

## Chapter 8 正激波以及相关概论

### 8.1 引言P550

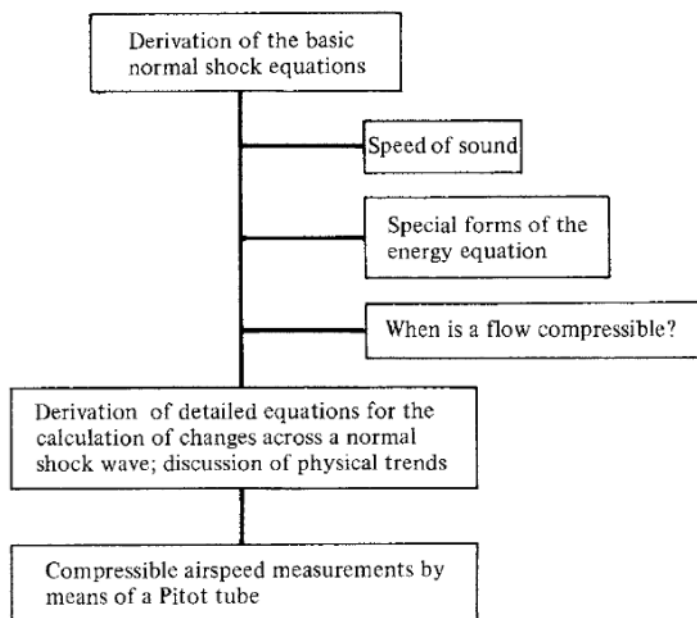


Figure 8.2 Road map for Chapter 8.

### 8.2 正激波基本方程P551

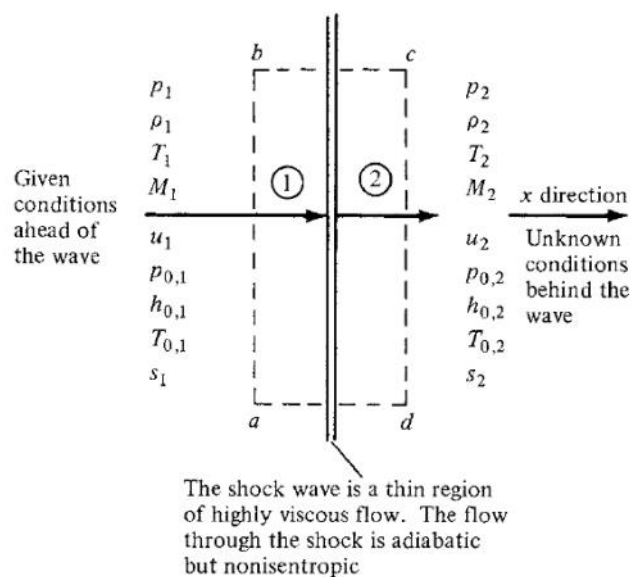


Figure 8.3 Sketch of a normal wave.

### 8.3 声速P555

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The speed of sound in a gas is given by

$$a = \sqrt{\left(\frac{\partial p}{\partial \rho}\right)_s} \quad (8.18)$$

For a calorically perfect gas,

$$a = \sqrt{\frac{\gamma p}{\rho}} \quad (8.23)$$

or

$$a = \sqrt{\gamma R T} \quad (8.25)$$

The speed of sound depends only on the gas temperature.

For a steady, adiabatic, inviscid flow, the energy equation can be expressed as

$$h_1 + \frac{u_1^2}{2} = h_2 + \frac{u_2^2}{2} \quad (8.29)$$

$$c_p T_1 + \frac{u_1^2}{2} = c_p T_2 + \frac{u_2^2}{2} \quad (8.30)$$

(continued)

$$\frac{a_1^2}{\gamma - 1} + \frac{u_1^2}{2} = \frac{a_2^2}{\gamma - 1} + \frac{u_2^2}{2} \quad (8.32)$$

$$\frac{a^2}{\gamma - 1} + \frac{u^2}{2} = \frac{a_0^2}{\gamma - 1} \quad (8.33)$$

$$\frac{a^2}{\gamma - 1} + \frac{u^2}{2} = \frac{\gamma + 1}{2(\gamma - 1)} a^{*2} \quad (8.35)$$

Total conditions in a flow are related to static conditions via

$$c_p T + \frac{u^2}{2} = c_p T_0 \quad (8.38)$$

$$\frac{T_0}{T} = 1 + \frac{\gamma - 1}{2} M^2 \quad (8.40)$$

$$\frac{p_0}{p} = \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{\gamma/(\gamma-1)} \quad (8.42)$$

$$\frac{\rho_0}{\rho} = \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{1/(\gamma-1)} \quad (8.43)$$

Note that the ratios of total to static properties are a function of local Mach number only. These functions are tabulated in Appendix A.

The basic normal shock equations are

*Continuity:*  $\rho_1 u_1 = \rho_2 u_2 \quad (8.2)$

*Momentum:*  $p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2 \quad (8.6)$

*Energy:*  $h_1 + \frac{u_1^2}{2} = h_2 + \frac{u_2^2}{2} \quad (8.10)$

These equations lead to relations for changes across a normal shock as a function of upstream Mach number  $M_1$  only:

$$M_2^2 = \frac{1 + [(\gamma - 1)/2] M_1^2}{\gamma M_1^2 - (\gamma - 1)/2} \quad (8.59)$$

(continued)

$$\frac{\rho_2}{\rho_1} = \frac{u_1}{u_2} = \frac{(\gamma + 1) M_1^2}{2 + (\gamma - 1) M_1^2} \quad (8.61)$$

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1) \quad (8.65)$$

$$\frac{T_2}{T_1} = \frac{h_2}{h_1} = \left[ 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1) \right] \frac{2 + (\gamma - 1) M_1^2}{(\gamma + 1) M_1^2} \quad (8.67)$$

$$s_2 - s_1 = c_p \ln \left\{ \left[ 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1) \right] \frac{2 + (\gamma - 1) M_1^2}{(\gamma + 1) M_1^2} \right\} \\ - R \ln \left[ 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1) \right] \quad (8.68)$$

$$\frac{p_{0,2}}{p_{0,1}} = e^{-(s_2 - s_1)/R} \quad (8.73)$$

The normal shock properties are tabulated versus  $M_1$  in Appendix B.

For a calorically perfect gas, the total temperature is constant across a normal shock wave:

$$T_{0,2} = T_{0,1}$$

However, there is a loss in total pressure across the wave:

$$p_{0,2} < p_{0,1}$$

For subsonic and supersonic compressible flow, the freestream Mach number is determined by the ratio of Pitot pressure to freestream static pressure. However, the equations are different:

$$\text{Subsonic flow: } M_1^2 = \frac{2}{\gamma - 1} \left[ \left( \frac{p_{0,1}}{p_1} \right)^{(\gamma-1)/\gamma} - 1 \right] \quad (8.74)$$

$$\text{Supersonic flow: } \frac{p_{0,2}}{p_1} = \left[ \frac{(\gamma + 1)^2 M_1^2}{4\gamma M_1^2 - 2(\gamma - 1)} \right]^{\gamma/(\gamma-1)} \frac{1 - \gamma + 2\gamma M_1^2}{\gamma + 1} \quad (8.80)$$

补充:  $M^*$ 特征马赫数的定义与计算公式

$$M^{*2} = \frac{(\gamma + 1)M^2}{2 + (\gamma - 1)M^2} \quad (8.48)$$

which gives  $M^*$  as a function of  $M$ . As can be shown by inserting numbers into Equation (8.48) (try some yourself),

$$\begin{aligned} M^* &= 1 & \text{if } M &= 1 \\ M^* &< 1 & \text{if } M &< 1 \\ M^* &> 1 & \text{if } M &> 1 \\ M^* &\rightarrow \sqrt{\frac{\gamma + 1}{\gamma - 1}} & \text{if } M &\rightarrow \infty \end{aligned}$$

Therefore,  $M^*$  acts qualitatively in the same fashion as  $M$  except that  $M^*$  approaches a finite value when the actual Mach number approaches infinity.

## 8.9 作业题P599