

Experiment-5

No Load and Blocked Rotor test on 3-phase Induction Motor.

Group Number : 9

200020031,200020042,180020010

AIM:

To determine the equivalent circuit parameters of an induction motor from no load and blocked rotor tests.

MACHINE SPECIFICATIONS:

3 Phase AC squirrel cage induction motor

Rated Voltage- 415 V

Rated Current – 1.6 A

Rated RPM – 15 W

CIRCUIT DIAGRAMS:

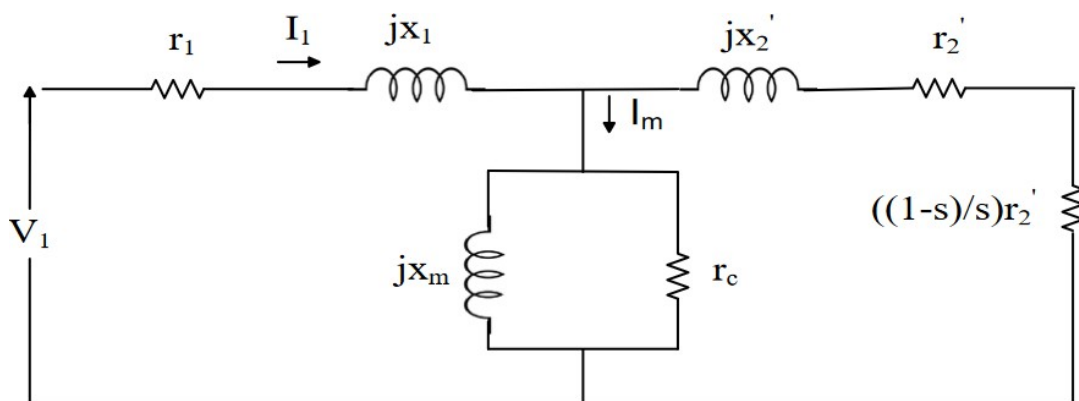
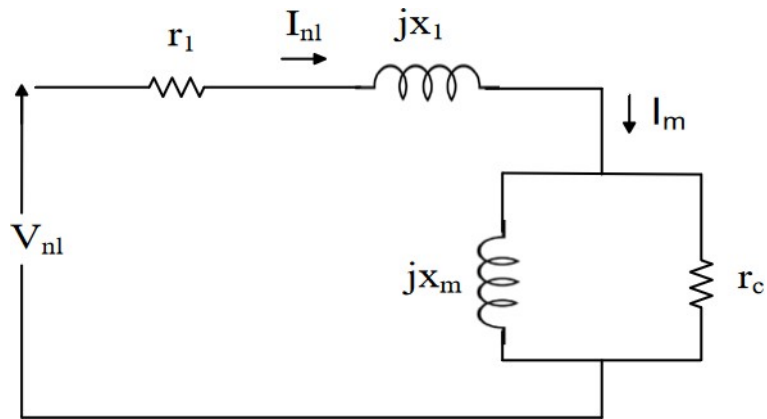
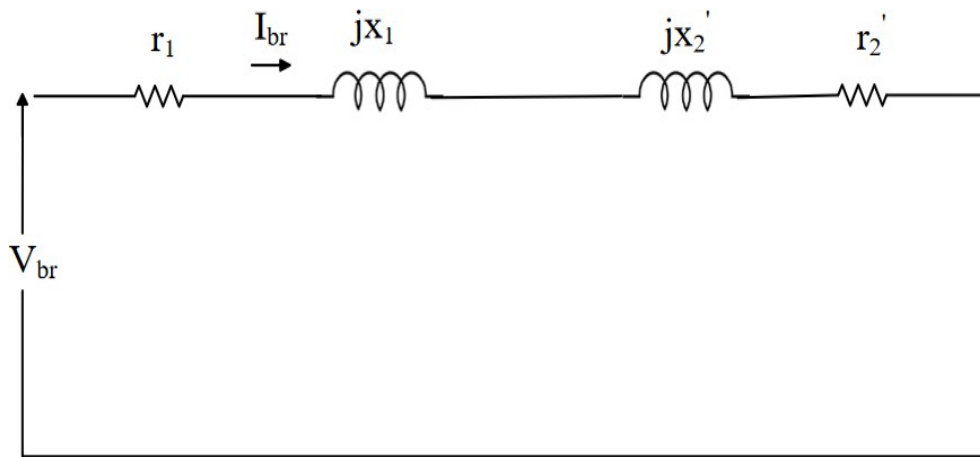


Fig. 1. Per phase equivalent circuit of 3-phase induction motor

No Load Test:



Blocked Rotor Test:



OBSERVATIONS:

No Load Test:

Voltage (V)	Current (A)	Power (KW)	Power (KVA)
414.6	1.309	0.145	0.966 0.955(r)
415.3	1.297		
416.3	1.371		

Blocked Rotor Test:

Voltage (V)	Current (A)	Power (KW)	Power (KVA)
119.6	1.831	0.194	0.379 0.326(r)
119.7	1.806		
121.1	1.846		

CALCULATIONS:

For no-load test:

The no-load test approximates the stator circuit (R_1 and X_1) and magnetization branch parameters (X_m) of an induction machine. The machine is brought to its rated speed by applying rated three phase volt-ages at the stator (V_{nl}). Corresponding no-load current (I_{nl}) and no-load real power input (P_{nl}) are recorded.

When no mechanical load is driven by the machine, slip (s) is a very small value. As a result, referring to Fig.(1), the rotor circuit branch resistance quantity, $R(1-s/s)$ carries a large value. The impedance of rotor circuit branch is thus much higher compared to the magnetization branch impedance and their parallel combination would turn out to be close to jX_m (neglecting core conductance).

R_s is large as compared to X_m

$$Z_{nl} = \frac{V_{nl}}{I_{nl}} = \frac{415}{1.297} = 319.96 \Omega$$

$$R_{nl} = \frac{P_{nl}(r)/3}{I_{nl}^2} = \frac{955/3}{1.297^2} = 189.3 \Omega$$

$$Z_{nl} = \sqrt{R_{nl}^2 + X_{nl}^2}$$

$$X_{nl} = \sqrt{Z_{nl}^2 - R_{nl}^2} = \sqrt{319.96^2 - 189.3^2} = 257.87 \Omega$$

For Blocked - rotor test:

The blocked rotor test is performed to estimate parameters that affect machine's performance under load such as its leakage impedance, similar to the short circuit test done for a transformer. In blocked rotor test, the machine shaft is locked or is prevented from rotating via external means.

With the rated current (I_{br}) flowing in the stator, we note the stator applied voltage (V_{br}) and the power input (P_{br}). It should be noted that the rotor position in blocked state affects the stator voltage (V_{br}) required for setting up I_{br} . Hence, an average calculated over different rotor positions can be taken. Assuming we have the stator circuit parameters R_s ready, the other machine parameters can be calculated as indicated below.

$$Z_{br} = \frac{V_{br}}{I_{br}} = \frac{119.7}{1.806} = 66.28 \Omega$$

$$R_{br} = \frac{P_{br}(r)/3}{I_{br}^2} = \frac{326/3}{1.806^2} = 33.31 \Omega$$

$$X_{br} = \sqrt{Z_{br}^2 - R_{br}^2} = \sqrt{66.28^2 - 33.31^2} = 57.3 \Omega$$

Again, in general, as $X_m \gg X_{r1}$, $\frac{X_2}{X_m}$ can be neglected which yields,

$$X_{br} \approx X_1 + X_2$$

For wound-rotor construction, one can assume that $X_1 \approx X_2$ resulting in

$$X_1 = X_2 = 0.5 \times X_{br} = 28.65 \Omega$$

$$X_m = X_{nl} - X_1$$

$$X_m = 257.87 - 28.65 = 229.22 \Omega$$

$$r_1 = R_{nl} = 189.3 \Omega$$

from network equation, after simplifying we got :

$$r_2 = (R_{nl} - R_{br}) \left(\frac{X_m}{X_2} \right)^2$$

$$r_2 = 9.98 \text{ k}\Omega$$

RESULT:

The parameters for the simplified model of the per-phase equivalent for a three-phase induction motor were calculated to be:

No-Load	Circuit Parameters	Blocked-Rotor
$R_{nl} = 189.30 \, \Omega$	$R_s = 189.30 \, \Omega$	$R_{br} = 33.31 \, \Omega$
$X_{nl} = 257.87 \, \Omega$	$X_1 = 28.65 \, \Omega$	$X_{br} = 57.3 \, \Omega$
$Z_{nl} = 319.96 \, \Omega$	$X_m = 229.22 \, \Omega$	$Z_{br} = 66.28 \, \Omega$