OpenFOAM Manual:

Transient dynamics in outflow of energy from system in nonequilibrium stationary state

Data S1

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The Data S1 Content

The Data set S1 contains:

- eRhoFullFOAM the OpenFOAM solver for solving equations (1);
- eRhoReducedFOAM the OpenFOAM solver for solving equations (2);
- statInitLine the OpenFOAM utility to set stationary state initial conditions;
- fullSolution the 1D case including travelling front;
- reducedSolution the 1D case including diffusive heat transport only;
- shortManual.pdf the short manual explaining the usage of the code

The content was written, used and tested under foam-extend 4.1 distribution.

Installation guide

To install use attached codes it is advised to have the foam-ext-4.1 version of the OpenFOAM. This code has not been tested under other OpenFOAM distributions. Next, to install all components it is sufficient to enter each <folder> (eRhoFullFOAM, eRhoReducedFOAM, statInitLine)

cd <folder>

and execute

wmake

command as for every standard <code>OpenFOAM</code> utility. The place of the installation can be changed by manipulating the content of

<foldr>/Make/files

file.

eRhoFullFOAM

nCorrectors

}

nNonOrthogonalCorrectors <integer>;

The solver eRhoFullFOAM is written to solve mass, momentum and

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\mathbf{v}\rho) = 0, \tag{1a}$$

$$\rho \left[\frac{\partial \mathbf{v}}{\partial t} + \nabla \cdot (\mathbf{v}\mathbf{v}) \right] = -\nabla p - \nabla \cdot \mathbf{\Pi}, \tag{1b}$$

$$\frac{3R}{2M}\frac{\partial\rho T}{\partial t} = -\nabla\cdot\left(\frac{3}{2}\frac{R}{M}\rho T\mathbf{v}\right) - p\nabla\cdot\mathbf{v} - \mathbf{\Pi}:\nabla\mathbf{v} + \kappa\nabla\cdot\nabla T,\tag{1c}$$

$$\mathbf{\Pi} = \frac{2}{3}\mu \left(\nabla \cdot \mathbf{v}\right)\mathbf{I} - \mu \left(\nabla \mathbf{v} + \left(\nabla \mathbf{v}\right)^{\mathrm{T}}\right),\tag{1d}$$

$$p = \rho \frac{RT}{M},\tag{1e}$$

$$u = \frac{3}{2} \frac{RT}{M}.$$
 (1f)

In the above ρ is density, t is time, \mathbf{v} is velocity, p is pressure, $\mathbf{\Pi}$ is dynamic part of stress tensor, R is gas constant, M is molar mass, $\mathbf{\Pi}$ is dynamic part of stress tensor, κ is thermal conductivity, μ is viscosity, \mathbf{I} denotes unit tensor and u is the internal energy per unit mass.

The equations are solved iteratively in a time loop with to deal with the pressure-velocity coupling problem in Navier-Stokes equation

subdictionary in the fvSolution dictionary. For nOuterCorrIons= 1 the solver uses the PISO algorithm for iterative solution of pressure-velocity coupling. In case nOuterCorrIons> 1 the solver uses PIMPLE algorithm.

<integer>;

The solver needs dictionaries thermophysicalProperties and turbulenceProperties specified in the constant folder. These dictionaries contain physical constants necessary for the solution defined in standard OpenFOAM manner. We added only explicit information if the computational domain has closed volume closedVolume inside thermophysicalProperties dictionary, which can be set either to true or false.

eRhoReducedFOAM

The diffusive solution follows reduced set of equations

$$\frac{\partial \left(\int \rho d\mathbf{r} \right)}{\partial t} = 0, \tag{2a}$$

$$\frac{3R}{2M}\frac{\partial\rho T}{\partial t} = \kappa\nabla\cdot\nabla T,\tag{2b}$$

$$p = \rho \frac{RT}{M} \tag{2c}$$

We implemented this solver to be compatible with eRhoPimpleFOAM thus the algorithm looks similar

```
{f for}\ i{=}1\ {f to}\ {f nOuterCorrectors}\ {f do}
  solve energy conservation equation (2b);
  for j=1 to nCorrectors do
    correct pressure for conserved mass (if closedVolume is true) (2a)
    calculate density profile (2c)
  end for
end for
```

The settings in case folder syste/fvSolution dictionary should be set to nOuterCorrectors= 1 and nCorrectors = 1.

statInitLine

To introduce initial state given by

$$T_{\rm st} = T_{\rm eq} + \nabla T x \tag{3a}$$

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$$p_{\rm st} = p_{\rm eq} \frac{\nabla T L}{T_{\rm eq}} \log(1 + \frac{\nabla T L}{T_{\rm eq}}) \tag{3b}$$

$$v = 0 (3c)$$

$$\rho_{\rm st} = \rho_{\rm eq} \frac{\frac{\nabla TL}{T_{\rm eq}}}{\log(1 + \frac{\nabla TL}{T_{\rm eq}})} \frac{1}{(1 + \frac{\nabla TL}{T_{\rm eq}} \frac{x}{L})}.$$
(3d)

First we specify equilibrium state by $p_{\rm eq}$ (p file), $T_{\rm eq}$ (T file) and $\mathbf{v}_{\rm eq} = 0$ (U file) inside 0 folder. The program will calculate ρ_{eq} using values from constant/thermophysicalProperties file automatically. Next, we need to specify the positions and temperatures on the boundaries using the constat/stationaryParameters file

```
<x position of wall 1>;
   <x position of wall 2>;
   <T at wall 1>;
t1
t2 <T at wall 2>;
```

The program will read equilibrium properties, calculate initial values corresponding to the prescribed stationary state having the same total mass as equilibrium state and write them out with _stat suffix in 0 folder.

fullSolution

The folder contains all necessary files to run the full simulation presented in the main paper. It is sufficient to run the

./Allrun

inside the folder. It will mesh geometry, create initial conditions, run the simulation for 2×10^{-6} s, which is sufficient for a front to travel twice the geometry length and finally create easy to visualise files in postProcessing folder.

reducedSolution

The folder contains all necessary files to run the diffusion only simulation presented in the main paper. It is sufficient to run the

./Allrun

inside the folder. It will mesh geometry, create initial conditions, run the simulation for 2×10^{-6} s, which is sufficient for a front to travel twice the geometry length and finally create easy to visualise files in postProcessing folder.