Turbulência Atmosférica e Parametrização da Camada Limite Planetária

lei do gas

$$\bar{\rho} = \bar{\rho} R_d \overline{T_v}$$

$$\overline{T_v} = T(1 + 0.61q_v - q_l)$$

Necessita ser parametrizado!

A = A + A'2nd ordem

Média de Reynolds

Temperatura virtual

momentum

$$\frac{\partial \overline{u_i}}{\partial t} + \overline{u_j} \frac{\partial \overline{u_i}}{\partial x_j} = -\delta_{i3}g + f_c \varepsilon_{ij3} \overline{u_j} - \frac{1}{\rho} \frac{\partial \overline{P}}{\partial x_i} + \frac{\upsilon \partial^2 \overline{u_i}}{\partial x_j^2} - \frac{\partial \overline{(u_i' u_j')}}{\partial x_j}$$

Advecção media

gravidade Coriolis

Gradiente de

Estresse **Transporte** Viscoso **Turbulento**

Pressão

$$\frac{\partial \overline{u_i}}{\partial x_j} = 0$$



$$\frac{\partial \theta}{\partial t} + \overline{u_j} \frac{\partial \overline{\theta}}{\partial x_j} = -\frac{1}{\overline{\rho} c_p} \frac{\partial \overline{F_j}}{\partial x_j} - \frac{\partial \overline{u_j' \theta'}}{\partial x_j}$$

Advecção media

radiação

Transporte Turbulento

Liberação de Calor Latente

Agua Total

$$\frac{\partial \overline{q_t}}{\partial t} + \overline{u_j} \frac{\partial \overline{q_t}}{\partial x_j} = \frac{S_{q_t}}{\overline{\rho}} - \frac{\partial \overline{u'_j q'_t}}{\partial x_j}$$
Advecção

Advecção media

precipitação

Transporte Turbulento

- Região da atmosfera que é fortemente influenciada pela presença da superfície terrestre e responde em escala temporal da ordem de horas ou menos
- Importante
 - Processos na superfície são complexos
 - A camada limite é muito turbulenta

 Na camada limite o transporte horizontal é dominado pelo vento médio e na vertical pela turbulência

$$\frac{\partial(\overline{u_i})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{u_i})}{\partial x_j} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_i} + g\frac{\overline{\rho}}{\rho_0}\delta_{i3} + 2\Omega\varepsilon_{ijk}\eta_j(\overline{u_k}) - \nu\frac{\partial^2(\overline{u_i})}{\partial x_j^2} = -\frac{\partial(\overline{u_j'u_i'})}{\partial x_j}$$

$$\frac{\partial(\overline{T})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{T})}{\partial x_j} - S_P \overline{\omega} = -\frac{\partial(\overline{u_j'T'})}{\partial x_j} + \frac{\overline{J}}{C_p}$$

$$\frac{\partial(\overline{q})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{q})}{\partial x_j} = -\frac{\partial(\overline{u_j'q'})}{\partial x_j} + \overline{S}$$

 As variáveis (vento, temperatura umidade) e são separadas na média e perturbação (turbulência)

Comparações

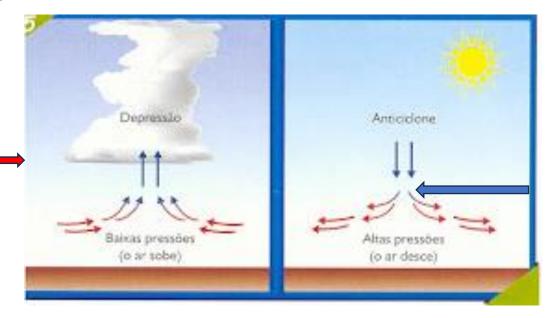
Camada limite

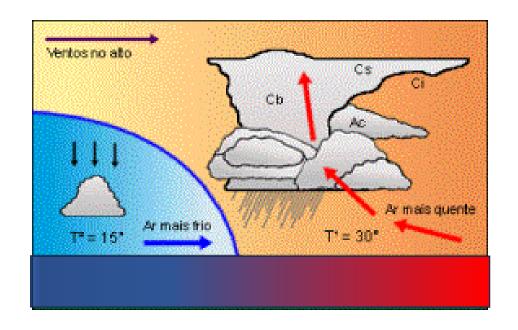
- Turbulência continua
- Forte arrastro, grande dissipação de energia
- Mistura turbulenta rápida
- Sub geostrófico
- Transporte vertical dominado pela turbulência
- Profundidade varia entre 100m e 3 km, variações diurnas

Atmosfera livre

- Em nuvens convectivas
- Pequena dissipação viscosa
- Pequena
- Ventos quase geostróficos
- Vento médio domina (cumulus)
- Menos variável 8-18 km
- variações temporais lentas

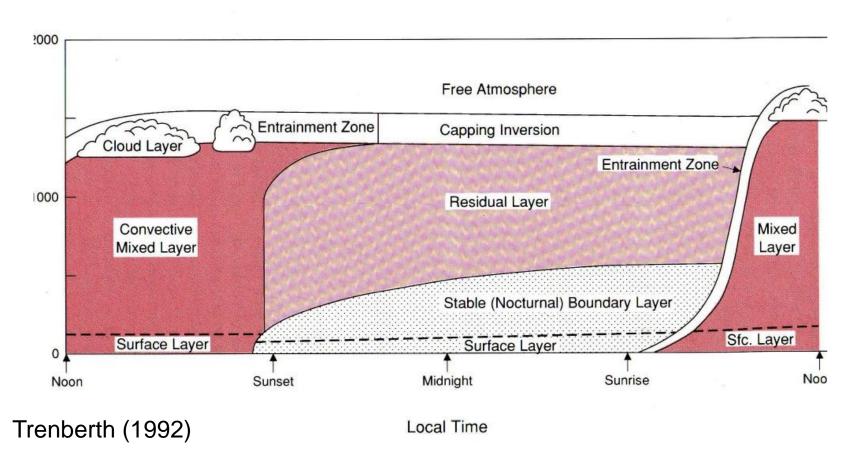
- A camada limite é usualmente rasa em regiões de altas pressões devido ao movimento descendente e a divergência horizontal decresce sua altura
- Em regiões de baixa pressão a altura da camada limite é mais profunda



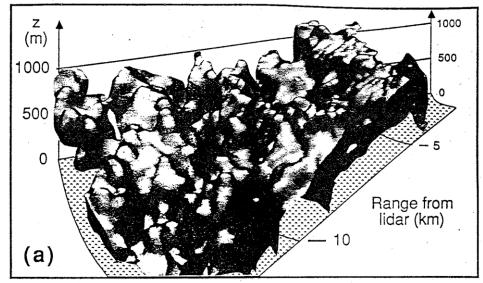


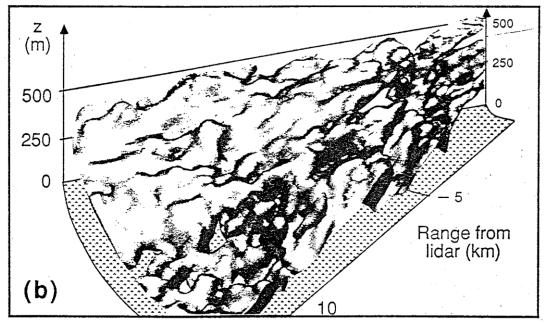
•O aquecimento superficial e o aprofundamento da camada limite é importante para a previsão

Camada Limite



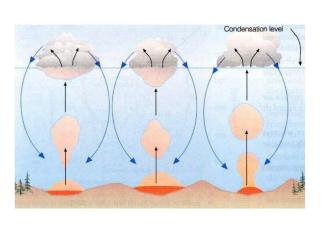
Exemplos

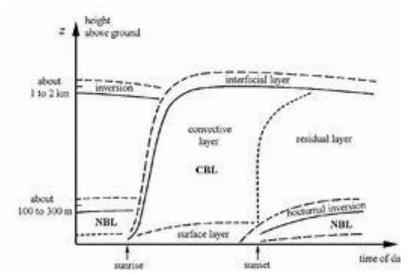




Camada limite

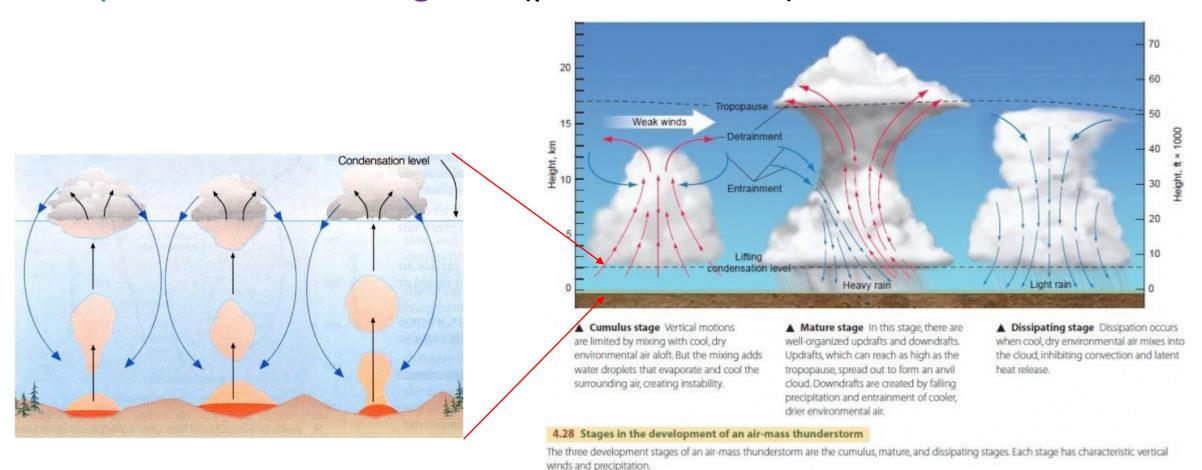
 Evolução das equações dependem da divergência de fluxos convectivos (calor, vapor, momentum) dirigido por movimentos não resolvidos na vertical





 Os processos na camada limite são parametrizados nos modelos por sua grosseira resolução vertical

 Convecção cumulus causa grandes fluxos verticais de calor e vapor na escala sub-grade (parametrizado) → física do modelo



$$\frac{\partial(\overline{u_i})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{u_i})}{\partial x_j} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_i} + g\frac{\overline{\rho}}{\rho_0}\delta_{i3} + 2\Omega\varepsilon_{ijk}\eta_j(\overline{u_k}) - \nu\frac{\partial^2(\overline{u_i})}{\partial x_j^2} = -\frac{\partial(\overline{u_j'u_i'})}{\partial x_j}$$

$$\frac{\partial(\overline{T})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{T})}{\partial x_j} - S_P \overline{\omega} = -\frac{\partial(\overline{u_j'T'})}{\partial x_j} + \frac{\overline{J}}{C_p}$$

$$\frac{\partial(\overline{q})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{q})}{\partial x_j} = -\frac{\partial(\overline{u_j'q'})}{\partial x_j} + \overline{S}$$

$$i = 1$$
 e $j = 1,2,3$ k = 1,2,3
$$\varepsilon_{ijk} = \begin{cases} 1 & (ijk) = (123), (231), (312) \\ -1 & (ijk) = (132), (213), (321) \\ 0 & else \end{cases}$$

$$\frac{\partial(\overline{u_i})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{u_i})}{\partial x_j} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_i} + g\frac{\overline{\rho}}{\rho_0}\delta_{i3} + 2\Omega\varepsilon_{ijk}\eta_j(\overline{u_k}) - \nu\frac{\partial^2(\overline{u_i})}{\partial x_j^2} = -\frac{\partial(\overline{u_j'u_i'})}{\partial x_j}$$

$$\begin{split} &\frac{\partial(\overline{u_1})}{\partial t} + (\overline{u_1})\frac{\partial(\overline{u_1})}{\partial x_1} + (\overline{u_2})\frac{\partial(\overline{u_1})}{\partial x_2} + (\overline{u_3})\frac{\partial(\overline{u_1})}{\partial x_3} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_1} + g\frac{\overline{\rho}}{\rho_0}\delta_{13} + 2\Omega\varepsilon_{111}\eta_1(\overline{u_1}) + 2\Omega\varepsilon_{121}\eta_2(\overline{u_1}) + 2\Omega\varepsilon_{131}\eta_3(\overline{u_1}) \\ &+ 2\Omega\varepsilon_{112}\eta_1(\overline{u_2}) + 2\Omega\varepsilon_{122}\eta_2(\overline{u_2}) + 2\Omega\varepsilon_{132}\eta_3(\overline{u_2}) + 2\Omega\varepsilon_{113}\eta_1(\overline{u_3}) + 2\Omega\varepsilon_{123}\eta_2(\overline{u_3}) + 2\Omega\varepsilon_{133}\eta_3(\overline{u_3}) - \nu\frac{\partial^2(\overline{u_2})}{\partial x_1^2} - \nu\frac{\partial^2(\overline{u_2})}{\partial x_2^2} \\ &- \nu\frac{\partial^2(\overline{u_2})}{\partial x_3^2} = -\frac{\partial(\overline{u_1'u_3'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_3'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_3'})}{\partial x_3} \end{split}$$

$$+2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0$$
 $2\Omega\varepsilon_{313}\eta_1(\overline{u_3})=0$

$$2\Omega\varepsilon_{313}\eta_1(\overline{u_3})=0$$

$$2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0$$

$$\frac{\partial(\overline{u_1})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_1})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_1})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_1})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_1} - 2\Omega \eta_3(\overline{u_2}) - \nu \frac{\partial^2(\overline{u_1})}{\partial x_1^2} - \nu \frac{\partial^2(\overline{u_1})}{\partial x_2^2} - \nu \frac{\partial^2(\overline{u_1})}{\partial x_3^2} = -\frac{\partial(\overline{u_1'u_1'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_1'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_1'})}{\partial x_3} - \frac{\partial(\overline{u_3'u_1'})}{\partial x_3} - \frac{\partial(\overline{u_1'u_1'})}{\partial x_3} - \frac{\partial(\overline{u_1'u_1'})}$$

$$i = 3$$
 e $j = 1,2,3$ $k = 1,2,3$

Equação governante para o escoamento zonal

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - \frac{2\Omega\eta_3(\overline{v})}{\partial x} - \frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{w'u$$

$$i = 2$$
 e $j = 1,2,3$ k = 1,2,3
$$\varepsilon_{ijk} = \begin{cases} 1 & (ijk) = (123), (231), (312) \\ -1 & (ijk) = (132), (213), (321) \\ 0 & else \end{cases}$$

$$\frac{\partial(\overline{u_i})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{u_i})}{\partial x_j} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_i} + g\frac{\overline{\rho}}{\rho_0}\delta_{i3} + 2\Omega\varepsilon_{ijk}\eta_j(\overline{u_k}) - \nu\frac{\partial^2(\overline{u_i})}{\partial x_j^2} = -\frac{\partial(\overline{u_j'u_i'})}{\partial x_j}$$

$$\begin{split} &\frac{\partial(\overline{u_2})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_2})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_2})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_2})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_2} + g \frac{\overline{\rho}}{\rho_0} \delta_{23} + 2\Omega \varepsilon_{211} \eta_1(\overline{u_1}) + 2\Omega \varepsilon_{221} \eta_2(\overline{u_1}) + 2\Omega \varepsilon_{231} \eta_3(\overline{u_1}) \\ &+ 2\Omega \varepsilon_{212} \eta_1(\overline{u_2}) + 2\Omega \varepsilon_{222} \eta_2(\overline{u_2}) + 2\Omega \varepsilon_{232} \eta_3(\overline{u_2}) + 2\Omega \varepsilon_{213} \eta_1(\overline{u_3}) + 2\Omega \varepsilon_{223} \eta_2(\overline{u_3}) + 2\Omega \varepsilon_{233} \eta_3(\overline{u_3}) - \nu \frac{\partial^2(\overline{u_2})}{\partial x_1^2} - \nu \frac{\partial^2(\overline{u_2})}{\partial x_2^2} \\ &- \nu \frac{\partial^2(\overline{u_2})}{\partial x_3^2} = -\frac{\partial(\overline{u_1'u_2'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_2'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_2'})}{\partial x_3} \end{split}$$

$$+2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0 \hspace{1cm} 2\Omega\varepsilon_{313}\eta_1(\overline{u_3})=0 \hspace{1cm} 2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0$$

$$\frac{\partial(\overline{u_2})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_2})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_2})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_2})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_2} + 2\Omega \eta_3(\overline{u_1}) - \nu \frac{\partial^2(\overline{u_2})}{\partial x_1^2} - \nu \frac{\partial^2(\overline{u_2})}{\partial x_2^2} - \nu \frac{\partial^2(\overline{u_2})}{\partial x_3^2} = -\frac{\partial(\overline{u_1'u_2'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_2'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_2'})}{\partial x_3} - \frac{\partial(\overline{u_3'u_2'})}{\partial x_3} - \frac{\partial(\overline{u_1'u_2'})}{\partial x_3} - \frac{\partial(\overline{u_1'u_2'})}$$

$$i = 3$$
 e $j = 1,2,3$ $k = 1,2,3$

Equação governante para o escoamento Meridional

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + \frac{2\Omega\eta_3(\overline{u})}{\partial y} - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{v'v'})}{\partial z} - \frac{\partial(\overline{v'v'}$$

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - 2\Omega\eta_3(\overline{v}) - \nu\frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - \frac{\partial(\overline{w'u'})}{\partial z}$$

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + \frac{2\Omega\eta_3(\overline{u})}{\partial y} - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{w'v'}$$

$$i = 3$$
 e $j = 1,2,3$ $k = 1,2,3$
$$\varepsilon_{ijk} = \begin{cases} 1 & (ijk) = (123), (231), (312) \\ -1 & (ijk) = (132), (213), (321) \\ 0 & else \end{cases}$$

$$\frac{\partial(\overline{u_i})}{\partial t} + (\overline{u_j})\frac{\partial(\overline{u_i})}{\partial x_j} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x_i} + g\frac{\overline{\rho}}{\rho_0}\delta_{i3} + 2\Omega\varepsilon_{ijk}\eta_j(\overline{u_k}) - \nu\frac{\partial^2(\overline{u_i})}{\partial x_j^2} = -\frac{\partial(\overline{u_j'u_i'})}{\partial x_j}$$

$$\frac{\partial(\overline{u_3})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_3})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_3})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_3})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_3} + g \frac{\overline{\rho}}{\rho_0} \delta_{33} + 2\Omega \varepsilon_{311} \eta_1(\overline{u_1}) + 2\Omega \varepsilon_{322} \eta_2(\overline{u_2}) + 2\Omega \varepsilon_{333} \eta_3(\overline{u_3}) + 2\Omega \varepsilon_{311} \eta_1(\overline{u_1}) + 2\Omega \varepsilon_{322} \eta_2(\overline{u_2}) + 2\Omega \varepsilon_{333} \eta_3(\overline{u_3}) + 2\Omega \varepsilon_{311} \eta_1(\overline{u_1}) + 2\Omega \varepsilon_{322} \eta_2(\overline{u_2}) + 2\Omega \varepsilon_{333} \eta_3(\overline{u_3}) - \nu \frac{\partial^2(\overline{u_3})}{\partial x_1^2} - \nu \frac{\partial^2(\overline{u_3})}{\partial x_2^2} - \nu \frac{\partial^2(\overline{u_3})}{\partial x_2^2} = -\frac{\partial(\overline{u_1'u_3'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_3'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_3'})}{\partial x_3}$$

$$+2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0 \hspace{1cm} 2\Omega\varepsilon_{313}\eta_1(\overline{u_3})=0 \hspace{1cm} 2\Omega\varepsilon_{33k}\eta_3(\overline{u_k})=0$$

$$\frac{\partial(\overline{u_3})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_3})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_3})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_3})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_3} + g \frac{\overline{\rho}}{\rho_0} \delta_{33} - v \frac{\partial^2(\overline{u_3})}{\partial x_1^2} - v \frac{\partial^2(\overline{u_3})}{\partial x_2^2} - v \frac{\partial^2(\overline{u_3})}{\partial x_3^2} \\
= -\frac{\partial(\overline{u_1'u_3'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_3'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_3'})}{\partial x_3}$$

$$i = 3$$
 e $j = 1,2,3$ $k = 3$

$$\frac{\partial(\overline{u_3})}{\partial t} + (\overline{u_1}) \frac{\partial(\overline{u_3})}{\partial x_1} + (\overline{u_2}) \frac{\partial(\overline{u_3})}{\partial x_2} + (\overline{u_3}) \frac{\partial(\overline{u_3})}{\partial x_3} + \frac{1}{\rho_0} \frac{\partial(\overline{P})}{\partial x_3} + g \frac{\overline{\rho}}{\rho_0} - v \frac{\partial^2(\overline{u_3})}{\partial x_1^2} - v \frac{\partial^2(\overline{u_3})}{\partial x_2^2} - v \frac{\partial^2(\overline{u_3})}{\partial x_3^2} \\
= -\frac{\partial(\overline{u_1'u_3'})}{\partial x_1} - \frac{\partial(\overline{u_2'u_3'})}{\partial x_2} - \frac{\partial(\overline{u_3'u_3'})}{\partial x_3}$$

Equação governante para o escoamento Vertical

$$\frac{\partial(\overline{w})}{\partial t} + (\overline{u})\frac{\partial(\overline{w})}{\partial x} + (\overline{v})\frac{\partial(\overline{w})}{\partial y} + (\overline{w})\frac{\partial(\overline{w})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial z} + g\frac{\overline{\rho}}{\rho_0} - \nu\frac{\partial^2(\overline{w})}{\partial x^2} - \nu\frac{\partial^2(\overline{w})}{\partial y^2} - \nu\frac{\partial^2(\overline{w})}{\partial z^2} = -\frac{\partial(\overline{u'w'})}{\partial x} - \frac{\partial(\overline{v'w'})}{\partial y} - \frac{\partial(\overline{w'w'})}{\partial z} - \frac{\partial(\overline{w'w'})}{$$

Equações governantes para o escoamento atmosférico

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - \frac{2\Omega\eta_3(\overline{v})}{\partial x} - \nu\frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{w'$$

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + 2\Omega\eta_3(\overline{u}) - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - \frac{\partial(\overline{w'v'})}{\partial z} + \frac{\partial(\overline{v'v'})}{\partial z} - \frac{\partial(\overline{v'v'})}{\partial z}$$

$$\frac{\partial(\overline{w})}{\partial t} + (\overline{u})\frac{\partial(\overline{w})}{\partial x} + (\overline{v})\frac{\partial(\overline{w})}{\partial y} + (\overline{w})\frac{\partial(\overline{w})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial z} + g\frac{\overline{\rho}}{\rho_0} - \nu\frac{\partial^2(\overline{w})}{\partial x^2} - \nu\frac{\partial^2(\overline{w})}{\partial y^2} - \nu\frac{\partial^2(\overline{w})}{\partial z^2} = -\frac{\partial(\overline{u'w'})}{\partial x} - \frac{\partial(\overline{v'w'})}{\partial y} - \frac{\partial(\overline{w'w'})}{\partial z} - \frac{\partial(\overline{w'w'})}{$$

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - 2\Omega\eta_3(\overline{v}) - \nu\frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{w'u'})}{\partial$$

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + 2\Omega\eta_3(\overline{u}) - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{v'v'})}{\partial z}$$

$$\frac{\partial(\overline{w})}{\partial t} + (\overline{u})\frac{\partial(\overline{w})}{\partial x} + (\overline{v})\frac{\partial(\overline{w})}{\partial y} + (\overline{w})\frac{\partial(\overline{w})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial z} + g\frac{\overline{\rho}}{\rho_0} - \nu\frac{\partial^2(\overline{w})}{\partial x^2} - \nu\frac{\partial^2(\overline{w})}{\partial y^2} - \nu\frac{\partial^2(\overline{w})}{\partial z^2} = -\frac{\partial(\overline{u'w'})}{\partial x} - \frac{\partial(\overline{v'w'})}{\partial y} - \frac{\partial(\overline{w'w'})}{\partial z} - \frac{\partial(\overline{w'w'})}{$$

$$\frac{\partial(\overline{T})}{\partial t} + (\overline{u})\frac{\partial(\overline{T})}{\partial x} + (\overline{v})\frac{\partial(\overline{T})}{\partial y} + (\overline{w})\frac{\partial(\overline{T})}{\partial z} - S_P\overline{\omega} = -\frac{\partial(\overline{u'T'})}{\partial x} - \frac{\partial(\overline{v'T'})}{\partial y} - \frac{\partial(\overline{w'T'})}{\partial z} + \frac{\overline{J}}{C_P}$$

$$\frac{\partial(\overline{q})}{\partial t} + (\overline{u})\frac{\partial(\overline{q})}{\partial x} + (v)\frac{\partial(\overline{q})}{\partial y} + (\overline{w})\frac{\partial(\overline{q})}{\partial z} = -\frac{\partial(\overline{u'q'})}{\partial x} - \frac{\partial(\overline{u'q'})}{\partial y} - \frac{\partial(\overline{w'q'})}{\partial z} + \overline{S}$$

$$u_3 = w$$

$$x_3 = z$$

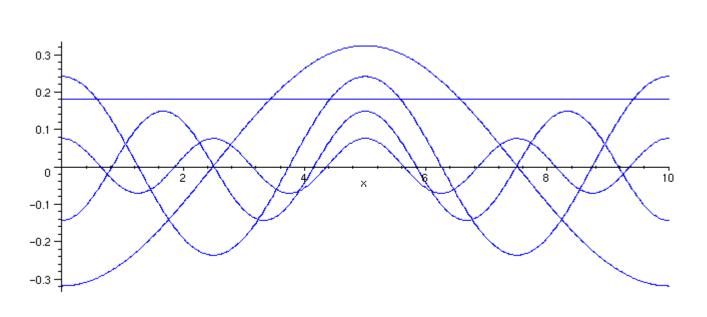
$$v \frac{\partial^2(\overline{u_3})}{\partial x_3^2} \cong 0$$

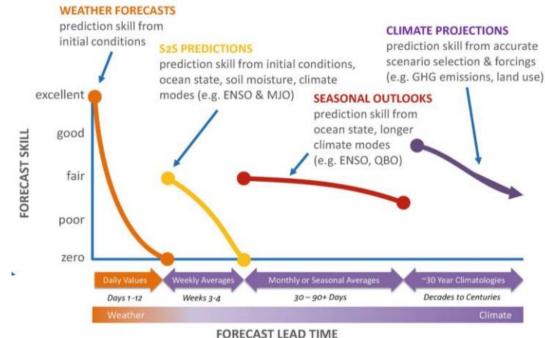
- Modelos de PNT/clima tem fronteiras na vertical
- Já que na atmosfera livre os termos dinâmicos nas equações para as variáveis média na grade são consideradas dominantes
 - (\overline{T}) (\overline{q}) (\overline{u}) (\overline{u}) (\overline{w})
- São acopladas à superfície através de uma camada turbulenta ou camada limite planetária (CLP)

• A CLP transfere calor, umidade e momentum

$$\frac{\partial \left(\overline{w'T'}\right)}{\partial z} \qquad \frac{\partial \left(\overline{w'q'}\right)}{\partial z} \qquad \frac{\partial \left(\overline{w'u'}\right)}{\partial z} \qquad \frac{\partial \left(\overline{w'v'}\right)}{\partial z}$$

• Em outras palavras a influencia da fricção, aquecimento superficial e evaporação tem importância para previsões na escala sinótica, que aumenta com o tempo de integração (clima)

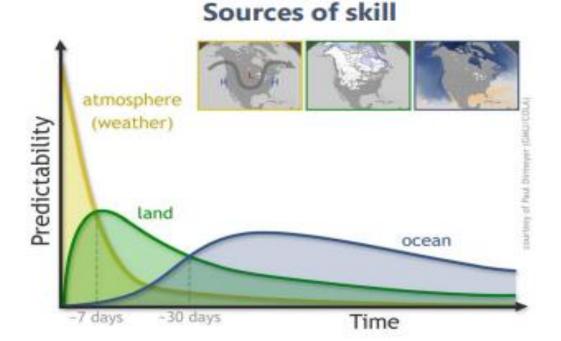




• Exemplos:

- Em 24 horas a evapotranspiração na superfície pode incrementar o conteúdo da umidade na CLP em 25%, o qual pode ser uma fonte importante de umidade para o desenvolvimento de ciclones tropicais
- Também, o fluxo de calor (aquecimento) superficial (principalmente em superfícies úmidas) determina a estabilidade da CLP e isto a convecção

- Fluxos superficiais são importantes no armazenagem de calor e umidade (clima) e na estabilidade (tempo e clima)
- Acredita-se que em previsões curtas é importante os prognósticos das variáveis de superfície



 Na camada atmosférica superficial (~50m) ou base da CLP os fluxos são computados comumente baseados na teoria de similaridade de Monin-Obukhov (modelos mais modernos)

 Os modelos de PNT devem calcular corretamente a redistribuição de calor e vapor por turbilhões próximos a superfície

 Esta camada tem uma profundidade que varia diurna, sazonalmente e geograficamente

 Devido a isto os modelos de PNT <u>devem</u> possuir suficientes níveis próximos a superfície para <u>resolver a estrutura vertical da CLP</u>

 Muitos níveis também não é desejável, devido a que a complexidade da CLP não pode ser resolvida com teorias simples (K)

• Um modelo de CLP pode ser complexo e custoso computacionalmente

 Em modelos de PNT o mais importante é o <u>intercambio de</u> <u>calor e umidade entre a CLP e a atmosfera livre</u> que uma detalhada CLP

 A transferência acima da CLP é acompanhada por convecção cumulus e ondas de gravidade, e por velocidades verticais da larga escala

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + \frac{2\Omega\eta_3(\overline{v})}{\partial y} - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{w'v'})}{\partial z} - \frac{\partial(\overline{v'v'})}{\partial z} - \frac{\partial(\overline{v'v'}$$

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - \frac{2\Omega\eta_3(\overline{u})}{\partial x} - \nu\frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{w'u'})}{\partial z} - \frac{\partial(\overline{u'u'})}{\partial z} - \frac{\partial(\overline{u'$$

$$\frac{\partial(\overline{w})}{\partial t} + (\overline{u})\frac{\partial(\overline{w})}{\partial x} + (\overline{v})\frac{\partial(\overline{w})}{\partial y} + (\overline{w})\frac{\partial(\overline{w})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial z} + g\frac{\overline{\rho}}{\rho_0} - \nu\frac{\partial^2(\overline{w})}{\partial x^2} - \nu\frac{\partial^2(\overline{w})}{\partial y^2} - \nu\frac{\partial^2(\overline{w})}{\partial z^2} = -\frac{\partial(\overline{u'w'})}{\partial x} - \frac{\partial(\overline{v'w'})}{\partial y} - \frac{\partial(\overline{w'w'})}{\partial z} - \frac{\partial(\overline{w'w'})}{$$

$$\frac{\partial(\overline{T})}{\partial t} + (\overline{u})\frac{\partial(\overline{T})}{\partial x} + (\overline{v})\frac{\partial(\overline{T})}{\partial y} + (\overline{w})\frac{\partial(\overline{T})}{\partial z} - S_{P}\overline{\omega} = -\frac{\partial(\overline{u'T'})}{\partial x} - \frac{\partial(\overline{v'T'})}{\partial y} - \frac{\partial(\overline{w'T'})}{\partial z} + \frac{\overline{J}}{C_{P}}$$

$$\frac{\partial(\overline{q})}{\partial t} + (\overline{u})\frac{\partial(\overline{q})}{\partial x} + (v)\frac{\partial(\overline{q})}{\partial y} + (\overline{w})\frac{\partial(\overline{q})}{\partial z} = -\frac{\partial(\overline{u'q'})}{\partial x} - \frac{\partial(\overline{u'q'})}{\partial y} - \frac{\partial(\overline{w'q'})}{\partial z} + \overline{S}$$

$$u_3 = w$$

$$x_3 = z$$

$$v \frac{\partial^2 (\overline{u_3})}{\partial x_3^2} \cong 0$$

$$\frac{\partial \overline{u_i}}{\partial t} + \overline{u_j} \frac{\partial \overline{u_i}}{\partial x_j} = -\delta_{i3}g + f_c \varepsilon_{ij3} \overline{u_j} - \frac{1}{\rho} \frac{\partial \overline{P}}{\partial x_i} + \frac{\upsilon \partial^2 \overline{u_i}}{\partial x_j^2} - \frac{\partial \overline{(u_i' u_j')}}{\partial x_j}$$

Como parameterizar os momentum de 2 ordem $w' \varphi'$

$$\frac{\partial \bar{u}_i}{\partial t} = \frac{\partial \overline{u_i' u_j'}}{\partial x_j}$$

$$\overline{w'\varphi'} = K(z)\frac{d\varphi}{dz}$$

Teoria do transporte gradiente ou teoria K

Os fluxos de momento, calor ou matéria são difundidos por movimentos turbulentos dentro da camada limite.

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz}$$

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz} \qquad \qquad \frac{\partial \overline{u}_i}{\partial t} = \frac{\partial \overline{u_i'u_j'}}{\partial x_j}$$

Como parameterizar os momentum de 2 ordem $w' \varphi'$

$$\frac{\partial \bar{u}_i}{\partial t} = \frac{\partial}{\partial x_j} \left(\mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz} \right)$$

Desprezando a variação dos fluxos na horizontal.

$$\frac{\partial \bar{u}}{\partial t} = \mathbf{K}(\mathbf{z}) \frac{\partial}{\partial z} \left(\frac{d\varphi}{dz} \right) + \frac{\partial \mathbf{K}(\mathbf{z})}{\partial z} \left(\frac{d\varphi}{dz} \right)$$

Qual a importância numérica da PBL nos MCGAs?

Como Parametrizar os Fluxos Turbulentos na camada limite superficial

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz}$$

$$\frac{\partial(\overline{u})}{\partial t} + (\overline{u})\frac{\partial(\overline{u})}{\partial x} + (\overline{v})\frac{\partial(\overline{u})}{\partial y} + (\overline{w})\frac{\partial(\overline{u})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial x} - 2\Omega\eta_3(\overline{v}) - \nu\frac{\partial^2(\overline{u})}{\partial x^2} - \nu\frac{\partial^2(\overline{u})}{\partial y^2} - \nu\frac{\partial^2(\overline{u})}{\partial z^2} = -\frac{\partial(\overline{u'u'})}{\partial x} - \frac{\partial(\overline{v'u'})}{\partial y} - K(z)\frac{\partial^2\overline{u}}{\partial z^2}$$

$$\frac{\partial(\overline{v})}{\partial t} + (\overline{u})\frac{\partial(\overline{v})}{\partial x} + (\overline{v})\frac{\partial(\overline{v})}{\partial y} + (\overline{w})\frac{\partial(\overline{v})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial y} + 2\Omega\eta_3(\overline{u}) - \nu\frac{\partial^2(\overline{v})}{\partial x^2} - \nu\frac{\partial^2(\overline{v})}{\partial y^2} - \nu\frac{\partial^2(v)}{\partial z^2} = -\frac{\partial(\overline{u'v'})}{\partial x} - \frac{\partial(\overline{v'v'})}{\partial y} - K(z)\frac{\partial^2\overline{v}}{\partial z^2}$$

$$\frac{\partial(\overline{w})}{\partial t} + (\overline{u})\frac{\partial(\overline{w})}{\partial x} + (\overline{v})\frac{\partial(\overline{w})}{\partial y} + (\overline{w})\frac{\partial(\overline{w})}{\partial z} + \frac{1}{\rho_0}\frac{\partial(\overline{P})}{\partial z} + g\frac{\overline{\rho}}{\rho_0} - \nu\frac{\partial^2(\overline{w})}{\partial x^2} - \nu\frac{\partial^2(\overline{w})}{\partial y^2} - \nu\frac{\partial^2(\overline{w})}{\partial z^2} = -\frac{\partial(\overline{u'w'})}{\partial x} - \frac{\partial(\overline{v'w'})}{\partial y} - \frac{\partial(\overline{w'w'})}{\partial z} - \frac{\partial(\overline{w'w'})}{$$

$$\frac{\partial(\overline{T})}{\partial t} + (\overline{u})\frac{\partial(\overline{T})}{\partial x} + (\overline{v})\frac{\partial(\overline{T})}{\partial y} + (\overline{w})\frac{\partial(\overline{T})}{\partial z} - S_P\overline{\omega} = -\frac{\partial(\overline{u'T'})}{\partial x} - \frac{\partial(\overline{v'T'})}{\partial y} - K(z)\frac{\partial^2\overline{T}}{\partial^2z} + \frac{\overline{J}}{C_p}$$

$$\frac{\partial(\overline{q})}{\partial t} + (\overline{u})\frac{\partial(\overline{q})}{\partial x} + (v)\frac{\partial(\overline{q})}{\partial y} + (\overline{w})\frac{\partial(\overline{q})}{\partial z} = -\frac{\partial(\overline{u'q'})}{\partial x} - \frac{\partial(\overline{u'q'})}{\partial y} - K(z)\frac{\partial^2\overline{q}}{\partial^2z} + \overline{S}$$

$$u_3 = w$$

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$$v \frac{\partial^2(\overline{u_3})}{\partial x_3^2} \cong 0$$

$$\frac{\partial(\overline{u})}{\partial t} = -\mathbf{K}(\mathbf{z}) \frac{\partial^2 \overline{u}}{\partial^2 \mathbf{z}}$$

$$\frac{\partial(\overline{v})}{\partial t} = -\mathbf{K}(\mathbf{z}) \frac{\partial^2 \overline{v}}{\partial^2 \mathbf{z}}$$

$$\frac{\partial(\overline{T})}{\partial t} = -K(z) \frac{\partial^2 \overline{T}}{\partial^2 z}$$

$$\frac{\partial(\overline{q})}{\partial t} = -K(z) \frac{\partial^2 \overline{q}}{\partial^2 z}$$

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz}$$

Teoria K

Assume-se um equilíbrio entre os fluxos verticais de sub-grade e a <u>estrutura</u>
 vertical na grade, <u>os fluxos horizontais na sub-grade são desprezíveis</u>

- Isto permite o tratamento da CLP de forma 1-D (somente estrutura vertical)

Magnitude of Reynolds stress at ground surface (8.2) $|\tau_z| = \rho_a \left[\left(\overline{w'u'} \right)^2 + \left(\overline{w'v'} \right)^2 \right]^{1/2}$ Kinematic vertical turbulent momentum flux (m² s²) (8.3) $\overline{w'u'} = -\frac{\tau_{zy}}{\rho_a}$ $\overline{w'v'} = -\frac{\tau_{zy}}{\rho_a}$

Vertical turbulent sensible-heat flux (W m⁻²) (8.4)
$$H_f = \rho_a c_{p,d} \overline{w'\theta'_v}$$
Kinematic vert turbulent sensible-heat flux (m K s⁻¹) (8.5)

Kinematic vert. turbulent sensible-heat flux (m K s⁻¹) (8.5)
$$\overline{w'\theta'_v} = \frac{H_f}{\rho_a c_{p,d}}$$

Vertical turbulent water vapor flux (kg m² s¹) (8.6)
$$E_f = \rho_a \overline{w' q'_v}$$
Kinematic vert. turbulent moisture flux (m kg s¹ kg¹) (8.7)
$$\overline{w' q'_v} = \frac{E_f}{w' q'_v}$$

$$\frac{\partial(\overline{u})}{\partial t} = -\mathbf{K}(\mathbf{z}) \frac{\partial^2 \overline{u}}{\partial^2 \mathbf{z}}$$

$$\frac{\partial(\overline{v})}{\partial t} = -\mathbf{K}(\mathbf{z}) \; \frac{\partial^2 \overline{v}}{\partial^2 z}$$

$$\frac{\partial(\overline{T})}{\partial t} = -K(z) \frac{\partial^2 \overline{T}}{\partial^2 z}$$

$$\frac{\partial(\overline{q})}{\partial t} = -K(z) \frac{\partial^2 \overline{q}}{\partial^2 z}$$

$$-C\emptyset_{j-1}^{n+1} + (1 + C)\emptyset_{j}^{n+1} = \emptyset_{j}^{n}$$

$$\begin{pmatrix} 1+C & 0 & 0 & 0 & 0 & 0 & -C \\ -C & 1+C & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -C & 1+C & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -C & 1+C & 0 & 0 & 0 & 0 \\ \vdots & \vdots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots \\ 0 & 0 & 0 & 0 & 0 & -C & 1+C & 0 \\ 0 & 0 & 0 & 0 & 0 & -C & 1+C & 0 \\ \end{pmatrix} \begin{pmatrix} \emptyset_1^{n+1} \\ \emptyset_2^{n+1} \\ \emptyset_3^{n+1} \\ \vdots \\ \emptyset_{j-1}^{n+1} \end{pmatrix} = \begin{pmatrix} \emptyset_1^n \\ \emptyset_2^n \\ \emptyset_2^n \\ \emptyset_3^n \\ \emptyset_4^n \\ \vdots \\ \emptyset_{j-2}^n \\ \emptyset_{j-1}^n \end{pmatrix}$$

 A equação anterior complica a solução e adiciona termos desconhecidos

Porém nos fornece algumas informações diagnosticas

Suposição no problema de fechamento: <u>relação linear fluxo-gradiente ou teoria K</u>

 Assume-se que o gradiente médio (temperatura ou umidade) dirige o fluxo turbulento (calor ou umedecimento)

Magnitude of Reynolds stress at ground surface (8.2)
$$|\tau_z| = \rho_a \left[\left(\overline{w'u'} \right)^2 + \left(\overline{w'v'} \right)^2 \right]^{1/2}$$
Kinematic vertical turbulent momentum flux (m² s²) (8.3)
$$\overline{w'u'} = -\frac{\tau_{zy}}{\rho_a}$$

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Vertical turbulent sensible-heat flux (W m²) (8.4)
$$H_f = \rho_a c_{p,d} \overline{w'} \Theta'_v$$
Kinematic vert. turbulent sensible-heat flux (m K s⁻¹) (8.5)
$$\overline{w'} \Theta'_v = \frac{H_f}{\rho_a c_{p,d}}$$

Vertical turbulent water vapor flux (kg m² s¹) (8.6)
$$E_f = \rho_a \overline{w'q'_{\nu}}$$
Kinematic vert. turbulent moisture flux (m kg s¹ kg¹) (8.7)
$$\overline{w'q'_{\nu}} = \frac{E_f}{\rho_a}$$

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz}$$

$$H = \rho_a c_{pd} K_h \frac{\partial \overline{\theta_v}}{\partial z}$$

 $H = \rho_a c_{pd} \overline{w' \theta_{v'}}$

$$\mathrm{Ef} = \rho_a L_v K_q \frac{\partial \bar{q}}{\partial z}$$

 $\mathrm{Ef} = \rho_{\alpha} L_{n} w' q'$

• Onde $K_H(z)$, m²s⁻¹ é a difusividade turbulenta para calor, γ_d é o lapse rate adiabático

• Da mesma forma para o fluxo de umidade

$$\overline{w'\varphi'} = \mathbf{K}(\mathbf{z}) \frac{d\varphi}{dz}$$

Onde K(z) é a difusividade turbulenta para φ

Como parameterizar os momentum de 2 ordem $w'\phi'$ na CL Superficial

$$F = \rho K(z) \frac{d\varphi}{dz}$$
 $(F = \overline{w'\varphi'})$

Formulação em diferenças finitas

$$F_{1.5} = \rho \mathbf{K}(\mathbf{z}_{1.5}) \frac{\varphi_2 - \varphi_1}{z_2 - z_1}$$

Integral da camada superfície:

$$\varphi_1$$
- φ_s = $\int_{z_{o\varphi}}^{z_1} \frac{F_{o\varphi}}{\rho K(z)} dz$

Camada de fluxo ϕ_1 - $\phi_s \approx \frac{F_0}{\rho} \int_{z_{0\phi}}^{z_1} \frac{1}{K(z)} dz$ constante:

Escoamento $K(\mathbf{z}) = \kappa \mathbf{z} u_*$ neutro:

$$zu_*$$

$$\phi_1 - \phi_s \approx \frac{F_{0\phi}}{\rho \kappa u_*} \int_{z_{0\phi}}^{z_1} \frac{dz}{z} \qquad \Rightarrow \quad \phi_1 - \phi_s = \frac{F_{0\phi}}{\rho \kappa u_*} \ln \left(\frac{z_1}{z_{o\phi}}\right)$$

κ: Von Karman constant (0.4)

u_∗ : Friction velocity

ρ : Density



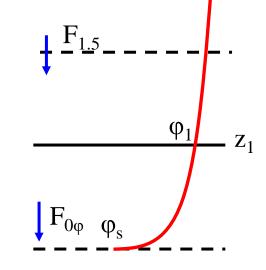
u,v,T,q

2 Nível do modelo

1.5 Nível dos fluxos

1 Nível do modelo

Superfície



Coeficientes de difusão de acordo com a similaridade MO

Conceito Básico de um modelo PBL

$$K_M = \frac{1}{\phi_m^2} l^2 \left| \frac{\partial U}{\partial z} \right|$$

$$K_{M} = \frac{1}{\phi_{m}^{2}} l^{2} \left| \frac{\partial U}{\partial z} \right| \qquad K_{H} = \frac{1}{\phi_{m} \phi_{h}} l^{2} \left| \frac{\partial U}{\partial z} \right| \qquad \bullet$$



Usando a relação entre R_i e $\frac{z}{r}$

$$R_{i} = \frac{g}{\theta_{v}} \frac{\frac{\partial \theta_{v}}{\partial z}}{\left|\frac{\partial U}{\partial z}\right|^{2}} = \frac{g}{\theta_{v}} \frac{z\theta_{*}\phi_{h}}{u_{*}^{2}\phi_{m}^{2}} = \frac{z}{\kappa L} \frac{\phi_{h}}{\phi_{m}^{2}}$$

$$\frac{1}{\phi_m^2} = \frac{\kappa L}{z \, \phi_h} R_i$$

$$\frac{1}{\phi_m \phi_h} = \frac{\phi_m \kappa L}{\phi_h^2} R_i$$

Resolver para
$$\frac{Z}{L} = \xi$$



$$K_M = l^2 \left| \frac{dU}{dz} \right| f_M(R_i)$$

$$K_H = l^2 \left| \frac{dU}{dz} \right| f_H(R_i)$$

Como parameterizar os momentum de 2 ordem $w'\phi'$, K_M , K_H

• Existe também a camada da superfície atmosférica nos 50 m próximos a superfície da CLP

 O movimento vertical e a mistura é limitado pela proximidade da superfície

 Os gradientes verticais do vento, temperatura e umidade são muitos grandes

Monin e Obuhkov estabeleceram uma teoria empírica da CS

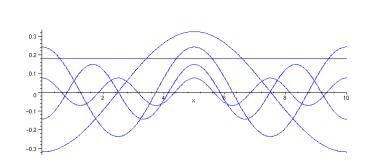
 Determinada pelos fluxos turbulentos de momentum e calor que a atravessam

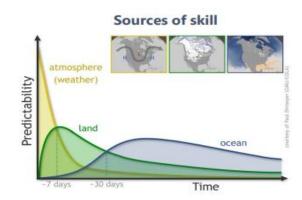
O problema da parametrização de camada limite planetária é determinar como será feita a difusão a cada instante do tempo

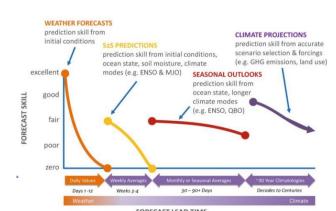
K(z, estabilidade, nebulosidade, radiação, turbulencia, etc)

K=K(z, estabilidade, nebulosidade, radiação, turbulencia, etc)?????? Precisa saber todos os fenômenos físicos que afetam o perfil vertical de de K_M , K_H

Como parameterizar os momentum de 2 ordem $w'\varphi'$, K_M , K_H







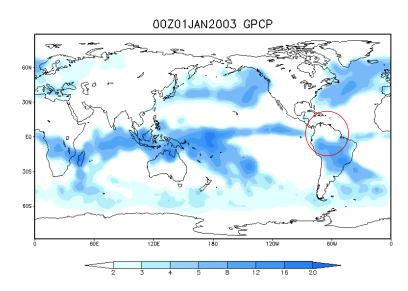
Desacoplamento das equações prognóstica da PBL e a Superfície

"ACOPLAMENTO" DO MCGA-CPTEC COM O IBIS "Precipitação"

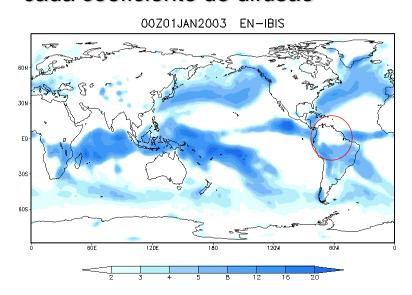
$$K_{h} = w_{1}K_{h_{MY}} + w_{2}K_{h_{TKE}} + w_{3}K_{h_{HB}}$$

$$K_{m} = w_{1}K_{m_{MY}} + w_{2}K_{m_{TKE}} + w_{3}K_{m_{HB}}$$

Observado GPCP



Simulação com o mesmo peso para cada coeficiente de difusão



Norte da AMAZ.:sul

NE:super.

Referências

- Stull, R. B., 1988: An Introduction to Boundary Layer Meteorology. Kluwer Academic, 666 pp.
- Chapter 5 of Holton, J. R., 1992: An Introduction to Dynamic Meteorology. Academic Press, New York, 511 pp.