

Data-driven controller design in the Loewner framework

Worshop MACS

Data-driven control and analysis of dynamical systems

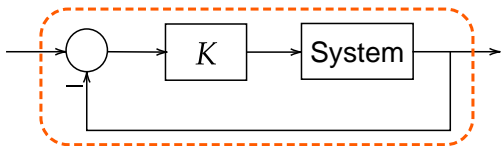
Pauline Kergus

Sept 30th & Oct 1st, 2025

Reference model based data-driven control

Given data from the system P , design K such that the resulting closed-loop is as close as possible to the reference model M

Reference model M



Main techniques:

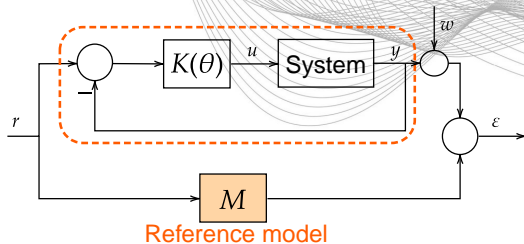
- ▶ Iterative Feedback Tuning (IFT)
- ▶ Correlation-based Tuning (CbT)
- ▶ Virtual Reference Feedback Tuning (VRFT)
- ▶ Loewner Data-Driven Control (L-DDC)

Overview of these methods - CbT and IFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2$$

CbT

$$\varepsilon(s) = \left(M - \frac{PK(\theta)}{1 + PK(\theta)} \right) r(s) + \frac{1}{1 + PK(\theta)} w(s)$$



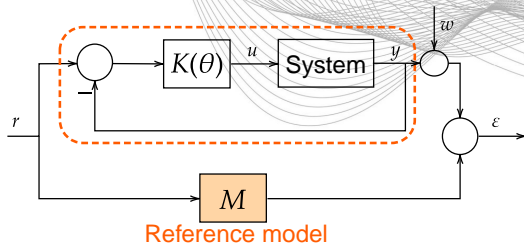
Iterative correlation-based controller tuning, Karimi et al. (2004).

Overview of these methods - CbT and IFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2$$

CbT

$$\varepsilon(s) = \left(M - \frac{PK(\theta)}{1 + PK(\theta)} \right) r(s) + \frac{1}{1 + PK(\theta)} w(s)$$



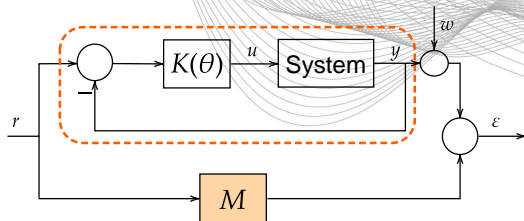
Iterative correlation-based controller tuning, Karimi et al. (2004).

Overview of these methods - CbT and IFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2$$

CbT

$$\varepsilon(s) = \left(M - \frac{PK(\theta)}{1 + PK(\theta)} \right) r(s) + \frac{1}{1 + PK(\theta)} w(s)$$



Reference model

IFT

$$\frac{\partial \varepsilon}{\partial \theta} = \frac{1}{K(\theta)} \frac{\partial K}{\partial \theta} \left(\frac{PK(\theta)}{1 + PK(\theta)} (r - y(\theta)) \right)$$

Iterative correlation-based controller tuning, Karimi et al. (2004).

Iterative feedback tuning: theory and applications, Hjalmarsson et al. (1998).

Overview of these methods - VRFT and L-DDC

VRFT

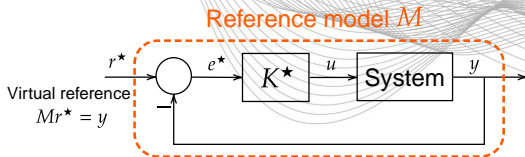
$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2 \rightarrow \min_{\theta} \|u - K(\theta)r^{\star}\|_2^2$$

Virtual reference feedback tuning: a direct method for the design of feedback controllers, Campi et al. (2002).

Overview of these methods - VRFT and L-DDC

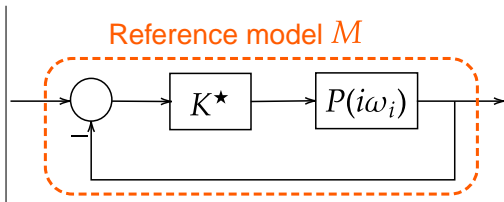
VRFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2 \rightarrow \min_{\theta} \|u - K(\theta)r^*\|_2^2$$



L-DDC

$$\frac{PK^*}{1 + PK^*} = M \rightarrow K(i\omega_i) = K^*(i\omega_i)$$



Virtual reference feedback tuning: a direct method for the design of feedback controllers, Campi et al. (2002).
Interpolation-based irrational model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin (2022).

Discussion

- ▶ These approaches consist in **approximating the ideal controller** K^*

$$\frac{PK^*}{1 + PK^*} = M$$

Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, *IEEE Control Systems Magazine*, 2023

Discussion

- ▶ These approaches consist in **approximating the ideal controller** K^*

$$\frac{PK^*}{1 + PK^*} = M$$

- ▶ There are underlying assumptions that
 - ▶ The ideal controller should be in the controller
 - ▶ The ideal controller gives internal stability

Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, *IEEE Control Systems Magazine*, 2023

Discussion

- ▶ These approaches consist in **approximating the ideal controller** K^*

$$\frac{PK^*}{1 + PK^*} = M$$

- ▶ There are underlying assumptions that
 - ▶ The ideal controller should be in the controller
 - ▶ The ideal controller gives internal stability
- ▶ Choose wisely the reference model!

Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, *IEEE Control Systems Magazine*, 2023

Discussion

- ▶ These approaches consist in **approximating the ideal controller** K^*

$$\frac{PK^*}{1 + PK^*} = M$$

- ▶ There are underlying assumptions that
 - ▶ The ideal controller should be in the controller
 - ▶ The ideal controller gives internal stability
- ▶ Choose wisely the reference model!
- ▶ All the presented methods (CbT, IFT, VRFT, L-DDC) are strongly linked to system identification

So why not go with models?

Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, IEEE Control Systems Magazine, 2023

Discussion

- ▶ These approaches consist in **approximating the ideal controller** K^*

$$\frac{PK^*}{1 + PK^*} = M$$

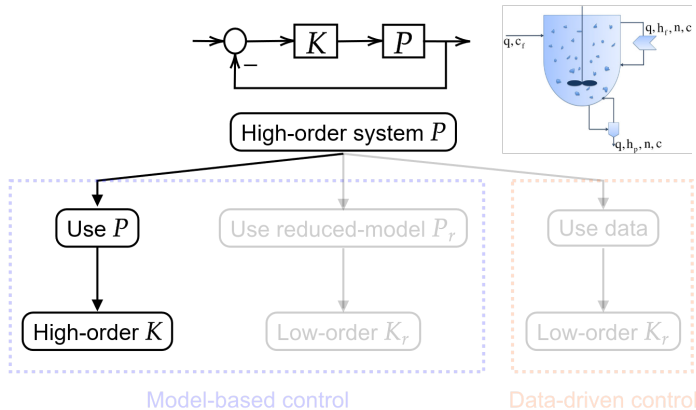
- ▶ There are underlying assumptions that
 - ▶ The ideal controller should be in the controller
 - ▶ The ideal controller gives internal stability
- ▶ Choose wisely the reference model!
- ▶ All the presented methods (CbT, IFT, VRFT, L-DDC) are strongly linked to system identification

So why not go with models?

- ▶ Overcoming complexity (high dimension, non-linearities, uncertainty)

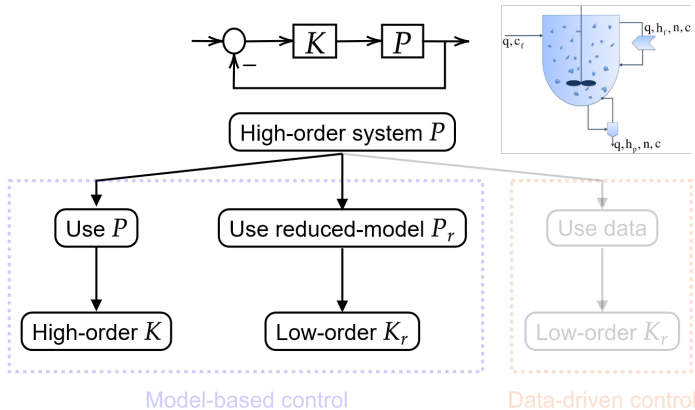
Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, *IEEE Control Systems Magazine*, 2023

Application to infinite dimensional systems



¹ Robust control of infinite dimensional systems: frequency-domain methods, Foias, Ozbya, Tannenbaum, 1969

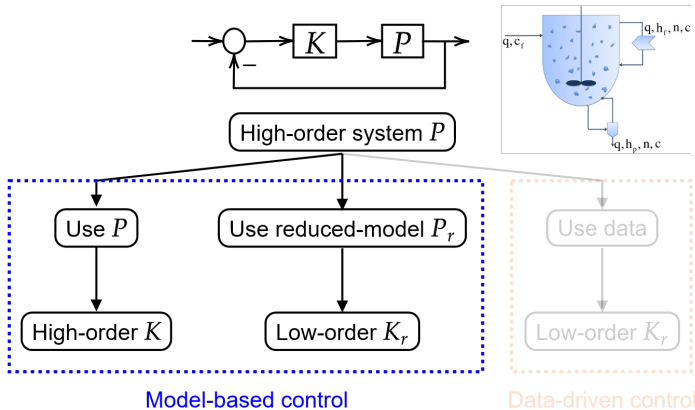
Application to infinite dimensional systems



¹ *Robust control of infinite dimensional systems: frequency-domain methods*, Foias, Ozbya, Tannenbaum, 1969

² *Control of systems governed by partial differential equations*, Morris, Levine, *The control theory handbook*, 2010.

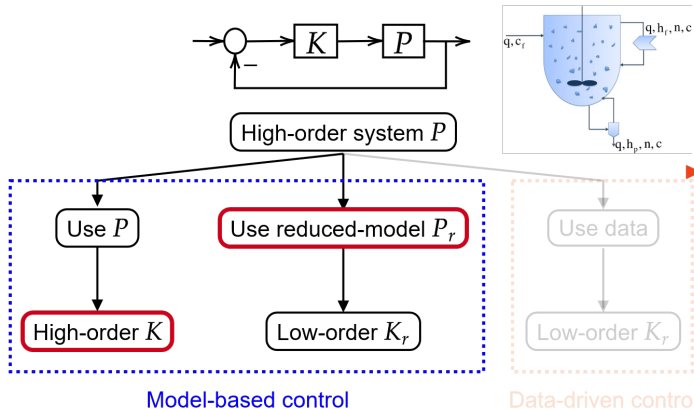
Application to infinite dimensional systems



¹ *Robust control of infinite dimensional systems: frequency-domain methods*, Foias, Ozbya, Tannenbaum, 1969

² *Control of systems governed by partial differential equations*, Morris, Levine, *The control theory handbook*, 2010.

Application to infinite dimensional systems

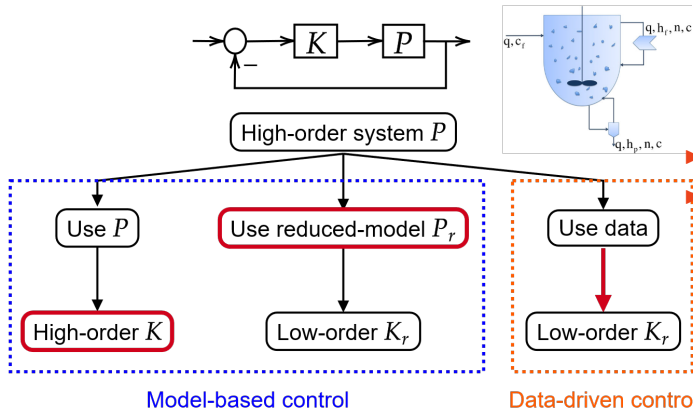


► Model Order Reduction is essential

¹ *Robust control of infinite dimensional systems: frequency-domain methods*, Foias, Ozbya, Tannenbaum, 1969

² *Control of systems governed by partial differential equations*, Morris, Levine, *The control theory handbook*, 2010.

Application to infinite dimensional systems



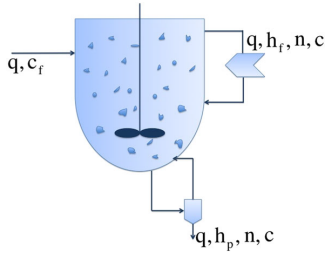
Model Order Reduction is essential
and it can also be used for
data-driven control.

¹ Robust control of infinite dimensional systems: frequency-domain methods, Foias, Ozbya, Tannenbaum, 1969

² Control of systems governed by partial differential equations, Morris, Levine, The control theory handbook, 2010.

³ From reference model selection to controller validation: Application to Loewner Data-Driven Control, Kergus, Olivi, Poussot-Vassal, Demourant, IEEE Control Systems Letters, 2019.

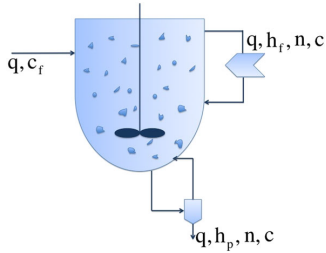
Case study: the continuous crystallizer



► **Goal:** stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$

1. *A mathematical model for continuous crystallization*, Rachah, Noll, Espitalier, Baillon, *Mathematical Methods in the Applied Sciences*, 2016.
2. *\mathcal{H}_∞ -Control of a continuous crystallizer*, Vollmer, Raisch, *Control Engineering Practice*, 2001.
3. *Structured \mathcal{H}_∞ -control of infinite dimensional systems*, Apkarian, Noll, *International Journal of Robust and Nonlinear Control*, 2018.

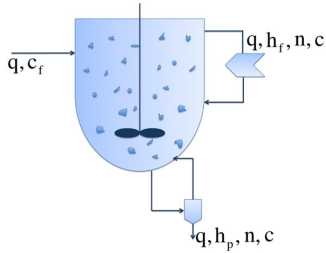
Case study: the continuous crystallizer



- ▶ **Goal:** stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$
- ▶ Unstable system and sustained oscillations

-
1. *A mathematical model for continuous crystallization*, Rachah, Noll, Espitalier, Baillon, *Mathematical Methods in the Applied Sciences*, 2016.
 2. *\mathcal{H}_∞ -Control of a continuous crystallizer*, Vollmer, Raisch, *Control Engineering Practice*, 2001.
 3. *Structured \mathcal{H}_∞ -control of infinite dimensional systems*, Apkarian, Noll, *International Journal of Robust and Nonlinear Control*, 2018.

Case study: the continuous crystallizer

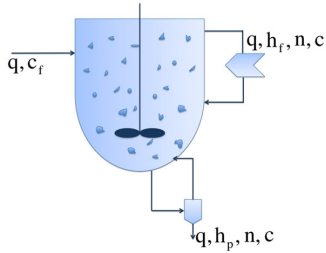


- ▶ **Goal:** stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$
- ▶ Unstable system and sustained oscillations
- ▶ Linearization of the PDEs around c_{ss}

$$P(s) = \frac{\Delta c(s)}{\Delta c_f(s)} = \frac{p_{12}(s)}{p_{13}(s) + q_{12}(s)e^{-s k_f} + r_{12}(s)e^{-s k_p}}$$

-
1. *A mathematical model for continuous crystallization*, Rachah, Noll, Espitalier, Baillon, *Mathematical Methods in the Applied Sciences*, 2016.
 2. *\mathcal{H}_∞ -Control of a continuous crystallizer*, Vollmer, Raisch, *Control Engineering Practice*, 2001.
 3. *Structured \mathcal{H}_∞ -control of infinite dimensional systems*, Apkarian, Noll, *International Journal of Robust and Nonlinear Control*, 2018.

Case study: the continuous crystallizer



- ▶ **Goal:** stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$
- ▶ Unstable system and sustained oscillations
- ▶ Linearization of the PDEs around c_{ss}

$$P(s) = \frac{\Delta c(s)}{\Delta c_f(s)} = \frac{p_{12}(s)}{p_{13}(s) + q_{12}(s)e^{-s k_f} + r_{12}(s)e^{-s k_p}}$$

→ Frequency-domain data easily accessible

$N = 500$ frequencies, logspaced between 10^{-3} and 1 rad.s^{-1}

-
1. *A mathematical model for continuous crystallization*, Rachah, Noll, Espitalier, Baillon, *Mathematical Methods in the Applied Sciences*, 2016.
 2. *\mathcal{H}_∞ -Control of a continuous crystallizer*, Vollmer, Raisch, *Control Engineering Practice*, 2001.
 3. *Structured \mathcal{H}_∞ -control of infinite dimensional systems*, Apkarian, Noll, *International Journal of Robust and Nonlinear Control*, 2018.

L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \boxed{\begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}}$$

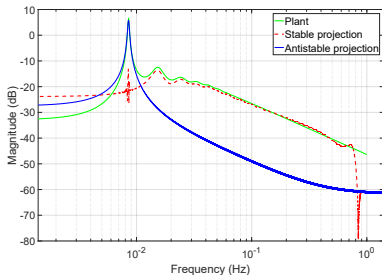
Is the system stable or unstable? non-minimum phase or not?

L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \boxed{\begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}}$$

Is the system stable or unstable? non-minimum phase or not?

$$\begin{aligned} \mathbf{P}(j\omega) &= \mathbf{P}_s(j\omega) + \mathbf{P}_{as}(j\omega) \\ \mathcal{L}_2 &= \mathcal{H}_2 \oplus \mathcal{H}_2^\perp \end{aligned}$$



Achievable performance of multivariable systems with unstable zeros and poles, Havre, Skogestad, *International Journal of Control*, 2001.

Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018.

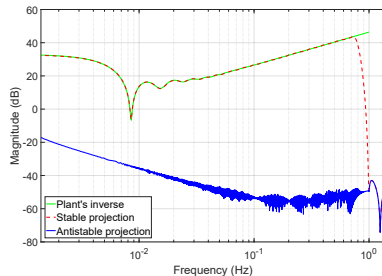
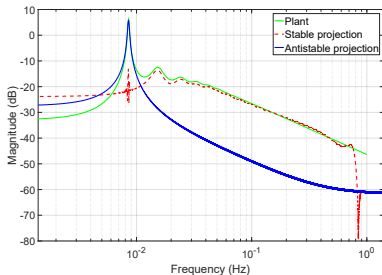
L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}$$

Is the system stable or unstable? non-minimum phase or not?

$$\begin{aligned} \mathbf{P}(j\omega) &= \mathbf{P}_s(j\omega) + \mathbf{P}_{as}(j\omega) \\ \mathcal{L}_2 &= \mathcal{H}_2 \oplus \mathcal{H}_2^\perp \end{aligned}$$

$$\mathbf{P}^{-1}(j\omega) = \mathbf{P}_s^{-1}(j\omega) + \mathbf{P}_{as}^{-1}(j\omega)$$



Achievable performance of multivariable systems with unstable zeros and poles, Havre, Skogestad, *International Journal of Control*, 2001.

Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018.

L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j} \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \boxed{\begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}}$$

Where are the system's instabilities?

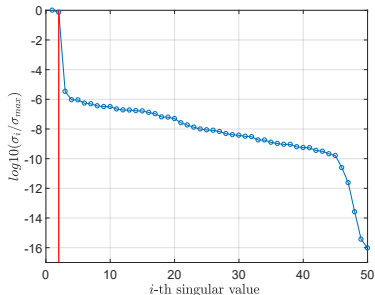
L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}$$

Where are the system's instabilities?

$$\begin{aligned} \mathbf{P}(j\omega) &= \mathbf{P}_s(j\omega) + \mathbf{P}_{as}(j\omega) \\ \mathcal{L}_2 &= \mathcal{H}_2 \oplus \mathcal{H}_2^\perp \end{aligned}$$

Principal Hankel Component analysis on P_{as}



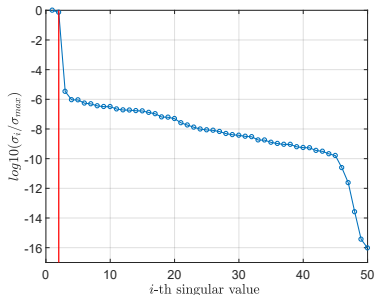
L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}$$

Where are the system's instabilities?

$$\begin{aligned} \mathbf{P}(j\omega) &= \mathbf{P}_s(j\omega) + \mathbf{P}_{as}(j\omega) \\ \mathcal{L}_2 &= \mathcal{H}_2 \oplus \mathcal{H}_2^\perp \end{aligned}$$

Principal Hankel Component analysis on P_{as}



- ▶ Estimated RHP poles :
 $1.07 \times 10^{-4} \pm 0.852 \times 10^{-2}j$
- ▶ RHP poles (direct search):
 $0.99 \times 10^{-4} \pm 0.89 \times 10^{-2}j$

L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \boxed{\begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}}$$

How to choose the reference model accordingly?

$$M_{init}(s) = \frac{1}{1 + \tau s}, \quad \tau = 1s$$

$$\boxed{M = 1 - (1 - M_{init})B_p}$$

$$B_p(s) = \prod_{j=1}^{n_p} \frac{s - p_j}{s + p_j}$$

$$\forall j = 1 \dots n_p, \quad B_p(p_j) = 0$$

$$\forall \omega, \quad |B_p(j\omega)| = 1$$

Interlude: the Loewner framework

Find \mathbf{g} such that $\begin{cases} \mathbf{g}(\lambda_j) = \mathbf{w}_j, & j = 1, \dots, k \\ \mathbf{g}(\mu_i) = \mathbf{v}_i, & i = 1, \dots, q \end{cases}$

Lagrangian form

$$\mathbf{g}(s) = \frac{\sum_{j=1}^{k_1} \frac{c_j \mathbf{w}_j}{s - \lambda_j}}{\sum_{j=1}^{k_1} \frac{c_j}{s - \lambda_j}}$$

Interlude: the Loewner framework

Find \mathbf{g} such that $\begin{cases} \mathbf{g}(\lambda_j) = \mathbf{w}_j, & j = 1, \dots, k \\ \mathbf{g}(\mu_i) = \mathbf{v}_i, & i = 1, \dots, q \end{cases}$

Lagrangian form

$$\mathbf{g}(s) = \frac{\sum_{j=1}^{k_1} \frac{c_j \mathbf{w}_j}{s - \lambda_j}}{\sum_{j=1}^{k_1} \frac{c_j}{s - \lambda_j}}$$

Loewner matrix

$$\begin{aligned} \mathbb{L} &\in \mathbb{C}^{q \times k} \\ (\mathbb{L})_{i,j} &= \frac{\mathbf{v}_i - \mathbf{w}_j}{\mu_i - \lambda_j} \end{aligned}$$

Null space

$$\text{span}(\mathbf{c}) = \mathcal{N}(\mathbb{L})$$

$$\mathbf{c} = \begin{bmatrix} c_1 \\ c_2 \\ \vdots \\ c_{k_1} \end{bmatrix} \in \mathbb{C}^{k_1}$$

Interlude: the Loewner framework

$$\begin{cases} \mathbf{E}\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u \\ y = \mathbf{C}\mathbf{x} \end{cases}$$

$$\mathbf{H}(s) = \mathbf{C}(s\mathbf{E} - \mathbf{A})^{-1}\mathbf{B}$$

Objective: Find $(\hat{\mathbf{E}}, \hat{\mathbf{A}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$ such that for a set of interpolation points $\{s_k\}$

$$\forall i, \hat{\mathbf{H}}(\lambda_i)\mathbf{r}_i = \mathbf{w}_i$$

$$\forall j, \mathbf{l}_j\hat{\mathbf{H}}(\mu_j) = \mathbf{v}_j$$

Interlude: the Loewner framework

$$\begin{cases} \mathbf{E}\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u \\ y = \mathbf{C}\mathbf{x} \end{cases}$$

$$\mathbf{H}(s) = \mathbf{C}(s\mathbf{E} - \mathbf{A})^{-1}\mathbf{B}$$

Objective: Find $(\hat{\mathbf{E}}, \hat{\mathbf{A}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$ such that for a set of interpolation points $\{s_k\}$

$$\forall i, \hat{\mathbf{H}}(\lambda_i)\mathbf{r}_i = \mathbf{w}_i$$

$$\forall j, \mathbf{l}_j\hat{\mathbf{H}}(\mu_j) = \mathbf{v}_j$$

- ▶ \mathbb{L} , \mathbb{L}_s , \mathbf{V} and \mathbf{W} are data matrices
- ▶ Model order reduction based on SVD of the pencil $(\mathbb{L}, \mathbb{L}_s)$

$$(\mathbb{L})_{i,j} = \frac{\mathbf{v}_i\mathbf{r}_i - \mathbf{l}_j\mathbf{w}_j}{\mu_i - \lambda_j} \quad (\mathbb{L}_s)_{i,j} = \frac{\mu_i\mathbf{v}_i\mathbf{r}_i - \lambda_j\mathbf{l}_j\mathbf{w}_j}{\mu_i - \lambda_j}$$

$$\begin{cases} -\mathbb{L}\dot{\tilde{\mathbf{x}}} = -\mathbb{L}_s\tilde{\mathbf{x}} + \mathbf{V}u \\ \tilde{y} = \mathbf{W}\tilde{\mathbf{x}} \end{cases}$$

Interlude: the Loewner framework

$$\begin{cases} \mathbf{E}\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u \\ y = \mathbf{C}\mathbf{x} \end{cases}$$

$$\mathbf{H}(s) = \mathbf{C}(s\mathbf{E} - \mathbf{A})^{-1}\mathbf{B}$$

Objective: Find $(\hat{\mathbf{E}}, \hat{\mathbf{A}}, \hat{\mathbf{B}}, \hat{\mathbf{C}})$ such that for a set of interpolation points $\{s_k\}$

$$\forall i, \hat{\mathbf{H}}(\lambda_i)\mathbf{r}_i = \mathbf{w}_i$$

$$\forall j, \mathbf{l}_j\hat{\mathbf{H}}(\mu_j) = \mathbf{v}_j$$

- ▶ $\mathbb{L}, \mathbb{L}_s, \mathbf{V}$ and \mathbf{W} are data matrices
- ▶ Model order reduction based on SVD of the pencil $(\mathbb{L}, \mathbb{L}_s)$

$$(\mathbb{L})_{i,j} = \frac{\mathbf{v}_i\mathbf{r}_i - \mathbf{l}_j\mathbf{w}_j}{\mu_i - \lambda_j} \quad (\mathbb{L}_s)_{i,j} = \frac{\mu_i\mathbf{v}_i\mathbf{r}_i - \lambda_j\mathbf{l}_j\mathbf{w}_j}{\mu_i - \lambda_j}$$

- ▶ Factorization in terms of the tangential generalized controllability \mathcal{R} and observability \mathcal{O} matrices:

$$\mathbb{L} = -\mathcal{O}\mathbf{E}\mathcal{R} \quad \mathbb{L}_s = -\mathcal{O}\mathbf{A}\mathcal{R} \quad \mathbf{V} = \mathbf{C}\mathcal{R} \quad \mathbf{W} = \mathcal{O}\mathbf{B}$$

$$\mathbf{A}\mathcal{R} + \mathbf{B}\mathcal{R} = \mathbf{E}\mathcal{R}\Lambda \quad \mathcal{O}\mathbf{A} + \mathbf{L}\mathcal{C} = \mathbf{M}\mathcal{O}\mathbf{E}$$

LDDC Step 2: Controller identification and reduction

Objective: obtain a rational model $\mathbf{K} = (E, A, B, C, D)$ such that:

$$\forall i = 1 \dots N, \mathbf{K}(j\omega_i) = \mathbf{K}^*(j\omega_i) = \frac{M(j\omega_i)}{P(j\omega_i)(1 - M(j\omega_i))}.$$

LDDC Step 2: Controller identification and reduction

Objective: obtain a rational model $\mathbf{K} = (E, A, B, C, D)$ such that:

$$\forall i = 1 \dots N, \mathbf{K}(j\omega_i) = \mathbf{K}^*(j\omega_i) = \frac{M(j\omega_i)}{P(j\omega_i)(1 - M(j\omega_i))}.$$

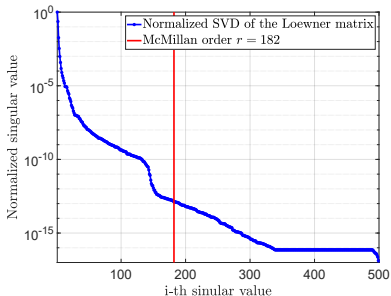


Figure: SVD of \mathbb{L} .

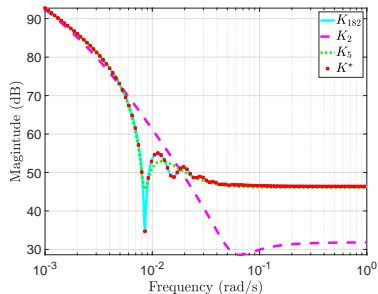
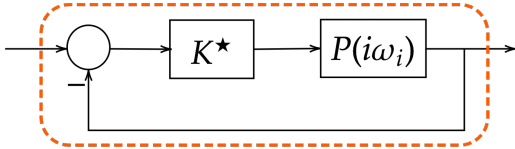


Figure: Obtained controllers.

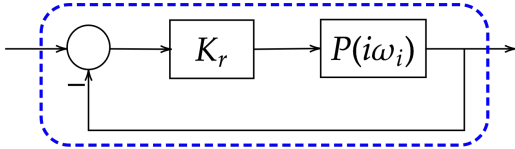
LDDC Step 3: Closed-loop stability analysis

Reference model M



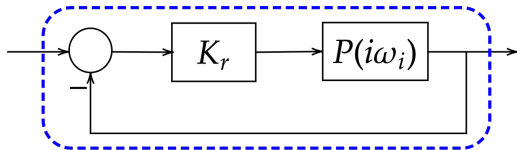
LDDC Step 3: Closed-loop stability analysis

Resulting closed-loop

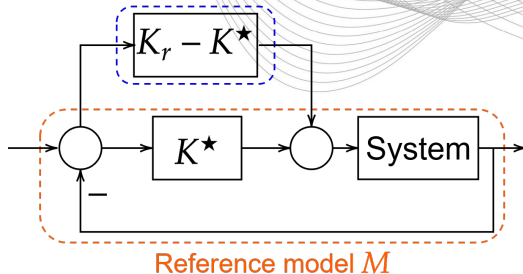


LDDC Step 3: Closed-loop stability analysis

Resulting closed-loop



Controller modelling error Δ



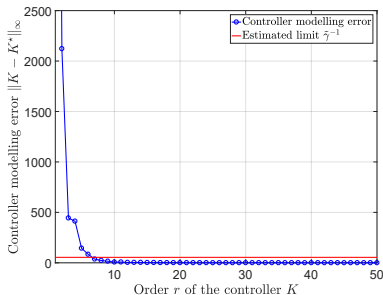
Application of the small-gain theorem

The closed-loop is well-posed and internally stable for all stable $\Delta = K - K^*$ such that $\|\Delta\|_\infty \leq \beta$ if and only if $\|(1 - \mathbf{M})\mathbf{P}\|_\infty < \frac{1}{\beta}$

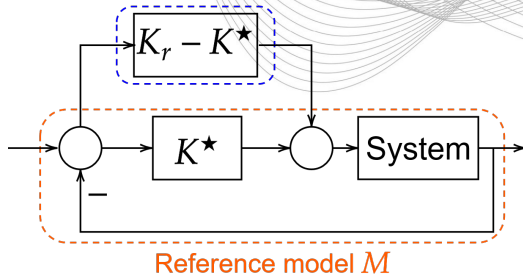
→ Limiting the controller modelling error allows to ensure closed-loop internal stability!

Data-driven controller validation, Van Heusden, Karimi, Bonvin, IFAC Proceedings, 2009.

LDDC Step 3: Closed-loop stability analysis



Controller modelling error Δ



Application of the small-gain theorem

The closed-loop is well-posed and internally stable for all stable $\Delta = K - K^*$ such that $\|\Delta\|_\infty \leq \beta$ if and only if $\|(1 - \mathbf{M})\mathbf{P}\|_\infty < \frac{1}{\beta}$

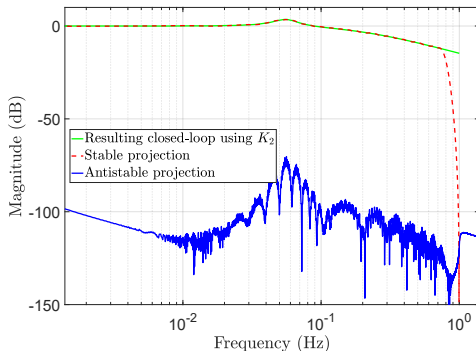
→ Limiting the controller modelling error allows to ensure closed-loop internal stability!

Data-driven controller validation, Van Heusden, Karimi, Bonvin, *IFAC Proceedings*, 2009.

Alternative closed-loop stability analysis

$$H(j\omega_i) = \frac{P(j\omega_i)K_r(j\omega_i)}{1 + P(j\omega_i)K_r(j\omega_i)}$$

1st option

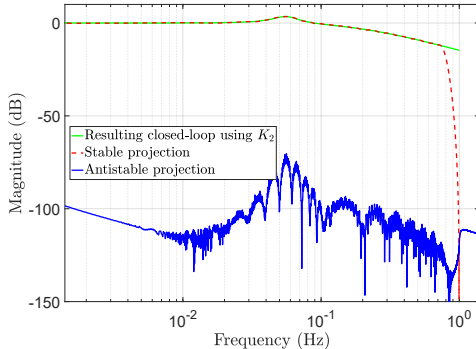


Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

Alternative closed-loop stability analysis

$$H(j\omega_i) = \frac{P(j\omega_i)K_r(j\omega_i)}{1 + P(j\omega_i)K_r(j\omega_i)}$$

1st option



2nd option

1. Loewner interpolation: $\hat{H}(j\omega_i) = H(j\omega_i)$

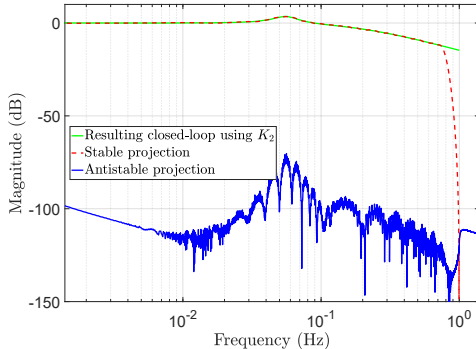
Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

Interpolation-based infinite dimensional model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin, chapter to appear.

Alternative closed-loop stability analysis

$$H(j\omega_i) = \frac{P(j\omega_i)K_r(j\omega_i)}{1 + P(j\omega_i)K_r(j\omega_i)}$$

1st option



2nd option

1. Loewner interpolation: $\hat{H}(j\omega_i) = H(j\omega_i)$
2. Stable projection on \mathcal{RH}_∞ :

$$\hat{H}_s = \arg \min_{H \in \mathbb{S}_{n,n_i,n_o}^+} \|H - \hat{H}\|_\infty$$

Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

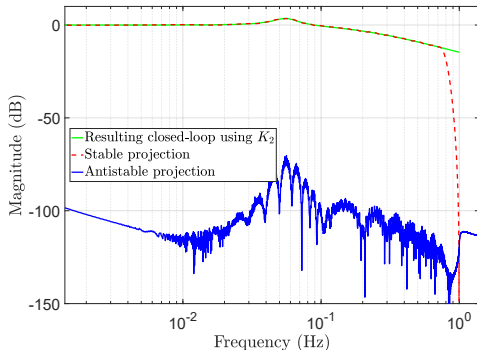
Interpolation-based infinite dimensional model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin, chapter to appear.

On the closest stable descriptor system in the respective spaces \mathcal{RH}_2 and \mathcal{RH}_∞ , Köhler, *Linear Algebra and its Applications*, 2014.

Alternative closed-loop stability analysis

$$H(j\omega_i) = \frac{P(j\omega_i)K_r(j\omega_i)}{1 + P(j\omega_i)K_r(j\omega_i)}$$

1st option



2nd option

1. Loewner interpolation: $\hat{H}(j\omega_i) = H(j\omega_i)$
2. Stable projection on \mathcal{RH}_∞ :

$$\hat{H}_s = \arg \min_{H \in \mathbb{S}_{n,n_i,n_o}^+} \|H - \hat{H}\|_\infty$$
3. Stability index $S = \|\hat{H}_s - \hat{H}\|_\infty$

$$S = 4.3511 \cdot 10^{-6}$$

Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

Interpolation-based infinite dimensional model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin, chapter to appear.

On the closest stable descriptor system in the respective spaces \mathcal{RH}_2 and \mathcal{RH}_∞ , Köhler, *Linear Algebra and its Applications*, 2014.

Results

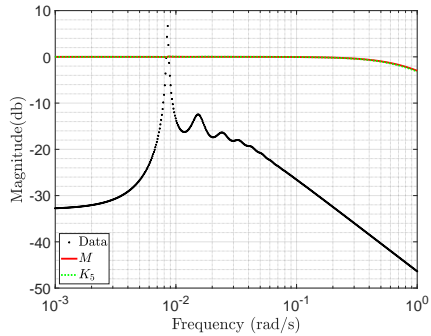


Figure: Closed-loop transfer functions.

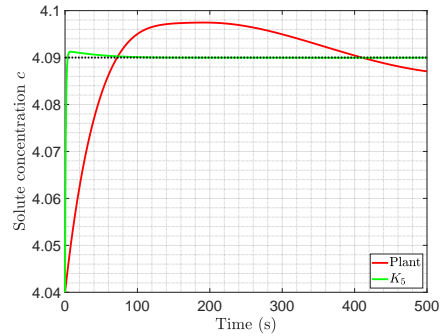


Figure: Time-domain simulation.

Results

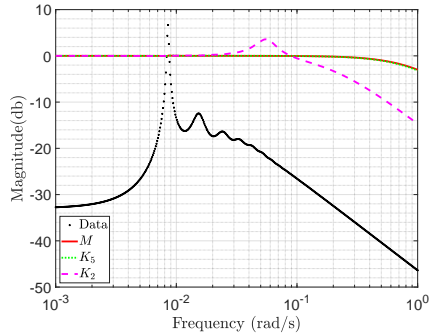


Figure: Closed-loop transfer functions.

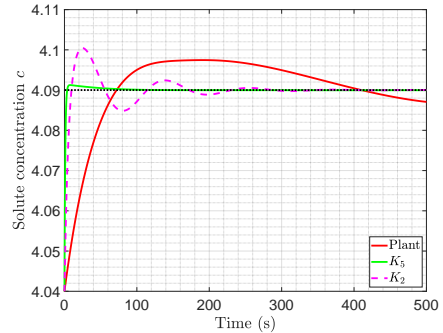


Figure: Time-domain simulation.

⇒ Impact of the **complexity-accuracy trade-off**

Results

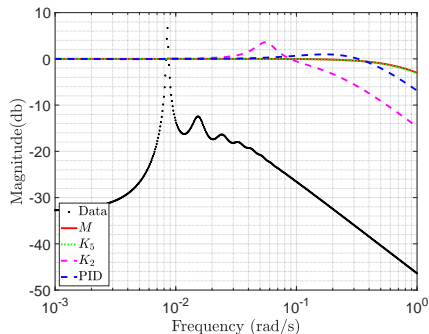


Figure: Closed-loop transfer functions.

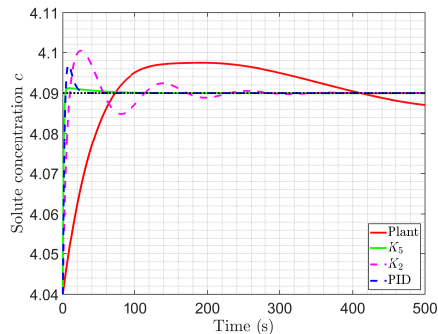


Figure: Time-domain simulation.

⇒ Impact of the **complexity-accuracy trade-off**

→ Impact of the reference model (comparison with a robust PID)

Results

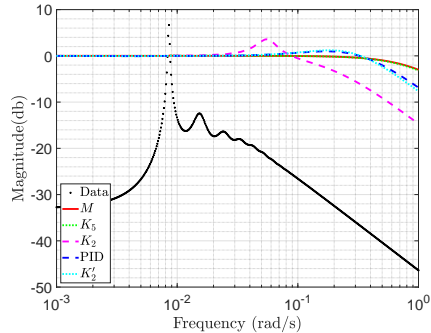


Figure: Closed-loop transfer functions.

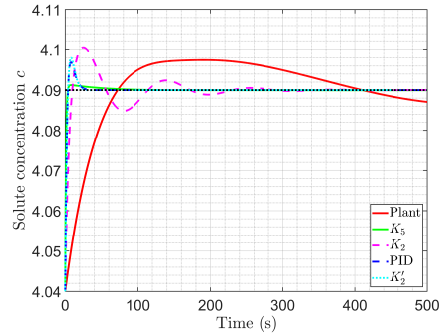
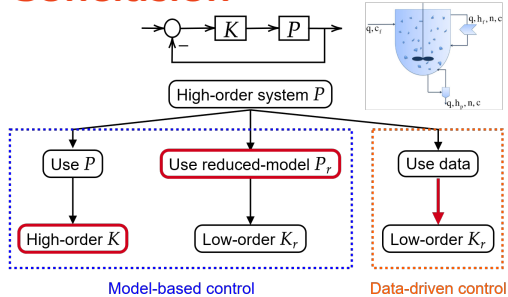


Figure: Time-domain simulation.

⇒ Impact of the **complexity-accuracy trade-off**

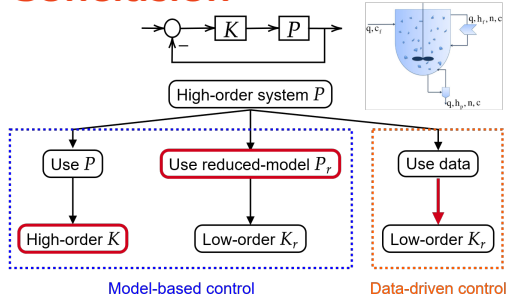
→ Impact of the reference model (comparison with a robust PID)

Conclusion



The Loewner framework can be used as a central tool for the control of infinite dimensional transfer functions.

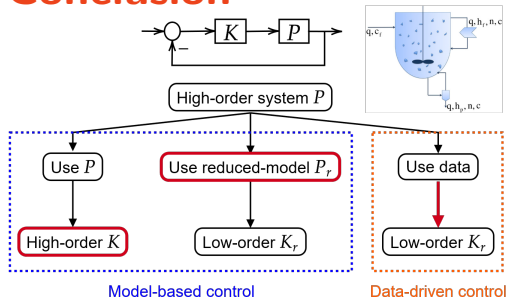
Conclusion



The Loewner framework can be used as a central tool for the control of infinite dimensional transfer functions.

	Model-based design	L-DDC
Method	more steps	direct
Controller structure	fixed order/poles	linear
Specifications	flexible (robust)	not flexible (only stability)
Stability guarantees	for P_r	conservative or not embedded

Conclusion



The Loewner framework can be used as a central tool for the control of infinite dimensional transfer functions.

Extension to other types of systems?

	Model-based design	L-DDC
Method	more steps	direct
Controller structure	fixed order/poles	linear
Specifications	flexible (robust)	not flexible (only stability)
Stability guarantees	for P_r	conservative or not embedded