

## UNIT 2

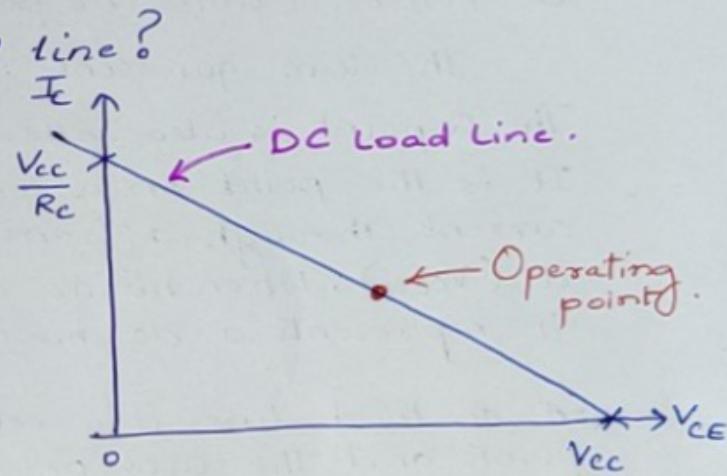
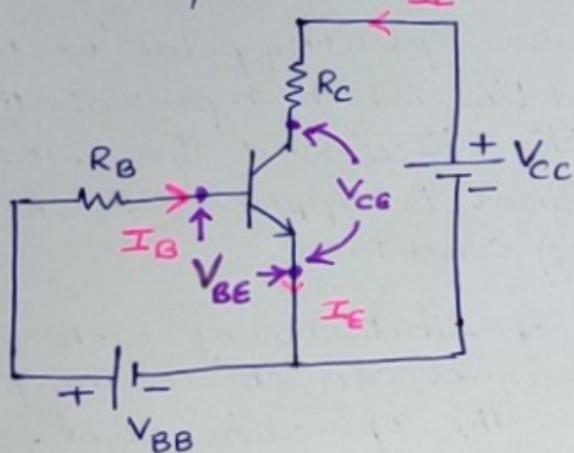
### # DC Load Line:

It is the line drawn on the OIP characteristic of the transistor. DC load line is used for analyzing the performance of an amplifier.

It is a graph of Collector current ( $I_c$ ) and Collector-Emitter voltage ( $V_{CE}$ ) for a given value of  $R_C$  and  $V_{CC}$ .

It is a graphical representation of all the possible operating points for the given circuit with the given DC biasing.

Q How to plot a DC load line?



Step 1:- Apply KVL at OIP section.

$$V_{CC} - I_c R_C - V_{CE} = 0$$

$$V_{CC} - V_{CE} = I_c R_C$$

$$I_c = \frac{V_{CC} - V_{CE}}{R_C}$$

$$I_c = -\frac{1}{R_C} V_{CE} + \frac{V_{CC}}{R_C} \quad \text{--- ①}$$

Equation for the slope of straight line.

$$y = mx + c \quad \text{--- ②}$$

Compare eqn 1 & 2

$$y = I_c$$

$$m = -\frac{1}{R_C}$$

$$x = V_{CE}$$

$$c = \frac{V_{CC}}{R_C} \left. \right\} \text{constant}$$

(fixed)

Step 2:-  $V_C = 0$  in eq 1.

$$\therefore 0 = -\frac{1}{R_C} V_{CE} + \frac{V_{CC}}{R_C}$$

$$\frac{V_{CE}}{R_C} = \frac{V_{CC}}{R_C}$$

$$V_{CE} = V_{CC}$$

Step 3:-  $V_{CE} = 0$  in eq 1.

$$I_C = \frac{V_{CC}}{R_C}$$

# Q-Point (Quiescent point or Operating point) :-

The term quiescent means quite, still or inactive.

The Q point is also called as 'operating point' or 'bias point'. It is the point on a load line which represents the dc current through a transistor ( $I_{CQ}$ ) and the voltage across it ( $V_{CEQ}$ ), when no ac signal is applied. In short it represents a dc biasing conditions.

A dc load line is a set of finite no. of such operating points and the user or designer can choose any point on the dc load line as the operating point.

The position of operating point on the load line depends on the application of transistor.

If the transistor is being used for 'amplification' purpose then the Q point should be at the center of load line.

# FACTORS AFFECTING STABILITY OF Q-POINT.

a) When I<sub>IP</sub> signal is applied, the OIP signal should not move the transistor either to saturation or to cut-off. However, this unwanted shift might occur due to various reasons outlined below.

a.) Change in the Temperature

b.) Change in the value of  $\beta$ .

What is the Requirement of Biasing Circuit?

The requirements of biasing circuit are

- 1) Establish the Q-point in the centre of the active region of the characteristics, so that on applying the I/P signal the instantaneous Q point does not move either to the saturation region or to the cut-off region, even at the extreme values of the I/P signal.
- 2) Stabilize the collector current ( $I_c$ ) against temperature variations.
- 3) Make the Q point independent of the transistor parameters so that it does not shift when the transistor is replaced by another of the same type in the circuit.

## # Biasing Circuits .

To avoid shift of Q-point, bias stabilization is necessary. Various biasing circuits can be used for this purpose.

- 1) Fixed bias.
- 2) Collector to base bias.
- 3) Fixed bias with emitter resistor .
- 4) Voltage divider bias.
- 5) Emitter bias.

## # FIXED BIAS:- (BASE BIASING).

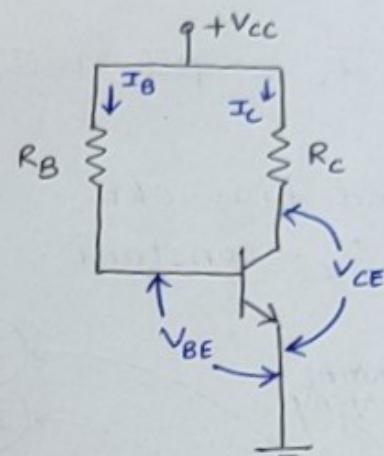
Simplest biasing ckt.

Step 1:-  $I_B$ .

Analysis of fixed bias.

Apply KVL at IIP side.

$$V_{CC} - I_B R_B - V_{BE} = 0$$



$$I_B R_B = V_{CC} - V_{BE}$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

$V_{BE} = 0.7V$  Si      very small so neglect  
 $V_{BE} = 0.3V$  Ge.

$$\therefore I_B = \frac{V_{CC}}{R_B}$$

This eqn is for base current corresponding to Q point.

$V_{CC}$  - constant } (fixed)  $\rightarrow$  hence fixed bias ckt.  
 $R_B$  - constant

Step 2:-  $I_c$ .

$$I_c = \beta I_B + I_{CEO}. \quad \text{But } I_{CEO} \ll \beta I_c.$$

$$I_{CQ} = \beta_{dc} I_B.$$

Step 3:-  $V_{CE}$  or  $V_{CQ}$ .

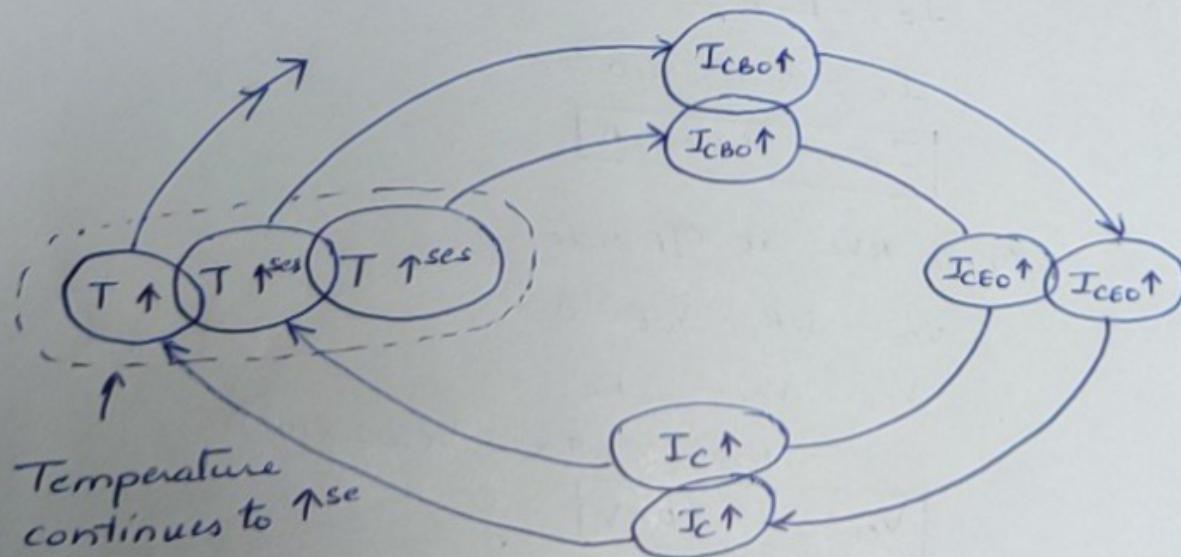
Apply KVL at OIP side.

$$V_{CC} - I_c R_C - V_{CE} = 0$$

$$V_{CE} = V_{CC} - I_c R_C$$

## # THERMAL RUNAWAY-

- ① With  $\uparrow^{se}$  in temperature, the leakage current  $I_{CBO}$   $\uparrow^{ses}$ .  $I_c = I_{c(\text{majority})} + I_{c(\text{minority})}$
- ② This  $\uparrow^{se}$  in  $I_{CBO}$ ,  $\uparrow^{ses}$   $I_{CEO}$   
 $\therefore I_{CEO} = (1+\beta) I_{CBO}$ .
- ③ As  $I_{CEO} \uparrow^{ses}$ , this leads to  $\uparrow^{se}$  in  $I_c$ .  
 $\therefore I_c = I_{c(\text{majority})} + I_{c(\text{minority})}$ .  
 $I_c = \beta I_B + I_{CEO}$ .
- ④ The further  $\uparrow^{se}$  in  $I_c$  leads to more amount of power producing heat at the collector region and more minority carriers  $\uparrow^{ses}$  as they are thermally generated.
- ⑤ With further  $\uparrow^{se}$  in temperature,  $I_{CBO}$  -thermally generated minority carriers  $\uparrow^{se}$  and the whole cycle is repeated.
- ⑥ This leads to a situation called 'THERMAL RUNAWAY'.



NOTE:-  $T \uparrow \rightarrow I_{CBO} \uparrow \rightarrow I_{CEO} \uparrow \rightarrow I_c \uparrow$

## # ADVANTAGES OF FIXED BIAS CIRCUIT :-

- (1) Simple ckt and less components.
- (2) Good flexibility as Q point can be set at any point in the region by just adjusting the value of  $R_B$ .

## # DISADVANTAGES OF FIXED BIAS CIRCUIT:-

- (1) Very poor thermal stability ( $s = 1 + \beta$ ),
- (2) With change in  $\beta$  due to changes in temperature - the operating point keeps on shifting its position.

Find  $I_B$ ,  $I_c$  &  $V_{CE}$  for the ckt shown. (15-16)  $\leftarrow 6\text{marks}$

Q.  
Sln

Apply KVL at I/P side,

$$V_{CC} - I_B R_B - V_{BE} = 0$$

$$V_{CC} - V_{BE} = I_B R_B .$$

$$I_B = \frac{V_{CC}}{R_B} - \frac{V_{BE}}{R_B} .$$

$$= \frac{18 - 0.7}{470 \times 10^3} = 36.8 \times 10^{-6} .$$

$$\boxed{I_B = 36.8 \mu\text{A}}$$

$$I_c = \beta I_B = 100 \times 36.8 \times 10^{-6} .$$

$$I_c = 3.68 \times 10^{-3} .$$

$$\boxed{I_c = 3.68 \text{mA}}$$

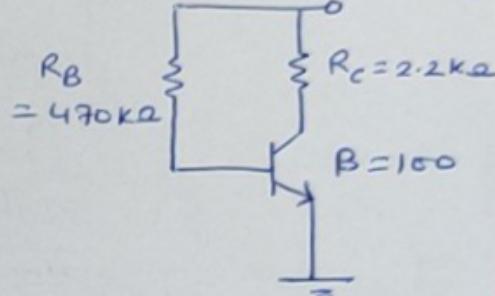
Apply KVL at O/P side.

$$V_{CC} - I_c R_C - V_{CE} = 0 .$$

$$V_{CE} = V_{CC} - I_c R_C$$

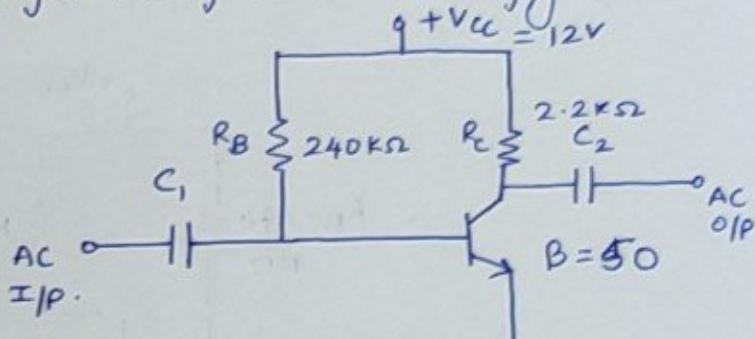
$$= 18 - (3.68 \times 10^{-3} \times 2.2 \times 10^3)$$

$$\boxed{V_{CE} = 9.904 \text{V}}$$



Q: Determine the following for the fixed bias configuration

- a)  $I_{BQ}$  &  $I_{CQ}$
- b)  $V_{CEQ}$
- c)  $V_B$  &  $V_C$ .
- d)  $V_{BC}$ .



$$\text{Soln:- } I_{BQ} = \frac{V_{CC} - V_{BE}}{R_B} = \frac{12 - 0.7}{240 \times 10^3} \\ = 47.08 \times 10^{-6}$$

$$I_{BQ} = 47.08 \mu\text{A.} //$$

$$I_{CQ} = \beta I_{BQ} \\ = 50 \times 47.08 \times 10^{-6} \\ = 2.354 \times 10^{-3} \\ I_{CQ} = 2.354 \text{ mA.} //$$

$$V_{CEQ} = V_{CC} - I_{CQ} R_C \\ = 12 - 2.354 \times 10^{-3} \times 2.2 \times 10^3 \\ = \cancel{12 - 6.8} \quad 6.8212 \text{ V.}$$

$$V_B = V_{BE} + V_E \\ = 0.7 + 0 \\ = 0.7 \text{ V.}$$

$$V_C = V_{CE} + V_E \\ = 6.8212 + 0 \\ V_C = 6.8212 \text{ V.}$$

$$V_{BC} = V_B - V_C \\ = 0.7 - 6.8212 \\ = -6.1212 \text{ V.}$$

Q Design a fixed circuit using a Si npn transistor which has  $\beta_{dc} = 150$ . The dc biasing point is at  $V_{CE} = 5V$  and  $I_C = 5mA$ . Supply voltage  $V_{CC} = 10V$ .

Soln.

$$n-p-n$$

$$\beta = 150$$

$$V_{CE} = 5V$$

$$I_C = 5mA$$

$$V_{CC} = 10V$$

$$I_B = \frac{I_C}{\beta} = \frac{5 \times 10^{-3}}{150} = 33.33 \mu A$$

$$V_{CC} - V_{BE} = I_B R_B$$

$$R_B = \frac{V_{CC} - V_{BE}}{I_B} = \frac{10 - 0.7}{33.33 \times 10^{-6}}$$

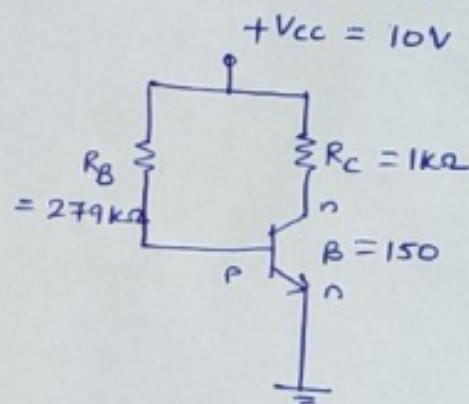
$$R_B = 279.02 k\Omega$$

$$V_{CC} - V_{CE} = I_C R_C$$

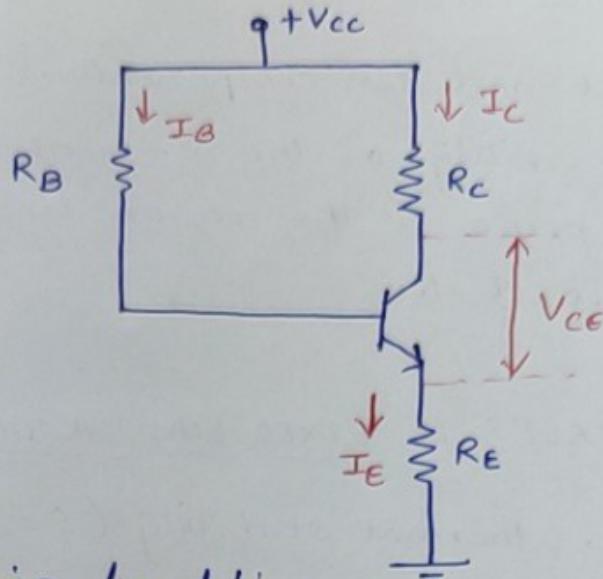
$$R_C = \frac{V_{CC} - V_{CE}}{I_C}$$

$$= \frac{10 - 5}{5 \times 10^{-3}}$$

$$R_C = 1k\Omega$$



## # MODIFIED FIXED BIAS CIRCUIT (EMITTER BIAS)



$R_E$  is added in fixed bias ckt. The emitter resistor improves the bias point stability.

Stabilization of Q point.

- 1) If  $I_c$  increases due to either increase in temperature or change in  $\beta$ . due to replacement of transistor then the  $I_E$  will also increase.
- 2) Due to increase in  $I_E$ , voltage drop across  $R_B$ . i.e.,  $V_E$  increases.
- 3)  $\therefore V_{BE}$  will decrease. This will reduce the value of  $I_B$  and therefore the increased  $I_c$  will reduce. Thus stabilization of Q point takes place.

Analysis:-

Step 1:-  $I_{BQ}$

Apply KVL to base ckt.

$$V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0.$$

$$I_B R_B = V_{CC} - V_{BE} - I_E R_E.$$

$$\begin{aligned} R_B I_B &= V_{CC} - V_{BE} - (I_B + I_C) R_E \\ &= V_{CC} - V_{BE} - (\beta I_B + I_B) R_E \\ &= V_{CC} - V_{BE} - (1 + \beta) I_B R_E \end{aligned}$$

$$R_B I_B + (1 + \beta) I_B R_E = V_{CC} - V_{BE}.$$

$$I_B [R_B + (1 + \beta) R_E] = V_{CC} - V_{BE},$$

$$I_{BQ} = \frac{V_{CC} - V_{BE}}{R_B + (1+\beta) R_E}$$

Step 2:-  $I_{CQ}$ .

$$I_{CQ} = \beta I_{BQ},$$

$$I_{CQ} = \beta \left[ \frac{V_{CC} - V_{BE}}{R_B + (1+\beta) R_E} \right]$$

$$I_{CQ} = \frac{\beta (V_{CC} - V_{BE})}{R_B + (1+\beta) R_E}$$

Step 3:-  $V_{CEQ}$ .

$$V_{CC} - I_C R_C - V_{CE} - I_E R_E = 0.$$

$$\begin{aligned} V_{CE} &= V_{CC} - I_C R_C - I_E R_E \\ &= V_{CC} - I_C R_C - (I_C - I_B) R_E \\ &= V_{CC} - I_C R_C - I_C R_E + I_B R_E \\ &= V_{CC} - I_C (R_C + R_E) + I_B R_E. \end{aligned}$$

$$V_{CC} \gg I_C R_E$$

$$V_{CE} = V_{CC} - I_C (R_C + R_E).$$

Q. For the emitter bias, find  $I_B$ ,  $I_C$ ,  $V_C$ ,  $V_E$  and  $V_{CE}$

Soln:-

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (1+\beta) R_E} = \frac{20 - 0.7}{500 \times 10^3 + (1+100) \times 1000}$$

$$I_B = 32.11 \mu A,$$

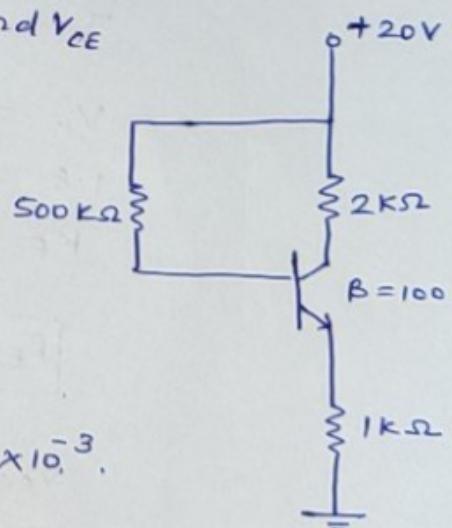
$$I_C = \beta I_B = 100 \times 32.11 \times 10^{-6},$$

$$I_C = 3.2113 \text{ mA}$$

$$I_E = I_B + I_C = 32.11 \times 10^{-6} + 3.2113 \times 10^{-3},$$

$$I_E = 3.2431 \text{ mA}$$

$$\begin{aligned} V_C &= V_{CC} - I_C R_C = 20 - (3.2113 \times 10^{-3} \times 2 \times 10^3) \\ &= 20 - 13.58 V \end{aligned}$$



$$V_E = I_E R_E = 3.2431 \times 10^{-3} \times 1000$$

$$V_E = 3.2431 V$$

$$V_{CE} = V_C - V_E$$

$$= 13.58 - 3.2431$$

$$V_{CE} = 10.337 V$$

- Q) Design the emitter bias ckt to satisfy the following
- $V_{CC} = 18 V$
- $I_{CQ} = 2 mA$
- $V_{CEQ} = 9 V$
- $\beta = 100$

Soln:-

$$I_{BQ} = \frac{I_C}{\beta} = \frac{2 \times 10^{-3}}{100} = \frac{2 \times 10^{-3}}{10^2} = 20 \mu A$$

For good Q point stability.

$$V_E = 0.1 V_{CC}$$

$$= 0.1 \times 18$$

$$V_E = 1.8 V$$

$$V_E = I_E R_E$$

$$I_E = I_B + I_C = 20 \times 10^{-6} + 2 \times 10^{-3}$$

$$I_E = 2.02 mA$$

$$V_E = I_E R_E$$

$$1.8 = 2.02 \times 10^{-3} \times R_E$$

$$R_E = \frac{1.8}{2.02 \times 10^{-3}}$$

$$R_E = 831 \Omega$$

$$V_{CC} - I_B R_B - V_{BE} - V_E = 0$$

$$18 - 20 \times 10^{-6} - 0.7 - 1.8 = 0$$

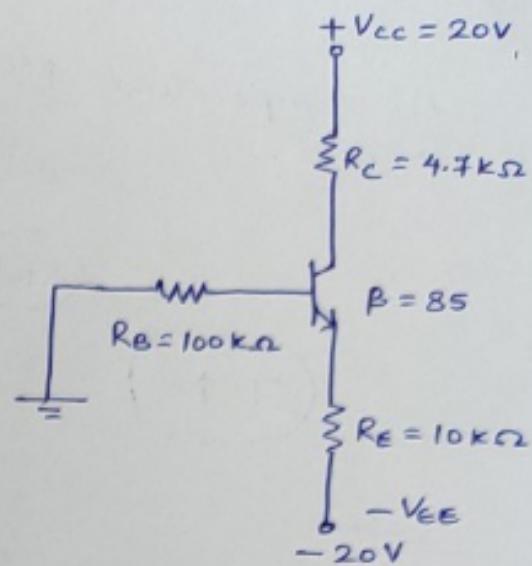
$$R_B = \frac{18 - 0.7 - 1.8}{20 \times 10^{-6}} = 775 k\Omega$$

Q. For the emitter bias ckt shown,  
Find  $I_E$ ,  $I_C$ ,  $V_c$  and  $V_{CE}$  for  
 $\beta = 85$  and  $V_{BE} = 0.7V$

$$\text{Solt: } I_E \approx I_C = \frac{V_{CC} - V_{BE}}{R_E + (R_B/\beta)}$$

$$I_E = \frac{20 - 0.7}{10 \times 10^3 + (100 \times 10^3 / 85)}$$

$$I_C = \boxed{I_E = 1.73 \text{ mA}}$$



$$V_C = V_{CC} - I_C R_C = 20 - (1.73 \times 10^{-3} \times 4.7 \times 10^3) = 11.9V$$

$$V_E = -V_{EE} + I_E R_E = -20 + (1.73 \times 10^{-3} \times 10 \times 10^3)$$

$$\boxed{V_E = -2.7V}$$

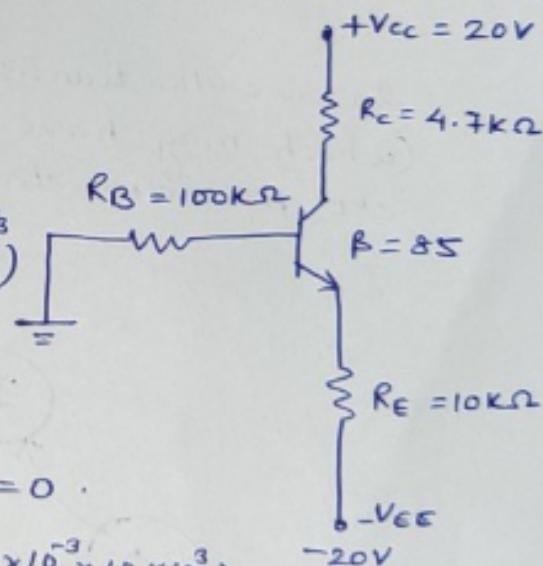
$$V_E = V_C - V_E = 11.9 - (-2.7) = 14.6V$$

B: Determine how much the Q-point in the fig change over a temperature range where  $\beta$  increases from 85 to 100 and  $V_{BE}$  decreases from 0.7V to 0.6V.

Solt: For  $\beta = 85$ . &  $V_{BE} = 0.7V$ .

$$I_C = \frac{V_{CC} - V_{BE}}{R_E + \left(\frac{R_B}{\beta}\right)} = \frac{20 - 0.7}{10 \times 10^3 + \left(\frac{100 \times 10^3}{85}\right)}$$

$$I_E = \boxed{I_C = 1.73 \text{ mA}}$$



$$V_{CC} - I_C R_C - V_{CE} - I_E R_E - (-V_{EE}) = 0$$

$$20 - (1.73 \times 10^{-3} \times 4.7 \times 10^3) - V_{CE} - (1.73 \times 10^{-3} \times 10 \times 10^3) + 20 = 0$$

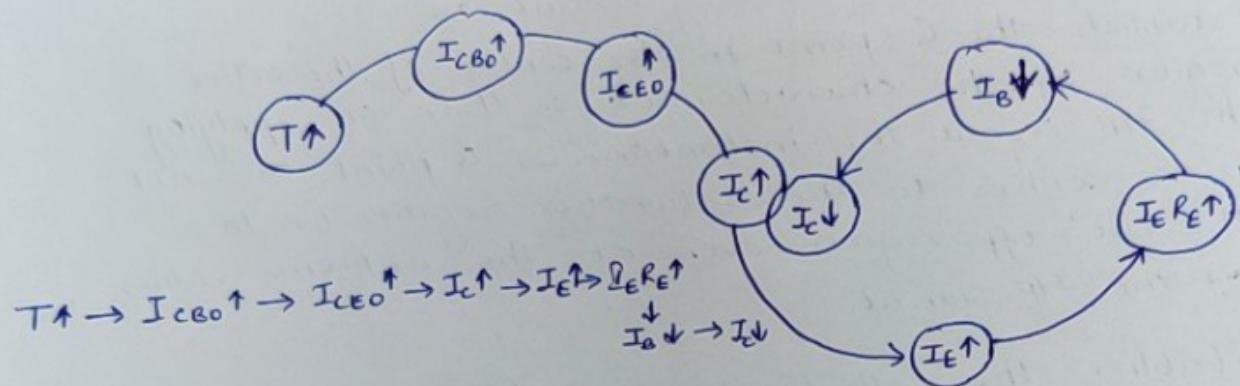
~~$$4.6 - 19.998 = V_{CE} - 17.3 + 20$$~~

$$V_C = V_{CC} - I_C R_C = 20 - (1.73 \times 10^{-3} \times 4.7 \times 10^3)$$

$$V_E = I_E R_E - V_{EE} = (1.73 \times 10^{-3} \times 10 \times 10^3) - 20 = -2.7V$$

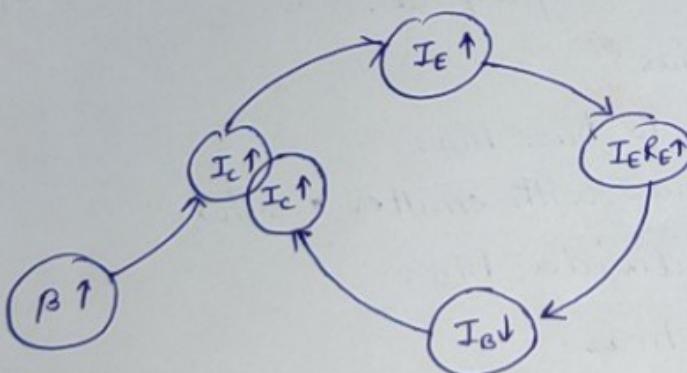
$$V_{CE} = V_C - V_E = 11.9 - (-2.7) = 14.6V$$

(1) As the temperature tends to  $\uparrow^{\text{se}}$ , the following sequence of events occurs



Because of  $\uparrow^{\text{se}}$  in temperature,  
The leakage current  $I_{CBO} \uparrow^{\text{se}}$ , and hence  $I_{CEO} \uparrow^{\text{se}}$  ( $I_{CEO} = (1+\beta)I_{CBO}$ ).  
This  $\uparrow^{\text{se}}$  the collector  $I_{CEO} \uparrow^{\text{se}}$ ,  $I_c \uparrow^{\text{se}}$ ,  $I_E = \beta I_B + I_{CEO}$ .  
With  $\uparrow^{\text{se}}$  in the collector current  $I_c$ ,  $I_E \uparrow^{\text{se}}$  as  $I_E = I_B + I_c$ .  
Thus the voltage drop across the emitter resistor  $R_E \uparrow^{\text{se}}$ .  
 $\therefore I_{ERET} \uparrow$ , further reduces  $I_B$ , and this leads to  
the reduction in the collector current  $I_c$ .  
Thus we see that  $I_c$  is not allowed to  $\uparrow^{\text{se}}$  to the extent it would have been in the absence of  $R_E$ .

(2) In case the transistor is replaced by another of the same type



①  $\beta \uparrow^{\text{se}}$ ,  $\beta = \frac{I_c}{I_B}$ , hence  $I_c \uparrow^{\text{se}}$ .

② As  $I_c \uparrow^{\text{se}}$ ,  $I_c = I_B + I_E$  and  $I_B$  is very small hence,  $I_E \uparrow^{\text{se}}$ .

③ Voltage drop across  $R_E \uparrow^{\text{se}}$  ( $V_E = I_{ERET} R_E \uparrow^{\text{se}}$ )

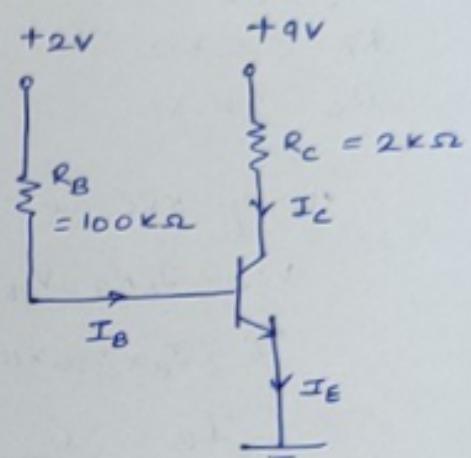
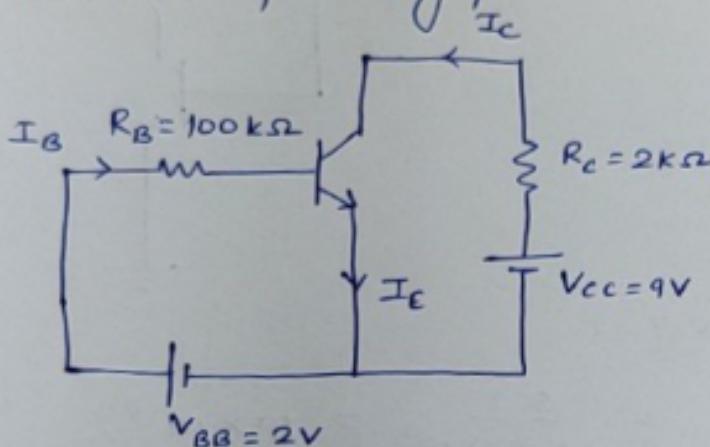
④ Which  $\downarrow^{\text{se}}$   $I_B$ , as  $I_B = \frac{V_{CC} - V_{BE} - V_E}{R_B}$

⑤ As  $V_{CC}$  is constant and  $V_{BE}$  also, then with  $\uparrow^{\text{se}}$  in  $V_E$   $I_B \downarrow^{\text{se}}$ . This leads to  $\uparrow^{\text{se}}$  in  $I_c$ .

Q. Figure shows biasing with base resistor method.

i) Determine the collector current  $I_c$  and collector-emitter voltage  $V_{CE}$ . Neglect small base-emitter voltage. Given that  $\beta = 50$ .

ii) If  $R_B$  in this ckt is changed to  $50\text{ k}\Omega$ , find the new operating point.



Soln: Apply KVL at IIP,

$$V_{BB} - I_B R_B - V_{BE} = 0$$

$$( \because V_{BE} = 0 \text{ given})$$

$$V_{BB} - I_B R_B = 0$$

$$2 - I_B \times 100 \times 10^3 = 0$$

$$I_B = \frac{2}{100 \times 10^3} = 20 \mu\text{A} //$$

$$I_C = \beta I_B = 50 \times 20 \times 10^{-6}$$

$$I_C = 1 \times 10^{-3}$$

$$I_C = 1 \text{ mA} //$$

Apply KVL at OIP,

$$V_{CC} - I_C R_C - V_{CE} = 0$$

$$9 - (1 \times 10^{-3} \times 2 \times 10^3) - V_{CE} = 0$$

$$9 - 2 = V_{CE}$$

$$V_{CE} = 7 \text{ V} //$$

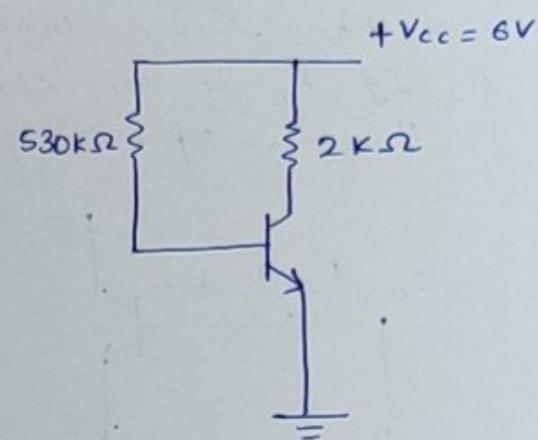
$$\text{When } R_B = 50 \text{ k}\Omega, \quad I_B = \frac{2}{50 \times 10^3} = 40 \mu\text{A}$$

$$I_C = \beta I_B = 50 \times 40 \times 10^{-6} = 2000 \mu\text{A} = 2 \text{ mA}$$

$$V_{CE} = V_{CC} - I_C R_C = 9 - (2 \times 10^{-3} \times 2 \times 10^3) = 5 \text{ V}$$

Q) Fig shows that a Si  $\text{XOR}$  with  $\beta = 100$  is biased by base resistor method. Draw the dc load line and determine the operating point. What is the stability factor?

Soln:  $V_{cc} = 6\text{V}$   
 $R_B = 530\text{k}\Omega$   
 $R_C = 2\text{k}\Omega$



Apply KVL at IIP.

$$V_{cc} - I_B R_B - V_{BE} = 0$$

$$6 - I_B \times 530 \times 10^3 - 0.7 = 0$$

$$I_B = \frac{6 - 0.7}{530 \times 10^3} = \frac{5.3}{530 \times 10^3} = 10 \times 10^{-6}$$

$$= 10 \mu\text{A}$$

$$I_C = \beta I_B$$

$$= 100 \times 10 \times 10^{-6}$$

$$= 1 \times 10^{-3}$$

$$= 1 \text{mA}$$

$$V_{CE} = V_{cc} - I_C R_C$$

$$= 6 - (1 \times 10^{-3} \times 2 \times 10^3)$$

$$= 6 - 2$$

$$= 4\text{V}$$

Stability factor =  $1 + \beta$ .

$$= 1 + 100$$

$$= 101$$

point A =  $I_{C\max} = \frac{V_{cc}}{R_C}$

$$= \frac{6}{2 \times 10^3} = 3 \times 10^{-3}$$

$$= 3 \text{mA}$$

point B =  $V_{CE\max} = V_{cc} = 6\text{V}$

