

Equações diferenciais dos modelos de superficies



MET-576-4

Modelagem Numérica da Atmosfera

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Os métodos numéricos, formulação e parametrizações utilizados nos modelos atmosféricos serão descritos em detalhe.

3 Meses 24 Aulas (2 horas cada)





Superfície:

Métodos numéricos utilizados para resolução de problemas relacionados a parametrização de superfície.





- \checkmark 1 Basic concept of the Surface model .
- √ 2 Urban Canopy model.
- √ 3 Water Body model.
- √ 4 Green area model.





Conceito Basico de um modelo LSM

A energia radiativa absorvida pelo solo e pela atmosfera é dividida em fluxos de:

calor sensível,

calor latente,

calor no solo.

Essa partição (redistribuição da energia absorvida) depende fortemente das características:

Cobertura da terra

Regime hidrológico.





4 Green area model 35 4.3 Prognostic equations of the green area model 41 4.3.2 Governing equations for intercepted water 42 4.3.3 Governing equations for soil moisture stores 43 4.5 Turbulent transfer and aerodynamic resistances 47 4.5.2 Within the transition layer $(z2 \le z \le zt)$ 48 4.5.3 Within the canopy air space (CAS) $(z1 \le z \le z2) \dots 48$ 4.5.5 Solution of momentum transfer equation set 49





4.1.2 Estrutura do Modelo

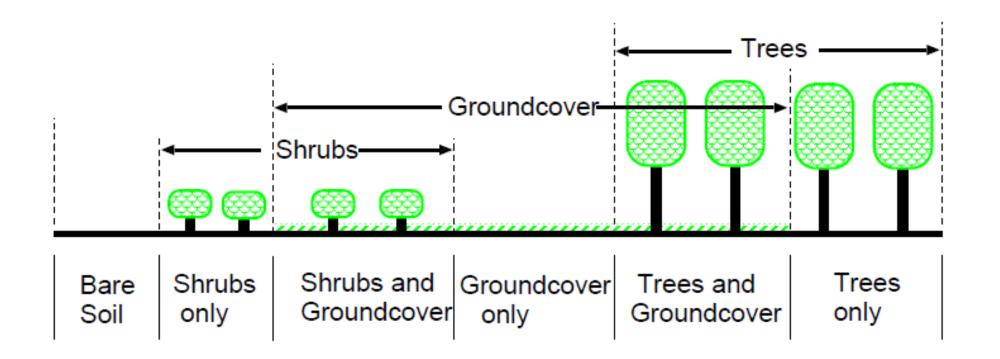


Figure 4.1: Vegetation morphology as represented in the Simple Biosphere (SiB). (Reproduced from Sellers et al., 1986)





4.1.2 Estrutura do Modelo

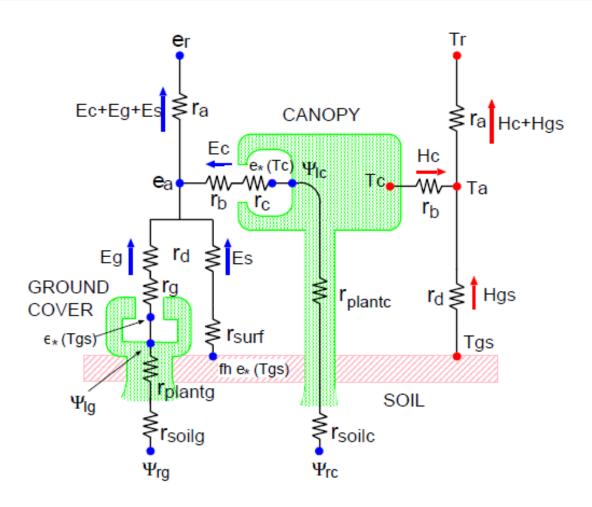


Figure 4.2: Framework of the SiB. The transfer pathways for latent and sensible heat fluxes are shown on the left- and right-hand sides of the diagram, respectively. (Reproduced from *Sellers et al.*, 1986; see this reference for symbol definitions.)





4.1.2 Estrutura do Modelo

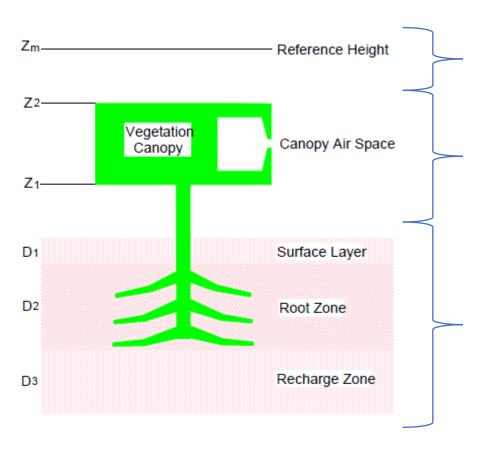


Figure 4.3: Structure of the green area model. (Reproduced from Sellers et al.,1996)





4.1.2 Structure of the Model

Interceptação da água pelo dossel

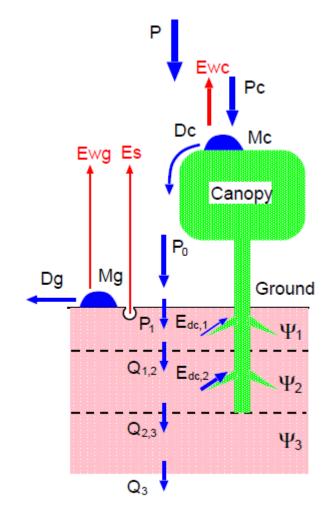


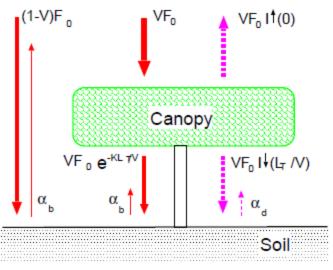
Figure 4.4: Schematic image of interception and water budget





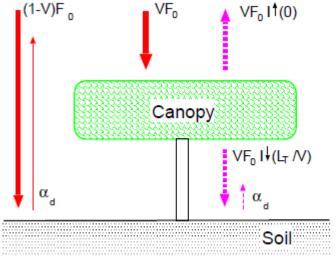
4.1.2 Estrutura do Modelo

Transferência radiativa de onda curta



Radiation Process (beam)

(a) direct beam



Radiation Process (diffuse)

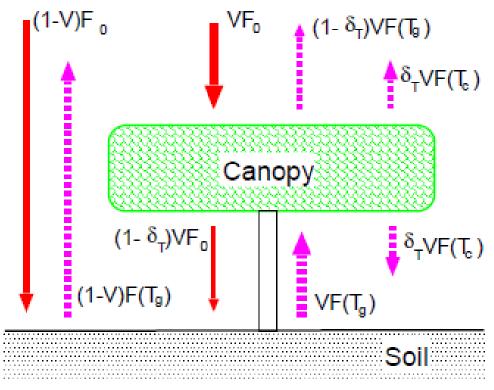
(b) diffuse





4.1.2 Estrutura do Modelo

Transferência radiativa de onda Longa



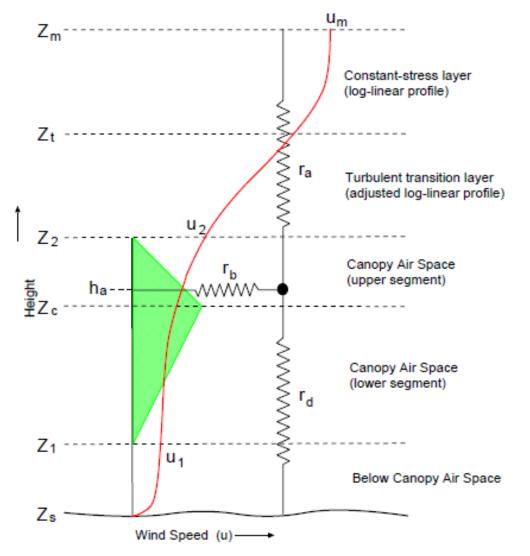
Radiation Process (TIR)

(c) thermal infrared





4.1.2 Estrutura do Modelo



Estrutura Aerodinâmica

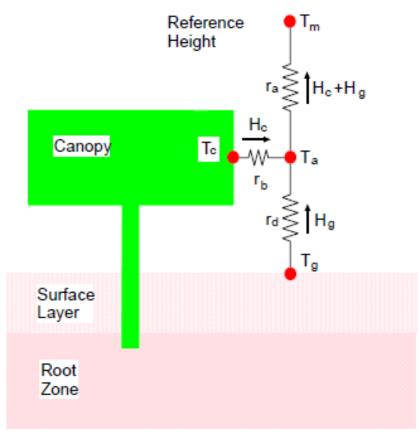
Figure 4.6: Turbulent transfer regimes considered in the first-order closure model. (Reproduced from Sellers et al.,1996)



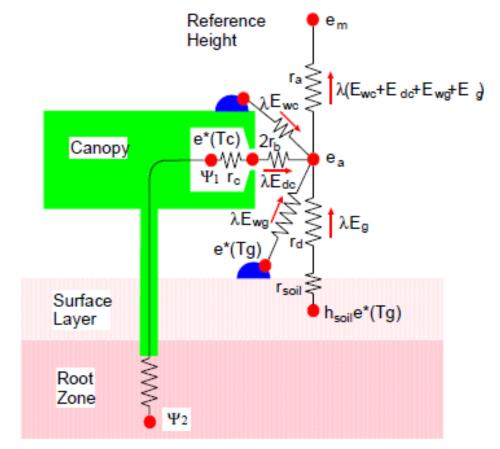


4.1.2 Estrutura do Modelo

Resistências (ra,rb,rd)



(a) Sensible heat flux



(b) Latent heat flux





4.8 Solução Numérica das Equações Prognosticas

Os fluxos de energia são funções explícitas das condições de contorno atmosférico, variáveis prognósticas, resistências aerodinâmicas e de superfície.

As equações prognósticas são resolvidas por um método implícito backward, usando derivadas parciais de cada termo.

Primeiro, considerando que os fluxos de energia nas equações prognósticas são funções da temperatura.

Em seguida, as equações prognósticas são expressas na forma de diferenciação explícita backward e um conjunto de equações simultâneas lineares relacionadas às mudanças de temperatura ao longo de um intervalo de tempo (Δt) é obtido.

Não apenas os fluxos de energia, mas também os termos de troca de calor dependem das temperaturas.

Agora, as equações prognósticas podem ser escritas em forma de tempo discreto.





4.8 Solução Numérica das Equações Prognosticas

$$C_c \frac{\partial T_c}{\partial t} = Rn_c - H_c - \lambda E_c$$

$$C_g \frac{\partial T_g}{\partial t} = Rn_g - H_g - \lambda E_g - \omega C_g (T_g - T_d)$$

$$C_d \frac{\partial T_d}{\partial t} = Rn_g - H_g - \lambda E_g$$

Supõem-se que <u>cada termo do lado direito da equação tenha uma variação infinitesimal</u> Expansão em série de Taylor

$$f(x) = f(x_0) + \frac{1}{1!} \frac{\partial f}{\partial x} (x - x_0)^1 + \frac{1}{2!} \frac{\partial^2 f}{\partial x^2} (x - x_0)^2 + \cdots$$





$$C_{c} \frac{\Delta T_{c}}{\Delta t} = Rn_{c} - H_{c} - \lambda E_{c} + \left(\frac{\partial Rn_{c}}{\partial T_{c}} - \frac{\partial H_{c}}{\partial T_{c}} - \frac{\partial \lambda E_{c}}{\partial T_{c}}\right) \Delta T_{c} + \left(\frac{\partial Rn_{c}}{\partial T_{g}} - \frac{\partial H_{c}}{\partial T_{g}} - \frac{\partial \lambda E_{c}}{\partial T_{g}}\right) \Delta T_{g}$$
(4.85)

$$C_{g} \frac{\Delta T_{g}}{\Delta t} = Rn_{g} - H_{g} - \lambda E_{g} - \omega C_{g} (T_{g} - T_{d}) + \left(\frac{\partial Rn_{g}}{\partial T_{c}} - \frac{\partial H_{g}}{\partial T_{c}} - \frac{\partial \lambda E_{g}}{\partial T_{c}}\right) \Delta T_{c}$$

$$+ \left(\frac{\partial Rn_{g}}{\partial T_{g}} - \frac{\partial H_{g}}{\partial T_{g}} - \frac{\partial \lambda E_{g}}{\partial T_{g}} - \omega C_{g}\right) \Delta T_{g} + \omega C_{g} \Delta T_{d}$$

$$(4.86)$$

$$C_{d} \frac{\Delta T_{d}}{\Delta t} = Rn_{g} - H_{g} - \lambda E_{g} + \left(\frac{\partial Rn_{g}}{\partial T_{c}} - \frac{\partial H_{g}}{\partial T_{c}} - \frac{\partial \lambda E_{g}}{\partial T_{c}}\right) \Delta T_{c} + \left(\frac{\partial Rn_{g}}{\partial T_{g}} - \frac{\partial H_{g}}{\partial T_{g}} - \frac{\partial \lambda E_{g}}{\partial T_{g}}\right) \Delta T_{g}$$
(4.87)





4.8 Solução Numérica das Equações Prognosticas

If it is written in matrix form,

$$KX = Y \longrightarrow X = K^{-1}Y$$

$$K = \begin{bmatrix} K_{1,1} & K_{1,2} & K_{1,3} \\ K_{2,1} & K_{2,2} & K_{2,3} \\ K_{3,1} & K_{3,2} & K_{3,3} \end{bmatrix} \qquad X = \begin{bmatrix} \Delta T_c \\ \Delta T_g \\ \Delta T_d \end{bmatrix}$$

$$\begin{split} K_{1,1} &= \frac{C_c}{\Delta t} - \frac{\partial Rn_c}{\partial T_c} + \frac{\partial H_c}{\partial T_c} + \frac{\partial \lambda E_c}{\partial T_c} & K_{1,2} = -\frac{\partial Rn_c}{\partial T_g} + \frac{\partial H_c}{\partial T_g} + \frac{\partial \lambda E_c}{\partial T_g} & K_{1,3} = 0 \\ K_{2,1} &= -\frac{\partial Rn_g}{\partial T_c} + \frac{\partial H_g}{\partial T_c} + \frac{\partial \lambda E_g}{\partial T_c} & K_{2,2} = \frac{C_g}{\Delta t} - \frac{\partial Rn_g}{\partial T_g} + \frac{\partial H_g}{\partial T_g} + \frac{\partial \lambda E_g}{\partial T_g} + \omega C_g & K_{2,3} = -\omega C_g \\ K_{3,1} &= -\frac{\partial Rn_g}{\partial T_c} + \frac{\partial H_g}{\partial T_c} + \frac{\partial \lambda E_g}{\partial T_c} & K_{3,2} = -\frac{\partial Rn_g}{\partial T_g} + \frac{\partial H_g}{\partial T_g} + \frac{\partial \lambda E_g}{\partial T_g} & K_{3,3} = \frac{C_d}{\Delta t} \end{split}$$





$$\begin{split} K_{1,1} &= \frac{C_c}{\Delta t} - \frac{\partial Rn_c}{\partial T_c} + \frac{\partial H_c}{\partial T_c} + \frac{\partial \lambda E_c}{\partial T_c} & K_{1,2} = -\frac{\partial Rn_c}{\partial T_g} + \frac{\partial H_c}{\partial T_g} + \frac{\partial \lambda E_c}{\partial T_g} & K_{1,3} = 0 \\ K_{2,1} &= -\frac{\partial Rn_g}{\partial T_c} + \frac{\partial H_g}{\partial T_c} + \frac{\partial \lambda E_g}{\partial T_c} & K_{2,2} = \frac{C_g}{\Delta t} - \frac{\partial Rn_g}{\partial T_g} + \frac{\partial H_g}{\partial T_g} + \frac{\partial \lambda E_g}{\partial T_g} + \omega C_g & K_{2,3} = -\omega C_g \\ K_{3,1} &= -\frac{\partial Rn_g}{\partial T_c} + \frac{\partial H_g}{\partial T_c} + \frac{\partial \lambda E_g}{\partial T_c} & K_{3,2} = -\frac{\partial Rn_g}{\partial T_g} + \frac{\partial H_g}{\partial T_g} + \frac{\partial \lambda E_g}{\partial T_g} & K_{3,3} = \frac{C_d}{\Delta t} \end{split}$$

$$Y = \begin{bmatrix} Rn_c - H_c - \lambda E_c \\ Rn_g - H_g - \lambda E_g - \omega C_g (T_g - T_d) \\ Rn_g - H_g - \lambda E_g \end{bmatrix}$$

$$KX = Y \longrightarrow X = K^{-1}Y$$





- As equações acima podem ser resolvidas em termos de mudanças de temperatura (ΔTc, ΔTg, ΔTd).
- Cada temperatura é atualizada para o valor no tempo $t_0 + \Delta t$ adicionando alterações de temperatura ao valor inicial no tempo t_0 .
- Além disso, os fluxos de energia são modificados para mostrar os valores médios ao longo de um intervalo de tempo (entre o tempo t_0 e o tempo $t_0 + \Delta t$).





$$f(x) = f(x_0) + \frac{1}{1!} \frac{\partial f}{\partial x} (x - x_0)^1 + \frac{1}{2!} \frac{\partial^2 f}{\partial x^2} (x - x_0)^2 + \cdots$$

$$Rn'_{c} = Rn_{c} + \frac{1}{2} \left(\frac{\partial Rn_{c}}{\partial T_{c}} \Delta T_{c} + \frac{\partial Rn_{c}}{\partial T_{g}} \Delta T_{g} \right)$$
 (4.88)

$$Rn'_g = Rn_g + \frac{1}{2} \left(\frac{\partial Rn_g}{\partial T_c} \Delta T_c + \frac{\partial Rn_g}{\partial T_g} \Delta T_g \right)$$
 (4.89)

$$H'_{c} = H_{c} + \frac{1}{2} \left(\frac{\partial H_{c}}{\partial T_{c}} \Delta T_{c} + \frac{\partial H_{c}}{\partial T_{g}} \Delta T_{g} \right)$$
 (4.90)

$$H'_g = H_g + \frac{1}{2} \left(\frac{\partial H_g}{\partial T_c} \Delta T_c + \frac{\partial H_g}{\partial T_g} \Delta T_g \right)$$
 (4.91)

$$\lambda E_c' = \lambda E_c + \frac{1}{2} \left(\frac{\partial \lambda E_c}{\partial T_c} \Delta T_c + \frac{\partial \lambda E_c}{\partial T_g} \Delta T_g \right)$$

$$(4.92)$$

$$\lambda E_g' = \lambda E_g + \frac{1}{2} \left(\frac{\partial \lambda E_g}{\partial T_c} \Delta T_c + \frac{\partial \lambda E_g}{\partial T_g} \Delta T_g \right)$$

$$(4.93)$$





$$Rn_{wb} = (F_{vb} + F_{nb})(1 - \alpha_b) + (F_{vd} + F_{nd})(1 - \alpha_d) + F_{td} - \varepsilon_w \sigma T_{wb}^4$$

$$H_{wb} = \rho C_p \frac{T_{wb} - T_m}{r_{aw}} = A(T_{wb} - T_m)$$

 $\lambda E_{wb} = \frac{\rho C_p}{\gamma} \frac{e_*(T_{wb}) - e_m}{r_{aw}} = D[e_*(T_{wb}) - e_m]$

$$\frac{\partial Rn_{wb}}{\partial T_{wb}} = -4\sigma \varepsilon_w T_{wb}^3$$

$$\frac{\partial H_{wb}}{\partial T_{wb}} = \frac{\rho_a C_p}{r_{aw}}$$

$$\frac{\partial \lambda E_{wb}}{\partial T_{wb}} = \frac{\rho C_p}{\gamma} \frac{e'_*(T_{wb})}{r_{aw}}$$





$$\lambda E_{c} = \lambda E_{wc} + \lambda E_{dc} = D(e_{*}(T_{c}) - e_{a}), \quad D = \frac{\rho C_{p}}{\gamma} \left[\frac{W_{c}}{2r_{b}} + \frac{1 - W_{c}}{r_{c} + 2r_{b}} \right]$$

$$\lambda E_{g} = \lambda E_{wg} + \lambda E_{s} = E(e_{*}(T_{g}) - e_{a}), \quad E = \frac{\rho C_{p}}{\gamma} \left[\frac{W_{g}}{r_{d}} + \frac{f_{h}e_{*}(T_{g}) - e_{a}}{(r_{surf} + r_{d})(e_{*}(T_{g}) - e_{a})} \right]$$

$$\lambda E_{c} + \lambda E_{g} = F(e_{a} - e_{m}), \quad F = \frac{\rho C_{p}}{\gamma r_{a}}$$

$$(4.81)$$

$$H_c = \frac{T_c - T_a}{r_b} \rho C_p = A(T_c - T_a), \quad A = \rho C_p/r_b$$
 (4.77)
 $H_g = \frac{T_g - T_a}{r_d} \rho C_p = B(T_g - T_a), \quad B = \rho C_p/r_d$ (4.78)
 $H_c + H_g = \frac{T_a - T_m}{r_a} \rho C_p = C(T_a - T_m), \quad C = \rho C_p/r_a$ (4.79)

$$F_{T,d(c)} = \delta_T V_c F_{T,d(0)} - 2\delta_T V_c \sigma T_c^4 + \delta_T V_c \sigma T_g^4$$

$$F_{T,d(g)} = (1 - \delta_T V_c) F_{T,d(0)} + \delta_T V_c \sigma T_c^4 - \sigma T_g^4$$

$$Rn_c = \sum_{\sigma} F_{\Lambda,\mu(c)} = F_{V,b(c)} + F_{N,b(c)} + F_{V,d(c)} + F_{N,d(c)} + F_{T,d(c)}$$

$$Rn_g = \sum_{\sigma} F_{\Lambda,\mu(g)} = F_{V,b(g)} + F_{N,b(g)} + F_{V,d(g)} + F_{N,d(g)} + F_{T,d(g)}$$