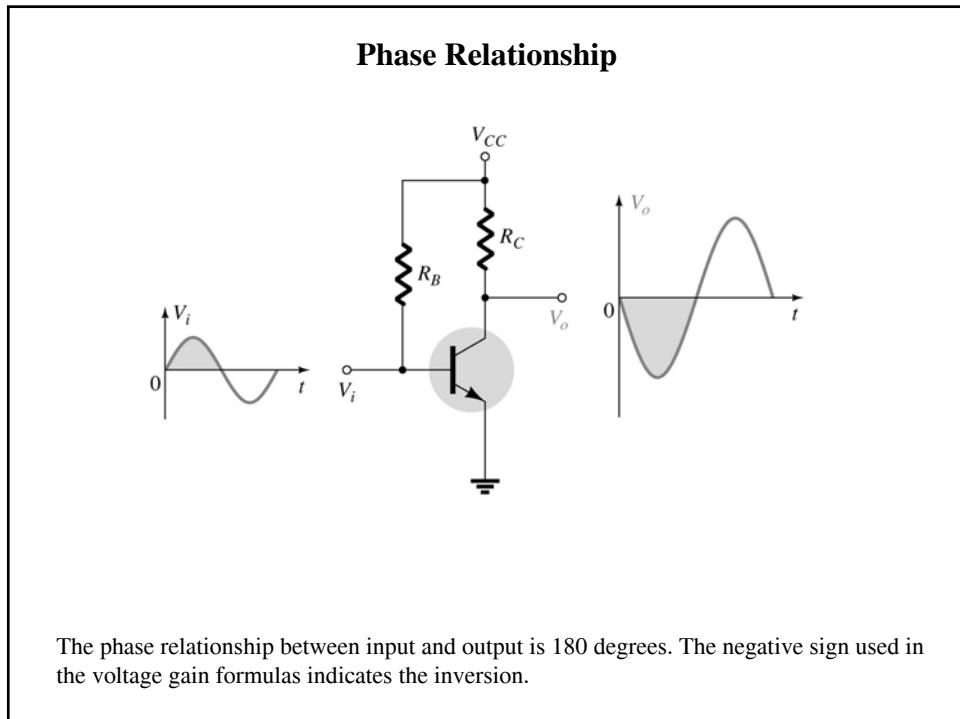
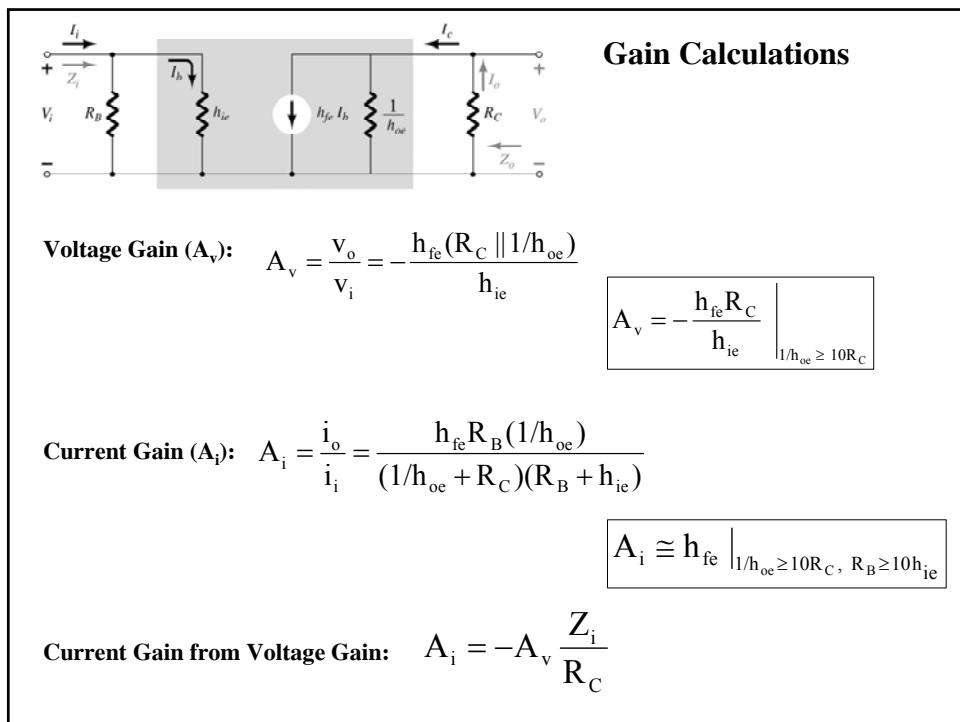


Input Impedance:
$$Z_i = R_B \parallel h_{ie}$$

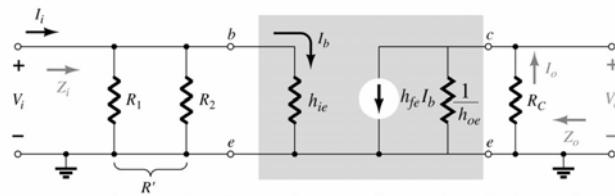
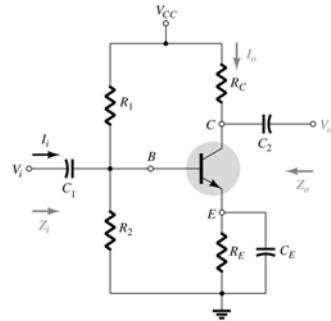
$$Z_i \cong h_{ie} \Big|_{R_B \geq 10h_{ie}}$$

Output Impedance:
$$Z_o = R_C \parallel \frac{1}{h_{oe}}$$

$$Z_o \cong R_C \Big|_{1/h_{oe} \geq 10R_C}$$

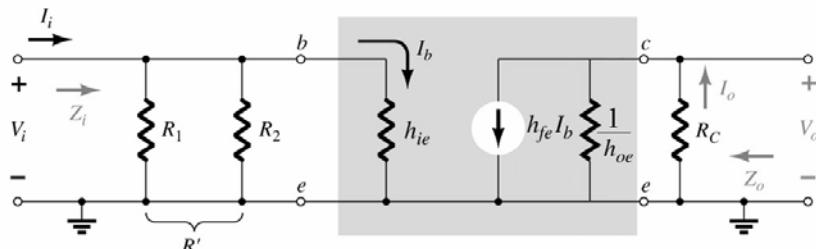


CE – Voltage-Divider Bias Configuration



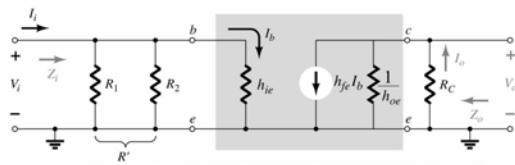
You still need to determine h_{fe} , h_{ie} , and h_{oe} .

Impedance Calculations



Input Impedance: $Z_i = R' \parallel h_{ie}$ $R' = R_1 \parallel R_2 = \frac{R_1 R_2}{R_1 + R_2}$

Output Impedance: $Z_o = R_C \parallel \frac{1}{h_{oe}}$ $Z_o \approx R_C \quad | \frac{1}{h_{oe}} \geq 10R_C$



Gain Calculations

Voltage Gain (A_v): $A_v = \frac{V_o}{V_i} = -h_{fe} \frac{R_C || 1/h_{oe}}{h_{ie}}$

$$A_v \cong -\frac{h_{fe} R_C}{h_{ie}} \quad \left| \begin{array}{l} \\ 1/h_{oe} \geq 10R_C \end{array} \right.$$

Current Gain (A_i): $A_i = \frac{i_o}{i_i} = \frac{h_{fe} R' (1/h_{oe})}{(1/h_{oe} + R_C)(R' + h_{ie})}$

$$A_i \cong \frac{h_{fe} R'}{R' + h_{ie}} \quad \left| \begin{array}{l} \\ 1/h_{oe} \geq 10R_C \end{array} \right.$$

$$A_i \cong h_{fe} \quad \left| \begin{array}{l} \\ 1/h_{oe} \geq 10R_C, R' \geq 10h_{ie} \end{array} \right.$$

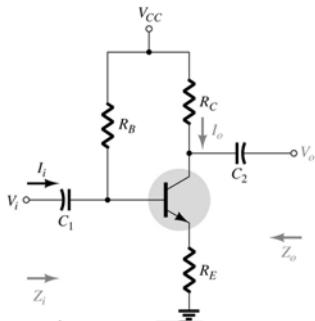
Current Gain from Voltage Gain: $A_i = -A_v \frac{Z_i}{R_C}$

Phase Relationship

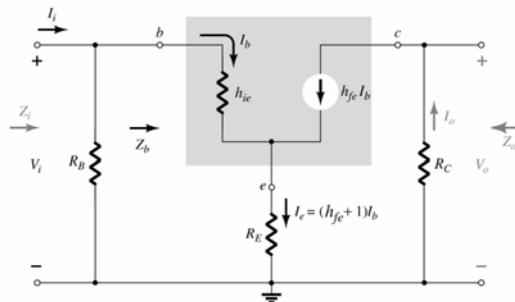
A CE amplifier configuration will always have a phase relationship between input and output is 180 degrees. This is independent of the DC bias.

CE Emitter-Bias Configuration

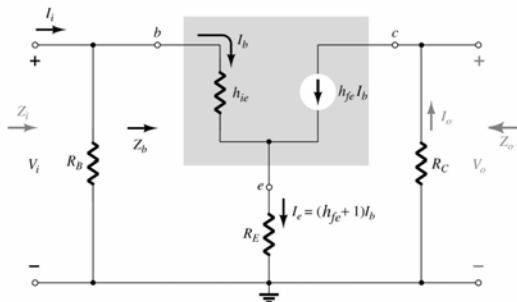
Unbypassed R_E



Again you need to determine h_{fe} , h_{ie} .



Impedance Calculations



Input Impedance:

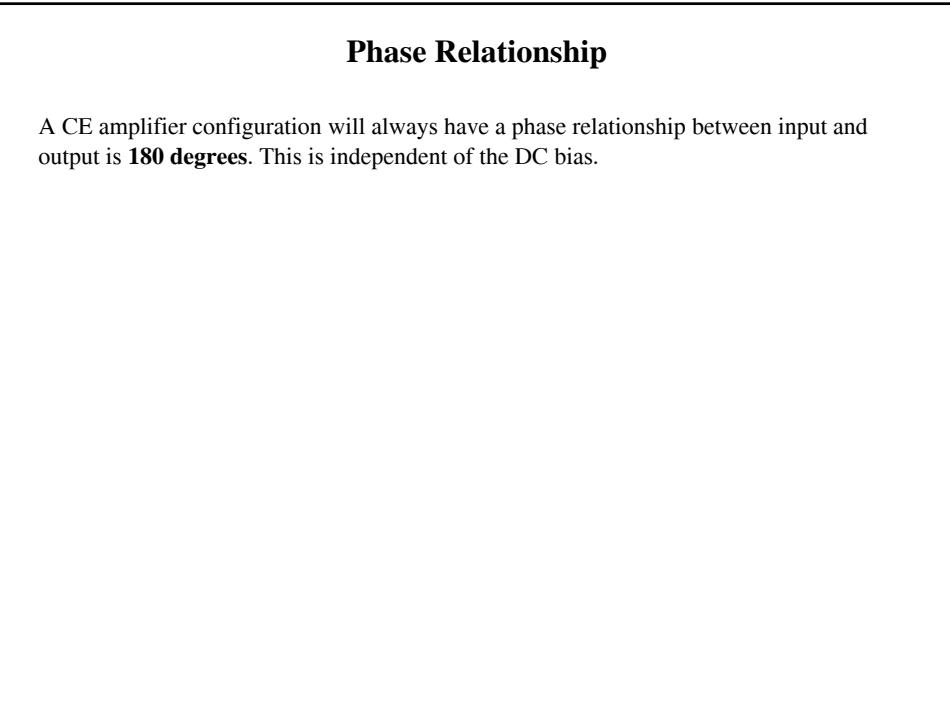
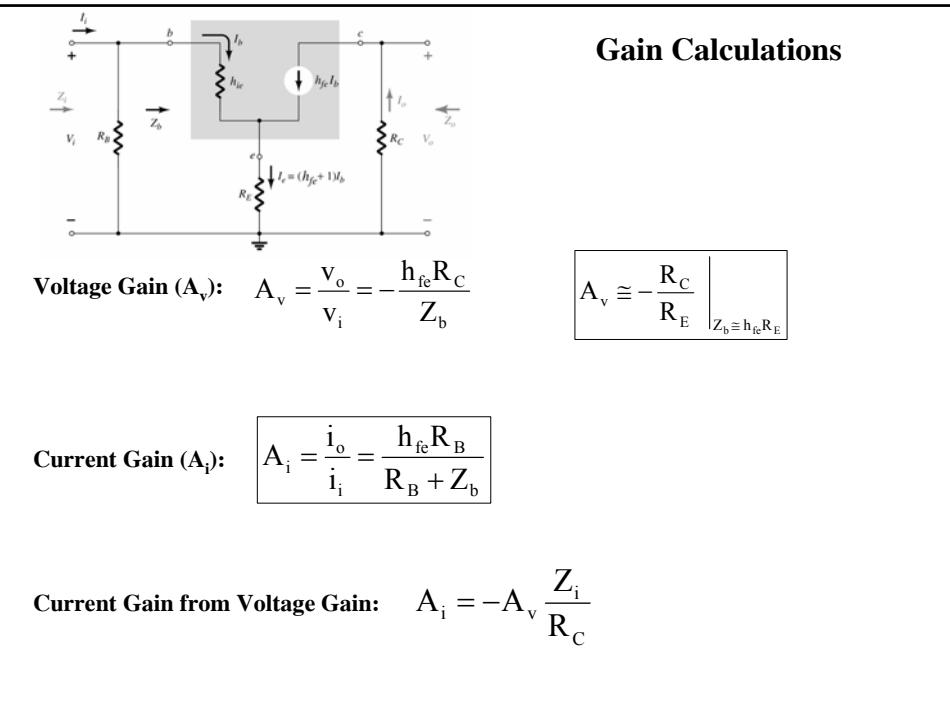
$$Z_i = R_B \parallel Z_b$$

$$Z_b = h_{ie} + (h_{fe} + 1)R_E$$

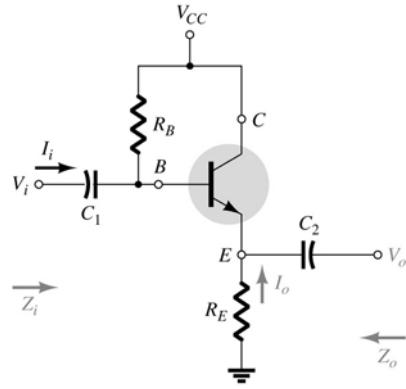
$$Z_b \cong h_{fe}R_E \Big|_{(h_{fe}+1)R_E \gg h_{ie}, h_{fe} \gg 1}$$

Output Impedance:

$$Z_o = R_C$$



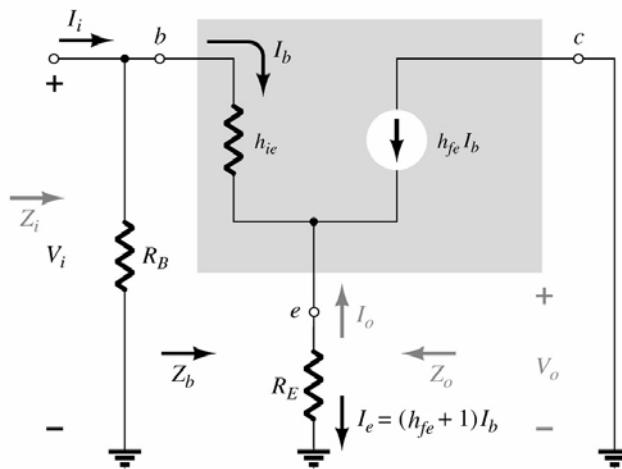
Emitter-Follower Configuration



You may recognize this as the Common-Collector configuration. Indeed they are the same circuit.

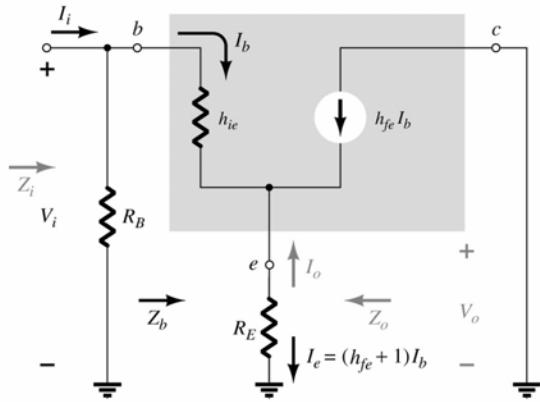
Note the input is on the base and the output is from the emitter.

Hybrid Equivalent Model



You still need to determine h_{fe} and h_{ie} .

Impedance Calculations

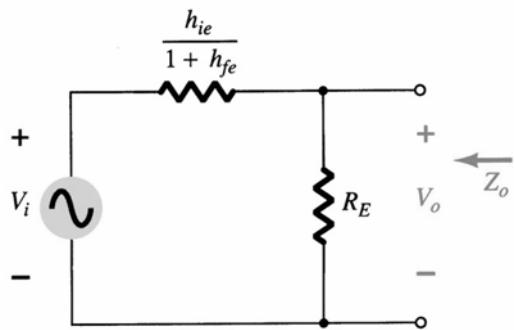


Input Impedance: $Z_i = R_B \parallel Z_b$

$$Z_b = h_{ie} + (h_{fe} + 1)R_E$$

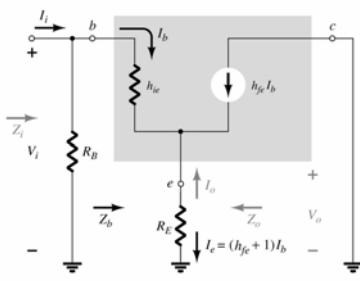
$$Z_b \approx h_{fe} R_E \Big|_{(h_{fe}+1)R_E \gg h_{ie}, h_{fe} \gg 1}$$

Impedance Calculations (cont'd)



Output Impedance: $Z_o = R_E \parallel \frac{h_{ie}}{h_{fe} + 1}$

$$Z_o \approx \frac{h_{ie}}{h_{fe}} \Big|_{(h_{fe}+1)R_E \gg h_{ie}, h_{fe} \gg 1}$$



Gain Calculations

Voltage Gain (A_v): $A_v = \frac{V_o}{V_i} = \frac{R_E}{R_E + h_{ie}/(h_{fe} + 1)}$

$$\boxed{A_v \cong 1 \Big|_{(h_{fe}+1)R_E \gg h_{ie}}}$$

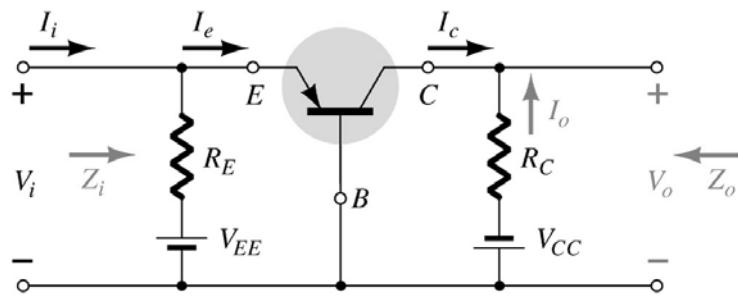
Current Gain (A_i): $A_i \cong \frac{i_o}{i_i} - \frac{h_{fe}R_B}{R_B + Z_b}$

Current Gain from Voltage Gain: $A_i = -A_v \frac{Z_i}{R_E}$

Phase Relationship

A CC amplifier or Emitter Follower configuration has **no phase shift** between input and output.

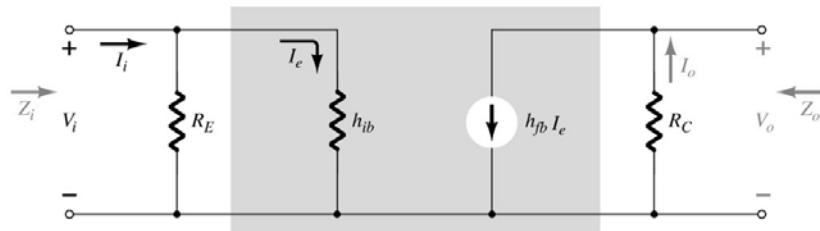
Common-Base (CB) Configuration



The input (V_i) is applied to the emitter and the output (V_o) is from the collector.

The Common-Base is characterized as having low input impedance and high output impedance with a current gain less than 1 and a very high voltage gain.

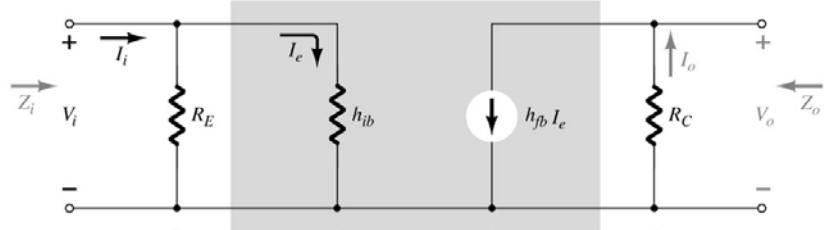
Hybrid Equivalent Model



You will need to determine h_{fb} and h_{ib} .

$$h_{ib} = \frac{h_{ie}}{h_{fe} + 1} = \frac{25\text{mV}}{I_{EQ}} \quad h_{fb} = -\alpha_{ac} \cong -1$$

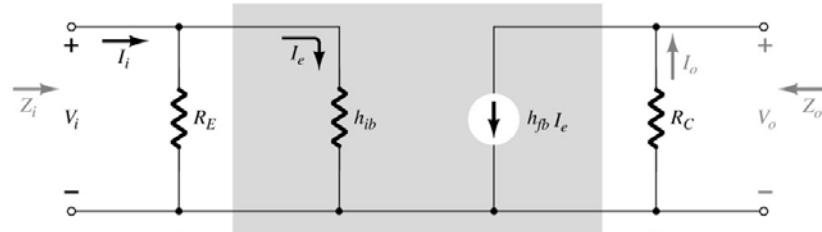
Impedance Calculations



$$\boxed{\text{Input Impedance: } Z_i = R_E \parallel h_{ib}}$$

$$\boxed{\text{Output Impedance: } Z_o = R_C}$$

Gain Calculations



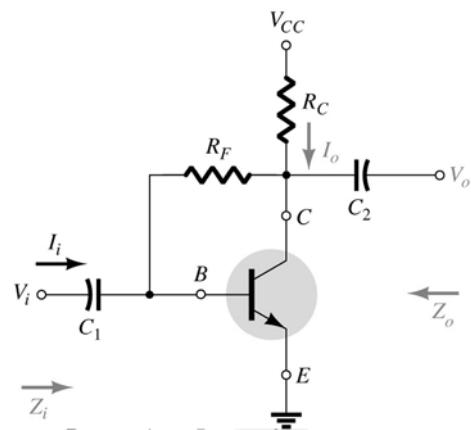
$$\boxed{\text{Voltage Gain (A}_v\text{): } A_v = \frac{V_o}{V_i} = \frac{h_{fb} R_C}{h_{ib}} \cong \frac{R_C}{h_{ib}}}$$

$$\boxed{\text{Current Gain (A}_i\text{): } A_i = \frac{i_o}{i_i} = h_{fb} \cong -1}$$

Phase Relationship

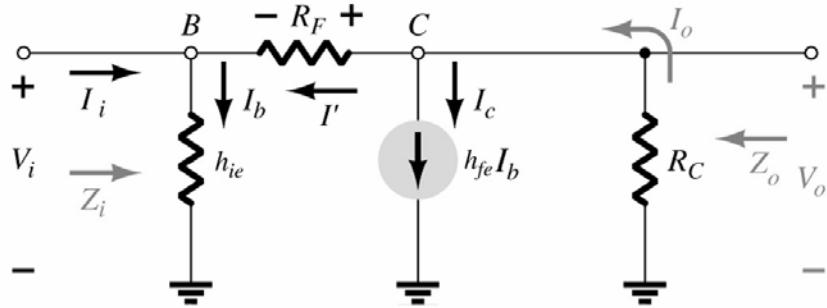
A CB amplifier configuration has **no phase shift** between input and output.

CE Collector Feedback Configuration



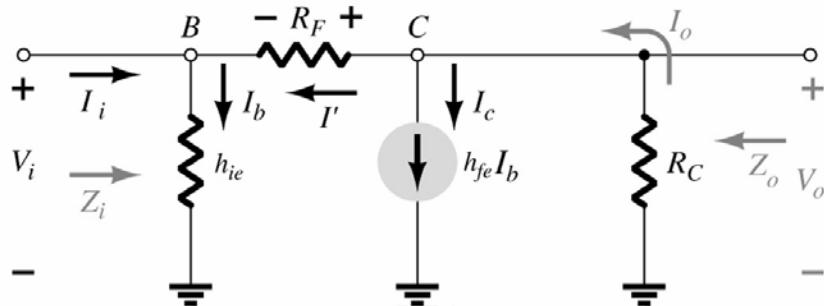
This is a variation of the CE Fixed-Bias configuration.

Hybrid Equivalent Model



You will need to determine h_{fe} and h_{ie} .

Impedance Calculations



Input Impedance:

$$Z_i = \frac{h_{ie}}{1 + h_{fe} \frac{R_C}{R_F}}$$

Output Impedance:

$$Z_o \cong R_C \parallel R_F$$

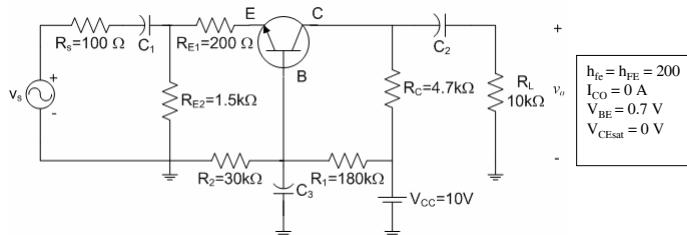
Gain Calculations

Voltage Gain (A_v): $A_v = \frac{V_o}{V_i} = -\frac{h_{fe} R_C}{h_{ie}}$

Current Gain (A_i): $A_i = \frac{I_o}{I_i} = \frac{h_{fe} R_F}{R_F + h_{fe} R_C}$

$$A_i = \frac{I_o}{I_i} \cong \frac{R_F}{R_C}$$

Example



According to the figure above

- Perform DC analysis and find the Q-point.
- Evaluate the voltage gain A_{vs} and the current gain A_i .
- Sketch v_o on the AC+DC load line graph when
 - $v_s = 100 \sin(\omega t) \text{ mV}$.
 - $v_s = 900 \sin(\omega t) \text{ mV}$.

