

Feedback and Poles

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An amplifier having a low-frequency gain of 1000 and poles at 10^4 Hz and 10^5 Hz is operated in a closed negative-feedback loop with a frequency-independent H .

- For what value of H do the closed-loop poles become coincident? At what frequency?
 - What is the low-frequency gain corresponding to the situation in (a)? What is the value of the closed-loop gain at the frequency of the coincident poles?
 - What is the value of Q corresponding to the situation in(a)?
 - If H is increased by a factor of 10, what are the new pole locations? What is the corresponding pole Q ?
- Find $G(s)$

Solution: Given, low frequency Gain and two poles. Therefore, $G(s)$ can be written as..,

$$G(s) = \frac{G_0}{\left(1 + \frac{s}{p_1}\right)\left(1 + \frac{s}{p_2}\right)} \quad (1.1)$$

where the parameters are tabulated in Table 1

Parameter	Value
Low Frequency Gain	1000
Pole 1 (p_1)	10^4 Hz
Pole 2 (p_2)	10^5 Hz

TABLE 1

- For what value of H do the closed-loop poles become coincident? At what frequency?

Solution: The closed loop transfer function is

$$T(s) = \frac{G(s)}{1 + G(s)H} \quad (2.1)$$

$$T(s) = \frac{G_0}{\frac{s^2}{p_1 p_2} + \left(\frac{1}{p_1} + \frac{1}{p_2}\right)s + HG_0 + 1} \quad (2.2)$$

upon substituting from (1.1) and simplifying. For (2.2) to have equal roots,

$$\left(\frac{1}{p_1} + \frac{1}{p_2}\right)^2 = \frac{4}{p_1 p_2} (G_0 H + 1) \quad (2.3)$$

$$\Rightarrow H = \frac{(p_1 - p_2)^2}{4G_0 p_1 p_2} \quad (2.4)$$

$$H = 2.025 \times 10^{-3} \quad (2.5)$$

yielding

$$T(s) = \frac{1000}{2.533 \times 10^{-11} s^2 + 1.750 \times 10^{-5} s + 3.025} \quad (2.6)$$

The following code computes the poles to be at $\omega_p = 345575.1$ rad/sec

codes/ee18btech11036/ee18btech11036_1.py

- Find $T(0)$ and $|T(j\omega_p)|$.

Solution: From 2.6,

$$T(0) = \frac{1000}{3.025} = 50.378 \text{ dB} \quad (3.1)$$

$$|T(j\omega_p)| = 44.3866 \quad (3.2)$$

- Find Q from (2.2).

Solution: If the denominator of (2.2) is expressed as

$$\begin{aligned} \frac{s^2}{p_1 p_2} + \left(\frac{1}{p_1} + \frac{1}{p_2}\right)s + HG_0 + 1 \\ = s^2 + 2\zeta\omega_n s + \omega_n^2 \end{aligned} \quad (4.1)$$

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then

$$\omega_n = \sqrt{(HG_0 + 1) p_1 p_2} \quad (4.2)$$

$$\zeta = \frac{2p_1 p_2}{\sqrt{(HG_0 + 1) p_1 p_2}} \quad (4.3)$$

and

$$Q = \frac{1}{2\zeta} \quad (4.4)$$

$$= \pm \frac{\sqrt{(1 + HG_0) p_1 p_2}}{p_1 + p_2} \quad (4.5)$$

$$= 0.5 \quad (4.6)$$

5. If H is increased by a factor of 10, what are the new pole locations? What is the corresponding pole Q?

Parameter	Value
H	0.002025
Gain (0 freq)	50.378
Gain (pole freq)	44.38
Q	0.5

TABLE 5

Solution: From (2.5),

$$H = 0.02025 \quad (5.1)$$

which, upon substitution in 2.2 yields

$$T(s) = \frac{1000}{2.533 \times 10^{-11} s^2 + 1.750 \times 10^{-5} s + 21.25} \quad (5.2)$$

The new pole locations are given by the following code

```
codes/ee18btech11036/ee18btech11036_3.py
```

and

$$Q = 1.325 \quad (5.3)$$

6. Find the step response of $T(s)$

Solution: The following code generates the desired response in Fig. 6.

```
codes/ee18btech11036/ee18btech11036_4.py
```

7. Design a circuit for $T(s)$ in (2.6).

Solution: A modular approach to make circuit is used here. The first op-amp corresponds to a

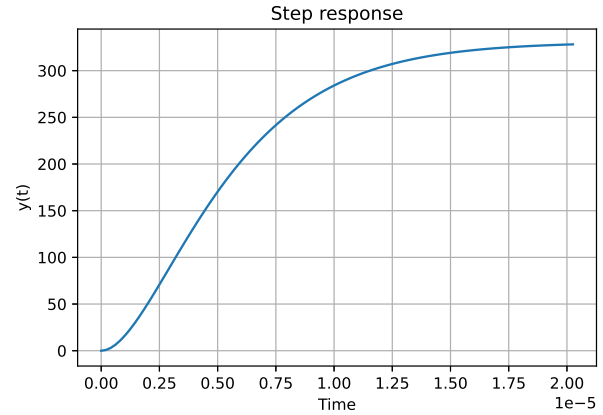


Fig. 6

simple voltage subtractor while the other two correspond to each of the poles p_1 and p_2 . Consider the circuit in Fig. 7.2.

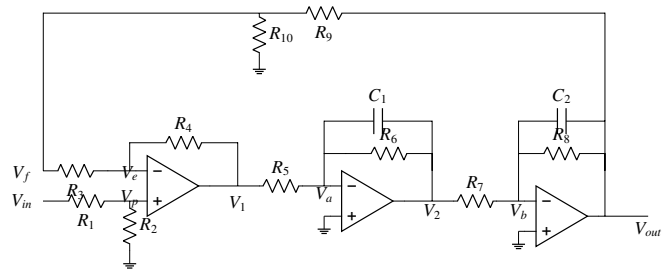


Fig. 7.2

$$T(s) = \frac{R_6 R_8}{(R_5 R_7 (s^2 C_1 C_2 R_6 R_8 + s(C_1 R_6 + C_2 R_8) + 1)) + H R_6 R_8} \quad (7.1)$$

Using parameters from 7 in (7.1), (2.6) is obtained.

Parameter	Value
R_1, R_2, R_3, R_4	$1k\Omega$
R_5, R_7	100Ω
R_6	$10k\Omega$
R_8	$1k\Omega$
R_9	4928Ω
R_{10}	10Ω
C_1, C_2	1.59 nF

TABLE 7

The value of negative feedback gain:

The circuit can be represented as block diagram as shown in Fig. 7.4

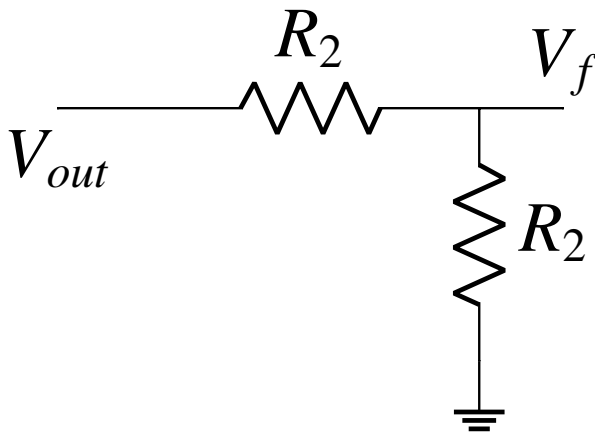


Fig. 7.3

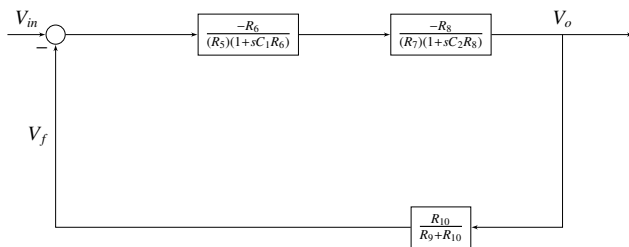


Fig. 7.4

The negative feedback gain :

$$I = \frac{V_{out}}{R_9 + R_{10}} \quad (7.2)$$

$$V_f = IR_{10} \quad (7.3)$$

$$\Rightarrow \frac{V_f}{V_{out}} = \frac{R_{10}}{R_{10} + R_9} \quad (7.4)$$

Solving this block diagram:

$$T(s) = \frac{G(s)}{1 + G(s)H(s)} \quad (7.5)$$

$$T(s) = \frac{\frac{R_6 R_8}{(R_5 R_7)(1+sC_1 R_6)(1+sC_2 R_8)}}{1 + \frac{R_6 R_8}{(R_5 R_7)(1+sC_1 R_6)(sC_2 R_8)} (H)} \quad (7.6)$$

$$\Rightarrow T(s) = \frac{R_6 R_8}{R_5 R_7 (s^2 C_1 C_2 R_6 R_8 + s(C_1 R_6 + C_2 R_8) + 1) + H R_6 R_8} \quad (7.7)$$

Transfer function was found to be same as given in equation 7.1

8. Verify the step response of the output from ngspice simulation.

Solution: The following netlist file does the transient analysis and store the Vout values with respect to time in a dat file.

```
codes/ee18btech11036/spice/ngspice_db.net
```

Following python code is to plot the step response.

```
codes/ee18btech11036/spice/
ee18btech11036_spice.py
```

The step response obtained is shown in Fig. 8. The graph has steady state value equal to 50.3 dB/330 V.

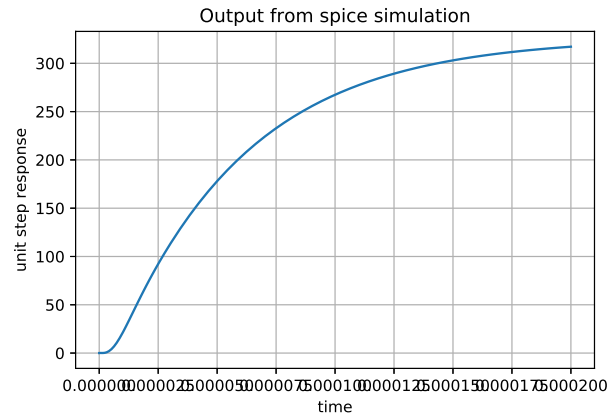


Fig. 8