

Chapter 10 Compressible Flow through Nozzles, Diffusers and Wind Tunnels

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Chapter 10 通过喷管、扩压器和风洞的可压缩流

10.1 引言P670

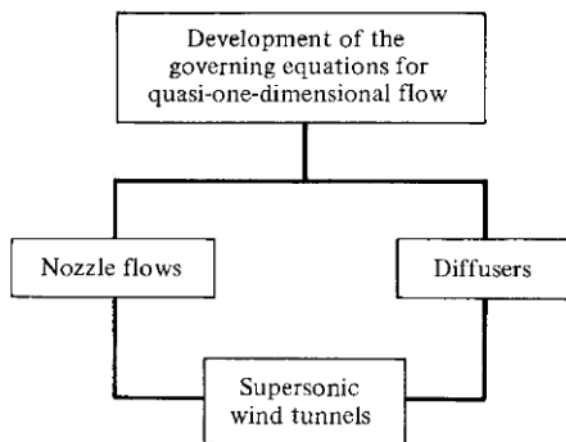


Figure 10.5 Road map for Chapter 10.

10.2 准一维流动的控制方程P672

10.3 喷管流动P681

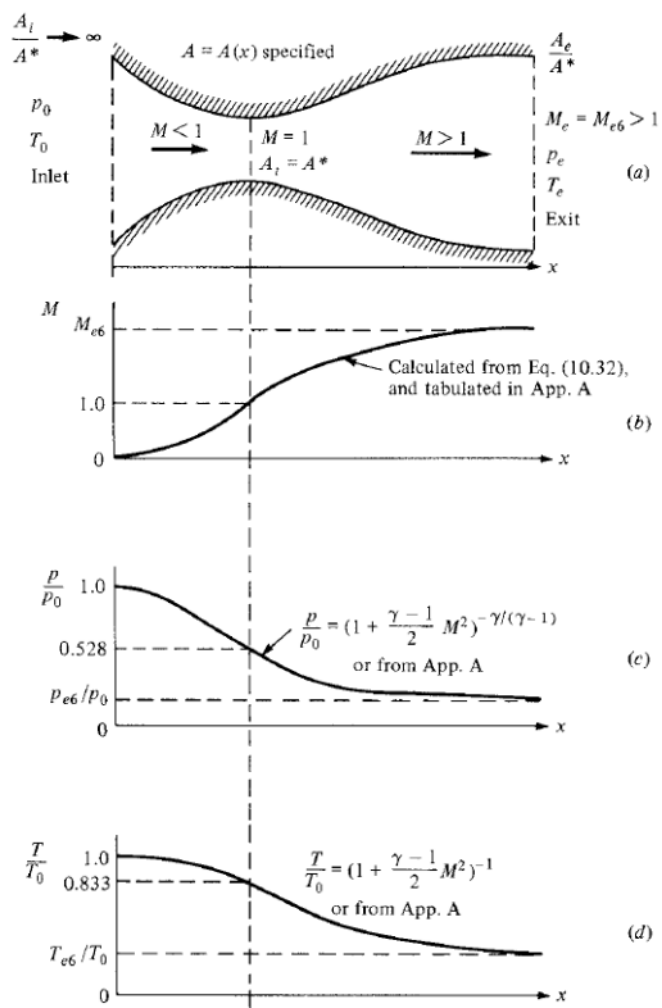
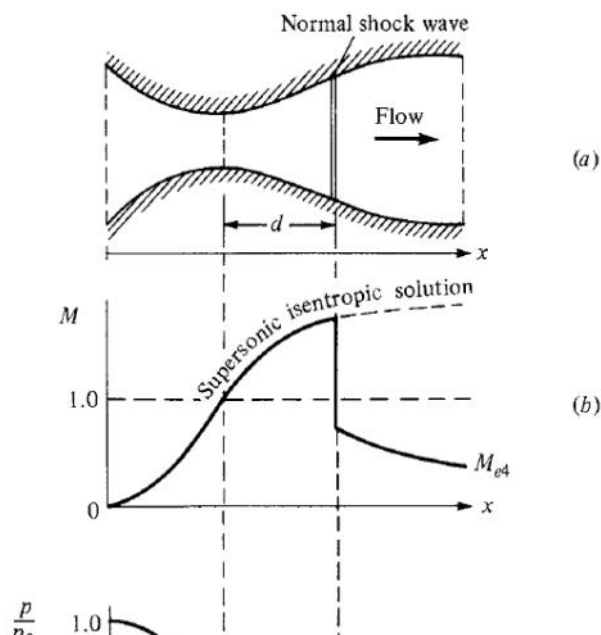
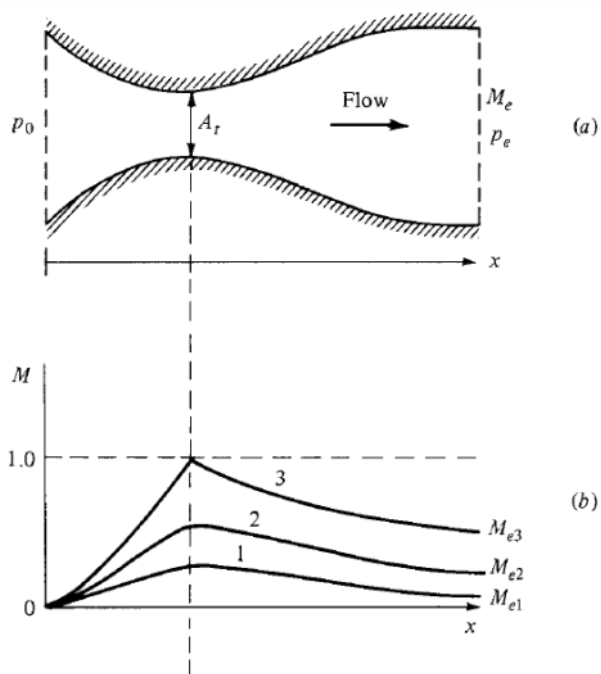


Figure 10.12 Isentropic supersonic nozzle flow.



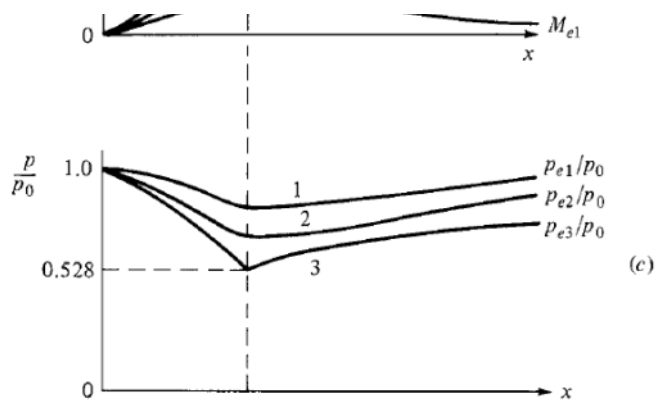


Figure 10.13 Isentropic subsonic nozzle flow.

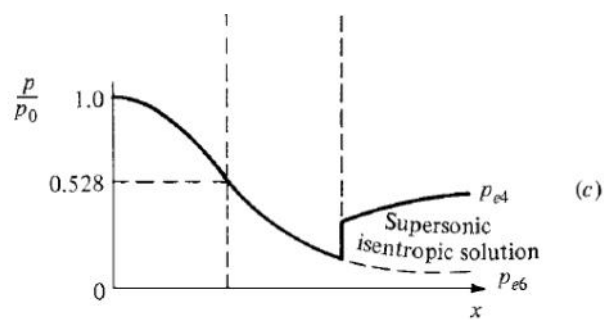


Figure 10.15 Supersonic nozzle flow with a normal shock inside the nozzle.

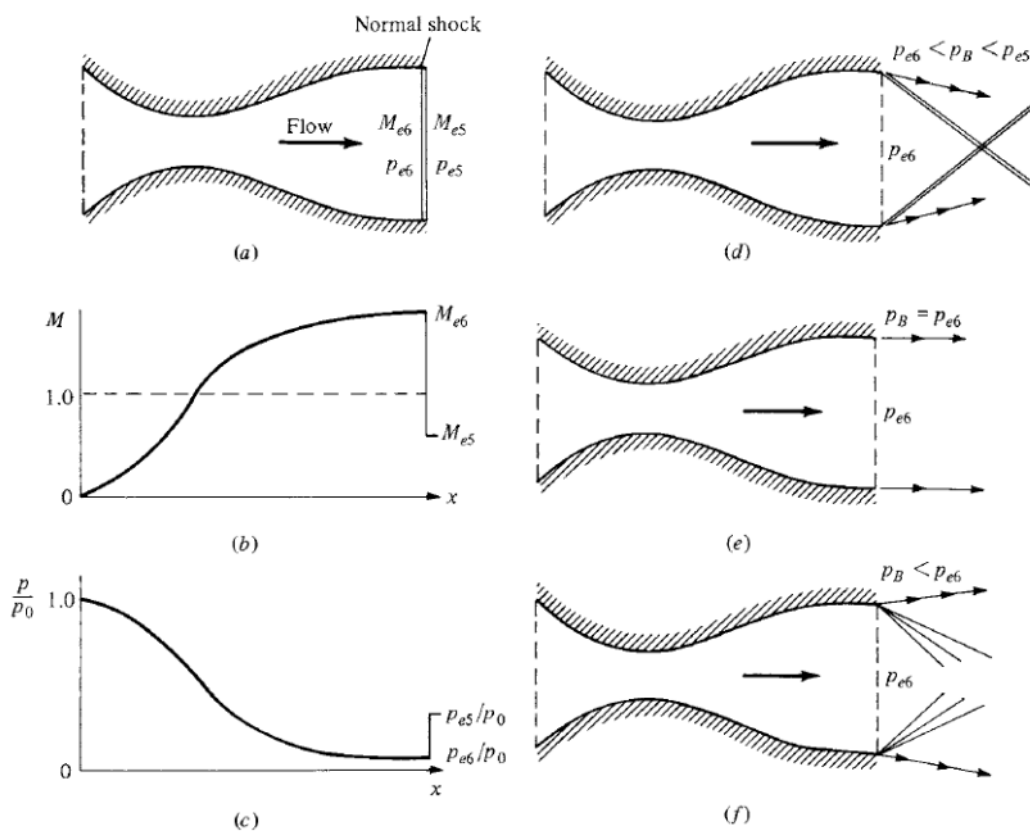
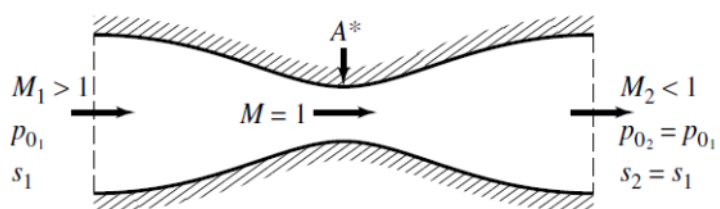


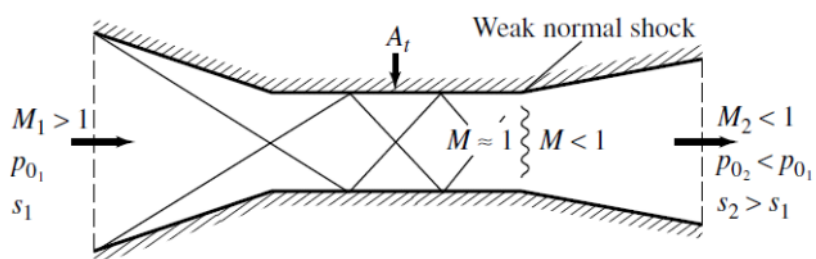
Figure 10.16 Supersonic nozzle flows with waves at the nozzle exit: (a), (b), and (c) pertain to a normal shock at the exit, (d) overexpanded nozzle, (e) isentropic expansion to the back pressure equal to the exit pressure, (f) underexpanded nozzle.

10.3.1 更多关于质量流的讨论P695

10.4 扩压器P696



(a) Ideal (isentropic) supersonic diffuser



(b) Actual supersonic diffuser

Figure 10.17 The ideal (isentropic) diffuser compared with the actual situation.

10.5 超声速风洞P698

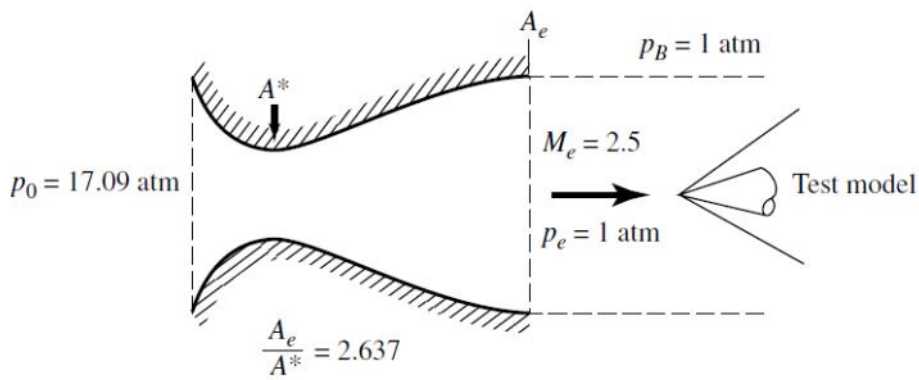


Figure 10.18 Nozzle exhausting directly to the atmosphere.

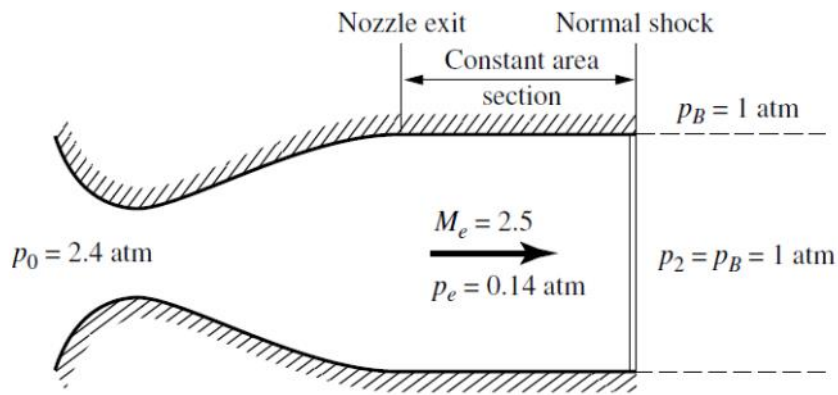


Figure 10.19 Nozzle exhausting into a constant-area duct, where a normal shock stands at the exit of the duct.

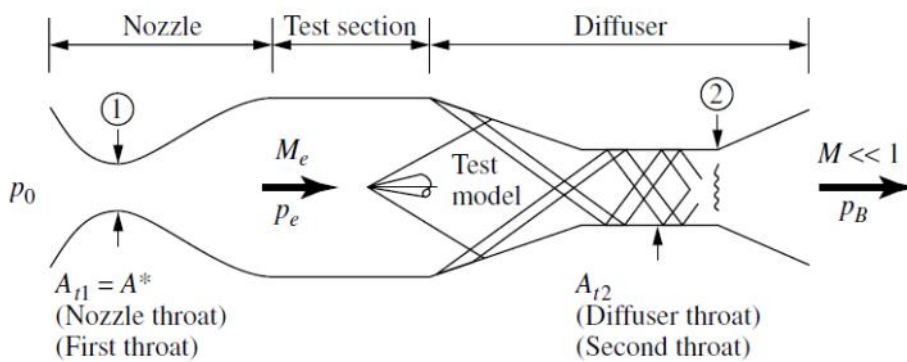


Figure 10.20 Sketch of a supersonic wind tunnel.

10.6 粘性流动：喷管内的激波/边界层干扰P704

10.7 总结P706

Quasi-one-dimensional flow is an approximation to the actual three-dimensional flow in a variable-area duct; this approximation assumes that $p = p(x)$, $u = u(x)$, $T = T(x)$, etc., although the area varies as $A = A(x)$. Thus, we can visualize the quasi-one-dimensional results as giving the mean properties at a given station, averaged over the cross section. The quasi-one-dimensional flow assumption gives reasonable results for many internal flow problems; it is a “workhorse” in the everyday application of compressible flow. The governing equations for this are

$$\text{Continuity:} \quad \rho_1 u_1 A_1 = \rho_2 u_2 A_2 \quad (10.1)$$

$$\text{Momentum:} \quad p_1 A_1 + \rho_1 u_1^2 A_1 + \int_{A_1}^{A_2} p \, dA = p_2 A_2 + \rho_2 u_2^2 A_2 \quad (10.5)$$

$$\text{Energy:} \quad h_1 + \frac{u_1^2}{2} = h_2 + \frac{u_2^2}{2} \quad (10.9)$$

The area velocity relation

$$\frac{dA}{A} = (M^2 - 1) \frac{du}{u} \quad (10.25)$$

tells us that

1. To accelerate (decelerate) a subsonic flow, the area must decrease (increase).
2. To accelerate (decelerate) a supersonic flow, the area must increase (decrease).
3. Sonic flow can only occur at a throat or minimum area of the flow.

The isentropic flow of a calorically perfect gas through a nozzle is governed by the relation

$$\left(\frac{A}{A^*}\right)^2 = \frac{1}{M^2} \left[\frac{2}{\gamma + 1} \left(1 + \frac{\gamma - 1}{2} M^2 \right) \right]^{(\gamma+1)/(\gamma-1)} \quad (10.32)$$

This tells us that the Mach number in a duct is governed by the ratio of local duct area to the sonic throat area; moreover, for a given area ratio, there are two values of Mach number that satisfy Equation (10.32)—a subsonic value and a supersonic value.

For a given convergent-divergent duct, there is only one possible isentropic flow solution for supersonic flow; in contrast, there are an infinite number of subsonic isentropic solutions, each one associated with a different pressure ratio across the nozzle, $p_0/p_e = p_0/p_B$.

In a supersonic wind tunnel, the ratio of second throat area to first throat area should be approximately

$$\frac{A_{t,2}}{A_{t,1}} = \frac{p_{0,1}}{p_{0,2}} \quad (10.39)$$

If $A_{t,2}$ is reduced much below this value, the diffuser will choke and the tunnel will unstart.

10.8 作业题P707