

Data-driven controller design in the Loewner framework

Worshop MACS

Data-driven control and analysis of dynamical systems

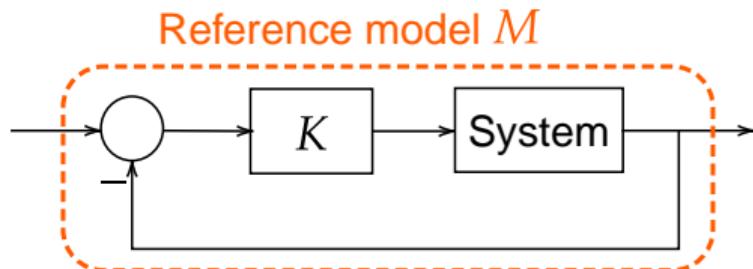
Pauline Kergus

Sept 30th & Oct 1st, 2025



Reference model based data-driven control

Given data from the system P , design K such that the resulting closed-loop is as close as possible to the reference model M



Main techniques:

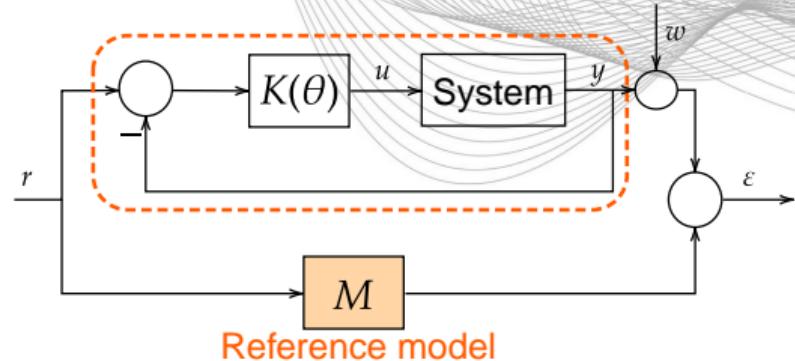
- ▶ Iterative Feedback Tuning (IFT)
- ▶ Correlation-based Tuning (CbT)
- ▶ Virtual Reference Feedback Tuning (VRFT)
- ▶ Loewner Data-Driven Control (L-DDC)

Overview of these methods - CbT and IFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2$$

CbT

$$\varepsilon(s) = \left(M - \frac{PK(\theta)}{1 + PK(\theta)} \right) r(s) + \frac{1}{1 + PK(\theta)} w(s)$$



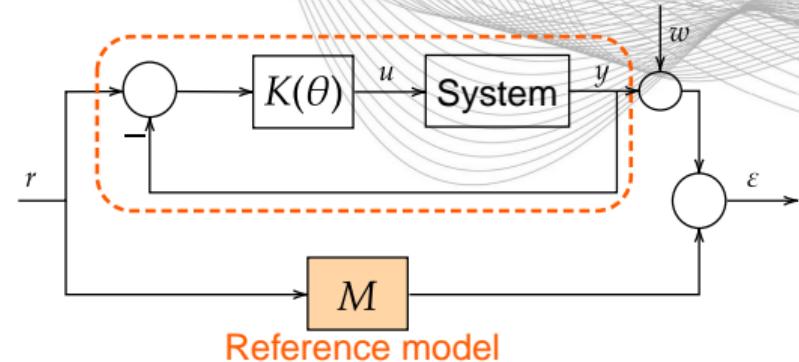
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Reference model

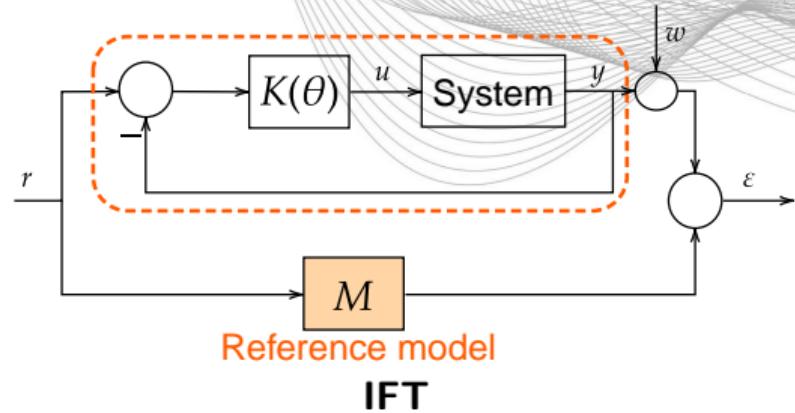
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IFT

$$\frac{\partial \varepsilon}{\partial \theta} = \frac{1}{K(\theta)} \frac{\partial K}{\partial \theta} \left(\frac{PK(\theta)}{1 + PK(\theta)} (r - y(\theta)) \right)$$

Iterative correlation-based controller tuning, Karimi et al. (2004).

Iterative feedback tuning: theory and applications, Hjalmarsson et al. (1998).

Overview of these methods - VRFT and L-DDC

VRFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2 \rightarrow \min_{\theta} \|u - K(\theta)r^{\star}\|_2^2$$

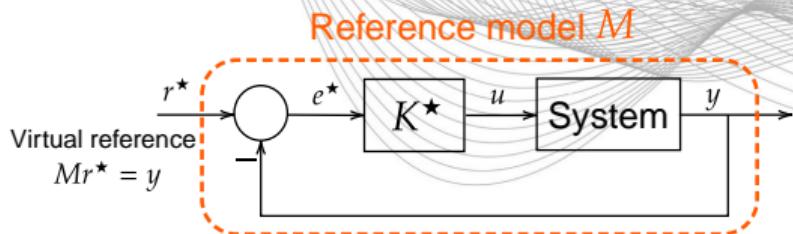


Virtual reference feedback tuning: a direct method for the design of feedback controllers, Campi et al. (2002).

Overview of these methods - VRFT and L-DDC

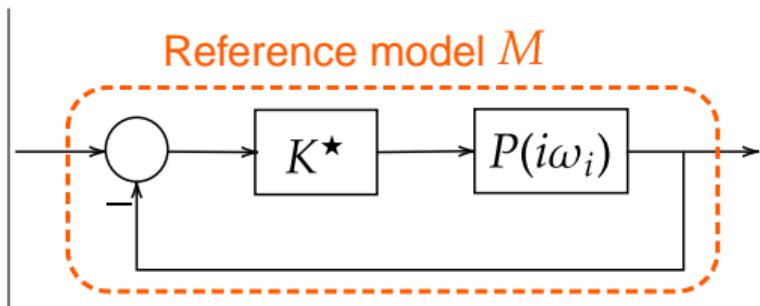
VRFT

$$\min_{\theta} \left\| \frac{PK(\theta)}{1 + PK(\theta)} - M \right\|_2^2 \rightarrow \min_{\theta} \|u - K(\theta)r^*\|_2^2$$



L-DDC

$$\frac{PK^*}{1 + PK^*} = M \rightarrow K(\omega_i) = K^*(\omega_i)$$

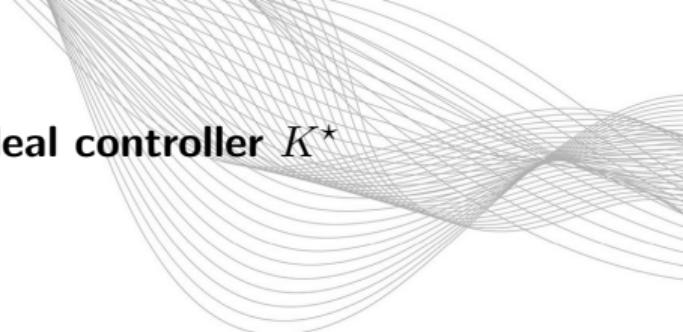


Virtual reference feedback tuning: a direct method for the design of feedback controllers, Campi et al. (2002).
Interpolation-based irrational model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin (2022).

Discussion

- ▶ These approaches consist in **approximating the ideal controller K^***

$$\frac{PK^*}{1 + PK^*} = M$$



Data-Driven Control: Part Two of Two: Hot Take: Why not go with Models?, F. Dörfler, IEEE Control Systems Magazine, 2023

Discussion

- ▶ These approaches consist in **approximating the ideal controller K^***

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- ▶ There are underlying assumptions that
 - ▶ The ideal controller should be in the controller
 - ▶ The ideal controller gives internal stability

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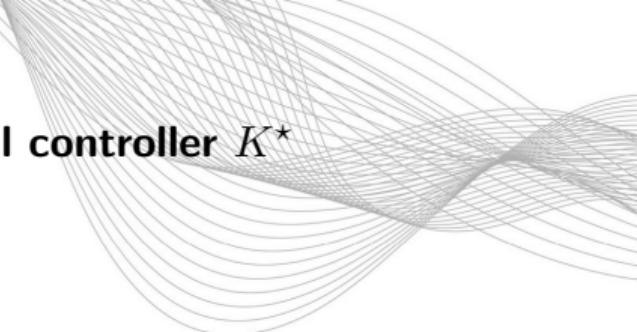
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- ▶ Choose wisely the reference model!

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- ▶ There are underlying assumptions that
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 - ▶ The ideal controller gives internal stability
- ▶ Choose wisely the reference model!
- ▶ All the presented methods (CbT, IFT, VRFT, L-DDC) are strongly linked to system identification

So why not go with models?

Discussion

- ▶ These approaches consist in **approximating the ideal controller K^***

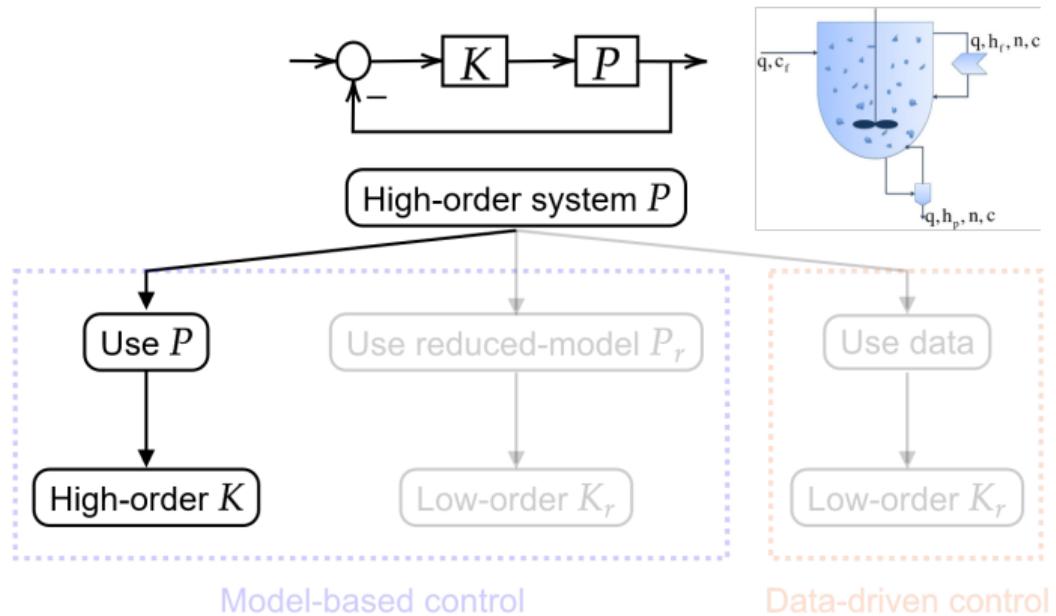
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So why not go with models?

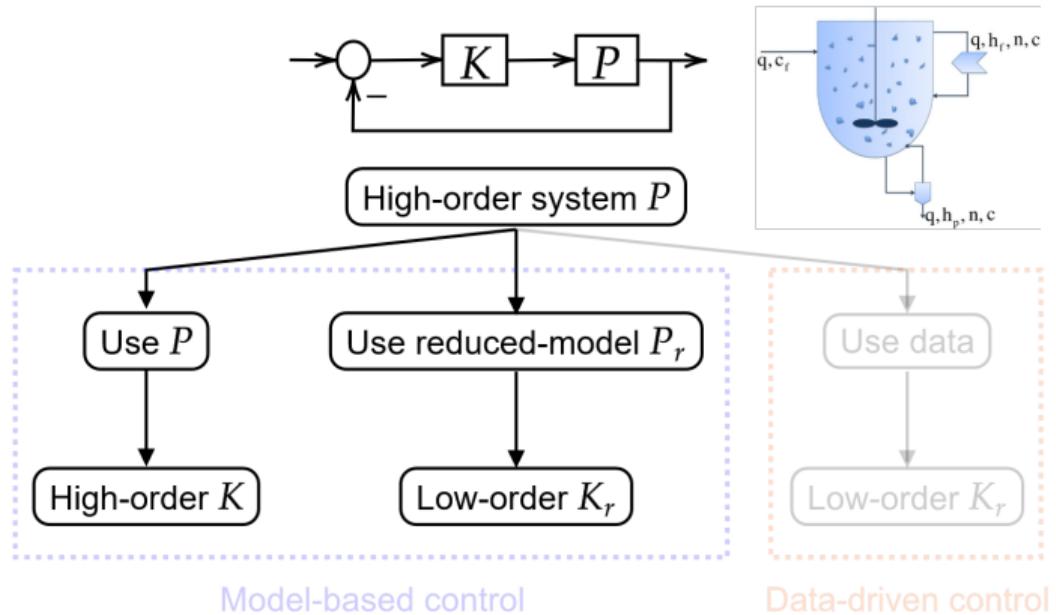
- ▶ Overcoming complexity (high dimension, non-linearities, uncertainty)

Application to infinite dimensional systems



¹ Robust control of infinite dimensional systems: frequency-domain methods, Foias, Ozbya, Tannenbaum, 1969

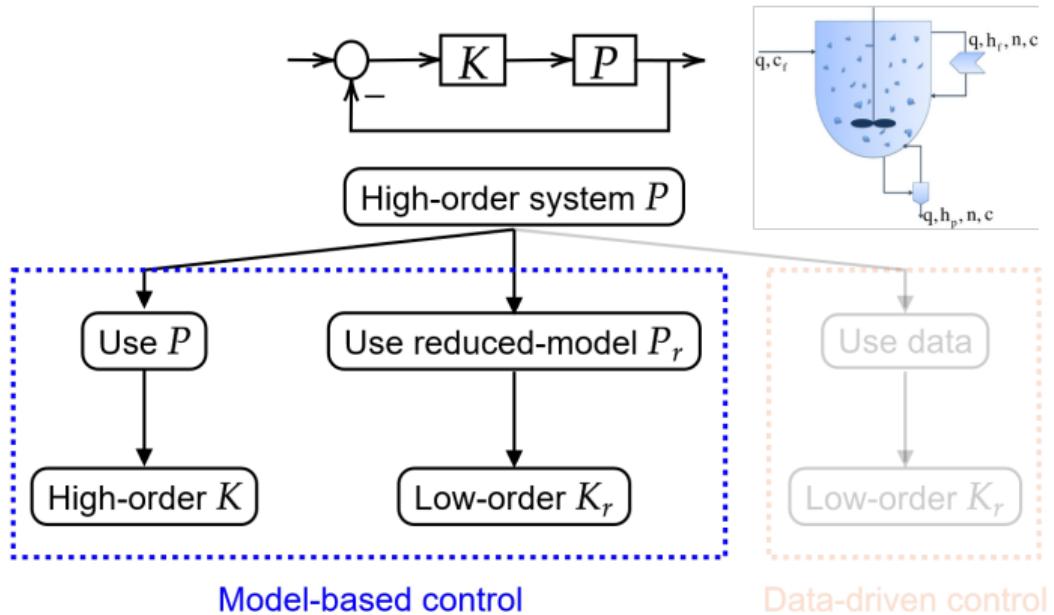
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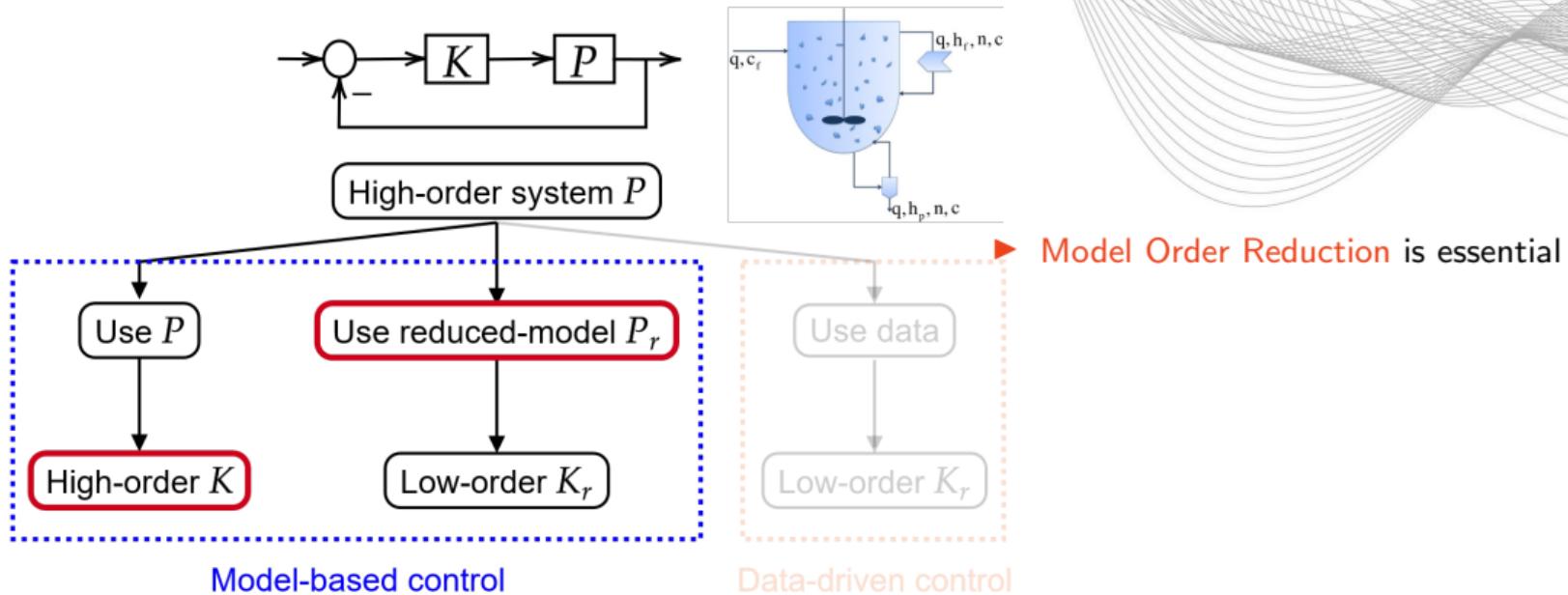
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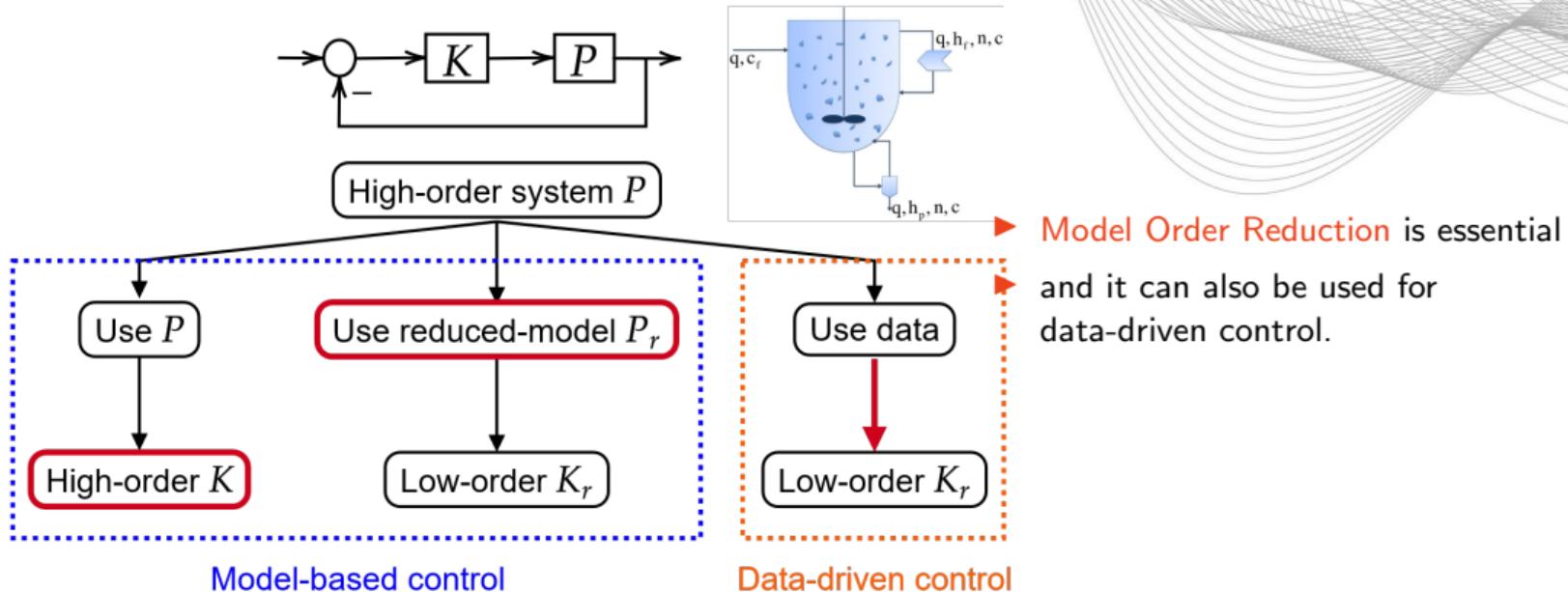
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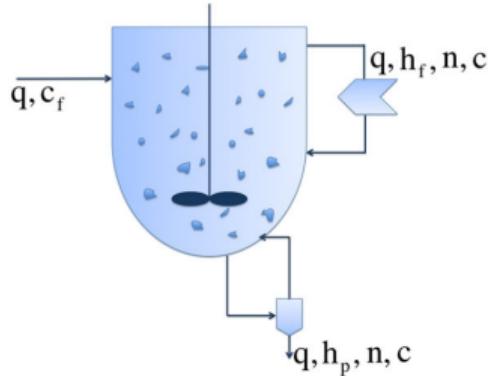


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³ From reference model selection to controller validation: Application to Loewner Data-Driven Control, Kergus, Olivi, Poussot-Vassal, Demourant, IEEE Control Systems Letters, 2019.

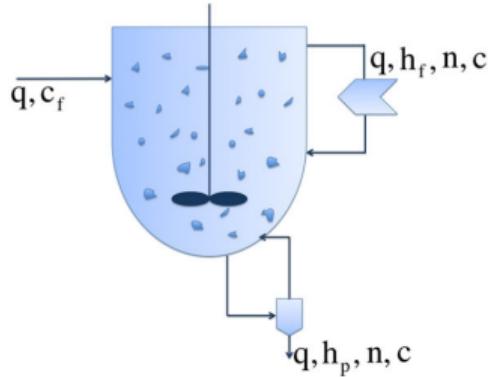
Case study: the continuous crystallizer



► Goal: stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$

-
1. A mathematical model for continuous crystallization, Rachah, Noll, Espitalier, Baillon, *Mathematical Methods in the Applied Sciences*, 2016.
 2. \mathcal{H}_∞ -Control of a continuous crystallizer, Vollmer, Raisch, *Control Engineering Practice*, 2001.
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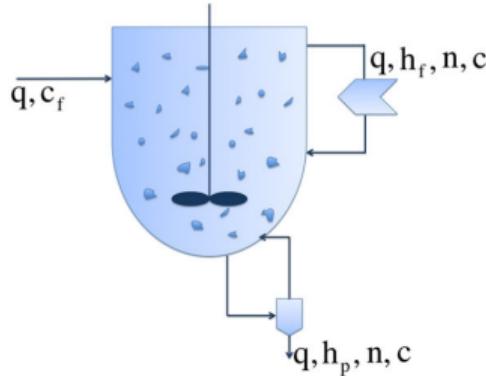
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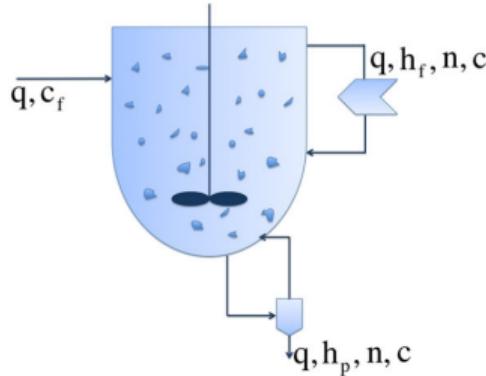


- ▶ Goal: stabilize the plant around $c_{ss} = 4.09 \text{ mol/L}$
- ▶ Unstable system and sustained oscillations
- ▶ Linearization of the PDEs around c_{ss}

$$P(s) = \frac{\Delta c(s)}{\Delta c_f(s)} = \frac{p_{12}(s)}{p_{13}(s) + q_{12}(s)e^{-sk_f} + r_{12}(s)e^{-sk_p}}$$

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→ Frequency-domain data easily accessible

$N = 500$ frequencies, logspaced between 10^{-3} and 1 rad.s^{-1}

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L-DDC Step 1: Building a reference model

$$\begin{cases} \mathbf{y}_{z_i}^T \mathbf{P}(z_i) = 0 \\ \mathbf{y}_{p_j}^T \mathbf{P}(p_j) = \infty \end{cases} \Rightarrow \boxed{\begin{cases} \mathbf{y}_{z_i}^T \mathbf{M}(z_i) = 0 \\ \mathbf{M}(p_j) \mathbf{y}_{p_j} = \mathbf{y}_{p_j} \end{cases}}$$

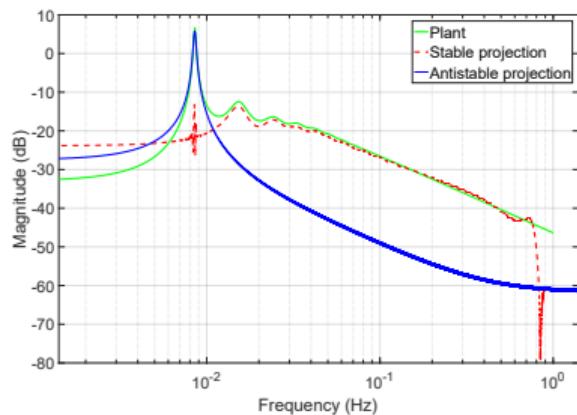
Is the system stable or unstable? non-minimum phase or not?

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$$\begin{aligned} \mathbf{P}(\omega) &= \mathbf{P}_s(\omega) + \mathbf{P}_{as}(\omega) \\ \mathcal{L}_2 &= \mathcal{H}_2 \oplus \mathcal{H}_2^\perp \end{aligned}$$



Achievable performance of multivariable systems with unstable zeros and poles, Havre, Skogestad, *International Journal of Control*, 2001.

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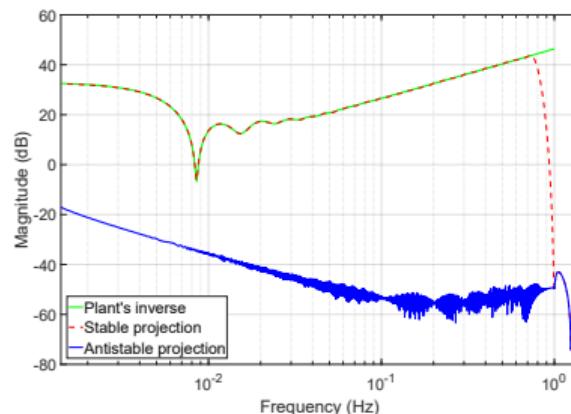
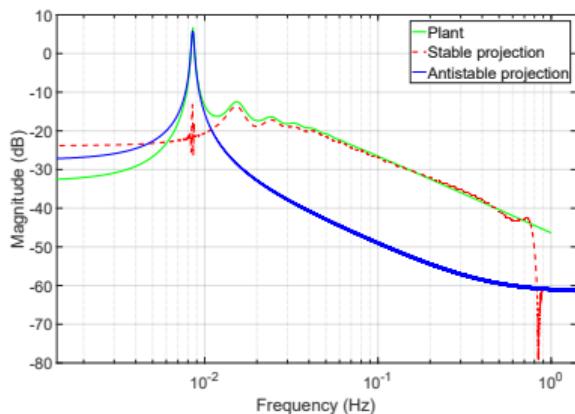
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Where are the system's instabilities?

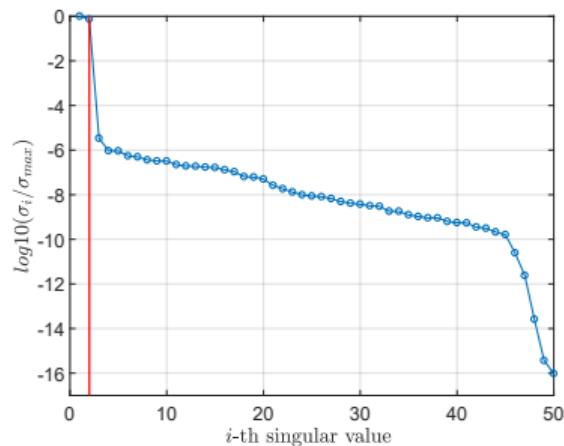
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Principal Hankel Component analysis on P_{as}



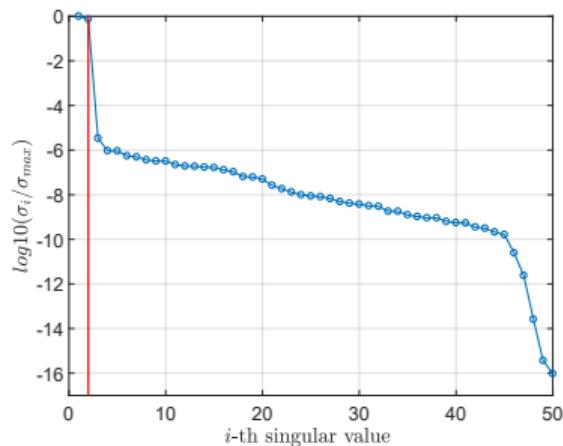
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Principal Hankel Component analysis on P_{as}



- ▶ Estimated RHP poles :
 $1.07 \times 10^{-4} \pm 0.852 \times 10^{-2} j$
- ▶ RHP poles (direct search):
 $0.99 \times 10^{-4} \pm 0.89 \times 10^{-2} j$

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How to choose the reference model accordingly?

$$M_{init}(s) = \frac{1}{1 + \tau s}, \quad \tau = 1s$$

$$\boxed{M = 1 - (1 - M_{init})B_p}$$

$$B_p(s) = \prod_{j=1}^{n_p} \frac{s - p_j}{s + p_j} \quad \begin{aligned} \forall j = 1 \dots n_p, \quad & B_p(p_j) = 0 \\ \forall \omega, \quad & |B_p(j\omega)| = 1 \end{aligned}$$

Interlude: the Loewner framework

Find \mathbf{g} such that $\begin{cases} \mathbf{g}(\lambda_j) = \mathbf{w}_j, & j = 1, \dots, k \\ \mathbf{g}(\mu_i) = \mathbf{v}_i, & i = 1, \dots, q \end{cases}$

Lagrangian form

$$\mathbf{g}(s) = \frac{\sum_{j=1}^{k_1} \frac{c_j \mathbf{w}_j}{s - \lambda_j}}{\sum_{j_1=1}^{k_1} \frac{c_j}{s - \lambda_j}}$$

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Null space

$$\text{span } (\mathbf{c}) = \mathcal{N}(\mathbb{L})$$

Loewner matrix

$$\mathbb{L} \in \mathbb{C}^{q \times k}$$

$$(\mathbb{L})_{i,j} = \frac{\mathbf{v}_i - \mathbf{w}_j}{\mu_i - \lambda_j}$$

$$\mathbf{c} = \begin{bmatrix} c_1 \\ c_2 \\ \vdots \\ c_{k_1} \end{bmatrix} \in \mathbb{C}^{k_1}$$

Interlude: the Loewner framework

$$\begin{cases} E\dot{x} = Ax + Bu \\ y = Cx \end{cases}$$

$$H(s) = C(sE - A)^{-1}B$$

Objective: Find $(\hat{E}, \hat{A}, \hat{B}, \hat{C})$ such that for a set of interpolation points $\{s_k\}$

$$\forall i, \hat{H}(\lambda_i)\mathbf{r}_i = \mathbf{w}_i$$

$$\forall j, l_j \hat{H}(\mu_j) = \mathbf{v}_j$$

Interlude: the Loewner framework

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- ▶ $\mathbb{L}, \mathbb{L}_s, \mathbf{V}$ and \mathbf{W} are data matrices
- ▶ Model order reduction based on SVD of the pencil $(\mathbb{L}, \mathbb{L}_s)$

$$(\mathbb{L})_{i,j} = \frac{\mathbf{v}_i \mathbf{r}_i - \mathbf{l}_j \mathbf{w}_j}{\mu_i - \lambda_j} \quad (\mathbb{L}_s)_{i,j} = \frac{\mu_i \mathbf{v}_i \mathbf{r}_i - \lambda_j \mathbf{l}_j \mathbf{w}_j}{\mu_i - \lambda_j}$$

$$\boxed{\begin{cases} -\mathbb{L}\dot{\tilde{\mathbf{x}}} = -\mathbb{L}_s\tilde{\mathbf{x}} + \mathbf{V}\mathbf{u} \\ \tilde{\mathbf{y}} = \mathbf{W}\tilde{\mathbf{x}} \end{cases}}$$

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- ▶ Factorization in terms of the tangential generalized controllability \mathcal{R} and observability \mathcal{O} matrices:

$$\mathbb{L} = -\mathcal{O}\mathcal{E}\mathcal{R} \quad \mathbb{L}_s = -\mathcal{O}\mathbf{A}\mathcal{R} \quad \mathbf{V} = \mathbf{C}\mathcal{R} \quad \mathbf{W} = \mathcal{O}\mathbf{B}$$

$$\mathbf{A}\mathcal{R} + \mathbf{B}\mathcal{R} = \mathbf{E}\mathcal{R}\Lambda \quad \mathcal{O}\mathbf{A} + \mathbf{L}\mathcal{C} = \cancel{\mathcal{M}\mathcal{O}\mathcal{E}}$$

~~Laplace~~

LDDC Step 2: Controller identification and reduction

Objective: obtain a rational model $\mathbf{K} = (E, A, B, C, D)$ such that:

$$\forall i = 1 \dots N, \mathbf{K}(j\omega_i) = \mathbf{K}^*(j\omega_i) = \frac{M(j\omega_i)}{P(j\omega_i)(1 - M(j\omega_i))}.$$

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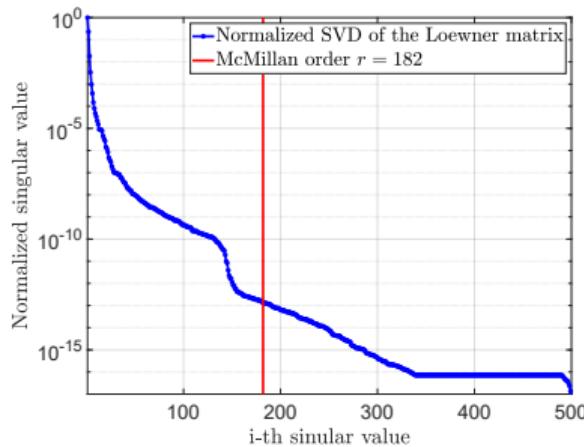


Figure: SVD of \mathbb{L} .

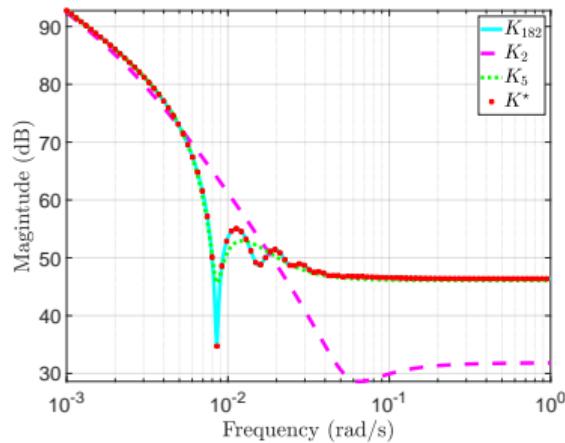
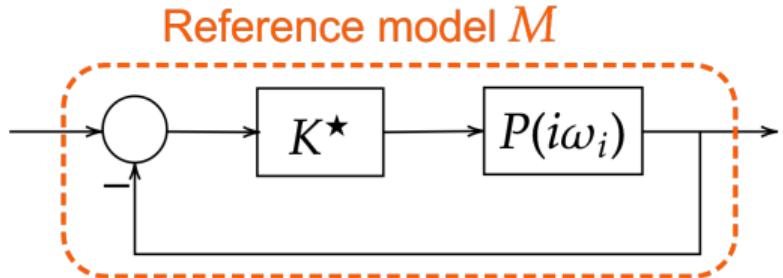
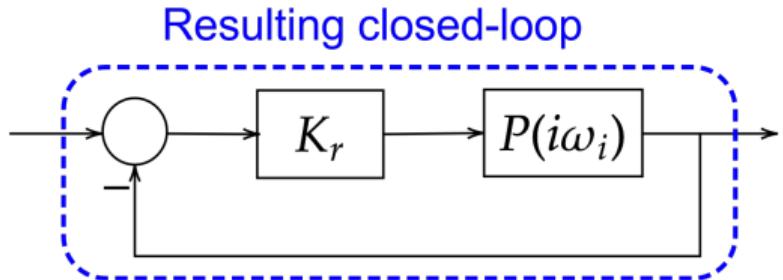


Figure: Obtained controllers.

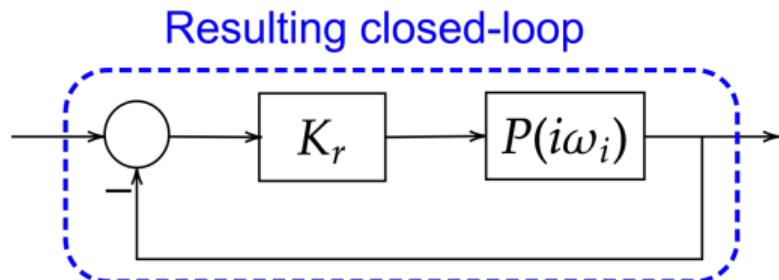
LDDC Step 3: Closed-loop stability analysis



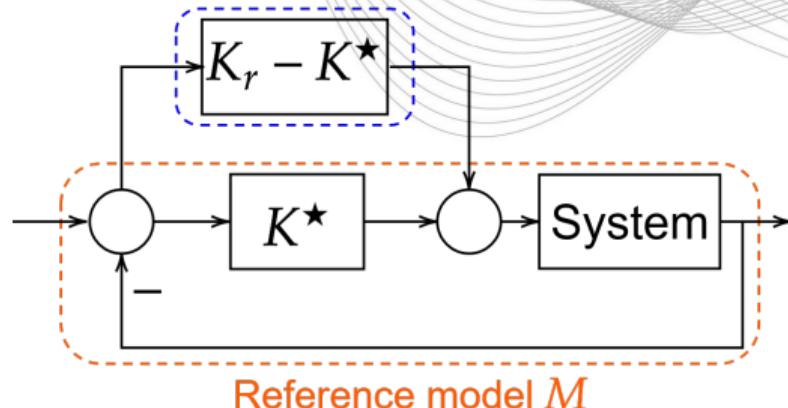
LDDC Step 3: Closed-loop stability analysis



LDDC Step 3: Closed-loop stability analysis



Controller modelling error Δ

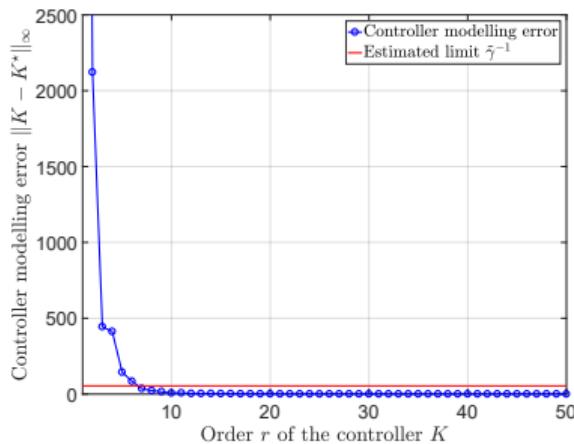


Application of the small-gain theorem

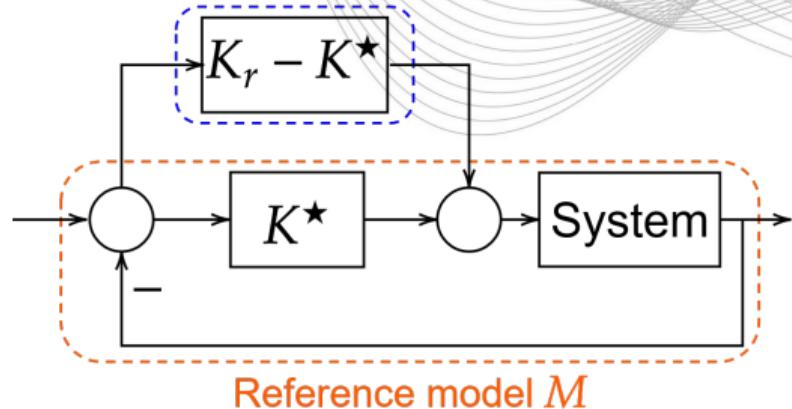
The closed-loop is well-posed and internally stable for all stable $\Delta = K - K^*$ such that $\|\Delta\|_\infty \leq \beta$ if and only if $\|(1 - M)\mathbf{P}\|_\infty < \frac{1}{\beta}$

→ Limiting the controller modelling error allows to ensure closed-loop internal stability!

LDDC Step 3: Closed-loop stability analysis



Controller modelling error Δ



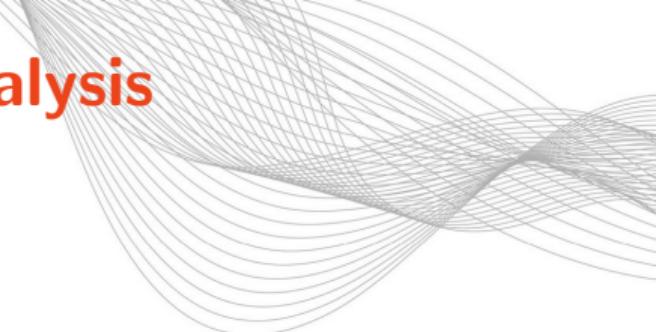
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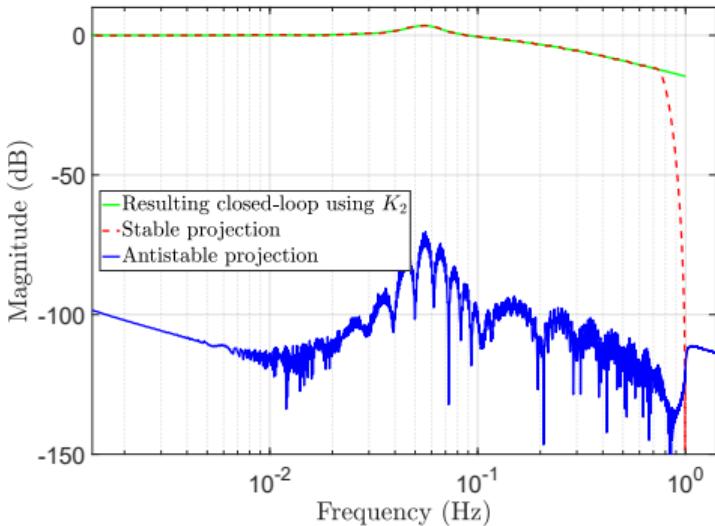
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Alternative closed-loop stability analysis

$$H(j\omega_i) = \frac{P(j\omega_i)K_r(j\omega_i)}{1 + P(j\omega_i)K_r(j\omega_i)}$$



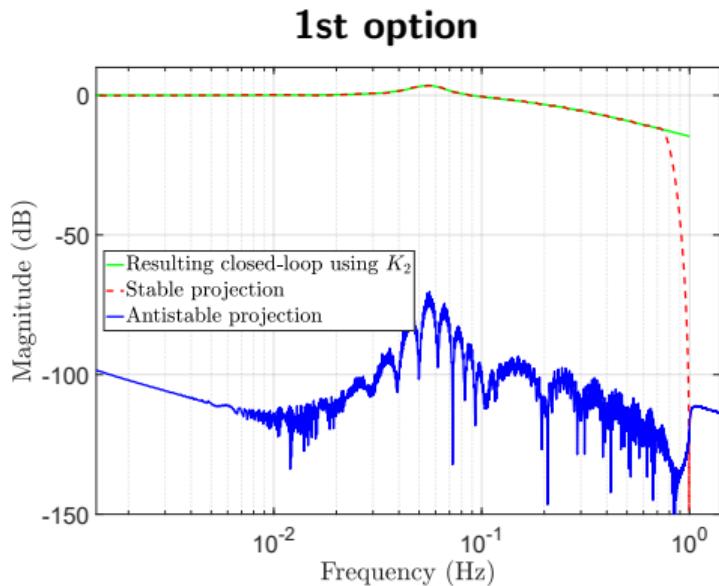
1st option



Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

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2nd option

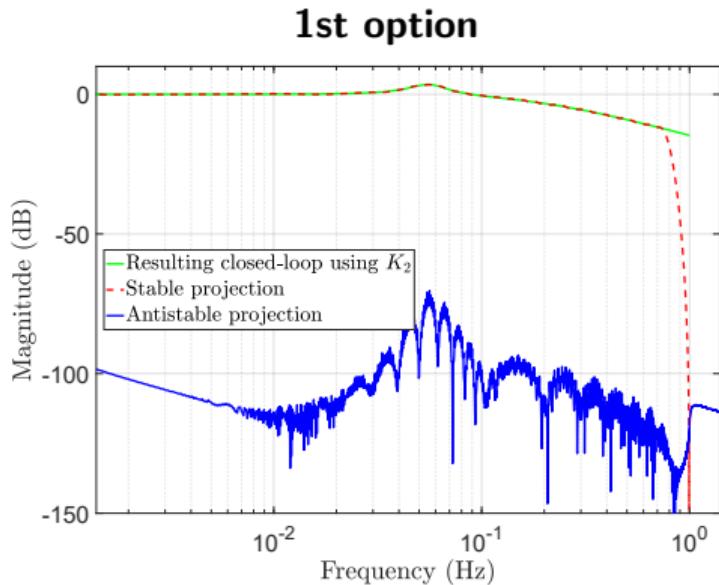
1. Loewner interpolation: $\hat{H}(j\omega_i) = H(j\omega_i)$

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Interpolation-based infinite dimensional model control design and stability analysis, Poussot-Vassal, Kergus, Vuillemin, *chapter to appear*.

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2nd option

1. Loewner interpolation: $\hat{H}(j\omega_i) = H(j\omega_i)$
2. Stable projection on \mathcal{RH}_∞ :
$$\hat{H}_s = \arg \min_{H \in \mathbb{S}_{n,n_i,n_o}^+} \|H - \hat{H}\|_\infty$$

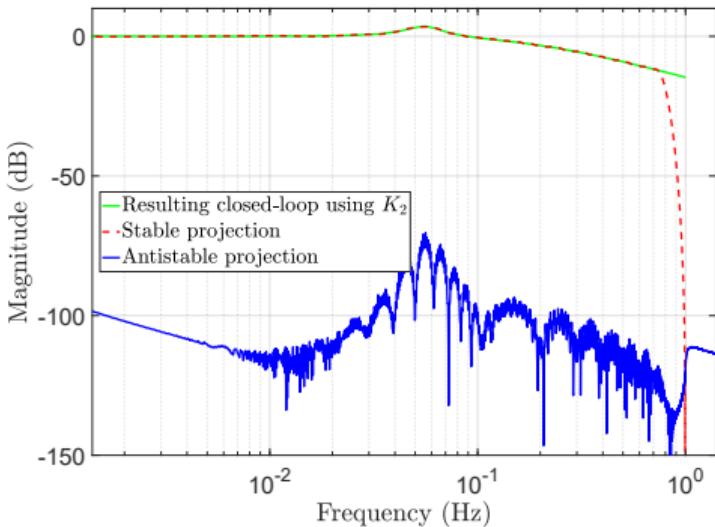
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On the closest stable descriptor system in the respective spaces \mathcal{RH}_2 and \mathcal{RH}_∞ , Köhler, *Linear Algebra and its Applications*, 2014.

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$$S = 4.3511 \cdot 10^{-6}$$

Model-free closed-loop stability analysis: A linear functional approach, Cooman, Seyfert, Olivi, Chevillard, Baratchart, *IEEE Transactions on Microwave Theory and Techniques*, 2018

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Results

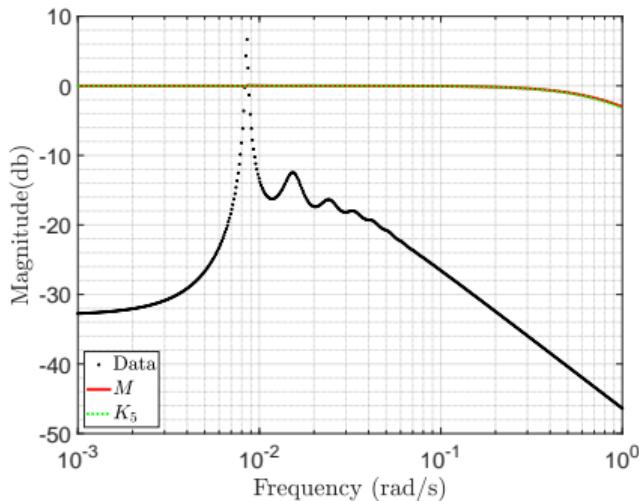


Figure: Closed-loop transfer functions.

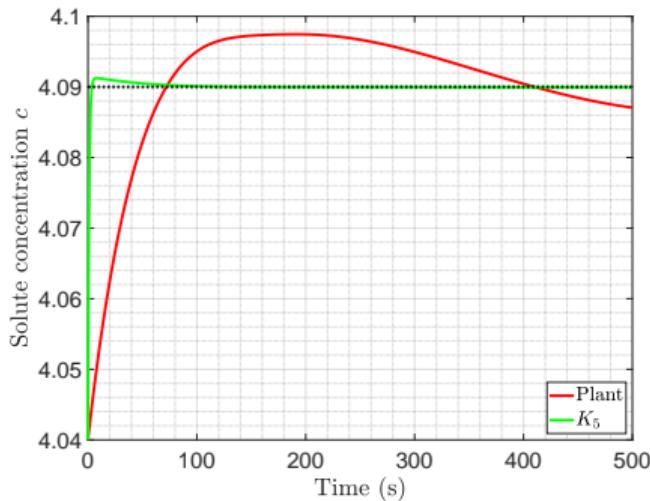


Figure: Time-domain simulation.

Results

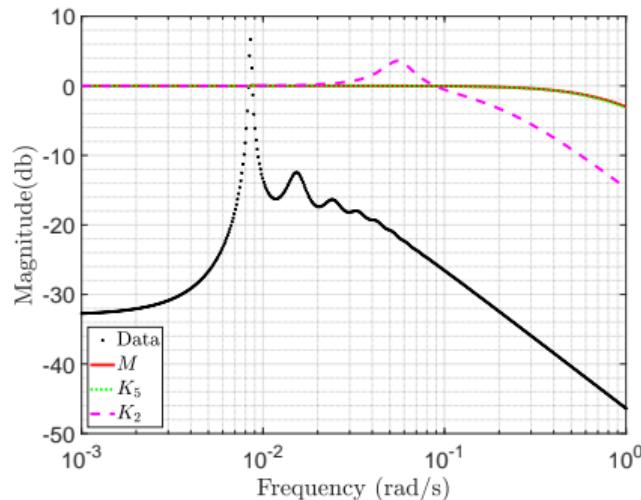


Figure: Closed-loop transfer functions.

⇒ Impact of the **complexity-accuracy trade-off**

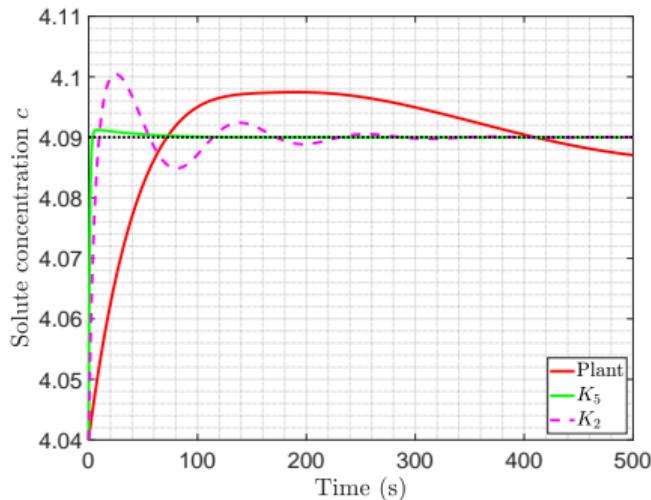


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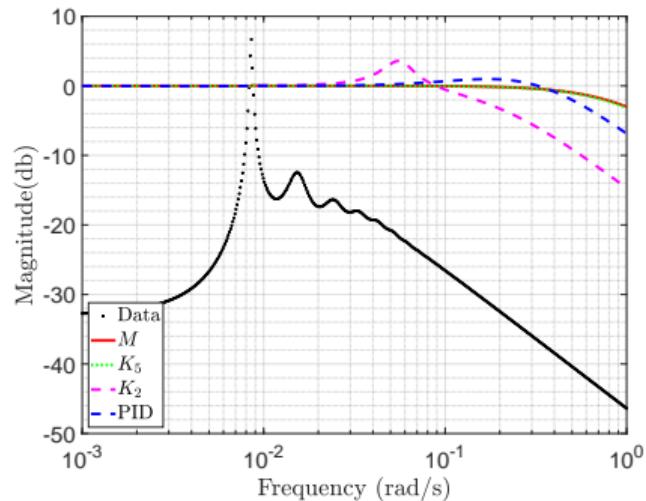


Figure: Closed-loop transfer functions.

- ⇒ Impact of the **complexity-accuracy trade-off**
- ⇒ Impact of the reference model (comparison with a robust PID)

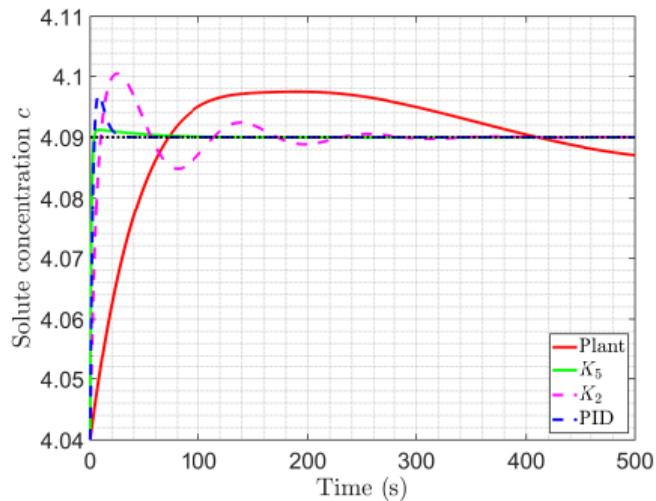


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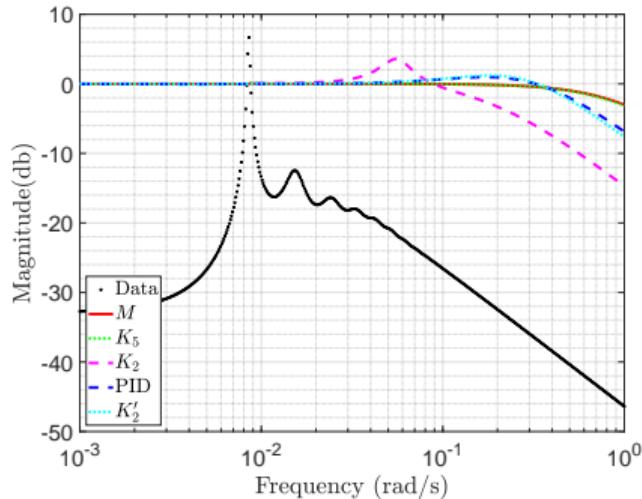


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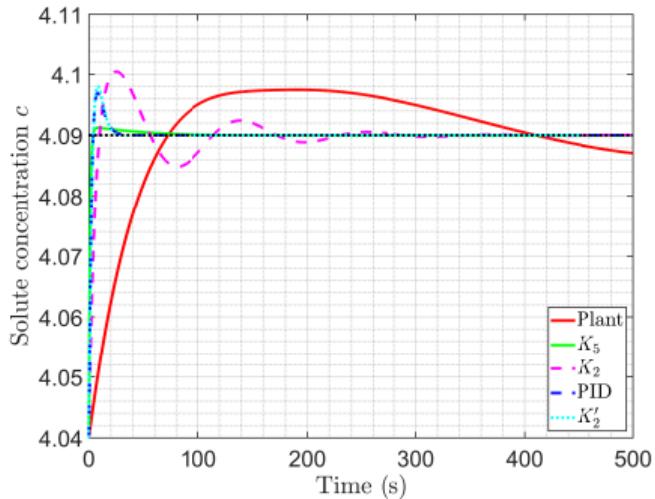
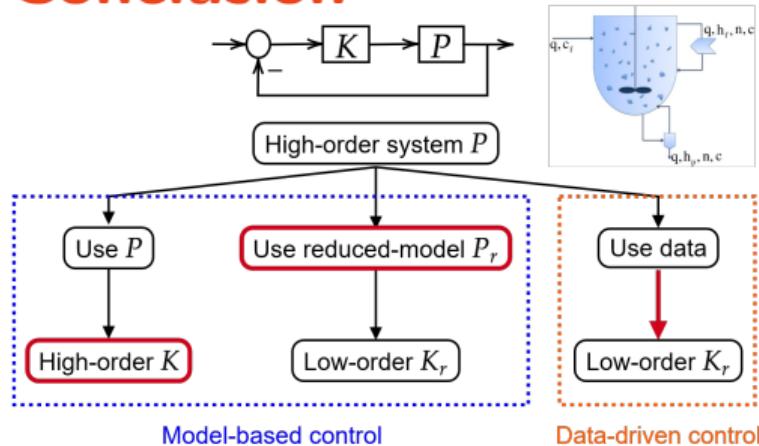


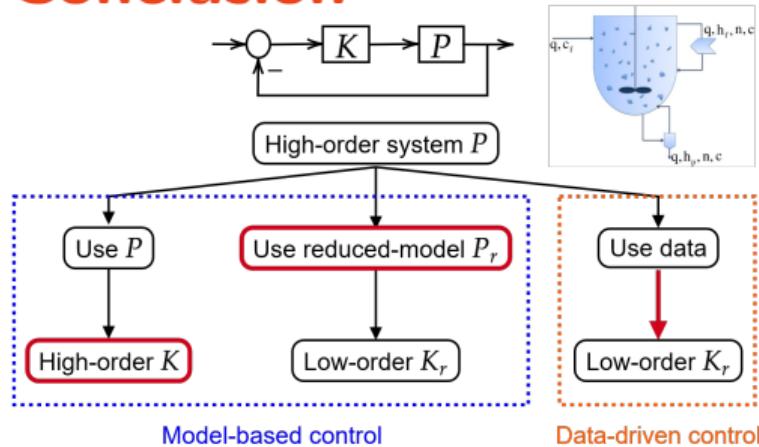
Figure: Time-domain simulation.

Conclusion



The Loewner framework can be used as a central tool for the control of infinite dimensional transfer functions.

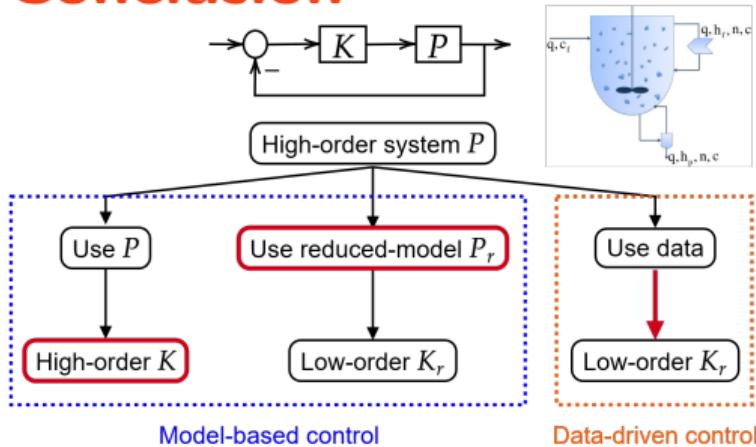
Conclusion



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	Model-based design	L-DDC
Method	more steps	direct
Controller structure	fixed order/poles	linear
Specifications	flexible (robust)	not flexible (only stability)
Stability guarantees	for P_r	conservative or not embedded

Conclusion



The Loewner framework can be used as a central tool for the control of infinite dimensional transfer functions.

Extension to other types of systems?

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Method	more steps	direct
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