6.2) Compute At and et for the following matrices

$$A_{7} \begin{bmatrix} 1 & 1 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad A_{1} \begin{bmatrix} 1 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}, \quad A_{3} \begin{bmatrix} 2 & 0 & 0 & 0 \\ 2 & 2 & 0 & 0 \\ 0 & 0 & 3 & 3 \\ 0 & 0 & 0 & 3 \end{bmatrix}$$

$$A^{\dagger} = \begin{bmatrix} 1 & \downarrow & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \lambda^{\downarrow} & \downarrow \lambda^{\downarrow} & 0 \\ 0 & \lambda^{\downarrow} & 0 \\ 0 & 0 & \lambda^{\downarrow} \end{bmatrix}$$

$$A = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$A^{2} = \begin{bmatrix} 1 & 1 & \alpha_{1} + 1 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$A^{2} = \begin{bmatrix} 1 & 1 & \alpha_{1} + 1 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$A^{3} = \begin{bmatrix} 1 & 1 & \alpha_{1} + 1 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$(S_{7}-A)^{7} = \begin{bmatrix} \frac{1}{5-1} & \frac{1}{5-1} & \frac{1}{5-1} \\ 0 & \frac{1}{5} & \frac{1}{5-1} \\ 0 & 0 & \frac{1}{5-1} \end{bmatrix} \qquad \begin{array}{c} \frac{1}{5-1} & \frac{1}{5-1} \\ \frac{1}{5-1} & \frac{1}{5-1} & \frac{1}{5-1} \\ \frac{1}{5-1} & \frac{1}{5-1} & \frac{1}{5-1} \end{array}$$

$$= \begin{bmatrix} (SI-4)^{-1} = \begin{bmatrix} \frac{1}{5} & \frac{1}{5} & \frac{1}{5} & \frac{1}{5} & \frac{1}{5} & \frac{1}{5} \\ 0 & 0 & \frac{1}{5} & \frac{1}{5} & \frac{1}{5} \end{bmatrix}$$

$$\lambda''(SP-4)'' = \begin{bmatrix} e^{t} & 1-e^{t} & 1-e^{t}+te^{t} \\ 0 & 1 & 1-e^{t} \\ 0 & 0 & e^{t} \end{bmatrix} U(t)$$

A3) A3=
$$\begin{bmatrix} 2000 \\ 2200 \\ 0033 \\ 0003 \end{bmatrix} = \begin{bmatrix} B_1 \\ 0 \\ B_2 \end{bmatrix}$$
 where $B_1 = \begin{bmatrix} 20 \\ 22 \end{bmatrix} = \begin{bmatrix} 33 \\ 03 \end{bmatrix}$

$$B_{2}^{+} = \begin{bmatrix} \lambda^{k} & k \lambda^{(k+1)} \\ 0 & \lambda^{k} \end{bmatrix}$$
 From $f_{113^{k}}$ per $f_{113^{k}}$ $f_{213^{k}}$ $f_{213^{k}}$

$$8_1 = \begin{bmatrix} 2 & G \\ 2 & Z \end{bmatrix}$$
 $\int_{1}^{1} (21 - 8) = \int_{-1}^{1} \begin{bmatrix} 2 - 2 & G \\ 2 & 2 & G \end{bmatrix} (21)^2 = \begin{bmatrix} 2 + 6 & G \\ 2 + G \end{bmatrix}$

$$B_{2} \begin{bmatrix} 3 & 3 \\ 0 & 3 \end{bmatrix} \quad A' \left(D - R_{2} \right) = \begin{bmatrix} 2^{2} & 3 & 2^{2} \\ 6 & 6^{3} & 3 \end{bmatrix}$$

7.2 2nd Edition)

Consider the modern
$$A = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 2 & 0 \\ 0 & 1 & 2 \end{bmatrix}$$

a) compute the characteristic & minimum polynomial of t.

$$dcf(2I-4) = \begin{vmatrix} s-1 & 1 & 0 \\ 0 & s-2 & 0 \\ 0 & 0 & s-2 \end{vmatrix} = (s-1)(s-2)^2 => (s-1)(s^2-4s+4)$$

$$0 & 0 & s-2 \end{vmatrix} => s^3-4s^2+4s-3^2+4s-4=s^3-5s^2+80S-4$$

b) Is this matrix diagonalizable? If so diagonalize it, otherwise compute its Jordan normal form.

$$V = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{bmatrix}$$
 $D = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 2 & 1 \\ 0 & 0 & 2 \end{bmatrix}$

7

8-2) For a given matrix A, Construct vectors for which (8.2) holds for each of the three norms 11-11s, 11-11z, and 11-11op.

(82) For every motion A E a vector x GIRM for which | 1411p = 11 x 11p

 $||A|_1 = \max_{1 \le j \le n} \frac{2}{|q_{ij}|} |q_{ij}|.$ Let x^{∞} be $e_i \in \mathbb{R}^n$ where i industry the non-zero element = to one. $||A||_1 = ||A x^{2}||_1 / ||x^{\alpha}||_1 = ||A e_i|| / ||e_i||_1 = \max_{1 \le j \le n} \frac{2}{i \le j} ||a_{ij}||_1$

||A|| = 18 ism \$\frac{2}{\infty} | a_{ij}| | or mux row sum

||A|| = 18 ism \$\frac{2}{\infty} | a_{ij}| | or mux row sum

||A|| = ||A x || ||A|| || = ||A x ||A|| ||A||

8.4) Consider a linear system with a state - transition matrix O(6,7) for which

See Mathb

c) compute the eigenvalues of
$$A(t)$$

$$det (A-SI) = det \begin{vmatrix} 3\cos(\varnothing)/2 - ^2z - S & 2-3\sin(\varnothing)/2 \\ -3\sin(\varnothing)/2 - 2 & -^{1}z-3\cos(\varnothing)/2 - S \end{vmatrix}$$
 where $\varnothing = 4t-4to$

8.6) Consider the Continuous time LTI system

 $\dot{x} = A_{x}$ $\lambda \in \mathbb{R}^{n}$

and suppose that there exists a positive constant 4 and positive definite matrices P, Q & R" for the Lyaponov equation

A'P + PA + 24P = -Q

Show that all eigenvalues of A have real parts less than -4.

For clearification Let B=A+UI then

B'P + PB = Qb => (A'+ui)P + Pb (4+ui) =- Qb => A'Pb + PbA' +2UPb =- Qb

Thus according to theorem 8-2 all of the eyen values of B have structly negative real parts. Cig (B) 60

 $B = A + UI = V^{\dagger} AV + UI$ wher $V \dagger A$ are the eigen vectors and eigen values of A, then

B= v'Av + vviv = v (_A + vI)v where AtvI are the eigen values of B thus A + vI & OI and A & - vI

Thus all the eigen values of A have real ports less than -U

- 8.7) Investigate whether or not the Solutions to the following nonlinear systems converge to the given equilibrium point when they start close enough to it
 - a) The State Space System

$$\dot{x}_1 = -x_1 + x_1(x_1^2 + x_2^2) = f(x_1/x_2)$$

 $\dot{x}_2 = -x_2 + \dot{x}_2(x_1^2 + x_2^2) = f(x_1/x_2)$

Whith equilibrium points X1 = X2 =0

$$\frac{\partial f_{0}(x_{1})|_{e_{1}^{2}}}{\partial f_{0}(x_{1})|_{e_{1}^{2}}} = 0 + 2x_{1}x_{2} |_{e_{1}^{2}} = 0$$

$$\frac{\partial f_{0}(x_{1})|_{e_{1}^{2}}}{\partial f_{0}(x_{2})|_{e_{1}^{2}}} = 0 + 2x_{1}x_{2} |_{e_{1}^{2}} = 0$$

$$\frac{\partial f_{0}(x_{1})|_{e_{1}^{2}}}{\partial f_{0}(x_{2})|_{e_{1}^{2}}} = 0 + 2x_{1}x_{2} |_{e_{2}^{2}} = 0$$

$$\frac{\partial f_{0}(x_{1})|_{e_{1}^{2}}}{\partial f_{0}(x_{2})|_{e_{1}^{2}}} = 0 + 2x_{1}x_{2} |_{e_{2}^{2}} = 0$$

$$\frac{\partial f_{0}(x_{1})|_{e_{1}^{2}}}{\partial f_{0}(x_{2})|_{e_{1}^{2}}} = 0 + 2x_{1}x_{2} |_{e_{2}^{2}} = 0$$

$$\bar{X} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} X$$
 thus $X(b) = C^{A} X(0)$ the eigen values of A care negative this true system will converge to the eigently number of the eigent

6) The Second order system

with the equilibrium point w= is=0. Determine for which values of 9(0) we can guarantee convergence, to the origin based on the local linearization

Let rewrit = f(win) - (f(wer, wee) -glo)-Sw - Sw) = O(11 Swil, 11 Svoll) baseally r is the error in the taylor series approximation.

Which means that there is a constant c and a ball B around equilibrium for which

Create the Lyapurou function

we need 900) > C[118w117+115w11]/115w11

Or in state space form

$$x = \begin{bmatrix} 0 & 1 \\ -1 & -99 \end{bmatrix} x$$
 eigen values are $3b(A - \chi I) = 3bt \begin{bmatrix} -1 & 1 \\ -1 & -99 - \chi \end{bmatrix} = -369(0)-3)-11$

$$= 3^{2} + 9(0)7 + 1$$

$$= 9(0)^{\frac{1}{2}} \sqrt{9(0)^{2} - 4}$$

Problem 8_4

Table of Contents

a) Compute the state transition matrix phi(t,t0)
b) Compute the matrix A(t) that corresponds to the given state transition matrix
c) Compute the eigen values of A(t)
d) Classify this system in terms of Lyapunov stability

a) Compute the state transition matrix phi(t,t0)

b) Compute the matrix A(t) that corresponds to the given state transition matrix

```
% Phi_dot = A(t)*PHI
PHI_dot = diff(PHI,t);
A = PHI_dot*inv(PHI);
A = simplify(A)
```

c) Compute the eigen values of A(t)

```
lambda = eig(A);
lambda = simplify(lambda)
```

d) Classify this system in terms of Lyapunov stability

We can look at the stability of the sytem by analyzing the the state transition matrix to see if it become arbitrarily large. The sin and cos functions are bounded between [-1,1], and the exponential functions are bounded between [0,0) depending on the value of t. Thus we can analyze the stability of PHI by looking at is as t -> infinity. By inspection, we can see that $|PHI| -> \inf$ and t -> inf. Thus the system is not stable.

```
parmas.m
PHI =
[\sin(2*t)*\sin(2*t0)*\exp(2*t0 - 2*t) + \cos(2*t)*\cos(2*t0)*\exp(t - t0),
\cos(2*t0)*\sin(2*t)*\exp(2*t0 - 2*t) - \cos(2*t)*\sin(2*t0)*\exp(t - t0)
[\cos(2*t)*\sin(2*t0)*\exp(2*t0 - 2*t) - \cos(2*t0)*\sin(2*t)*\exp(t - t0),
 \cos(2*t)*\cos(2*t0)*\exp(2*t0 - 2*t) + \sin(2*t)*\sin(2*t0)*\exp(t - t0)]
A =
[(3*\cos(4*t))/2 - 1/2, 2 - (3*\sin(4*t))/2]
[-(3*\sin(4*t))/2 - 2, -(3*\cos(4*t))/2 - 1/2]
lambda =
 -(7^{(1/2)*1i})/2 - 1/2
   (7^{(1/2)*1i})/2 - 1/2
Undefined variable "parmas" or class "parmas.m".
Error in Prob8 4 (line 46)
parmas.m
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```

Table of Contents

Aircraft Dynamics	- 1
a	1
b	. 1
C	2
d	
TEST	

Aircraft Dynamics

```
x_dot = A*x + B*u
P.A = [-0.038]
                  18.984
                            0
                                    -32.174;...
        -0.001
                 -0.632
                                     0;...
         0
                  -0.759
                            -0.518
                                      0;...
         0
                                      0];
P.B =
         [10.1
                      0;...
                     -0.0086;...
           0
           0.025
                     -0.011;...
                      0];
```

a.

Compute the modes of this system The mode is defined as exp(lambda_i*t)Vi

```
[V,lambda] = eig(P.A);
```

b.

Analyze these modes physically by looking at how the physical states play a role in each mode. Are there some modes that deal more with the pitch? Others that have more effect on the angle of attack?

```
V r = [0.9953]
                  0.9953
                             1.0000
                                        1.0000;...
       0.0562
                  0.0562
                            -0.0005
                                       -0.0005;...
      -0.0191
                 -0.0191
                             0.0007
                                        0.0007;...
       0.0500
                  0.0500
                            -0.0011
                                       -0.0011];
lambda r = [-0.5825 ; ...
             -0.5825 ; . . .
             -0.0115 ;...
             -0.0115];...
```

We can analyze these modes physically by looking at their real parts. If the initial state of the aircraft is along the span of any of these modes, then the states of the aircraft will evolve as $X(t) = \text{sigma exp}(\text{lambda_i*t})X(0)$ where $X(0) = \text{sigma*V_i}$ and sigma is a scalar. By looking at the eigen vector associated with the mode, we can see how some physical states are affected vs other physical states. In all of the modes, velocity is affected the most. The first two modes seem to have more affect on the pitch and and angle of attack than the other two modes.

C.

Aircraft generally exhibit two longitudinal motions (also called modes), a phugoid and short period mode. Phugoid represents the coupling between the vehicle altitude and the airspeed, while the short period mode (whith much faster dynamics) is the coupling between the angle of attack and the pitch rate. Identify the values from (a) that best represent the phugoid and short period modes respectively.

The first two modes show a strong coupling between the angle of attack and the pitch rate, and they have faster dynamics since the eigen values are larger, these must be the short period modes. By default the other two modes must be the phugoid modes.

d.

Given an input this aircraft wil respond along a linear combination of the modes. Determine how strongly each of the inputs will effect each of the different modes. Will one input effect one physical parameter more strongly?

```
W = inv(V);
% Throttle along mode one
th_v1 = W(1,:)*P.B(:,1)
% Throttle along mode two
th_v2 = W(2,:)*P.B(:,1)
% Throttle along mode three
th_v3 = W(3,:)*P.B(:,1)
% Throttle along mode four
th_v4 = W(4,:)*P.B(:,1)
% Elevator along mode one
el v1 = W(1,:)*P.B(:,2)
% Elevator along mode two
el_v2 = W(2,:)*P.B(:,2)
% Elevator along mode three
el_v3 = W(3,:)*P.B(:,2)
% Elevator along mode four
el_v4 = W(4,:)*P.B(:,2)
th v1 =
 -0.0326 - 0.1605i
th_v2 =
 -0.0326 + 0.1605i
```

```
th_v3 =

5.0825 + 1.9645i

th_v4 =

5.0825 - 1.9645i

el_v1 =

-0.0214 + 0.1176i

el_v2 =

-0.0214 - 0.1176i

el_v3 =

0.0213 - 0.0557i

el_v4 =

0.0213 + 0.0557i
```

Throttle affects modes 3 and 4 the most, and the elevator commands affects all the modes about equally in magnitude. This makes sense since modes 3 and 4 are more for air speed and throttle should affect the air speed most.

TEST

```
% syms c11 c12 c13 c21 c22 c23 c31 c32 c33
% syms v11 v12 v13 v21 v22 v23 v31 v32 v33
% syms e1 e2 e3
% syms x1 x2 x3
% C =[c11 c12 c13; c21 c22 c23; c31 c32 c33];
% V = [v11 v12 v13; v21 v22 v23; v31 v32 v33];
% E = [e1 0 0; 0 e2 0; 0 0 e3];
% X = [x1;x2;x3];
%
% C*E*V*X
% W = inv(P.V)
```

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