

# Non-reflecting boundary conditions and domain decomposition methods for industrial flow acoustics

Philippe Marchner

University of Lorraine, University of Liège

Soutenance de thèse  
Nancy, June 16th, 2022



X. Antoine



C. Geuzaine



H. Bériot/P. Barabinot

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

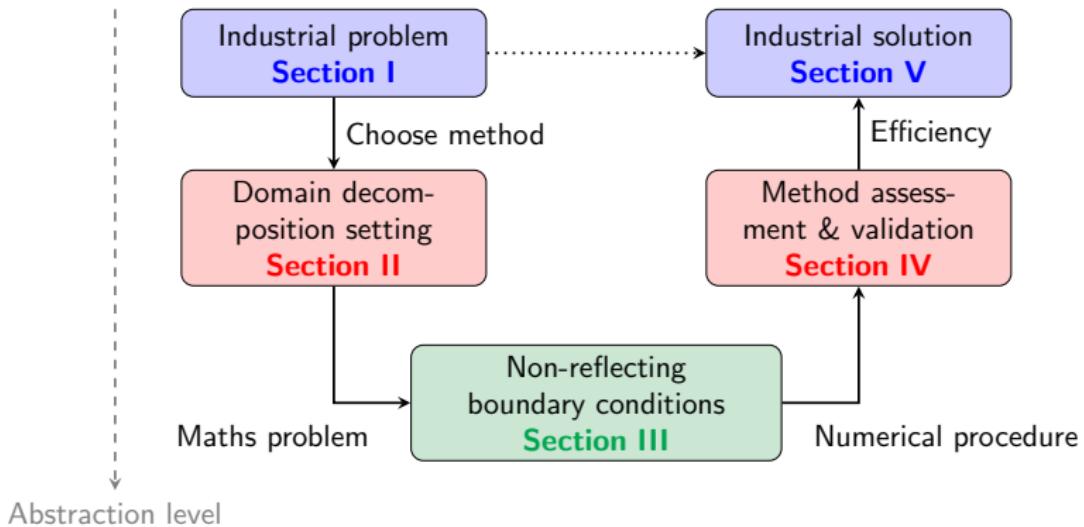
## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Outline



# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

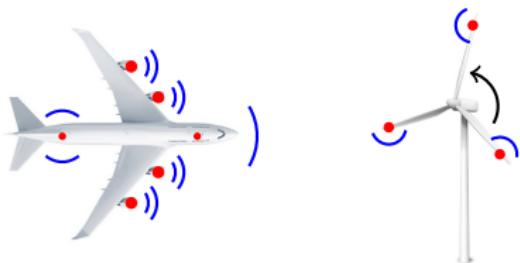
- Numerical results for the turbofan problem
- Solver weak scalability

# Industrial context

## Long term perspective

Predict noise from bodies in motion for the transport industry

### Computational (aero)acoustics



1. analyze & extract **sources**
2. understand **sound propagation**
3. find solutions (new material or design)

### Industrial objective

Provide a “*ready-to-use*” **sound propagation** simulation tool

- suitable to modern computer architectures
- applicable to large, complex industrial problems

→ can serve as basis for optimization routines

# Outline

## 1. Industrial context

Physical models for sound propagation

Reaching the memory limit

Objective of the thesis

## 2. Domain decomposition framework

Method overview

Flow acoustics formulation

Updated objective

## 3. ABCs for heterogeneous and convected problems

Microlocal analysis

Application to the Linearized Potential Equation

Numerical examples

## 4. Application to non-overlapping domain decomposition

Heterogeneous waveguide problems

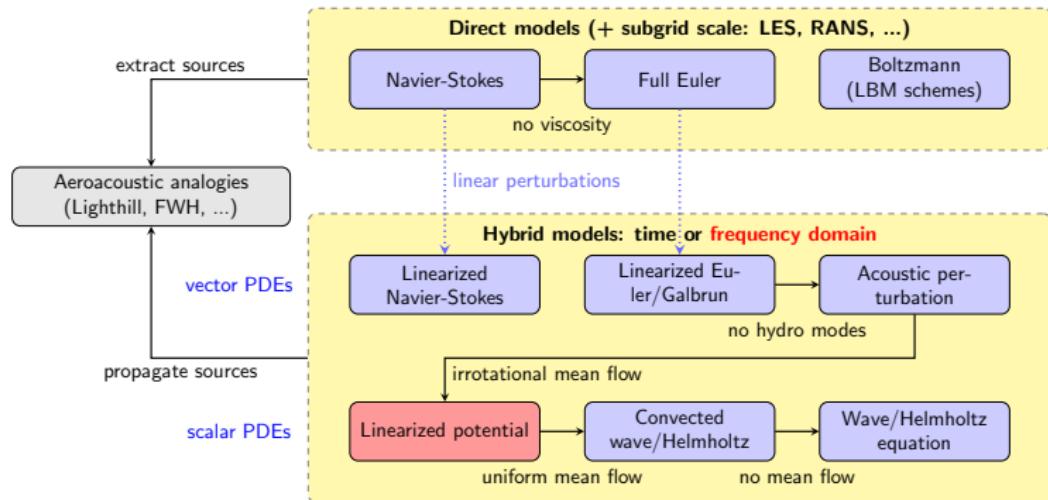
Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

Numerical results for the turbofan problem

Solver weak scalability

# Physical models for sound propagation



**Hybrid model** - solve mean flow and acoustic perturbations separately

- we choose the **time-harmonic Linearized Potential Equation**
- simple but accurate for single tones of turbofan engine intakes

# Physical model - Linearized Potential Equation

Scalar equation for the acoustic velocity potential  $\mathbf{v} = \nabla u$

## Linearized Potential Equation (LPE)

$$\rho_0(\mathbf{x}) \frac{D_0}{Dt} \left( \frac{1}{c_0(\mathbf{x})^2} \frac{D_0 u}{Dt} \right) - \nabla \cdot (\rho_0(\mathbf{x}) \nabla u) = f, \quad \frac{D_0}{Dt} = i\omega + \mathbf{v}_0(\mathbf{x}) \cdot \nabla$$

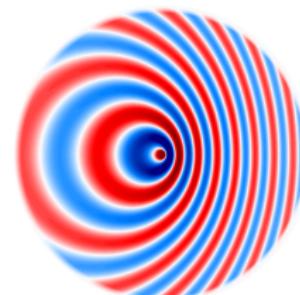
Helmholtz-type problem with **convection** and **heterogeneities**

### Mathematical difficulties

- oscillatory, non-local solution
- complex valued, strongly indefinite with  $\omega$
- unbounded domain
- convection effects

does not converge with classical iterative methods [Ernst, Gander 2012]  
→ use a **direct solver**

### Point source in a uniform flow



$$M = \|\mathbf{v}_0\| / c_0 = 0.6 \\ M < 1 \text{ (Subsonic flow)}$$

# Outline

## 1. Industrial context

Physical models for sound propagation

Reaching the memory limit

Objective of the thesis

## 2. Domain decomposition framework

Method overview

Flow acoustics formulation

Updated objective

## 3. ABCs for heterogeneous and convected problems

Microlocal analysis

Application to the Linearized Potential Equation

Numerical examples

## 4. Application to non-overlapping domain decomposition

Heterogeneous waveguide problems

Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

Numerical results for the turbofan problem

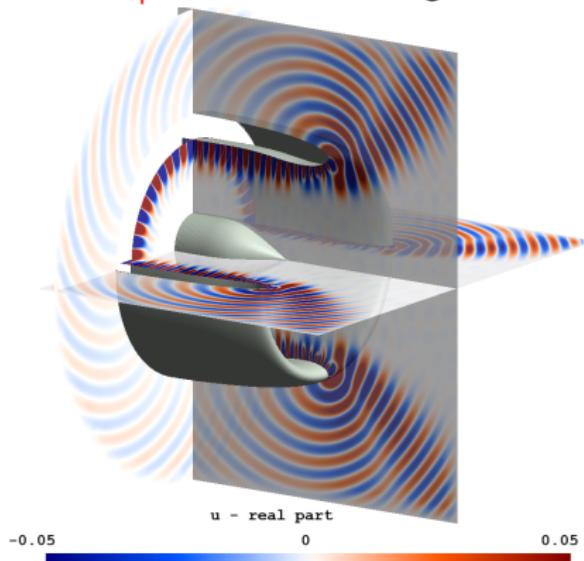
Solver weak scalability

# Reaching the high frequency limit

**Industrial example :** single tone turbofan intake radiation

**Current solver :** high-order  $p$ -FEM with direct solver (MUMPS)

$\omega_{\text{bpf}} \leftrightarrow \approx 25$  wavelengths



$\omega_{\text{bpf}}, N_{\text{dofs}} = 10M, \text{nnz} = 730M$   
Direct solver  $\rightarrow 740$  Gb of RAM

$\Downarrow$  increase  $\omega$  ?

$2 \times \omega_{\text{bpf}}, N_{\text{dofs}} = 73M, \text{nnz} = 5B$   
Direct solver  $\approx 6$  Tb of RAM ...

$O(\omega^3)$  scaling in memory & time ...

can we distribute the memory cost ?  $\rightarrow$  domain decomposition

# Outline

## 1. Industrial context

Physical models for sound propagation

Reaching the memory limit

**Objective of the thesis**

## 2. Domain decomposition framework

Method overview

Flow acoustics formulation

Updated objective

## 3. ABCs for heterogeneous and convected problems

Microlocal analysis

Application to the Linearized Potential Equation

Numerical examples

## 4. Application to non-overlapping domain decomposition

Heterogeneous waveguide problems

Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

Numerical results for the turbofan problem

Solver weak scalability

# Objective of the thesis

## Industrial objective

Provide a (scalable) parallel solver to increase the upper frequency limit

## Starting point of the thesis

### Discretization

- high-order finite elements  
→ reduce discretization error  
(interpolation & dispersion)
- adaptive order based on *a-priori* error indicator [Bériot et al. 2016]  
→ less unknowns

### Parallelization

- algebraic parallelization is hard for Helmholtz problems
- instead, “divide and conquer” at the continuous (PDE) level  
→ domain decomposition
- lots of approaches, but common framework [Gander, Zhang 2019]

## Selected solution - 1st objective

Extend the non-overlapping optimal Schwarz domain decomposition framework [Boubendir et al. 2012] to the Linearized Potential Equation

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

### Method overview

- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

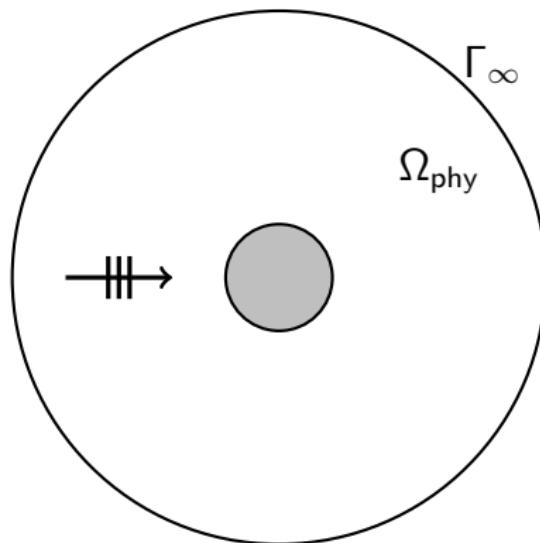
- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Overview - Non-overlapping optimal Schwarz

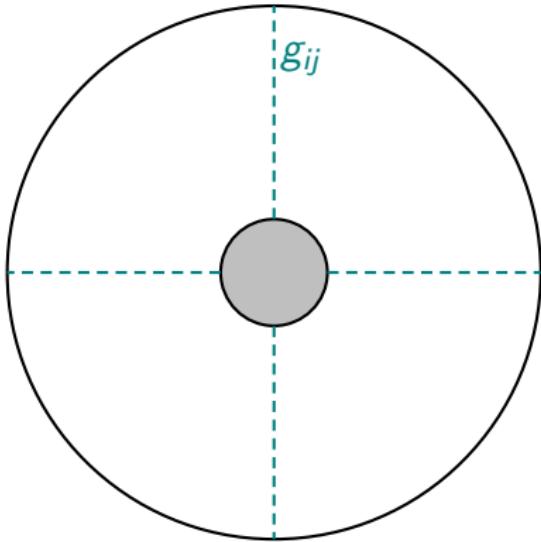
Toy example: disk scattering by a plane wave



# Overview - Non-overlapping optimal Schwarz

Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$  into **subdomains**



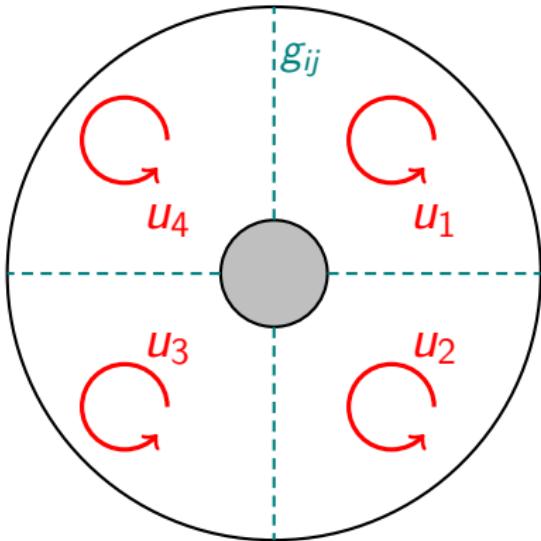
# Overview - Non-overlapping optimal Schwarz

Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$  into **subdomains**

Iterate until convergence

1. Solve the **volume subproblems**  $u_i$  with boundary conditions



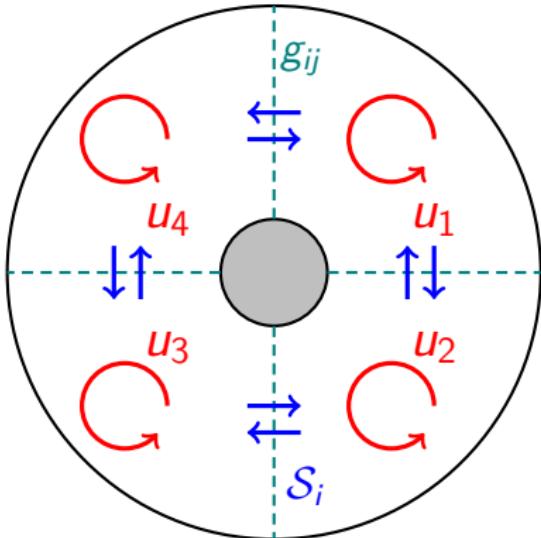
# Overview - Non-overlapping optimal Schwarz

Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$  into **subdomains**

Iterate until convergence

1. Solve the **volume subproblems**  $u_i$  with boundary conditions
2. update the **interfaces unknowns**  $\mathbf{g} = (g_{ij}, g_{ji})$  through **transmission conditions**  $(\mathcal{S}_i, \mathcal{S}_j) \Leftrightarrow$  solve surface problem



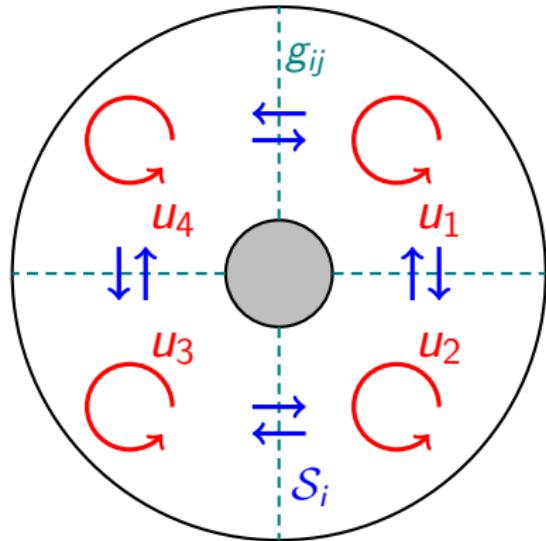
# Overview - Non-overlapping optimal Schwarz

Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$  into subdomains

Iterate until convergence

1. Solve the volume subproblems  $u_i$  with boundary conditions
2. update the interfaces unknowns  $\mathbf{g} = (g_{ij}, g_{ji})$  through transmission conditions  $(\mathcal{S}_i, \mathcal{S}_j) \Leftrightarrow$  solve surface problem



- convergence ? [Després 1991]
- How to choose the operators  $(\mathcal{S}_i, \mathcal{S}_j)$  ?  $\rightarrow$  numerous works ...

Optimal convergence with the  
**Dirichlet-to-Neumann** operator

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation**
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Flow acoustics formulation

In each subdomain  $\Omega_i$ , solve the boundary value problems

## Non-overlapping optimal Schwarz formulation

$$\begin{cases} \rho_0 \frac{D_0}{Dt} \left( \frac{1}{c_0^2} \frac{D_0 u_i}{Dt} \right) - \nabla \cdot (\rho_0 \nabla u_i) = 0 \text{ in } \Omega_i, \text{ (LPE)} \\ \rho_0 (1 - M_{\mathbf{n}}^2) (\partial_{\mathbf{n}_i} u_i + i \tilde{\Lambda}^+ u_i) = 0, \text{ on } \Gamma_i^\infty \text{ (radiation condition)} \\ \rho_0 (1 - M_{\mathbf{n}}^2) (\partial_{\mathbf{n}_i} u_i + i \mathcal{S}_i u_i) = g_{ij}, \text{ on } \Sigma_{ij}, \text{ (interface condition)} \end{cases}$$

Introduce the interface coupling on  $\Sigma_{ij}$

$$\begin{aligned} g_{ij} &= \rho_0 (1 - M_{\mathbf{n}}^2) (-\partial_{\mathbf{n}_j} u_j + i \mathcal{S}_j u_j) \\ &= -g_{ji} + i \rho_0 (1 - M_{\mathbf{n}}^2) (\mathcal{S}_i + \mathcal{S}_j) u_j := \mathcal{T}_{ji} g_{ji} + b_{ji} \end{aligned}$$

Rewrite the coupling as a linear system for  $\mathbf{g} = (g_{ij}, g_{ji})^T$

$$\underbrace{(\mathcal{I} - \mathcal{A})}_{\text{iteration matrix interface unknowns}} \underbrace{\mathbf{g}}_{\text{physical sources}} = \underbrace{\mathbf{b}}_{\text{physical sources}}, \quad \mathcal{A} = \begin{pmatrix} 0 & \mathcal{T}_{ji} \\ \mathcal{T}_{ij} & 0 \end{pmatrix}$$

$\mathcal{T}_{ij}$  and  $\mathcal{T}_{ji}$  are the **iteration operators**, and can be written in terms of  $\tilde{\Lambda}^+$

# High-level algorithmic procedure

## Surface iteration operators

$$\mathcal{T}_{ji} = \frac{\mathcal{S}_i - \tilde{\Lambda}^+}{\mathcal{S}_j + \tilde{\Lambda}^+}, \quad \mathcal{T}_{ij} = \frac{\mathcal{S}_j + \tilde{\Lambda}^-}{\mathcal{S}_i - \tilde{\Lambda}^-}$$

Iteration matrix eigenvalues:  $\lambda_{(\mathcal{I}-\mathcal{A})} = 1 \pm \sqrt{\mathcal{T}_{ji}\mathcal{T}_{ij}}$

If we choose  $\mathcal{S}_i = \tilde{\Lambda}^+$  and  $\mathcal{S}_j = -\tilde{\Lambda}^-$ , we have optimal convergence

Parallel iterative algorithm for the process  $i$

Do in  $\Omega_i$  at iteration  $(n+1)$ ,  $\forall j \in D_i$

1. given  $g_{ij}^{(n)}$ , solve  $u_i^{(n+1)}$  in  $\Omega_i$ ,

2. update the  $(n+1)$  neighbourhood data through

$$g_{ji}^{(n+1)} = -g_{ij}^{(n)} + \varpi_0 (1 - M_n^2) (\mathcal{S}_i + \mathcal{S}_j) u_i^{(n+1)} \text{ on } \Sigma_{ij},$$

# High-level algorithmic procedure

## Surface iteration operators

$$\mathcal{T}_{ji} = \frac{\mathcal{S}_i - \tilde{\Lambda}^+}{\mathcal{S}_j + \tilde{\Lambda}^+}, \quad \mathcal{T}_{ij} = \frac{\mathcal{S}_j + \tilde{\Lambda}^-}{\mathcal{S}_i - \tilde{\Lambda}^-}$$

Iteration matrix eigenvalues:  $\lambda_{(\mathcal{I}-\mathcal{A})} = 1 \pm \sqrt{\mathcal{T}_{ji}\mathcal{T}_{ij}}$

If we choose  $\mathcal{S}_i = \tilde{\Lambda}^+$  and  $\mathcal{S}_j = -\tilde{\Lambda}^-$ , we have optimal convergence

Parallel iterative algorithm for the process  $i$

Do in  $\Omega_i$  at iteration  $(n+1)$ ,  $\forall j \in D_i$

1. given  $g_{ij}^{(n)}$ , solve  $u_i^{(n+1)}$  in  $\Omega_i$ ,
2. update the  $(n+1)$  neighbourhood data through  
 $g_{ji}^{(n+1)} = -g_{ij}^{(n)} + \varpi_0 (1 - M_n^2) (\mathcal{S}_i + \mathcal{S}_j) u_i^{(n+1)}$  on  $\Sigma_{ij}$ ,

$(\tilde{\Lambda}^+, -\tilde{\Lambda}^-)$  are **non-local DtN maps** for the LPE

→ design **sparse approximations**  $\mathcal{S}_i \approx \tilde{\Lambda}^+$  and  $\mathcal{S}_j \approx -\tilde{\Lambda}^-$

↔ approximate **Schur complements** at the algebraic level

# Algebraic interpretation of domain decomposition

Global problem for two subdomains  $(i, j)$  with a common interface  $\Sigma$

$$\begin{pmatrix} \mathbb{K}_i^\Omega & 0 & \mathbb{K}_i^{\Omega, \Sigma} \\ 0 & \mathbb{K}_j^\Omega & \mathbb{K}_j^{\Omega, \Sigma} \\ \mathbb{K}_i^{\Sigma, \Omega} & \mathbb{K}_j^{\Sigma, \Omega} & \mathbb{K}_i^{\Sigma, \Sigma} + \mathbb{K}_j^{\Sigma, \Sigma} \end{pmatrix} \begin{pmatrix} u_i^\Omega \\ u_j^\Omega \\ u^\Sigma \end{pmatrix} = \begin{pmatrix} f_i^\Omega \\ f_j^\Omega \\ f_i^\Sigma + f_j^\Sigma \end{pmatrix}$$

Direct parallel solver  $\rightarrow$  block LU factorization per subdomain

$$\begin{pmatrix} \mathbb{I} & 0 & 0 \\ 0 & \mathbb{I} & 0 \\ \mathbb{K}_i^{\Sigma, \Omega}(\mathbb{K}_i^\Omega)^{-1} & \mathbb{K}_j^{\Sigma, \Omega}(\mathbb{K}_j^\Omega)^{-1} & \mathbb{I} \end{pmatrix} \begin{pmatrix} \mathbb{K}_i^\Omega & 0 & 0 \\ 0 & \mathbb{K}_j^\Omega & 0 \\ 0 & 0 & \mathbb{L} \end{pmatrix} \begin{pmatrix} \mathbb{I} & 0 & (\mathbb{K}_i^\Omega)^{-1}\mathbb{K}_i^{\Omega, \Sigma} \\ 0 & \mathbb{I} & (\mathbb{K}_j^\Omega)^{-1}\mathbb{K}_j^{\Omega, \Sigma} \\ 0 & 0 & \mathbb{I} \end{pmatrix},$$

The **Schur complement**  $\mathbb{L} = \mathbb{L}_i + \mathbb{L}_j$  is dense  $\Leftrightarrow$  discrete DtN map  
 $\rightarrow$  advances on dense Block Low-Rank factorization [Amestoy et al. 2019]

The non-overlapping Schwarz approach can be seen as an iterative solver  
for  $\mathbb{L}$  preconditioned by **interfaces conditions**  
 $\rightarrow$  approximate block LU factorization at the continuous level

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective**

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Summary and updated objective

Non-overlapping domain decomposition for flow acoustics

- similar to the Helmholtz formulation, common framework
- quick convergence relies on sparse approximations of the DtN map  
     $\Leftrightarrow$  Non-reflecting boundary conditions

# Summary and updated objective

Non-overlapping domain decomposition for flow acoustics

- similar to the Helmholtz formulation, common framework
- quick convergence relies on sparse approximations of the DtN map  
⇒ Non-reflecting boundary conditions

## Updated objective

Design non-reflecting boundary conditions for **heterogeneous** and  
**convected** time-harmonic problems

Two techniques were studied during the thesis

1. Absorbing Boundary Conditions (ABC) [*Marchner et al. SIAP 2022*],
2. Perfectly Matched Layers (PML) [*Marchner et al. JCP 2021*],

# Summary and updated objective

Non-overlapping domain decomposition for flow acoustics

- similar to the Helmholtz formulation, common framework
- quick convergence relies on sparse approximations of the DtN map  
⇒ Non-reflecting boundary conditions

## Updated objective

Design non-reflecting boundary conditions for **heterogeneous** and  
**convected** time-harmonic problems

Two techniques were studied during the thesis

1. Absorbing Boundary Conditions (ABC) [*Marchner et al. SIAP 2022*],
2. Perfectly Matched Layers (PML) [*Marchner et al. JCP 2021*],

## Next section

Focus on the construction of Absorbing Boundary Conditions

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

### Microlocal analysis

- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Microlocal analysis - DtN operator

Goal: find local approximations to the **Dirichlet-to-Neumann map**

DtN operator on  $\Sigma$

$$\widetilde{\Lambda^+} : \begin{cases} H^{1/2}(\Sigma) \rightarrow H^{-1/2}(\Sigma) \\ u|_{\Sigma} \mapsto \partial_n u|_{\Sigma} = -i \widetilde{\Lambda^+} u|_{\Sigma} \end{cases}$$

through pseudo-differential calculus

[Engquist and Majda 1977, 1979] [Antoine et al. 1999]

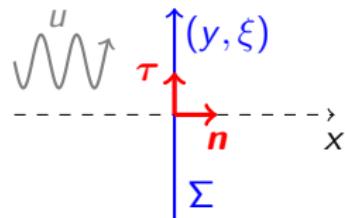
Example : 2D heterogeneous Helmholtz half-space problem

$$\begin{aligned} \mathcal{L} &= \rho_0^{-1} \partial_x (\rho_0 \partial_x) + \rho_0^{-1} \partial_y (\rho_0 \partial_y) + \omega^2 c_0^{-2} \\ &\stackrel{?}{\approx} \left( \partial_x + i \sqrt{\omega^2 c_0^{-2} + \rho_0^{-1} \partial_y (\rho_0 \partial_y)} \right) \left( \partial_x - i \sqrt{\omega^2 c_0^{-2} + \rho_0^{-1} \partial_y (\rho_0 \partial_y)} \right) \end{aligned}$$

We cannot formally factorize  $\mathcal{L}$  when  $\partial_x(\rho_0) \neq 0$  or  $\partial_x(c_0) \neq 0$

- Apply the principle to the **symbol**  $\lambda^+$  of  $\Lambda^+$

→ work on polynomials in the co-tangent Fourier space  $\xi$



# Pseudo-differential operator

We define a differential operator of order  $m$ ,

$$\mathcal{P}(x, \partial_x) = \sum_{|\alpha| \leq m} (-i)^{\alpha} a_{\alpha}(x) \partial_x^{\alpha}, \quad x \in \mathbb{R}^d, \quad \alpha = (\alpha_1, \dots, \alpha_d) \in \mathbb{N}^d,$$

through its inverse Fourier representation  $\rightarrow$  more general framework

Pseudo-differential operator of order  $m$

$$\mathcal{P}(x, \partial_x) u(x) = \frac{1}{(2\pi)^d} \int_{\mathbb{R}^d} e^{ix \cdot \xi} p(x, \xi) \hat{u}(\xi) d\xi, \quad \xi \in \mathbb{R}^d$$

$p$  is the **symbol** of the operator  $\mathcal{P}$ , and is a smooth function of  $(x, \xi)$

Symbol of the operator  $\mathcal{P}$

$$p(x, \xi) = \sum_{|\alpha| \leq m} a_{\alpha}(x) \xi^{\alpha}, \quad \xi^{\alpha} = \xi_1^{\alpha_1} \dots \xi_d^{\alpha_d}$$

The highest order term is the **principal symbol**. We use **classical symbols**  $S_{\text{cl}}^m$

$$\left| \partial_x^{\beta} \partial_{\xi}^{\alpha} p(x, \xi) \right| \leq C(\alpha, \beta, K) (1 + |\xi|)^{m - |\alpha|}, \quad \forall (x, \xi) \in K \times \mathbb{R}^d,$$

Notations:

$$\mathcal{P} = \text{Op}(p) \in \text{OPS}^m, \quad p \in S_{\text{cl}}^m \Leftrightarrow \mathcal{P} \in \text{OPS}^m, \quad \text{OPS}^{-\infty} = \bigcap_{m \in \mathbb{R}} \text{OPS}^m$$

# Derivation of the DtN symbol - Helmholtz case

Nirenberg's factorization theorem: there exists  $(\Lambda^+, \Lambda^-) \in \text{OPS}^1$

$$\begin{aligned}\mathcal{L} &= (\partial_x + i\Lambda^-)(\partial_x + i\Lambda^+) \quad \text{mod } \text{OPS}^{-\infty} \\ &= \partial_x^2 + i(\Lambda^+ + \Lambda^-)\partial_x + i\text{Op}\{\partial_x \lambda^+\} - \Lambda^- \Lambda^+ \quad \text{mod } \text{OPS}^{-\infty}.\end{aligned}$$

Identify with the Helmholtz operator and get a system for  $(\Lambda^+, \Lambda^-)$

$$\begin{cases} \Lambda^+ + \Lambda^- = -i\rho_0^{-1}\partial_x(\rho_0) \\ (\Lambda^+)^2 + i\rho_0^{-1}\partial_x(\rho_0)\Lambda^+ + i\text{Op}\{\partial_x \lambda^+\} = \omega^2 c_0^{-2} + \rho_0^{-1}\partial_y(\rho_0 \partial_y) \end{cases}$$

→ “One-way” reformulation of the equation

“High frequency” asymptotic expansion for the total symbol  $\lambda^+$

$$\lambda^+ \sim \sum_{j=-1}^{\infty} \lambda_{-j}^+ = \lambda_1^+ + \lambda_0^+ + \lambda_{-1}^+ + \dots \quad (\text{classical symbol expansion})$$

Each symbol  $\lambda_{-j}^+$  is homogeneous in  $(\omega, \xi)^{-j}$ .

Once  $\lambda_1^+$  is fixed, the expansion is unique and can be computed formally

$$\lambda_1^+ = \sqrt{\omega^2 c_0^{-2} - \xi^2}, \quad \lambda_0^+ = -i \left( \frac{\partial_x(\rho_0)}{2\rho_0} + \frac{\xi \partial_y(\rho_0)}{2\rho_0 \lambda_1^+} + \frac{\omega^2 \partial_x(c_0^{-2})}{4(\lambda_1^+)^2} + \frac{\xi \omega^2 \partial_y(c_0^{-2})}{4(\lambda_1^+)^3} \right)$$

# Microlocal zones

Hyperbolic zone:  $\Re(\lambda_1^+) > 0 \rightarrow$  outgoing propagative waves

Elliptic zone:  $\Im(\lambda_1^+) < 0 \rightarrow$  outgoing evanescent waves

Rotation of the square-root branch-cut [Milinazzo et al. 1997]

$$\lambda_1^+ = e^{i\alpha/2} \sqrt{e^{-i\alpha} (\omega^2 c_0^{-2} - \xi^2)}, \quad \alpha \in [0, -\pi], \text{ (+}\imath\omega t\text{ convention)}$$

The branch-cut is rotated by an angle  $\alpha$  in the complex plane

- Hyperbolic zone:  $\omega c_0^{-1} > |\xi| \rightarrow \alpha = 0,$
- Elliptic zone:  $\omega c_0^{-1} < |\xi| \rightarrow \alpha = -\pi,$
- Grazing zone:  $\omega c_0^{-1} = |\xi|,$  ill-posed problem

In practice we choose  $\alpha \in (0, -\pi/2]$

→ trade-off to capture both propagative and evanescent waves

# Summary - building the DtN approximation

Approximate DtN operator with the  $M$  first symbols

$$\partial_n u = -i\Lambda_M^+ u, \quad \Lambda_M^+ = \sum_{j=-1}^{M-2} \text{Op}\left(\lambda_{-j}^+\right)$$

Take the trace on the boundary  $\Sigma$  to get  $\tilde{\Lambda}_M^+$ , such that

$$\left(\tilde{\Lambda}^+ - \tilde{\Lambda}_M^+\right) \in \text{OPS}^{1-M}$$

## Technical difficulties

- the formal computation of  $\lambda_{-j}^+$  can be involved (PDE dependent)
- the operator  $\text{Op}\left(\lambda_{-j}^+\right)$  is in general not unique and still non-local
- limited *a priori* to smooth variations of  $p_0$  and  $c_0$

## Next step - original contribution

- Apply the theory to flow acoustics

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation**
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# DtN symbol computation

**Step 1** Nirenberg's factorization theorem for the flow acoustics operator

$$\mathcal{L} = \frac{D_0}{Dt} \left( \frac{1}{c_0^2} \frac{D_0}{Dt} \right) - \rho_0^{-1} \nabla \cdot (\rho_0 \nabla), \quad \frac{D_0}{Dt} = \imath\omega + \mathbf{v}_0 \cdot \nabla$$

We note  $M_x = v_{0,x}/c_0$ ,  $M_y = v_{0,y}/c_0$ ,  $M = \|\mathbf{v}_0\|/c_0$ ,  $k_0 = \omega/c_0$

**Step 2** Derive an operator equation for the outgoing characteristic  $\Lambda^+$

$$(1 - M_x^2)(\Lambda^+)^2 - \imath(\mathcal{A}_1 + \mathcal{A}_0)\Lambda^+ + \imath(1 - M_x^2)\text{Op}\{\partial_x \lambda^+\} = \mathcal{B}_2 + \mathcal{B}_1 \text{ mod OPS}^{-\infty}$$

with  $\imath(\Lambda^+ + \Lambda^-) = (\mathcal{A}_1 + \mathcal{A}_0)/(M_x^2 - 1)$ ,  $\sigma(\mathcal{A}_j), \sigma(\mathcal{B}_j) \in \mathcal{S}_{\text{cl}}^j$ ,  $j = \{0, 1, 2\}$

**Step 3** Classical symbol expansion, identify 2nd order terms in  $(\omega, \xi)$

DtN principal symbol for flow acoustics

$$\lambda_1^\pm = \frac{1}{1 - M_x^2} \left[ -M_x(k_0 - \xi M_y) \pm \sqrt{k_0^2 - 2k_0 M_y \xi - (1 - M^2) \xi^2} \right]$$

Microlocal zones delimited by  $\omega c_0^{-1} = (M_y \pm \sqrt{1 - M_x^2}) \xi$

Subsonic flow  $M < 1 \Rightarrow$  two characteristic lines of opposite sign

# DtN symbol computation

## Step 3 - bis

Compute the next symbols of the expansion ...

$$\lambda_0^+ = \frac{\sigma(\mathcal{B}_1) + i\sigma(\mathcal{A}_0)\lambda_1^+ + i(1 - \textcolor{blue}{M}_x^2)(\partial_\xi\lambda_1^+\partial_y\lambda_1^+ - \partial_x\lambda_1^+)}{2\sqrt{k_0^2 - 2k_0\textcolor{teal}{M}_y\xi - (1 - \textcolor{blue}{M}^2)\xi^2}}.$$

If  $\textcolor{teal}{M}_y = 0$  we have the simplification

Zeroth order symbol for an  $x$ -oriented flow

$$\lambda_0^+ = -i\frac{\partial_x(\rho_0)}{2\rho_0} \frac{k_0^2 - \xi^2}{k_0^2 - (1 - \textcolor{blue}{M}_x^2)\xi^2} + i\frac{\partial_x(c_0)}{2c_0} \frac{k_0^2 + \textcolor{blue}{M}_x^2\xi^2}{k_0^2 - (1 - \textcolor{blue}{M}_x^2)\xi^2}$$

$$\lambda_{-1}^+ = \dots, \quad \lambda_{-2}^+ = \dots$$

# Going back to the operator level

**Final step** go back to the operator level

Approximate DtN operator

$$\begin{aligned}\tilde{\Lambda}_1^+ &= \text{Op}(\lambda_1^+) = \frac{k_0}{1 - \mathbf{M}_n^2} \left( -\mathbf{M}_n + i\mathbf{M}_n \mathbf{M}_T \frac{\nabla_\Sigma}{k_0} + \sqrt{1 + X} \right) \\ X &= -2i\mathbf{M}_T \frac{\nabla_\Sigma}{k_0} + (1 - \mathbf{M}^2) \frac{\Delta_\Sigma}{k_0^2}, \quad \mathbf{M} = \|\mathbf{v}_0\| / c_0\end{aligned}$$

For the half-space problem with constant coefficients

$$\tilde{\Lambda}^+ = \tilde{\Lambda}_1^+ \mod \text{OPS}^{-\infty}$$

For variable coefficients and/or in the tangent plane approximation  $(\mathbf{n}, \tau)$

$$\tilde{\Lambda}^+ = \tilde{\Lambda}_1^+ \mod \text{OPS}^0$$

The choice for  $\text{Op}(\lambda_1^+)$  is not unique, but has  $\lambda_1^+$  as principal symbol

**Issue:** the approximate DtN map  $\tilde{\Lambda}_1^+$  is still non-local  
→ we need a local representation for  $\sqrt{1 + X}$

# Localization procedure

High-frequency approximation for  $\sqrt{1 + \textcolor{teal}{X}}$ ,  $\textcolor{teal}{X} \rightarrow 0$  ( $\omega \rightarrow +\infty$ )  
Use complexified Padé or Taylor approximations ( $N, \alpha$ ) for

$$\Lambda(\textcolor{blue}{Z}) = \textcolor{red}{e}^{\imath\alpha/2}\sqrt{1 + \textcolor{blue}{Z}}, \quad \textcolor{blue}{Z} = [\textcolor{red}{e}^{-\imath\alpha}(1 + \textcolor{teal}{X}) - 1],$$

with  $\textcolor{blue}{Z}$  a surfacic second order differential operator on the boundary  $\Sigma$

## Taylor approximation

$$\Lambda(\textcolor{blue}{Z}) \approx \textcolor{red}{e}^{\imath\alpha/2} \sum_{\ell=0}^N \binom{1/2}{\ell} (\textcolor{red}{e}^{-\imath\alpha}(1 + \textcolor{teal}{X}) - 1)^\ell$$

## Padé approximation

$$\Lambda(\textcolor{blue}{Z}) \approx K_0(\alpha) + \sum_{\ell=1}^N A_\ell(\alpha) \textcolor{teal}{X} (1 + B_\ell(\alpha) \textcolor{teal}{X})^{-1}$$

## Resulting local Absorbing Boundary Conditions

Complex Padé approximants:  $\tilde{\Lambda}_1^+ \rightarrow \text{ABC}_1^{N,\alpha}$

Complex Taylor approximants:  $\tilde{\Lambda}_1^+ \rightarrow \text{ABC}_1^{T0,\alpha}$  and  $\text{ABC}_1^{T2,\alpha}$

# High-order FEM implementation

Discretization on a conformal, high-order  $H^1$ -basis

Weak formulation for the linearized potential equation

$$\forall v \in V \subseteq H^1(\Omega), \quad \int_{\Omega} \left[ \rho_0 \nabla u \cdot \nabla v - \frac{\rho_0}{c_0^2} \frac{D_0 u}{Dt} \frac{\overline{D_0 v}}{Dt} \right] d\Omega + i \int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Omega} f \bar{v} d\Omega$$

The boundary operator  $\mathcal{G}$  takes the same form as in the Helmholtz case

$$\int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Sigma} e^{i\alpha/2} \rho_0 k_0 \sqrt{1 + Z} u \bar{v} d\Sigma$$

$$\text{with } Z = e^{-i\alpha} \left( 1 - 2iM_\tau \frac{\nabla_\Sigma}{k_0} + (1 - M^2) \frac{\Delta_\Sigma}{k_0^2} \right) - 1$$

# High-order FEM implementation

Discretization on a conformal, high-order  $H^1$ -basis

Weak formulation for the linearized potential equation

$$\forall v \in V \subseteq H^1(\Omega), \quad \int_{\Omega} \left[ \rho_0 \nabla u \cdot \nabla v - \frac{\rho_0}{c_0^2} \frac{D_0 u}{Dt} \frac{\overline{D_0 v}}{Dt} \right] d\Omega + i \int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Omega} f \bar{v} d\Omega$$

The boundary operator  $\mathcal{G}$  takes the same form as in the Helmholtz case

$$\int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Sigma} e^{i\alpha/2} \rho_0 k_0 \sqrt{1 + Z} u \bar{v} d\Sigma$$

$$\text{with } Z = e^{-i\alpha} \left( 1 - 2iM_T \frac{\nabla_{\Sigma}}{k_0} + (1 - M^2) \frac{\Delta_{\Sigma}}{k_0^2} \right) - 1$$

**Taylor approximants:** ABC<sub>1</sub><sup>T2,  $\alpha$</sup>

$$\begin{aligned} \int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma &= \cos(\alpha/2) \int_{\Sigma} \rho_0 k_0 u \bar{v} d\Sigma \\ &\quad + e^{-i\alpha/2} \left( \int_{\Sigma} \rho_0 M_T \nabla_{\Sigma} u \bar{v} d\Sigma - \int_{\Sigma} \rho_0 \frac{(1 - M^2)}{2k_0} \nabla_{\Sigma} u \nabla_{\Sigma} \bar{v} d\Sigma \right) \end{aligned}$$

# High-order FEM implementation - Padé case

Padé approximants: ABC<sub>1</sub><sup>N,α</sup>

$$\int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Sigma} \rho_0 k_0 K_0(\alpha) u \bar{v} d\Sigma + \sum_{\ell=1}^N \int_{\Sigma} \rho_0 k_0 A_{\ell}(\alpha) X \varphi_{\ell} \bar{v} d\Sigma$$

$$\text{with } X = -2i M_{\tau} \frac{\nabla_{\Sigma}}{k_0} + (1 - M^2) \frac{\Delta_{\Sigma}}{k_0^2}$$

Introduce auxiliary fields  $\varphi_{\ell} = (1 + B_{\ell} X)^{-1} u$  to obtain a sparse discretization of inverse operators

→ augmented system of  $N$  surfacic equations

$$\forall \ell \in [1, N], \forall v_{\ell} \in H^1(\Sigma)^N, \quad \int_{\Sigma} (1 + B_{\ell}(\alpha) X) \varphi_{\ell} \bar{v}_{\ell} d\Sigma = \int_{\Sigma} u \bar{v}_{\ell} d\Sigma$$

Global linear system of size  $[N_{\text{dof}, \Omega} + (N \times N_{\text{dof}, \Sigma})]$

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

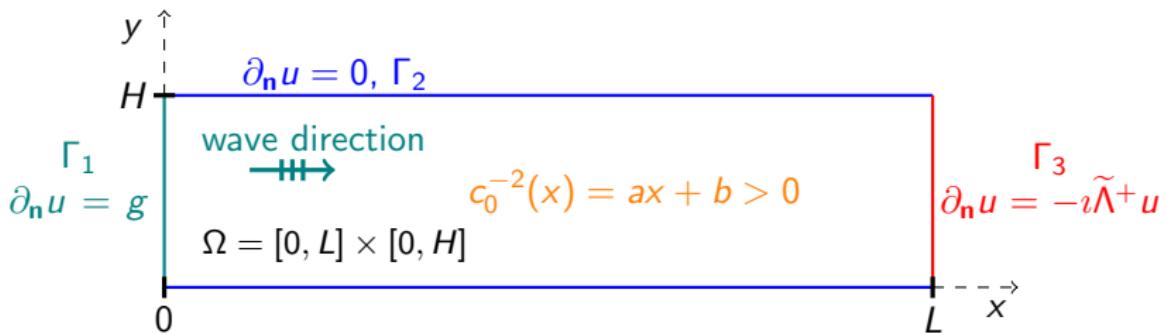
- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Longitudinal heterogeneous waveguide

Example 1: No mean flow, single mode propagation in a heterogeneous waveguide:  $\rho_0 = 1$ ,  $c_0(x, y) = c_0(x)$



Single mode analytic solution for a linear profile

$$u_{\text{ex}}^n(x, y) = \cos(k_y y) \text{Ai}\left(e^{-\frac{2i\pi}{3} \frac{k_y^2 - \omega^2(ax+b)}{(a\omega^2)^{2/3}}}\right), \quad k_y = \frac{n\pi}{H}, \quad n \in \mathbb{N}$$

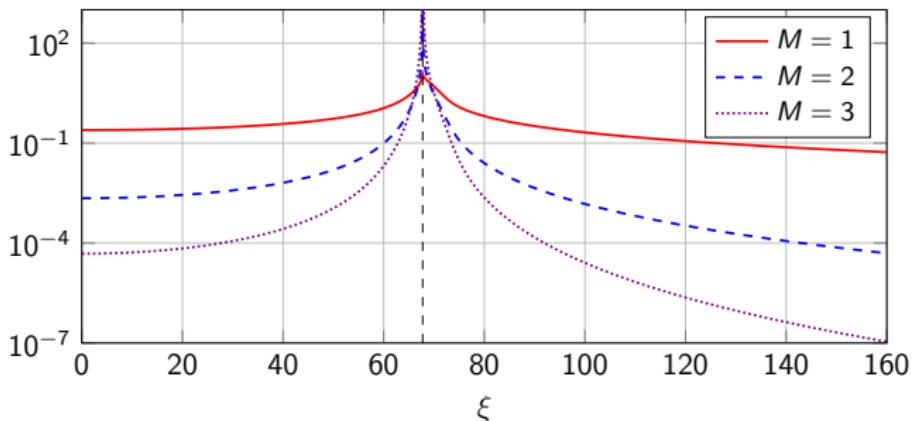
# Approximation at the symbol level

$$c_0^{-2}(x) = 5x + 0.1, L = 1 \text{ at fixed frequency } \omega = 30$$

## Analytic total symbol

$$\lambda^+ = -\imath e^{-\frac{2\imath\pi}{3}} (a\omega^2)^{1/3} \frac{\text{Ai}'(\zeta)}{\text{Ai}(\zeta)}, \quad \zeta = e^{-\frac{2\imath\pi}{3}} \frac{\xi^2 - \omega^2(aL+b)}{(a\omega^2)^{2/3}}$$

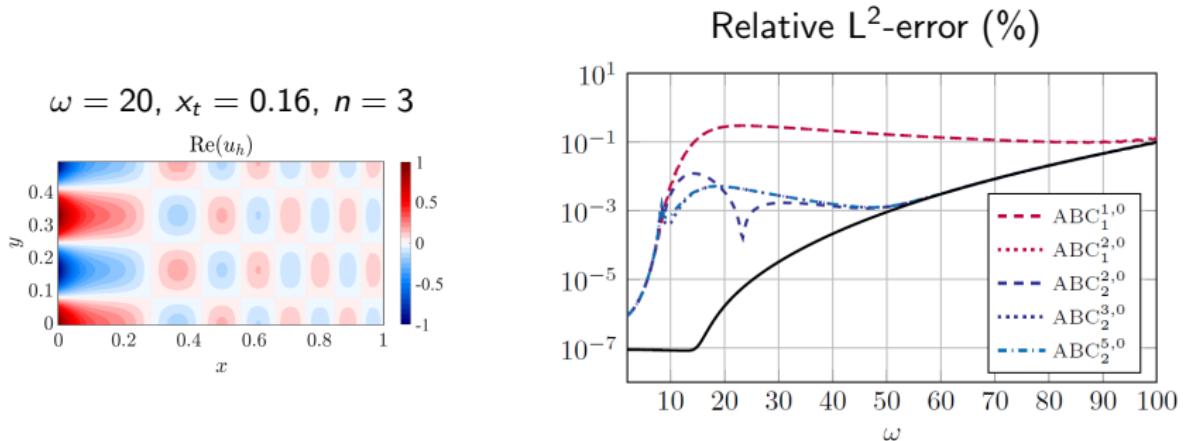
$$\left| \lambda^+ - \sum_{j=-1}^{M-2} \lambda_{-j}^+ \right|$$



- singularity in the grazing regime  $\xi \approx \omega c_0^{-1}$

# Numerical results

$\text{ABC}_M^{N,\alpha}$ : Local Padé approximation of  $\tilde{\Lambda}_M^+$  with rotation branch-cut  $\alpha$



Use the derivative of  $c_0 \Rightarrow$  more accurate ABC:  $\text{ABC}_2^{N+1,\alpha} > \text{ABC}_1^{N,\alpha}$

Gain of  $\approx$  two order of magnitude

Precision limited by the DtN symbol truncation

Similar conclusion with Taylor approximations of order 0 and 2

# Point source convection in free field

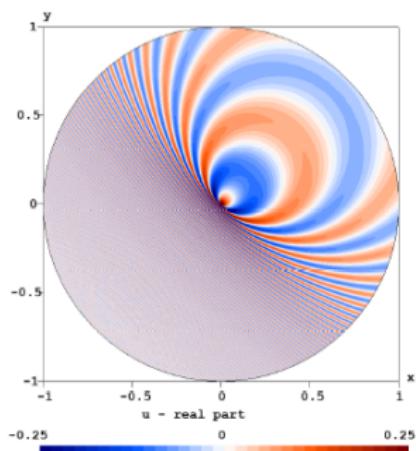
Example 2:  $\rho_0 = c_0 = 1$ , point source in uniform mean flow of angle  $\theta$

Padé approximants  $\rightarrow \text{ABC}_1^{N,\alpha}$ , Taylor approximants  $\rightarrow \text{ABC}_1^{\text{T}0,\alpha}$ ,  $\text{ABC}_1^{\text{T}2,\alpha}$

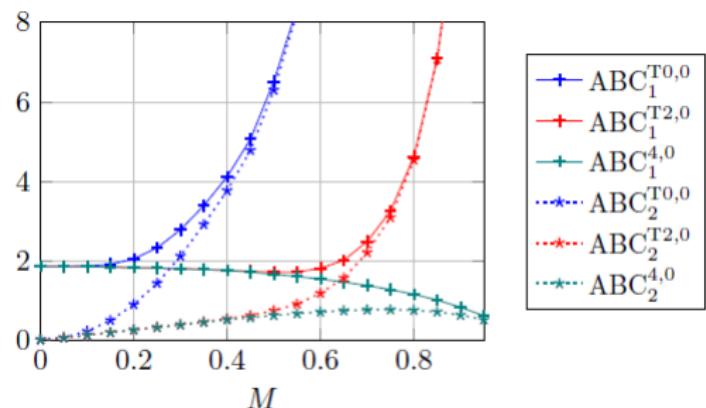
Attempt to incorporate curvature effects from  $\lambda_0^+$  (circle of radius  $R$ )

$$\text{ABC}_2 = \text{ABC}_1 + (1 - M^2)/(2R)$$

$$k_0 = 6\pi, M = 0.95, R = 1, \theta = \pi/4$$



Relative  $L^2$ -error (%)



$\text{ABC}_1^{N,\alpha}$  is robust for high Mach numbers - wavelength ratio  $(1 + M)/(1 - M)$

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

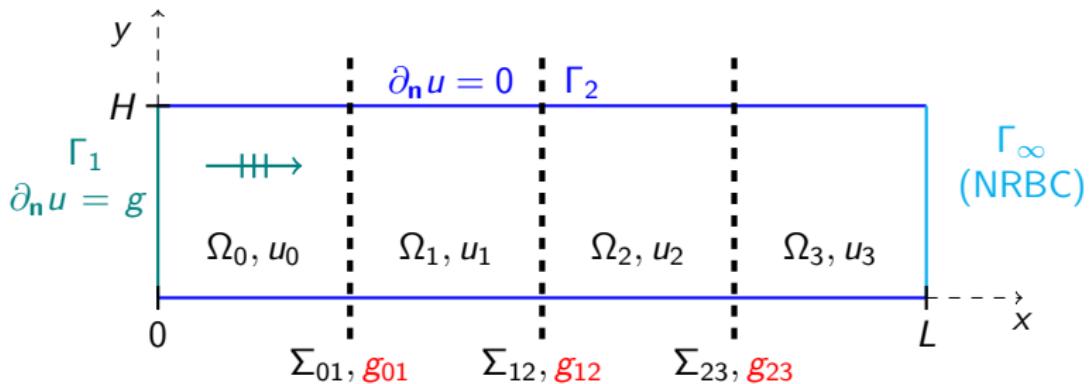
- Heterogeneous waveguide problems**
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Waveguide problem with straight partitions

Domain partition:  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$ ,  $\Sigma_{ij} = \overline{\partial\Omega_i \cap \partial\Omega_j}$ ,  $j \neq i$



Two test cases

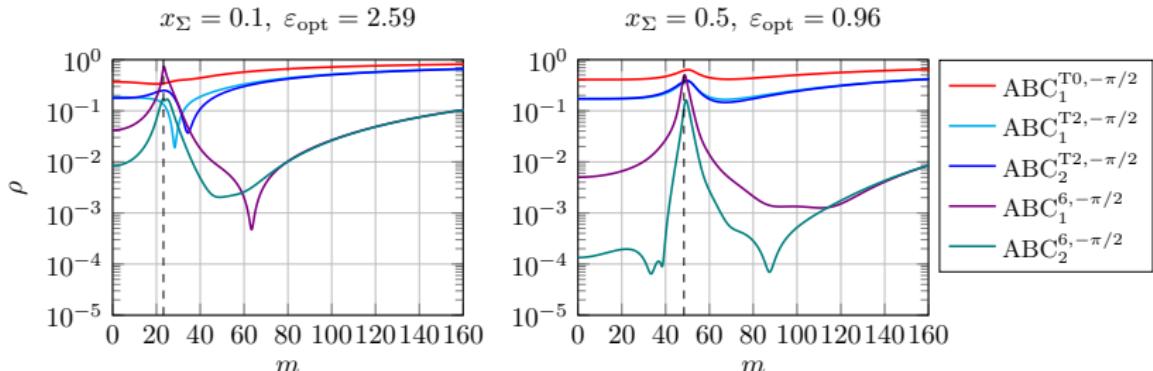
1. Linear speed of sound profile :  $c_0^{-2}(x) = ax + b$
2. Transverse density and/or speed of sound :  $c_0(y), \rho_0(y)$

# Longitudinal heterogeneous waveguide

Reminder - ABC study

- $\text{ABC}_2^{N+1,\alpha} > \text{ABC}_1^{N,\alpha}$
- Precision limited by the truncation of the total DtN symbol  $\lambda^+$

Plot theoretical convergence radius  $\rho(m, x) = \sqrt{|\mathcal{T}_{ij}^m \mathcal{T}_{ji}^m|}$  at  $\omega = 30$



DDM waveguide study - input boundary condition with the 21 first modes

$N_{\text{dom}}$	$\text{ABC}_1^{T0,\alpha}$	$\text{ABC}_1^{T2,\alpha}$	$\text{ABC}_1^{6,\alpha}$	$\text{ABC}_2^{6,\alpha}$
8	76 (dnc)	51 (87)	34 (37)	24 (27)

Table: GMRES(Jacobi) iterations to  $10^{-6}$  at  $\omega = 40$ ,  $\alpha = -\pi/4$ ,  $d_\lambda = 12$

# Transverse heterogeneous waveguide

Gaussian waveguide:  $c_0(y) = 1.25 \left(1 - 0.4e^{-32(y-H/2)^2}\right)$ ,  $\rho_0(y) = c_0^2(y)$

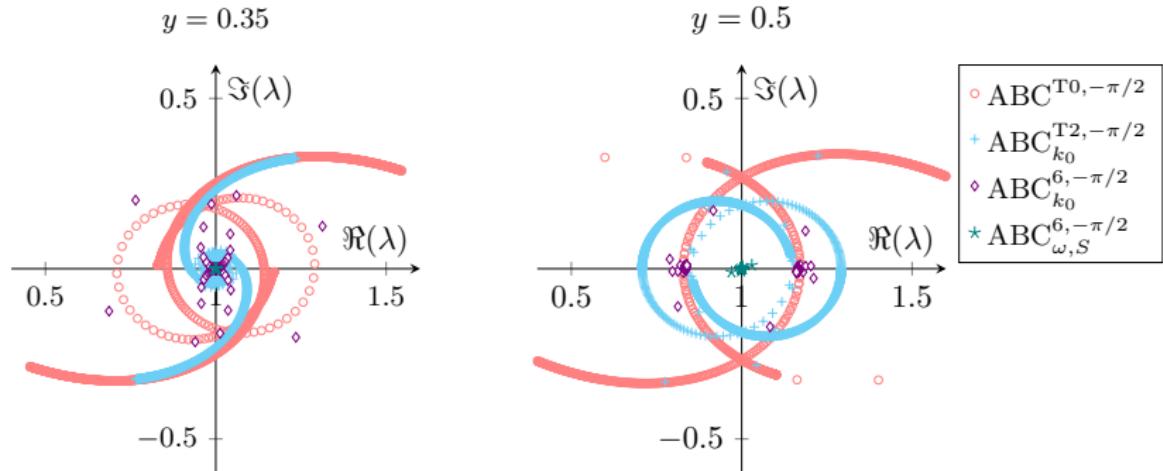


Figure: Theoretical eigenvalues of the DDM iteration matrix,  $\omega = 50$

- Usual Padé approximation (classical principal symbol) -  $S_i = \text{ABC}_{k_0}^{N,\alpha}$
- New approximation (semi-classical principal symbol) -  $S_i = \text{ABC}_{\omega,S}^{N,\alpha}$   
→ almost perfect clustering

# Illustration for a Gaussian waveguide

DDM - large PML on  $\Gamma_\infty$  - input mode  $n = 4$  -  $N_{\text{dom}} = 8$

$N_{\text{dom}}$	$\text{ABC}_{k_0}^{\text{T}0, -\pi/4}$	$\text{ABC}_{k_0}^{\text{T}2, -\pi/4}$	$\text{ABC}_{k_0}^{4(8), -\pi/4}$	$\text{ABC}_\omega^{4(8), -\pi/4}$
8	111	74	42 (42)	20 (8)

Table: GMRES iterations to  $10^{-6}$  at  $\omega = 160$ ,  $d_\lambda = 24$

Convergence in  $N_{\text{dom}}$  iterations  $\rightarrow$  continuous block LU factorization

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

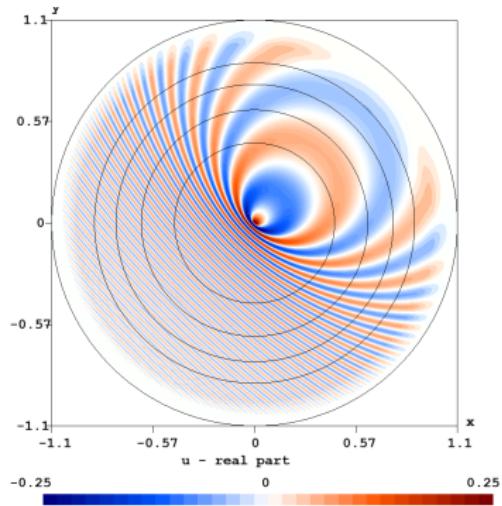
## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

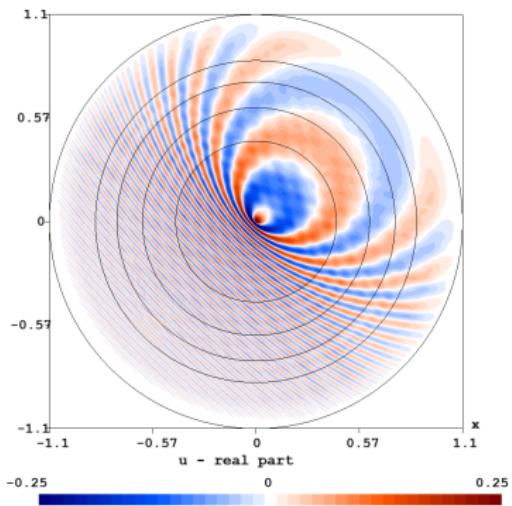
## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Convected problem in freefield - circular interfaces



(a)  $\text{ABC}_1^{4,-\pi/4}, \mathcal{E}_{L^2} = 1.7\%$



(b)  $\text{ABC}_1^{T2,-\pi/4}, \mathcal{E}_{L^2} = 24\%$

Numerical solution after 4 GMRES iterations.

Parameters:  $M = 0.9$ ,  $\theta = \pi/4$ ,  $p = 9$ ,  $d_\lambda = 8$ ,  $N_{\text{dom}} = 5$ ,  $\omega = 6\pi$ .  
 $L^2$ -error “PML-analytical solution” : 0.8%.

Padé conditions are robust for **high Mach numbers**

# Mach number variation - circular interfaces

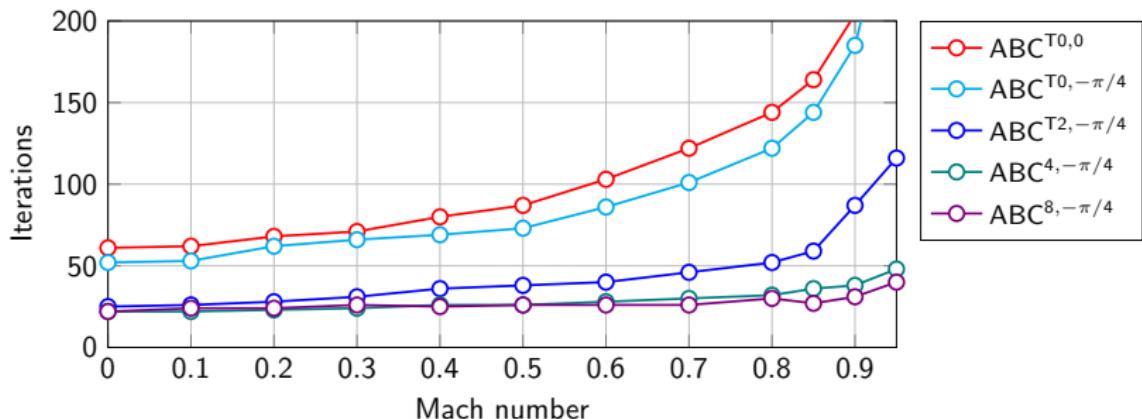


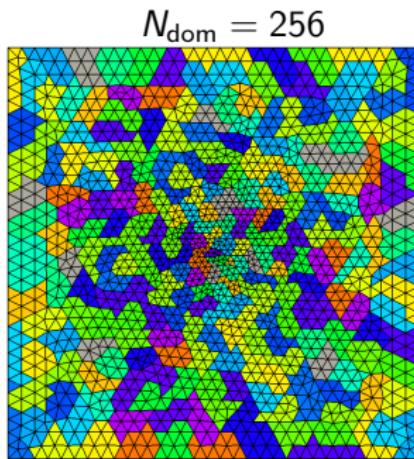
Figure: GMRES iterations to reach  $10^{-6}$  for  $N_{\text{dom}} = 5$ ,  $\omega = 6\pi$

- Only Padé conditions are robust for high Mach numbers
- Layered partition: iteration number increases as  $\mathcal{O}(N_{\text{dom}})$

# Convected problem in freefield - arbitrary decomposition

## Automatic partitioning

- Cross-points  
→ harder to design ABCs
- Industrial need - good load balancing between subproblems
- Shorter connectivity graph -  
 $\mathcal{O}(\sqrt{N_{\text{dom}}})$

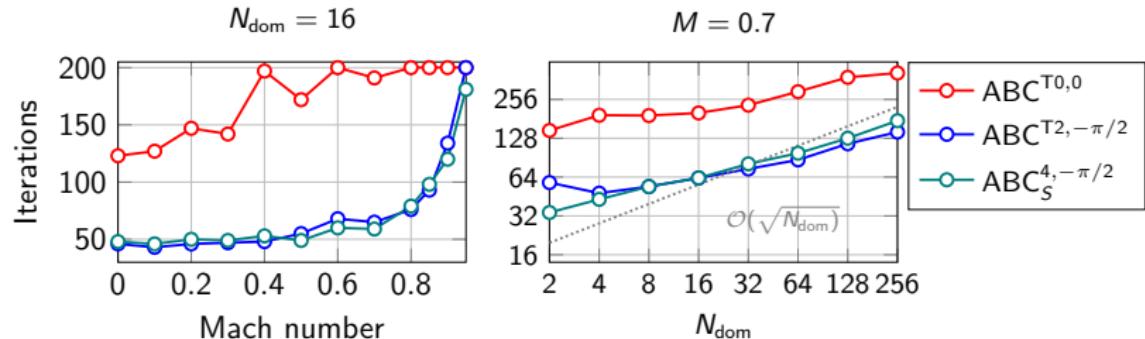


**Corner problem :** use Padé approximants on edges with Sommerfeld-type condition on corners → approximate corner treatment

Resulting condition  $\text{ABC}_S^{N,\alpha}$

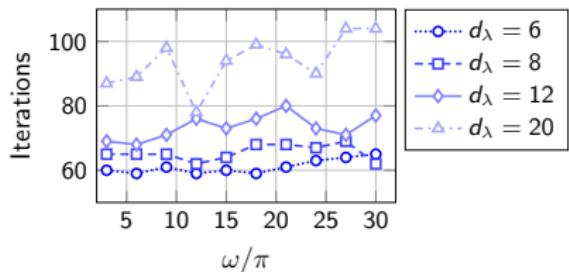
Are such Padé conditions still effective for domain decomposition ?

# Numerical study - arbitrary decomposition



GMRES iterations to reach  $10^{-6}$  for  $\omega = 6\pi$ ,  $d_\lambda = 8$

- lost of robustness for high Mach numbers
- $\text{ABC}^{T2,-\pi/2}$ ,  $\text{ABC}_S^{4,-\pi/2}$  → similar performance
- $\text{ABC}^{T2,-\pi/2}$  is cheaper (and easier) to implement



$M = 0.7$ ,  $N_{\text{dom}} = 16$ ,  $\text{ABC}^{T2,-\pi/2}$

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

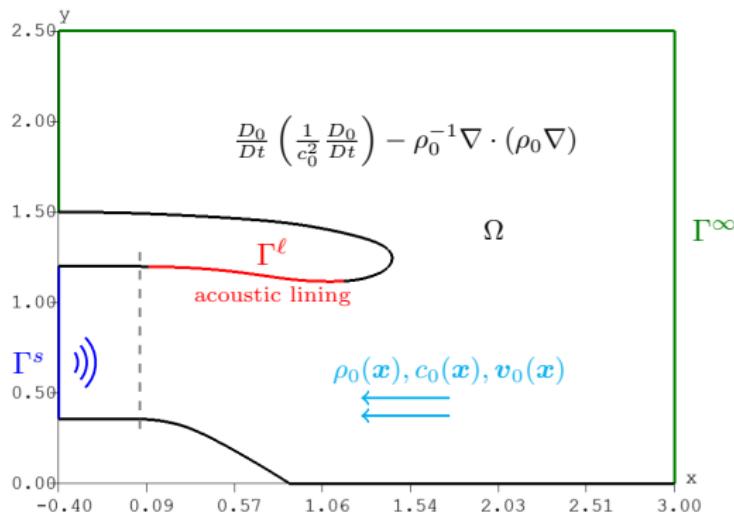
- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# The boundary value problem

Given a flight configuration (mean flow), predict the radiated noise from the fan, at multiples of the blade passing frequency  $\omega_{\text{bpf}}/(2\pi) = 1300$  Hz



## Boundary conditions

- Ingard-Myers on  $\Gamma_\ell$
- PML (active) on  $\Gamma^s$
- Fixed annular Bessel mode on  $\Gamma^s$
- PML (passive) on  $\Gamma^\infty$

The mean flow is pre-computed and **interpolated** on the acoustic mesh

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

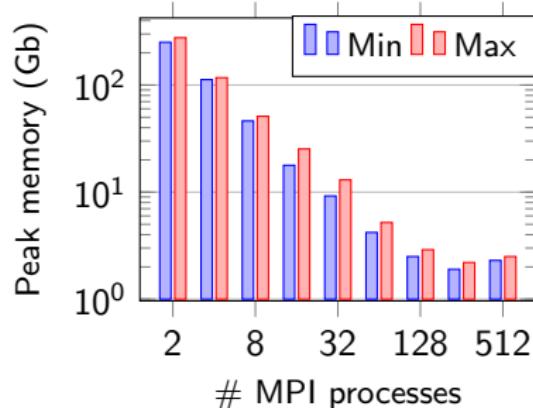
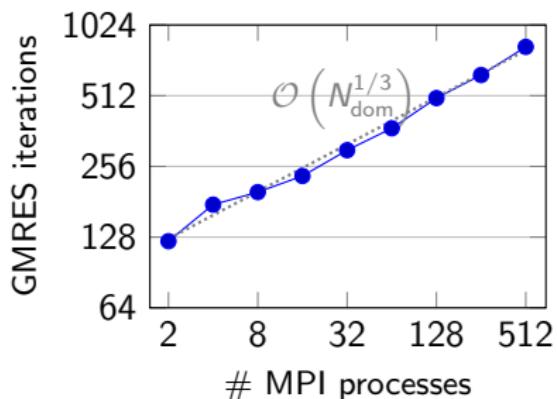
- Numerical results for the turbofan problem
- Solver weak scalability

# DDM for the 3D turbofan problem

$\omega_{\text{bpf}} - N_{\text{dofs}} = 10\text{M} - \text{nnz} = 730\text{M}$

$\approx 25$  wavelengths in  $\Omega$

Direct solver  $\rightarrow$  740 Gb RAM for factorization



Parallel GmshDDM solver (mono-thread)

From  $N_{\text{dom}} > 128$ , under 10 minutes and less than 3Gb per process

Iterations for  $N_{\text{dom}} = 64$

- $\text{ABC}^{\text{T}2,-\pi/2}$ : 372 GMRES iterations to  $10^{-6}$
- $\text{ABC}^{\text{T}0,0}$ : > 2000 GMRES iterations to reach  $10^{-3}$

# DDM for the 3D turbofan problem

$$2 \times \omega_{\text{bpf}} - N_{\text{dofs}} = 73M - \text{nnz} = 5B \quad \approx 50 \text{ wavelengths in } \Omega$$

Parallel GmshDDM solver (mono-thread),  $N_{\text{dom}} = \# \text{ MPI} = 128$

→ 2hours 3min, 26 Gb peak memory, 712 GMRES iterations (with lining)

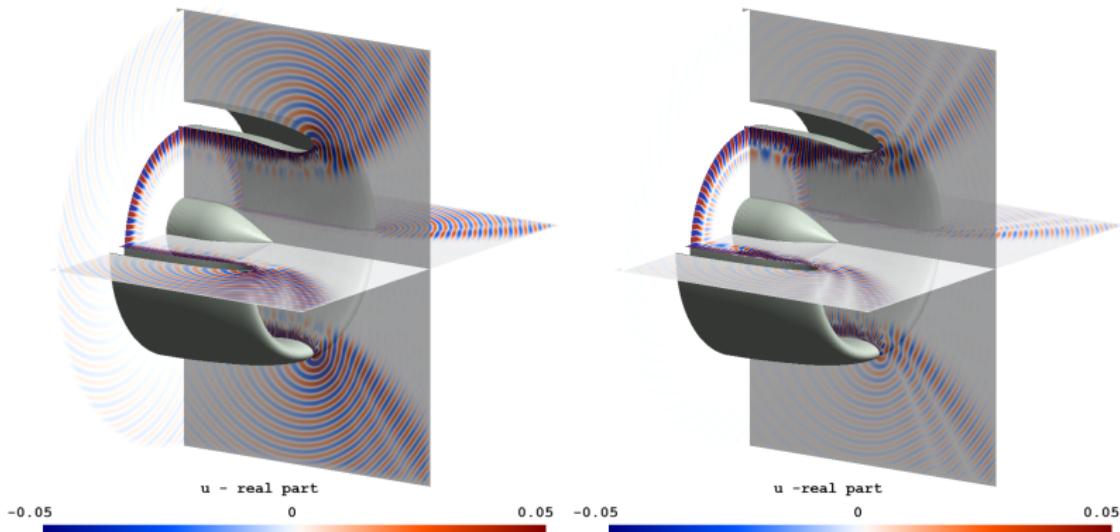


Figure: Real part of the acoustic velocity potential for the mode (48, 1) at  $2 \times \omega_{\text{bpf}}$  (2600 Hz) without (left) and with (right) acoustic lining treatment.

# Outline

## 1. Industrial context

- Physical models for sound propagation
- Reaching the memory limit
- Objective of the thesis

## 2. Domain decomposition framework

- Method overview
- Flow acoustics formulation
- Updated objective

## 3. ABCs for heterogeneous and convected problems

- Microlocal analysis
- Application to the Linearized Potential Equation
- Numerical examples

## 4. Application to non-overlapping domain decomposition

- Heterogeneous waveguide problems
- Convected problem in freefield

## 5. The 3D turbofan intake radiation problem

- Numerical results for the turbofan problem
- Solver weak scalability

# Weak scalability assessment

3D Helmholtz problem with  $d_\lambda = 7.5$  points per wavelength

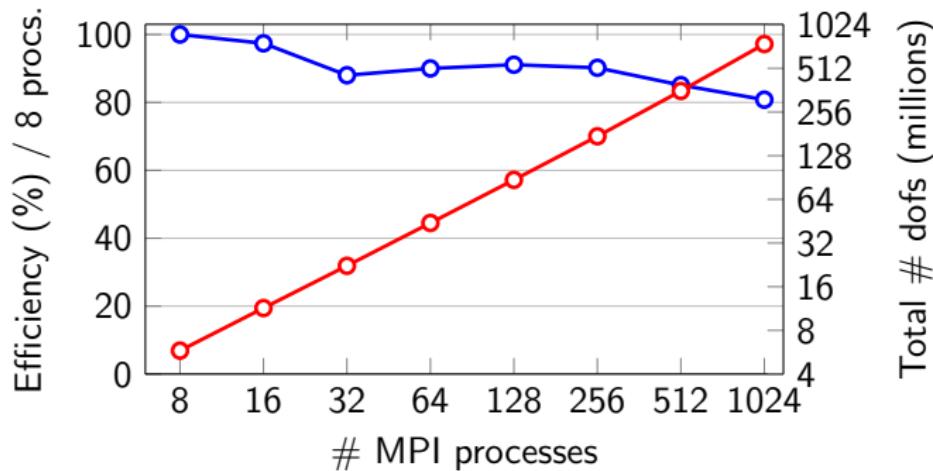


Figure: Weak scaling timing for 1 iteration

## Limitations

- memory load balancing: [20-34] Gb for 1024 processes
- number of iterations scales as  $\mathcal{O}(N_{\text{dom}}^{1/3})$  in 3D

# General summary and conclusion

Distributed memory solver for high frequency flow acoustics

1. Extension of a generic domain decomposition method to flow acoustics
2. Development of non-reflecting boundary conditions: ABCs and PMLs
  - ▶ extension to media with heterogeneities and convection
  - ▶ general PML procedure for flow acoustics
3. Code development (`GmshDDM`), validation and assessment of ABCs in a domain decomposition context
4. Proof of concept - turbofan intake
5. 80% scalability up to 700M high-order unknowns and 1024 MPI processes

# General summary and conclusion

## Limitations

- The iterative solver does not scale with  $N_{\text{dom}} \rightarrow$  requires coarse space
- Theoretical limitations - corners, curved boundaries, PML-DDM, etc.

## Future developments

- Extension to Pierce equation  $\rightarrow$  turbofan exhaust [*Spieser, Bailly 2020*]
- Modern discretization techniques such as HDG or HHO [*Li et al. 2013*]
- Interfaces through the mesh  $\rightarrow$  immersed transmission conditions

# General summary and conclusion

## Limitations

- The iterative solver does not scale with  $N_{\text{dom}} \rightarrow$  requires coarse space
- Theoretical limitations - corners, curved boundaries, PML-DDM, etc.

## Future developments

- Extension to Pierce equation  $\rightarrow$  turbofan exhaust [*Spieser, Bailly 2020*]
- Modern discretization techniques such as HDG or HHO [*Li et al. 2013*]
- Interfaces through the mesh  $\rightarrow$  immersed transmission conditions

Thank you !