



EXCELLABUST

EXCELLING LABUST IN MARINE ROBOTICS

Modelling and Simulation of Marine Craft KINEMATICS

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Kinematics

Reference Frames

ECEF Frame

NED Frame

BODY Frame

UNITY Frame

UTM

Transformations BODY – NED

Euler Angles

Quaternions

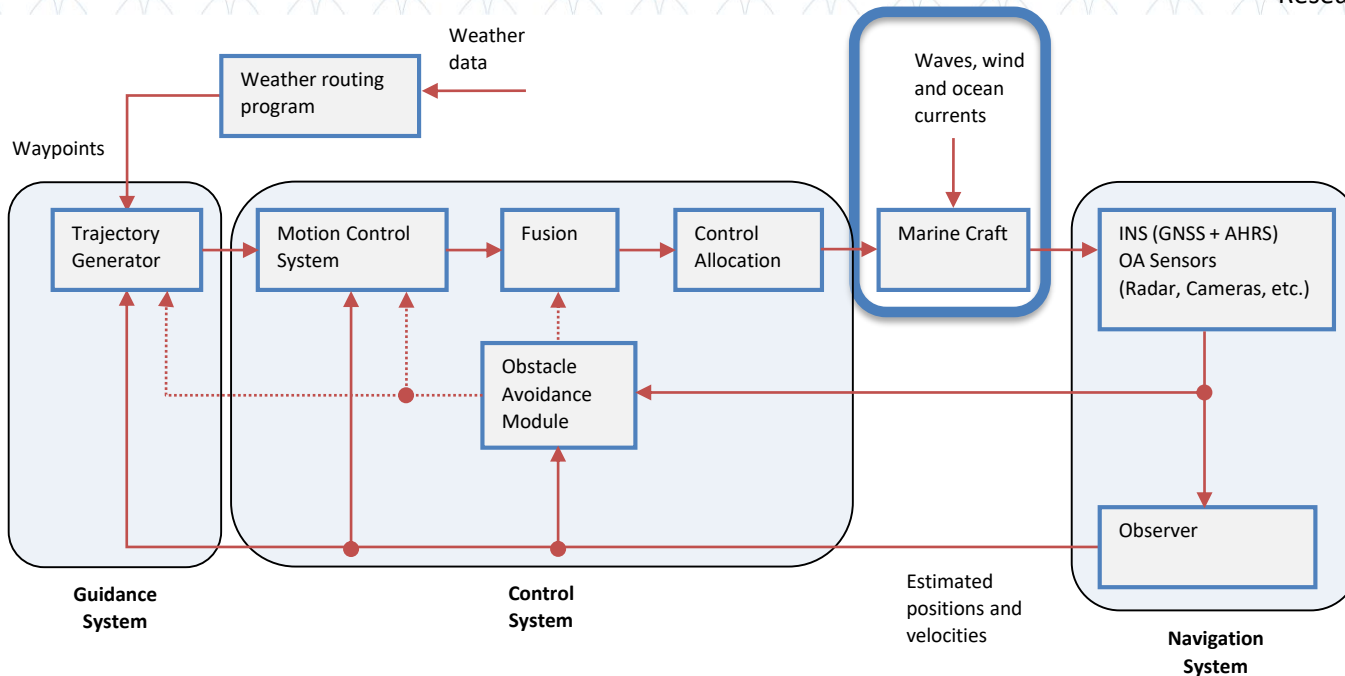
Quaternions from Euler Angles

Euler Angles from Quaternions

Transformations ECEF – NED

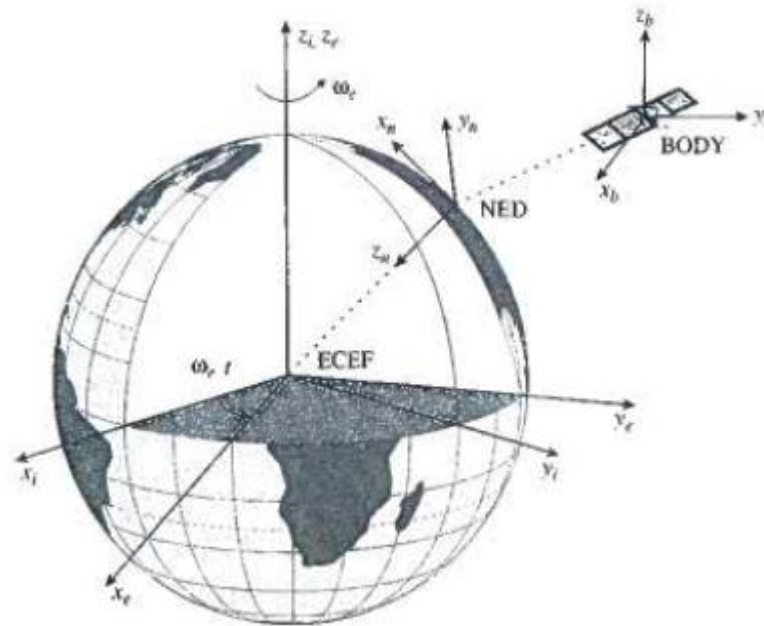
Lat-Lon from ECEF Coordinates

ECEF Coordinates from Lat-Lon



GNC Signal Flow

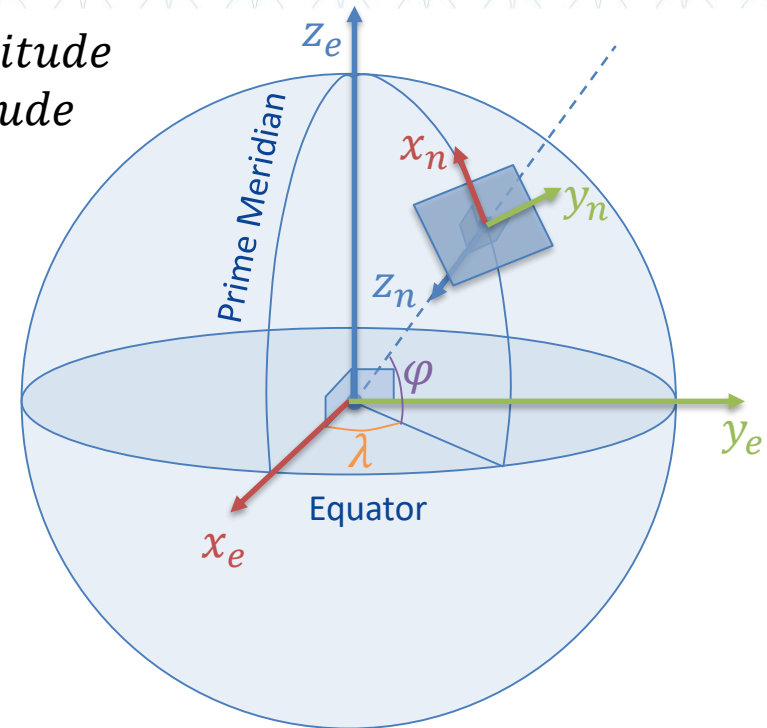
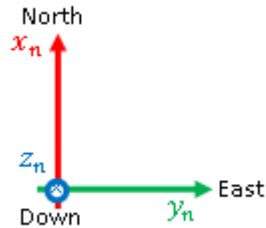
ECEF Frame



Symbol	$\{e\} = (x_e, y_e, z_e)$
Definition	The Earth-centered Earth-fixed frame which rotate around North-South axis with angular speed $w_e = 7.2921 \times 10^{-5} \text{ rad/s}$
Type	Right-handed
Axes	x_e (from origin through intersection of Prime Meridian and Equator) y_e z_e (from origin through North pole)
Origin	Location of ECEF origin o_e is fixed to the Centre of the Earth.
Assumption	For marine craft moving at relatively low speed the Earth rotation can be neglected and $\{e\}$ can be considered to be inertial, such that Newton's laws apply.
Application	Typically used for global guidance, navigation and control (for example, to describe motion and location of ships in transit between continents).

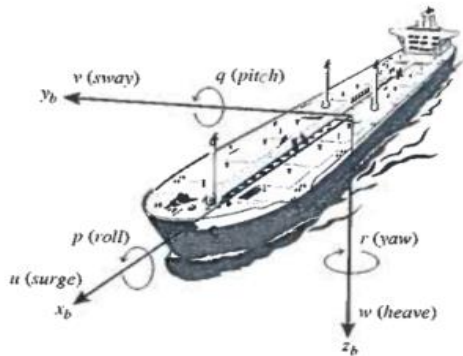
NED Frame

λ – Longitude
 φ – Latitude



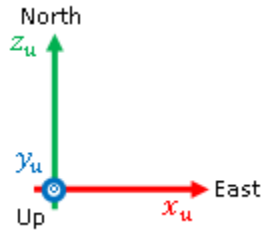
Symbol	$\{n\} = (x_n, y_n, z_n)$
Definition	Tangent plane on the surface of Earth reference ellipsoid WGS 1984.
Type	Right-handed
Axes	x_n = North y_n = East z_n = Downwards, normal to the surface.
Origin	Location of NED origin o_n relative to ECEF frame $\{e\} = (x_e, y_e, z_e)$ is determined using Lat and Lon.
Assumption	$\{n\}$ is inertial, such that Newton's laws apply.
Application	The position and orientation of the craft are described relative to $\{n\}$.

BODY Frame



Symbol	$\{b\} = (x_b, y_b, z_b)$
Definition	Moving frame fixed to the craft.
Type	Right-handed
Axes	x_b = longitudinal axis (directed toward front); y_n = transversal axis (directed toward starboard); z_n = normal axis (directed toward bottom)
Origin	Location of BODY origin o_b is usually chosen to coincide with a point midships in the water line for marine crafts.
Application	The linear and angular velocities of the vessel are described relative to $\{b\}$.

UNITY Frame



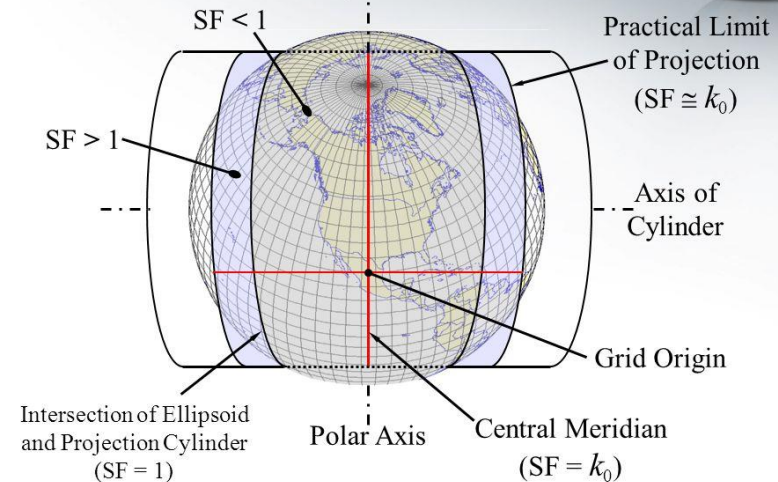
Symbol	$\{u\} = (x_u, y_u, z_u)$
Definition	Frame used for 3D visualisation in Unity 3D.
Type	Left-handed
Axes	x_u = East y_u = Up z_u = North.
Origin	Location of UNITY origin o_u relative to ECEF frame $\{e\} = (x_e, y_e, z_e)$ is determined using Lat and Lon.
Application	The position and orientation of all vessels are sent to Unity 3D for visualisation.

UTM



Projected Coordinate Systems

- Transverse Mercator Projection



Symbol	$\{UTM\} = (x_{UTM}, y_{UTM}, z_{UTM})$
Definition	The UTM system divides the Earth into 60 zones and uses a secant transverse Mercator projection in each zone (conformal projection) to give location on the surface of the Earth. Each zone is segmented into 20 latitude bands.
Type	Right-handed
Axes	x_{UTM} = Northing y_{UTM} = Easting z_{UTM} = Downwards, normal to the surface.
Origin	Location of UTM origin o_{UTM} is shifted such that Northing and Easting coordinates are always positive. For this purpose artificial offset False Easting is added in Northern hemisphere, while both False Easting and False Northing are used in Southern hemisphere. In vertical plane the UTM origin is at sea level.

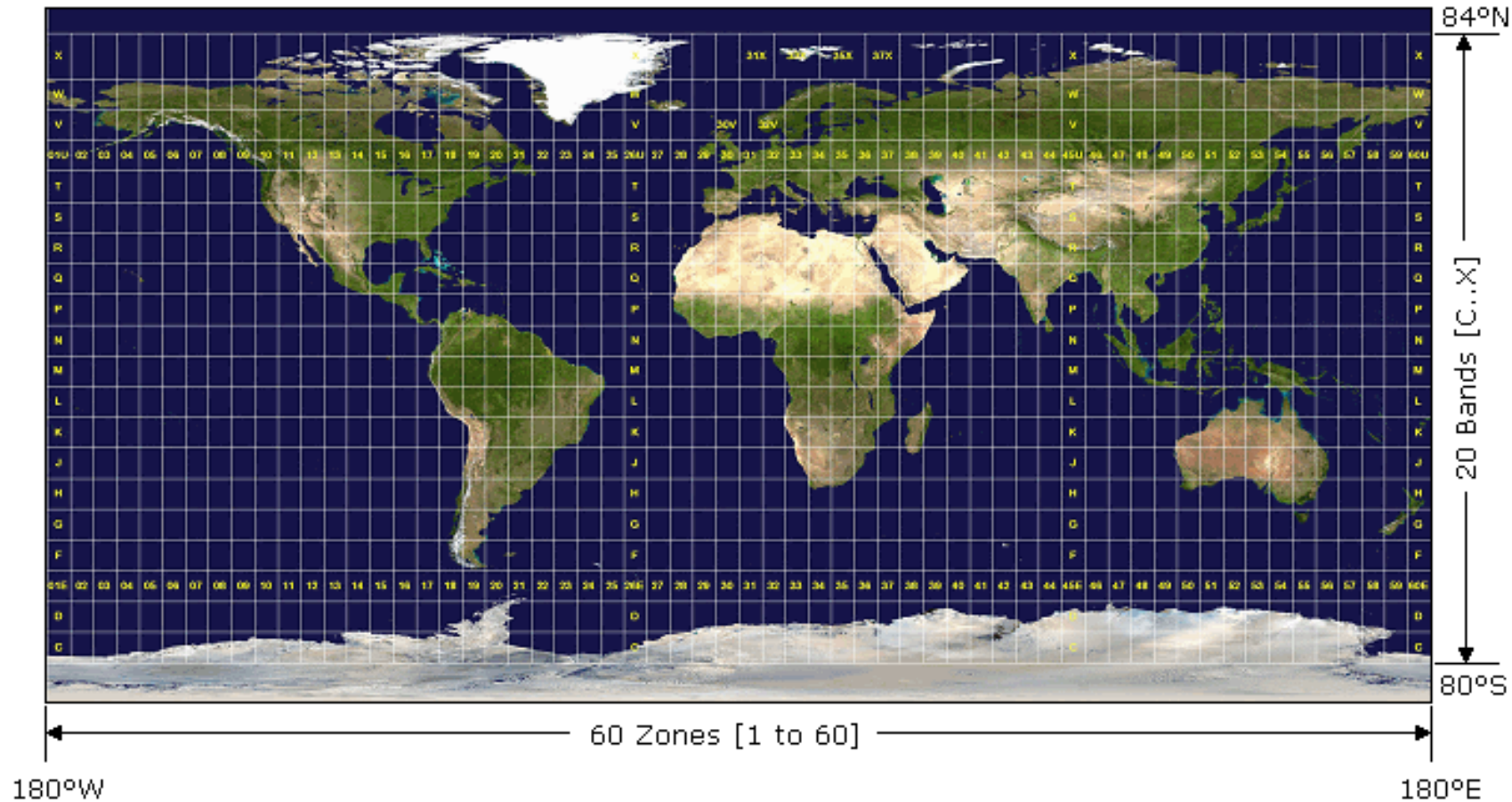
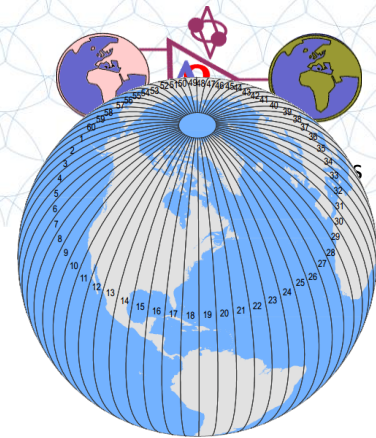
Kinematics

Reference Frames

UTM (cont.)



ck



Notation

$$\mathbf{v}_{to} = \mathbf{R}_{from}^{to} \mathbf{v}_{from}$$

ECEF position $\mathbf{p}_{b/e}^e = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \in \mathbb{R}^3$

Longitude and latitude $\Theta_{en} = \begin{bmatrix} l \\ \mu \end{bmatrix} \in \mathcal{S}^2$

NED position $\mathbf{p}_{b/n}^n = \begin{bmatrix} N \\ E \\ D \end{bmatrix} \in \mathbb{R}^3$

Attitude (Euler angles) $\Theta_{nb} = \begin{bmatrix} \phi \\ \theta \\ \psi \end{bmatrix} \in \mathcal{S}^3$

Body-fixed linear velocity $\mathbf{v}_{b/n}^b = \begin{bmatrix} u \\ v \\ w \end{bmatrix} \in \mathbb{R}^3$

Body-fixed angular velocity $\omega_{b/n}^b = \begin{bmatrix} p \\ q \\ r \end{bmatrix} \in \mathbb{R}^3$

Body-fixed force $\mathbf{f}_b^b = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix} \in \mathbb{R}^3$

Body-fixed moment $\mathbf{m}_b^b = \begin{bmatrix} K \\ M \\ N \end{bmatrix} \in \mathbb{R}^3$

$\mathbf{p}_{b/UTM}^{UTM} = \begin{bmatrix} x_{UTM} \\ y_{UTM} \\ z_{UTM} \end{bmatrix}$	Position of vessel $\{o_b\}$ in UTM	$\mathbf{p}_{b/n}^n = \begin{bmatrix} x_n \\ y_n \\ z_n \end{bmatrix}$	Position of vessel $\{o_b\}$ in NED
$\mathbf{v}_{b/n}^b = \begin{bmatrix} u \\ v \\ w \end{bmatrix}$	Linear velocity of $\{o_b\}$ with respect to $\{n\}$ expressed in $\{b\}$	$\mathbf{v}_{b/n}^n$	Linear velocity of $\{o_b\}$ with respect to $\{n\}$ expressed in $\{n\}$
$\theta_{nb} = \begin{bmatrix} R \\ P \\ Y \end{bmatrix}$	Attitude (Euler angles) between $\{n\}$ and $\{b\}$	$\mathbf{w}_{b/n}^b = \begin{bmatrix} p \\ q \\ r \end{bmatrix}$	Angular velocity of $\{b\}$ with respect to $\{n\}$ expressed in $\{b\}$
$\mathbf{p}_{n/UTM}^{UTM}$	Position of NED origin $\{o_n\}$ in UTM	$\dot{\theta}_{nb} = \begin{bmatrix} \dot{R} \\ \dot{P} \\ \dot{Y} \end{bmatrix}$	Euler rate vector
$\mathbf{R}_b^n(\theta_{nb})$	Transformation matrix of linear velocity vector $\mathbf{v}_{b/n}^b$ from $\{b\}$ to $\mathbf{v}_{b/n}^n$ in $\{n\}$	$\mathbf{T}_\theta(\theta_{nb})$	Transformation matrix of angular velocity vector $\mathbf{w}_{b/n}^b$ from $\{b\}$ to Euler rate vector $\dot{\theta}_{nb}$ in $\{n\}$

$$\lambda \times a := S(\lambda)a$$

$$S(\lambda) = -S^T(\lambda) = \begin{bmatrix} 0 & -\lambda_3 & \lambda_2 \\ \lambda_3 & 0 & -\lambda_1 \\ -\lambda_2 & \lambda_1 & 0 \end{bmatrix}, \quad \lambda = \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix}$$

Euler's Rotation Theorem:

Geometry perspective

Any displacement of a rigid-body in 3D, such that a point on the rigid body remains fixed, is equivalent to a single rotation about some axis that passes through the fixed point.

Linear Algebra perspective

Any two Cartesian coordinate systems in 3D with a common origin are related by a rotation about some fixed axis passing through the origin.

Theorem 2.1 (Euler's Theorem on Rotation)

Every change in the relative orientation of two rigid bodies or reference frames $\{A\}$ and $\{B\}$ can be produced by means of a simple rotation of $\{B\}$ in $\{A\}$.

$$\mathbf{v}_{b/n}^a = \mathbf{R}_b^a \mathbf{v}_{b/n}^b, \quad \mathbf{R}_b^a := \mathbf{R}_{\lambda, \beta}$$

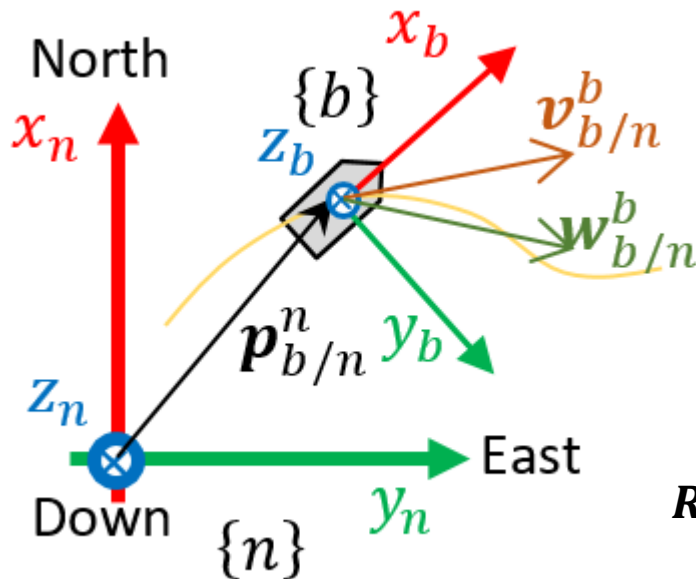
$$\mathbf{R}_{\lambda, \beta} = \mathbf{I}_{3 \times 3} + \sin(\beta) \mathbf{S}(\lambda) + [1 - \cos(\beta)] \mathbf{S}^2(\lambda)$$

$$\mathbf{S}^2(\lambda) = \lambda \lambda^T - \mathbf{I}_{3 \times 3}$$

Linear Velocity Transformation

$$\dot{\mathbf{p}}_{b/n}^n = \mathbf{v}_{b/n}^n = \mathbf{R}_b^n(\boldsymbol{\theta}_{nb}) \mathbf{v}_{b/n}^b = \mathbf{R}_{z,Y} \mathbf{R}_{y,P} \mathbf{R}_{x,R} \mathbf{v}_{b/n}^b$$

$$\mathbf{R}_{x,R} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & cR & -sR \\ 0 & sR & cR \end{bmatrix}, \mathbf{R}_{y,P} = \begin{bmatrix} cP & 0 & sP \\ 0 & 1 & 0 \\ -sP & 0 & cP \end{bmatrix}, \mathbf{R}_{z,Y} = \begin{bmatrix} cY & -sY & 0 \\ sY & cY & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



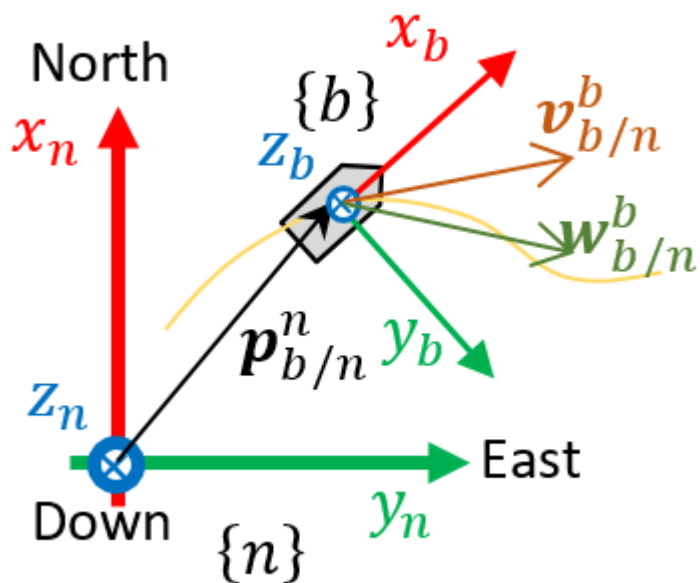
$$\mathbf{R}_b^n(\boldsymbol{\theta}_{nb})^{-1} = \mathbf{R}_b^n(\boldsymbol{\theta}_{nb})^T$$

$$\mathbf{R}_b^n(\boldsymbol{\theta}_{nb}) = \begin{bmatrix} cYcP & -sYcR + cYsPsR & sYsR + cYcRsP \\ sYcP & cYcR + sYsPsR & -cYsR + sPsYcR \\ -sP & cPsR & cPcR \end{bmatrix}$$

Angular Velocity Transformation

$$\dot{\theta}_{nb} = \mathbf{T}_{\theta}(\theta_{nb}) \mathbf{w}_{b/n}^b = \begin{bmatrix} 1 & sRtP & cRtP \\ 0 & cR & -sR \\ 0 & sR/cP & cR/cP \end{bmatrix} \mathbf{w}_{b/n}^b$$

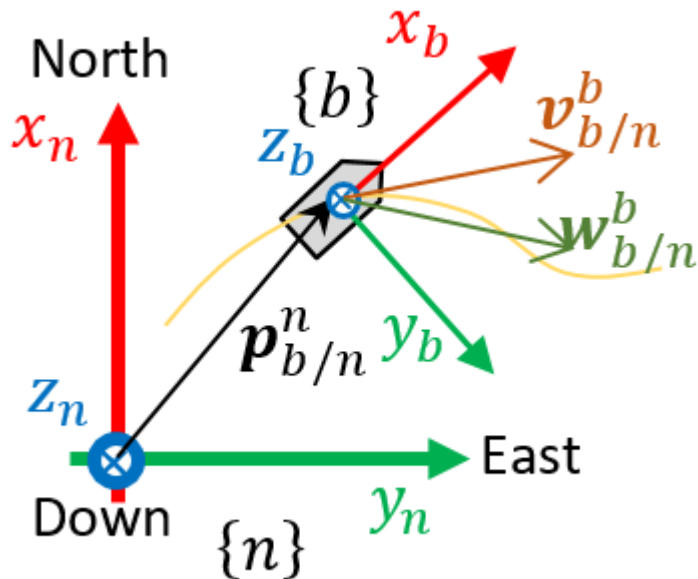
Singularity for $P = \pm 90^\circ$



6 DOF Kinematic Equations

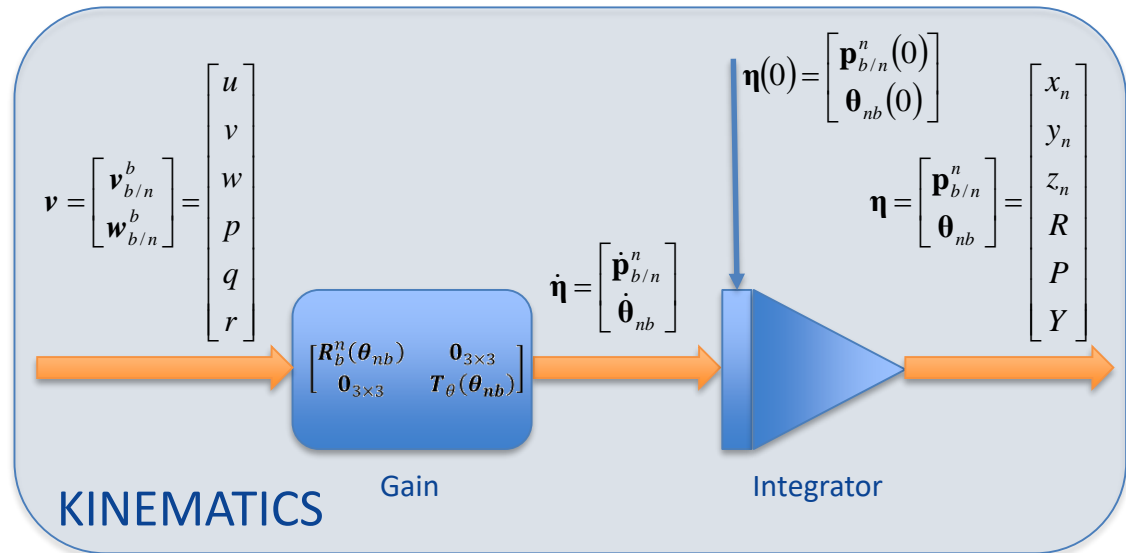
$$\begin{bmatrix} \dot{\mathbf{p}}_{b/n}^n \\ \dot{\boldsymbol{\theta}}_{nb} \end{bmatrix} = \begin{bmatrix} \mathbf{R}_b^n(\boldsymbol{\theta}_{nb}) & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{T}_{\theta}(\boldsymbol{\theta}_{nb}) \end{bmatrix} \begin{bmatrix} \mathbf{v}_{b/n}^b \\ \mathbf{w}_{b/n}^b \end{bmatrix}$$

$$\dot{\boldsymbol{\eta}} = \mathbf{J}_{\boldsymbol{\theta}}(\boldsymbol{\eta}) \mathbf{v}$$



Simulation Model

Attitude representation: **Euler Angles**



$$H \equiv \mathbb{R}^4$$

Basis: $\mathbf{1}, \mathbf{i}, \mathbf{j}, \mathbf{k}$

$$i^2 = j^2 = k^2 = ijk = -1$$

$$\begin{aligned} ij &= k, & ji &= -k, \\ jk &= i, & kj &= -i, \\ ki &= j, & ik &= -j, \end{aligned}$$

$$q = \underbrace{a\mathbf{1}}_{\text{Scalar part}} + \underbrace{b\mathbf{i} + c\mathbf{j} + d\mathbf{k}}_{\text{Vector part}}$$

“Real” quaternions: $a\mathbf{1} + 0\mathbf{i} + 0\mathbf{j} + 0\mathbf{k}$

“Pure” quaternions: $0\mathbf{1} + b\mathbf{i} + c\mathbf{j} + d\mathbf{k}$

**Noncommutativity
of quaternion
multiplication**

x	1	i	j	k
1	1	i	j	k
i	i	-1	k	-j
j	j	-k	-1	i
k	k	j	-i	-1

Addition:

$$\begin{aligned} &(a_1\mathbf{1} + b_1\mathbf{i} + c_1\mathbf{j} + d_1\mathbf{k}) + (a_2\mathbf{1} + b_2\mathbf{i} + c_2\mathbf{j} + d_2\mathbf{k}) \\ &= (a_1 + a_2)\mathbf{1} + (b_1 + b_2)\mathbf{i} + (c_1 + c_2)\mathbf{j} + (d_1 + d_2)\mathbf{k} \end{aligned}$$

Scalar

Multiplication:

$$\alpha(a\mathbf{1} + b\mathbf{i} + c\mathbf{j} + d\mathbf{k}) = \alpha a\mathbf{1} + \alpha b\mathbf{i} + \alpha c\mathbf{j} + \alpha d\mathbf{k}$$

Quaternion

Multiplication:

$$\begin{aligned} &(a_1\mathbf{1} + b_1\mathbf{i} + c_1\mathbf{j} + d_1\mathbf{k})(a_2\mathbf{1} + b_2\mathbf{i} + c_2\mathbf{j} + d_2\mathbf{k}) \\ &= (a_1a_2 - b_1b_2 - c_1c_2 - d_1d_2)\mathbf{1} \\ &\quad + (a_1b_2 + b_1a_2 + c_1d_2 - d_1c_2)\mathbf{i} \\ &\quad + (a_1c_2 - b_1d_2 + c_1a_2 + d_1b_2)\mathbf{j} \\ &\quad + (a_1d_2 + b_1c_2 - c_1b_2 + d_1a_2)\mathbf{k} \end{aligned}$$

$$q = (\overbrace{r}^{\text{Scalar part}}, \underbrace{\vec{v}}_{\text{Vector part}})$$

Addition: $(r_1, \vec{v}_1) + (r_2, \vec{v}_2) = (r_1 + r_2, \vec{v}_1 + \vec{v}_2)$

Scalar
Multiplication: $\alpha(r, \vec{v}) = (\alpha r, \alpha \vec{v})$

Quaternion
Multiplication: $(r_1, \vec{v}_1)(r_2, \vec{v}_2) = (r_1 r_2 - \vec{v}_1 \cdot \vec{v}_2, r_1 \vec{v}_2 + r_2 \vec{v}_1 + \vec{v}_1 \times \vec{v}_2)$

$$q = (\overbrace{r}^{\text{Scalar part}}, \underbrace{\vec{v}}_{\text{Vector part}}) = r\mathbf{1} + v_x\mathbf{i} + v_y\mathbf{j} + v_z\mathbf{k}$$

Conjugate: $q^* = (r, -\vec{v}) = r\mathbf{1} - v_x\mathbf{i} - v_y\mathbf{j} - v_z\mathbf{k}$

$$qq^* = (r, \vec{v})(r, -\vec{v}) = (r^2 + |\vec{v}|^2, \vec{0}) = (r^2 + v_x^2 + v_y^2 + v_z^2)\mathbf{1} + 0\mathbf{i} + 0\mathbf{j} + 0\mathbf{k}$$

$$q^*q = (r, -\vec{v})(r, \vec{v}) = (r^2 + |\vec{v}|^2, \vec{0}) = qq^*$$

$$(q_1q_2)^* = q_2^*q_1^*$$

Norm: $\|q\| = \sqrt{qq^*} = \sqrt{(r^2 + |\vec{v}|^2)} = \sqrt{(r^2 + v_x^2 + v_y^2 + v_z^2)}$

$$\|pq\|^2 = (pq)(pq)^* = pqq^*p^* = p\|q\|^2p^* = pp^*\|q\|^2 = \|p\|^2\|q\|^2$$

Inverse: $q^{-1} = \frac{q^*}{\|q\|^2}$

$$q^{-1}q = qq^{-1} = 1$$

Unit Quaternion: $\|q\| = 1 \Rightarrow r^2 + |\vec{v}|^2 = 1 \Rightarrow \exists \theta \in [0, \pi]: \cos \theta = r, \sin \theta = |\vec{v}|$

$$\|q\| = 1 \Rightarrow q = (r, \vec{v}) = \overbrace{r}^{\cos \theta} + \overbrace{|\vec{v}|}^{\sin \theta} \underbrace{\frac{\vec{v}}{|\vec{v}|}}_{\vec{\hat{v}}} = \cos \theta + \sin \theta \vec{\hat{v}} = e^{(0, \theta \vec{\hat{v}})}$$

Polar
Decomposition:

$$q = \|q\| \overbrace{\left(\frac{q}{\|q\|} \right)}^{\text{Unit Quaternion}} = \|q\| \overbrace{(\cos \theta + \sin \theta \vec{\hat{v}})}^{\text{Unit Quaternion}} = \|q\| \overbrace{e^{(0, \theta \vec{\hat{v}})}}^{\text{Unit Quaternion}}$$

Power:

$$q^p = \|q\|^p e^{(0, (p\theta) \vec{\hat{v}})} = \|q\|^p (\cos(p\theta) + \sin(p\theta) \vec{\hat{v}})$$

Euler Formula
(General Case):

$$e^{(r, \vec{v})} = e^{(r, \vec{0}) + (0, |\vec{v}| \vec{\hat{v}})} = e^{(r, \vec{0})} e^{(0, \theta \vec{\hat{v}})} = e^r e^{(0, \theta \vec{\hat{v}})} = e^r (\cos \theta, \sin \theta \vec{\hat{v}})$$

Euler Formula (“Pure” Quaternion):

$$q = (0, \vec{v})$$

$$q^2 = (0, \vec{v})(0, \vec{v}) = (-|\vec{v}|^2, \vec{0})$$

$$q^3 = (-|\vec{v}|^2, \vec{0})(0, \vec{v}) = (0, -|\vec{v}|^2 \vec{v})$$

$$q^4 = (0, -|\vec{v}|^2 \vec{v})(0, \vec{v}) = (|\vec{v}|^4, \vec{0})$$

$$q^5 = (|\vec{v}|^4, \vec{0})(0, \vec{v}) = (0, |\vec{v}|^4 \vec{v})$$

$$q^6 = (0, |\vec{v}|^4 \vec{v})(0, \vec{v}) = (-|\vec{v}|^6, \vec{0})$$

$$q^7 = (-|\vec{v}|^6, \vec{0})(0, \vec{v}) = (0, -|\vec{v}|^6 \vec{v})$$

⋮

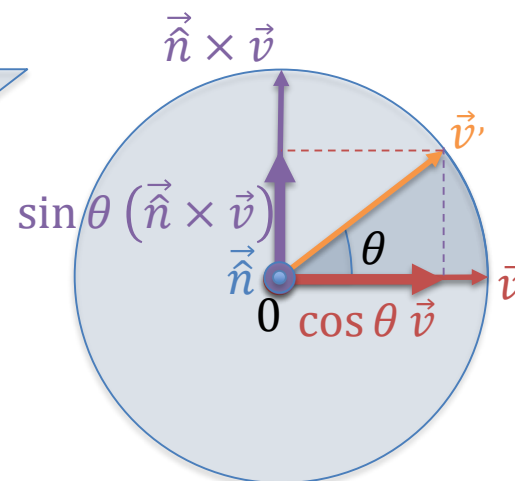
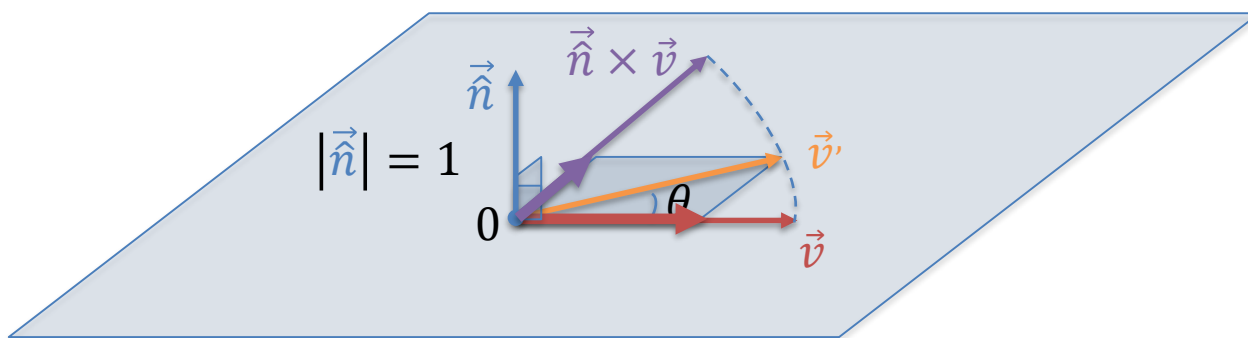
$$e^q = 1 + q + \frac{q^2}{2!} + \frac{q^3}{3!} + \frac{q^4}{4!} + \frac{q^5}{5!} + \frac{q^6}{6!} + \frac{q^7}{7!} \dots$$

$$e^{(0, \vec{v})} = (1, 0) + (0, \vec{v}) + \frac{(-|\vec{v}|^2, 0)}{2!} + \frac{(0, -|\vec{v}|^2 \vec{v})}{3!} + \frac{(|\vec{v}|^4, 0)}{4!} + \frac{(0, |\vec{v}|^4 \vec{v})}{5!} \dots$$

$$e^{(0, \vec{v})} = \left(\left(1 - \frac{|\vec{v}|^2}{2!} + \frac{|\vec{v}|^4}{4!} \dots \right), \left(1 - \frac{|\vec{v}|^2}{3!} + \frac{|\vec{v}|^4}{5!} \dots \right) \frac{\vec{v}}{|\vec{v}|} \right) = (\cos|\vec{v}|, \sin|\vec{v}| \hat{v})$$

Special case: Rotation About Perpendicular Axis

$$\vec{v}' = \cos \theta \vec{v} + \sin \theta (\vec{n} \times \vec{v})$$



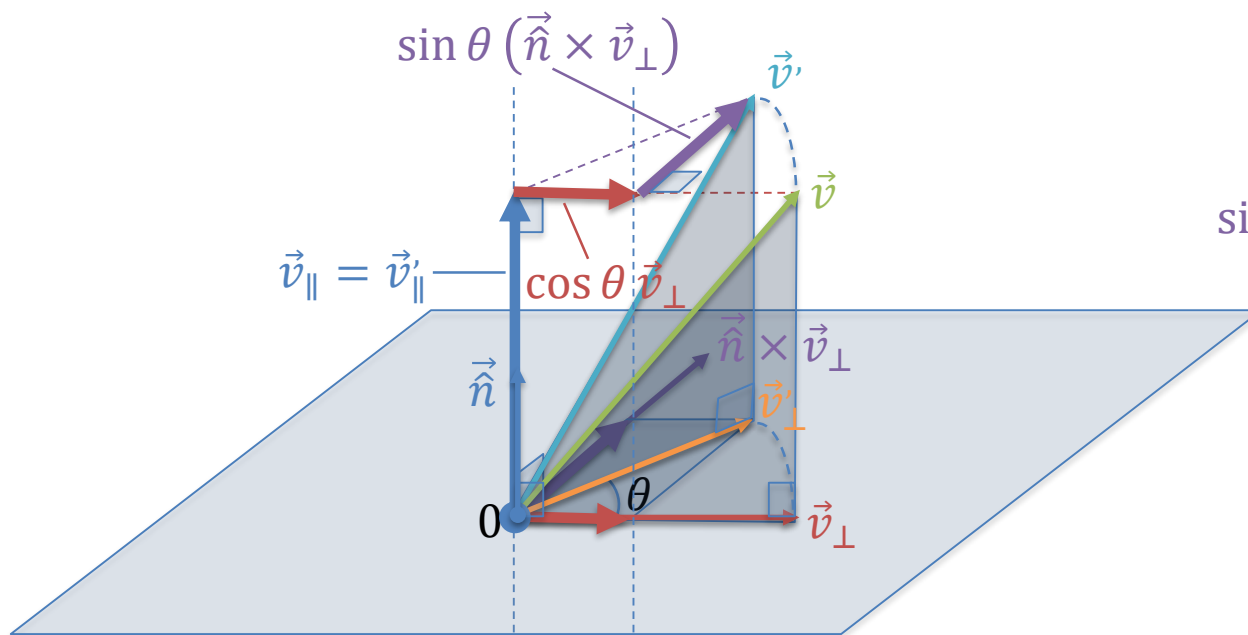
Solution using Quaternions:

$$\left. \begin{aligned} v &= (0, \vec{v}) \\ n &= (0, \vec{n}) \end{aligned} \right\} \begin{aligned} nv &= (0, \vec{n})(0, \vec{v}) = (0, \vec{n} \times \vec{v}) \\ n^2 &= (0, \vec{n})(0, \vec{n}) = (-1, \vec{0}) \end{aligned}$$

$$v' = (0, \vec{v}') = (0, \cos \theta \vec{v} + \sin \theta (\vec{n} \times \vec{v})) = (\cos \theta, \sin \theta \vec{n})(0, \vec{v}) = e^{(0, \theta \vec{n})}(0, \vec{v}) = e^{(0, \theta \vec{n})}v$$

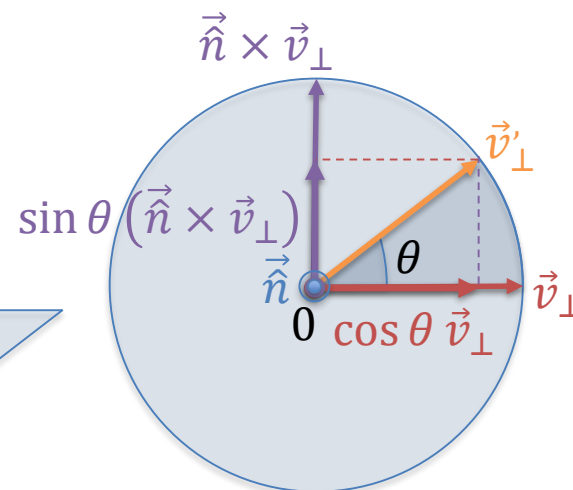
$$v' = e^{(0, \theta \vec{n})}v$$

Rotation About General Axis

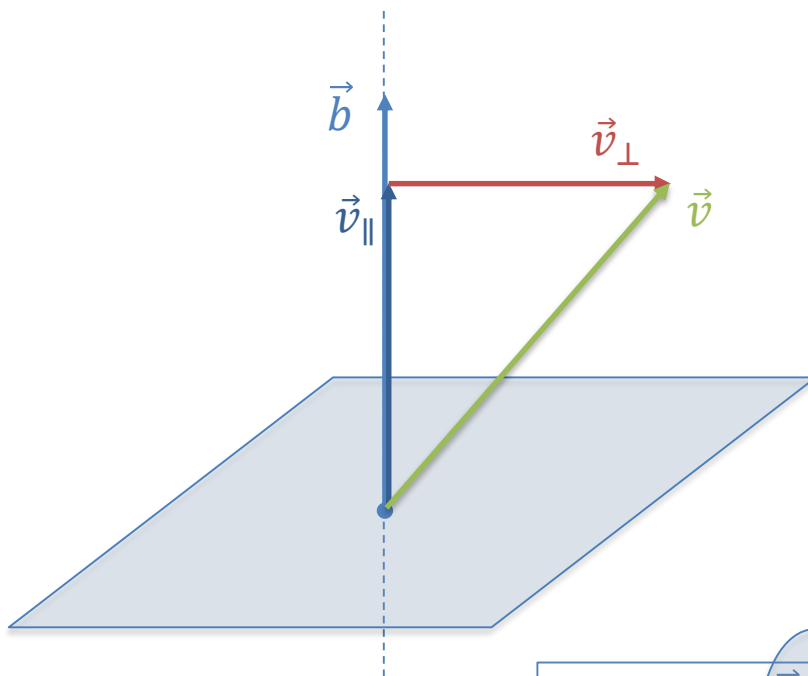


$$\vec{v}' = \vec{v}'_{\parallel} + \vec{v}'_{\perp} = \vec{v}_{\parallel} + \cos \theta \vec{v}_{\perp} + \sin \theta (\vec{n} \times \vec{v}_{\perp})$$

$$\vec{v}'_{\perp} = \cos \theta \vec{v}_{\perp} + \sin \theta (\vec{n} \times \vec{v}_{\perp})$$



Vector Projection onto Line



$$\vec{v}_{\parallel} = \alpha \vec{b}$$

$$\vec{v} = \vec{v}_{\parallel} + \vec{v}_{\perp} \Rightarrow \vec{v}_{\perp} = \vec{v} - \vec{v}_{\parallel} = \vec{v} - \alpha \vec{b}$$

$$\vec{b} \perp \vec{v}_{\perp} \Rightarrow \vec{b} \cdot \vec{v}_{\perp} = 0$$

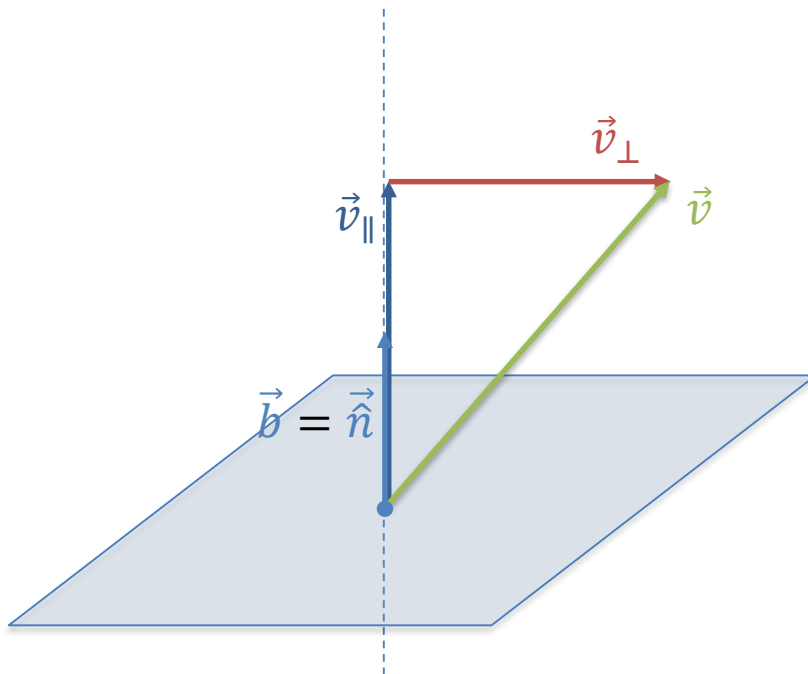
$$\vec{b} \cdot (\vec{v} - \alpha \vec{b}) = 0$$

$$\vec{b} \cdot \vec{v} - \alpha (\vec{b} \cdot \vec{b}) = 0$$

$$\alpha = \frac{\vec{b} \cdot \vec{v}}{\vec{b} \cdot \vec{b}} = \frac{\vec{b}^T \vec{v}}{\vec{b}^T \vec{b}}$$

$$\vec{v}_{\parallel} = \alpha \vec{b} = \underbrace{\frac{\vec{b} \cdot \vec{v}}{\vec{b} \cdot \vec{b}}}_{\text{Scalar}} \vec{b} = \frac{\vec{b}^T \vec{v}}{\vec{b}^T \vec{b}} \vec{b} = \vec{b} \frac{\vec{b}^T \vec{v}}{\vec{b}^T \vec{b}} = \underbrace{\frac{\vec{b} \vec{b}^T}{\vec{b}^T \vec{b}}}_{\text{Projection Matrix}} \vec{v}$$

Special Case: $\vec{b} = \vec{\hat{n}} \quad |\vec{\hat{n}}| = 1$



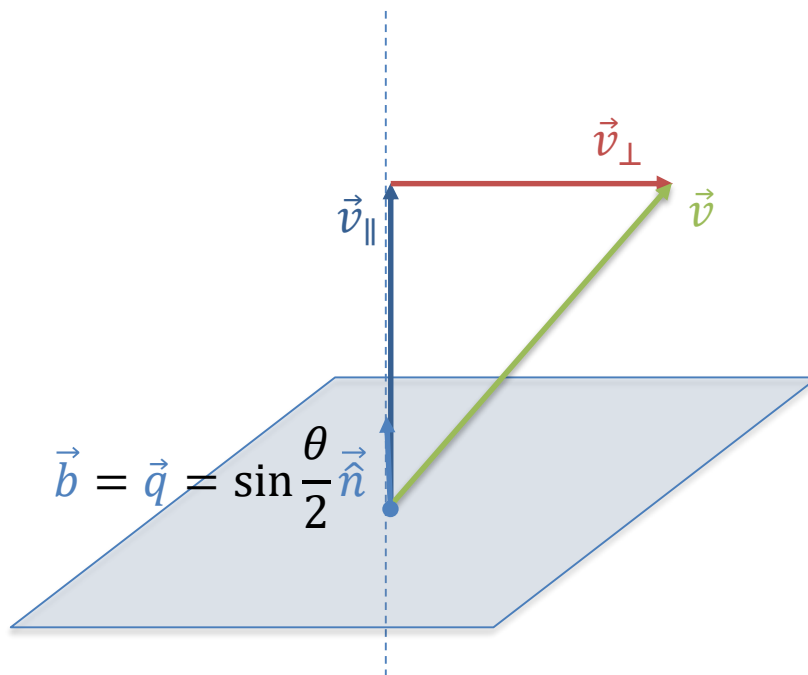
$$\vec{v}_{\parallel} = \frac{\vec{\hat{n}} \cdot \vec{v}}{\vec{\hat{n}} \cdot \vec{\hat{n}}} \vec{\hat{n}} = \frac{\vec{\hat{n}} \cdot \vec{v}}{|\vec{\hat{n}}|^2} \vec{\hat{n}} = (\underbrace{\vec{\hat{n}} \cdot \vec{v}}_{\text{Scalar}}) \vec{\hat{n}}$$

Scalar

$$\vec{v}_{\parallel} = \frac{\vec{\hat{n}} \vec{\hat{n}}^T}{\vec{\hat{n}}^T \vec{\hat{n}}} \vec{v} = \frac{\vec{\hat{n}} \vec{\hat{n}}^T}{|\vec{\hat{n}}|^2} \vec{v} = (\underbrace{\vec{\hat{n}} \vec{\hat{n}}^T}_{\text{Projection Matrix}}) \vec{v}$$

Projection
Matrix

Special Case: $\vec{b} = \vec{q} = \sin \frac{\theta}{2} \vec{n}$ $|\vec{q}| = \sin \frac{\theta}{2}$



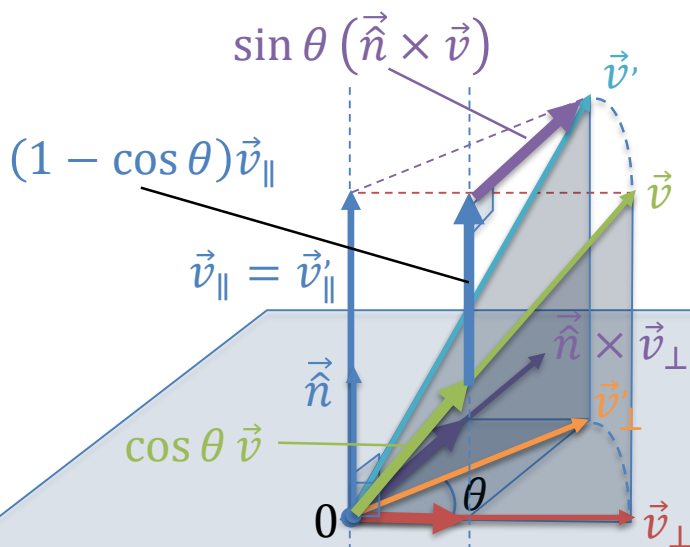
$$\vec{v}_{\parallel} = \frac{\vec{q} \cdot \vec{v}}{\vec{q} \cdot \vec{q}} \vec{q} = \frac{\vec{q} \cdot \vec{v}}{|\vec{q}|^2} \vec{q} = \frac{\vec{q} \cdot \vec{v}}{\sin^2 \frac{\theta}{2}} \vec{q}$$

Scalar

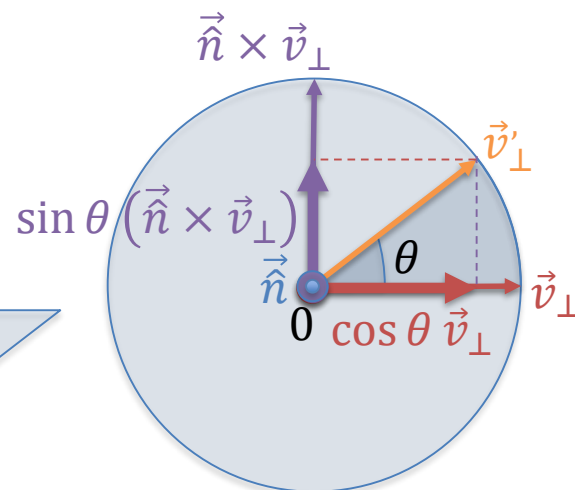
$$\vec{v}_{\parallel} = \frac{\vec{q} \vec{q}^T}{\vec{q}^T \vec{q}} \vec{v} = \frac{\vec{q} \vec{q}^T}{|\vec{q}|^2} \vec{v} = \frac{\vec{q} \vec{q}^T}{\sin^2 \frac{\theta}{2}} \vec{v}$$

Projection
Matrix

Rotation About General Axis



$$\vec{v}'_{\perp} = \cos \theta \vec{v}_{\perp} + \sin \theta (\vec{n} \times \vec{v}_{\perp})$$



$$\begin{aligned} \vec{v}' &= \vec{v}'_{\parallel} + \vec{v}'_{\perp} = \vec{v}_{\parallel} + \cos \theta \vec{v}_{\perp} + \sin \theta (\vec{n} \times \vec{v}_{\perp}) = \vec{v}_{\parallel} + \cos \theta (\vec{v} - \vec{v}_{\parallel}) + \sin \theta (\vec{n} \times (\vec{v} - \vec{v}_{\parallel})) \\ &= (1 - \cos \theta) \vec{v}_{\parallel} + \cos \theta \vec{v} + \sin \theta (\vec{n} \times \vec{v}) - \sin \theta \vec{n} \times \vec{v}_{\parallel} \end{aligned}$$

$$\vec{v}_{\parallel} = (\vec{v} \cdot \vec{n}) \vec{n}$$

Rodrigues Rotation Formula:

$$\vec{v}' = \cos \theta \vec{v} + (1 - \cos \theta) \underbrace{(\vec{v} \cdot \vec{n}) \vec{n}}_{\vec{v}_{\parallel}} + \sin \theta (\vec{n} \times \vec{v})$$

Rotation About General Axis: Solution using Quaternions

$$v = (0, \vec{v})$$

$$n = (0, \vec{n})$$

$$v_{\parallel} = (0, \vec{v}_{\parallel})$$

$$v_{\perp} = (0, \vec{v}_{\perp})$$

$$v' = (0, \vec{v}')$$

$$\vec{v}' = \vec{v}'_{\parallel} + \vec{v}'_{\perp} = \vec{v}_{\parallel} + \vec{v}'_{\perp}$$

$$v' = (0, \vec{v}') = (0, \vec{v}'_{\parallel} + \vec{v}'_{\perp}) = (0, \vec{v}_{\parallel} + \vec{v}'_{\perp})$$

$$v' = v_{\parallel} + v'_{\perp} = v_{\parallel} + e^{(0, \theta \vec{n})} v_{\perp}$$

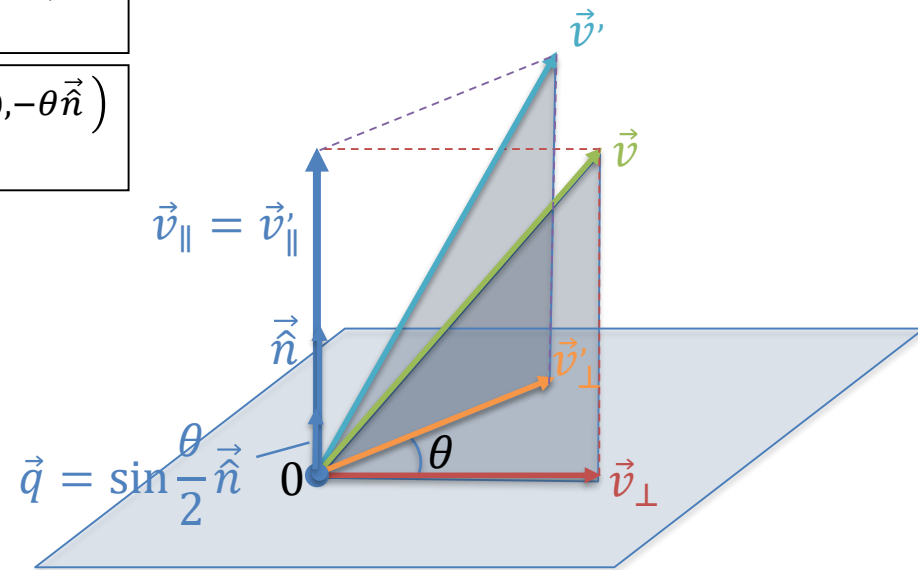
$$v' = e^{(0, \frac{\theta}{2} \vec{n})} e^{(0, -\frac{\theta}{2} \vec{n})} v_{\parallel} + e^{(0, \frac{\theta}{2} \vec{n})} e^{(0, \frac{\theta}{2} \vec{n})} v_{\perp} = e^{(0, \frac{\theta}{2} \vec{n})} v_{\parallel} e^{(0, -\frac{\theta}{2} \vec{n})} + e^{(0, \frac{\theta}{2} \vec{n})} v_{\perp} e^{(0, -\frac{\theta}{2} \vec{n})}$$

Lema 1

Lema 2

$$v' = e^{(0, \frac{\theta}{2} \vec{n})} (v_{\parallel} + v_{\perp}) e^{(0, -\frac{\theta}{2} \vec{n})} = e^{(0, \frac{\theta}{2} \vec{n})} v e^{(0, -\frac{\theta}{2} \vec{n})}$$

$$\vec{v}_{\parallel} = \frac{\vec{q} \cdot \vec{v}}{\vec{q} \cdot \vec{q}} \vec{q}$$



Rodrigues Rotation Formula: $\vec{v}' = \cos \theta \vec{v} + (1 - \cos \theta)(\vec{v} \cdot \vec{n})\vec{n} + \sin \theta (\vec{n} \times \vec{v})$

$$\begin{aligned}\vec{v}' &= (1 - \cos \theta) \left((\vec{v} \cdot \vec{n})\vec{n} - \vec{v} + \vec{v} \right) + \cos \theta \vec{v} + \sin \theta (\vec{n} \times \vec{v}) \\ &= (1 - \cos \theta) \left((\vec{v} \cdot \vec{n})\vec{n} - \vec{v} \right) + (1 - \cos \theta + \cos \theta)\vec{v} + \sin \theta (\vec{n} \times \vec{v})\end{aligned}$$

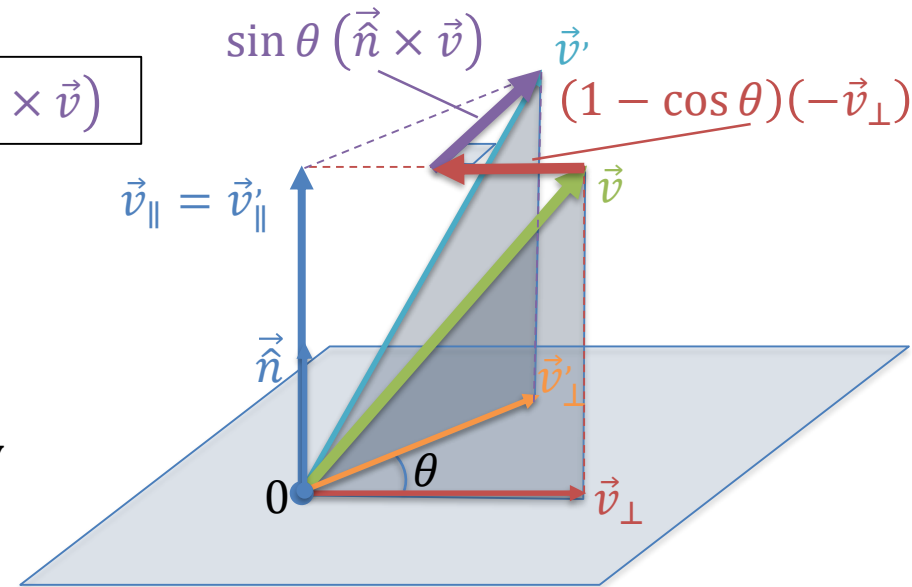
$$\vec{v}' = \vec{v} + (1 - \cos \theta) \left(\underbrace{(\vec{v} \cdot \vec{n})\vec{n} - \vec{v}}_{-\vec{v}_\perp} \right) + \sin \theta (\vec{n} \times \vec{v})$$

$$\vec{n} \times \vec{v} := \mathbf{S}(\mathbf{n})\mathbf{v}$$

$$\vec{n} \times (\vec{n} \times \vec{v}) = (\vec{v} \cdot \vec{n})\vec{n} - \vec{v} = -\vec{v}_\perp$$

$$\begin{aligned}\mathbf{S}(\mathbf{n})(\mathbf{S}(\mathbf{n})\mathbf{v}) &= \mathbf{S}^2(\mathbf{n})\mathbf{v} = (\mathbf{n}\mathbf{n}^T - \mathbf{I}_{3 \times 3})\mathbf{v} \\ &= (\mathbf{n}\mathbf{n}^T)\mathbf{v} - \mathbf{I}_{3 \times 3}\mathbf{v} = \mathbf{v}_\parallel - \mathbf{v} = -\mathbf{v}_\perp\end{aligned}$$

$$\mathbf{v}' = \underbrace{(\mathbf{I}_{3 \times 3} + (1 - \cos \theta)\mathbf{S}^2(\mathbf{n}) + \sin \theta \mathbf{S}(\mathbf{n}))}_{\mathbf{R}_{\mathbf{n}, \theta}} \mathbf{v}$$



Rotation Formula
using Quaternions:

$$v' = e^{(0, \frac{\theta}{2} \vec{n})} (v_{\parallel} + v_{\perp}) e^{(0, -\frac{\theta}{2} \vec{n})} = e^{(0, \frac{\theta}{2} \vec{n})} v e^{(0, -\frac{\theta}{2} \vec{n})} = q v q^*$$

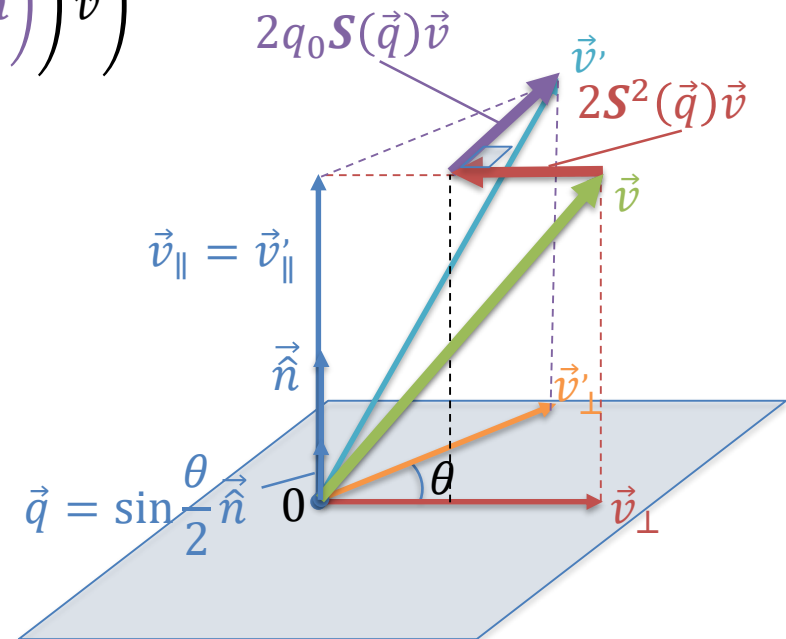
$$q = e^{(0, \frac{\theta}{2} \vec{n})} = \left(\cos \frac{\theta}{2}, \sin \frac{\theta}{2} \vec{n} \right) = (q_0, \vec{q}), \quad q_0^2 + |\vec{q}|^2 = 1$$

$$\begin{aligned} v' &= (0, (\mathbf{I}_{3 \times 3} + (1 - \cos \theta) \mathbf{S}^2(\mathbf{n}) + \sin \theta \mathbf{S}(\mathbf{n})) \vec{v}) = \\ &= \left(0, \left(\mathbf{I}_{3 \times 3} + 2 \sin^2 \frac{\theta}{2} \mathbf{S}^2(\mathbf{n}) + 2 \sin \frac{\theta}{2} \cos \frac{\theta}{2} \mathbf{S}(\mathbf{n}) \right) \vec{v} \right) \end{aligned}$$

$$v' = \left(0, \left(\mathbf{I}_{3 \times 3} + 2 \mathbf{S}^2 \left(\sin \frac{\theta}{2} \mathbf{n} \right) + 2 \cos \frac{\theta}{2} \mathbf{S} \left(\sin \frac{\theta}{2} \mathbf{n} \right) \right) \vec{v} \right)$$

$$v' = (0, \underbrace{(\mathbf{I}_{3 \times 3} + 2 \mathbf{S}^2(\vec{q}) + 2 q_0 \mathbf{S}(\vec{q})) \vec{v}}_{\mathbf{R}_b^n(q) = \mathbf{R}_{(q_0, \vec{q})}})$$

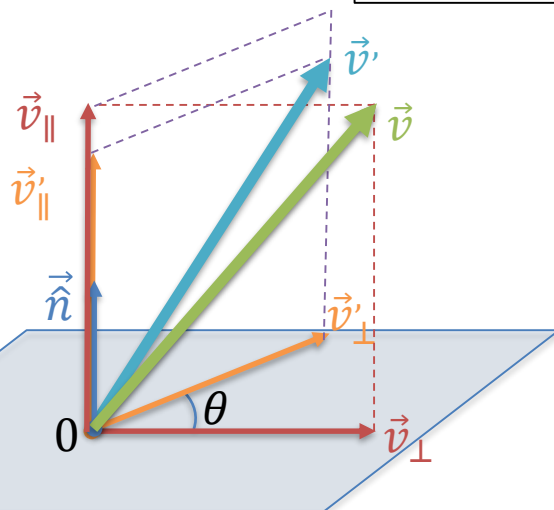
$$\mathbf{S}^2(\vec{q}) = \vec{q} \vec{q}^T - |\vec{q}|^2 \mathbf{I}_{3 \times 3}$$



Wrong Formula:

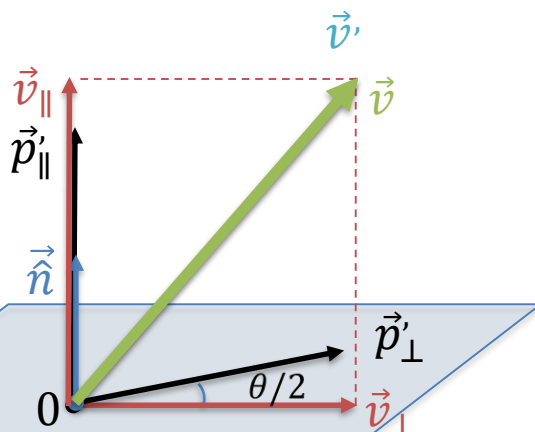
$$v' = e^{(0, \theta \vec{n})} (v_{\parallel} + v_{\perp}) = e^{(0, \theta \vec{n})} v_{\parallel} + e^{(0, \theta \vec{n})} v_{\perp}$$

\vec{v}'_{\parallel} **X** \vec{v}'_{\perp} **✓**

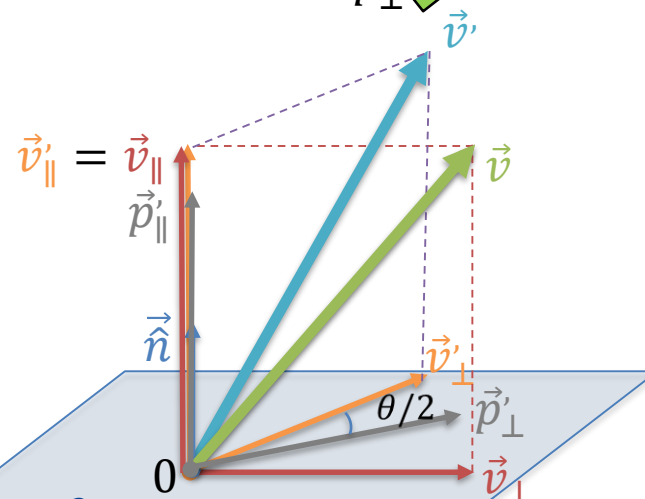


Correct Formula:

$$\begin{aligned} v' &= e^{(0, \frac{\theta}{2} \vec{n})} (v_{\parallel} + v_{\perp}) e^{(0, -\frac{\theta}{2} \vec{n})} = \\ &= \underbrace{\left[e^{(0, \frac{\theta}{2} \vec{n})} v_{\parallel} \right]}_{\vec{p}'_{\parallel} \text{ ✓}} e^{(0, -\frac{\theta}{2} \vec{n})} + \underbrace{\left[e^{(0, \frac{\theta}{2} \vec{n})} v_{\perp} \right]}_{\vec{p}'_{\perp} \text{ ✓}} e^{(0, -\frac{\theta}{2} \vec{n})} \end{aligned}$$



Step 1:



Step 2:

Rotation Formula
using Quaternions:

$$v' = e^{(0, \frac{\theta}{2} \vec{n})} (v_{\parallel} + v_{\perp}) e^{(0, -\frac{\theta}{2} \vec{n})} = e^{(0, \frac{\theta}{2} \vec{n})} v e^{(0, -\frac{\theta}{2} \vec{n})} = q v q^*$$

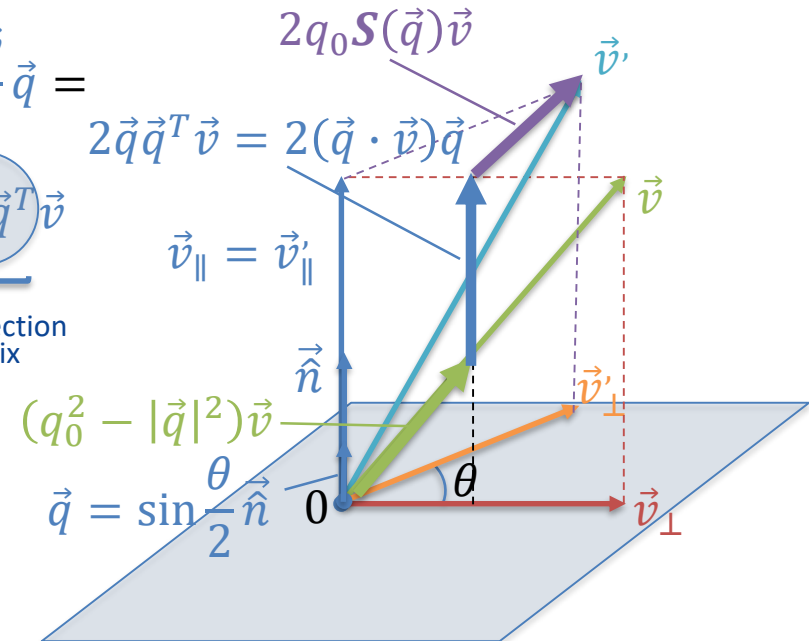
$$q = e^{(0, \frac{\theta}{2} \vec{n})} = \left(\cos \frac{\theta}{2}, \sin \frac{\theta}{2} \vec{n} \right) = (q_0, \vec{q}), \quad q_0^2 + |\vec{q}|^2 = 1$$

Quaternion Rotation Operator:

$$v' = L_q(v) := q v q^* = (q_0, \vec{q})(0, \vec{v})(q_0, -\vec{q}) = \left(0, (q_0^2 - |\vec{q}|^2) \vec{v} + 2(\vec{q} \cdot \vec{v}) \vec{q} + 2q_0(\vec{q} \times \vec{v}) \right)$$

$$(q_0^2 - |\vec{q}|^2) \vec{v} = (q_0^2 + |\vec{q}|^2 - 2|\vec{q}|^2) \vec{v} = \left(1 - 2\sin^2 \frac{\theta}{2} \right) \vec{v} = \cos \theta \vec{v}$$

$$\begin{aligned} (1 - \cos \theta) \vec{v}_{\parallel} &= \left(2\sin^2 \frac{\theta}{2} \right) \frac{\vec{q} \cdot \vec{v}}{\vec{q} \cdot \vec{q}} \vec{q} = \left(2\sin^2 \frac{\theta}{2} \right) \frac{\vec{q} \cdot \vec{v}}{|\vec{q}|^2} \vec{q} = \\ &= \left(2\sin^2 \frac{\theta}{2} \right) \frac{\vec{q} \cdot \vec{v}}{\sin^2 \frac{\theta}{2}} \vec{q} = \underbrace{2(\vec{q} \cdot \vec{v})}_{\text{Scalar}} \vec{q} = 2\vec{q}(\vec{q}^T \vec{v}) = \underbrace{2\vec{q}\vec{q}^T}_{\text{Projection Matrix}} \vec{v} \end{aligned}$$



$$v' = \left(0, \left((q_0^2 - |\vec{q}|^2) \mathbf{I}_{3 \times 3} + 2\vec{q}\vec{q}^T + 2q_0 \mathbf{S}(\vec{q}) \right) \vec{v} \right)$$

Linear Velocity Transformation

$$\dot{\mathbf{p}}_{b/n}^n = \mathbf{v}_{b/n}^n = \mathbf{R}_b^n(\mathbf{q}) \mathbf{v}_{b/n}^b$$

$$\mathbf{R}_b^n(\mathbf{q}) = \mathbf{R}_{(q_0, \vec{q})} = \mathbf{I}_{3 \times 3} + 2\mathbf{S}^2(\vec{q}) + 2q_0\mathbf{S}(\vec{q})$$

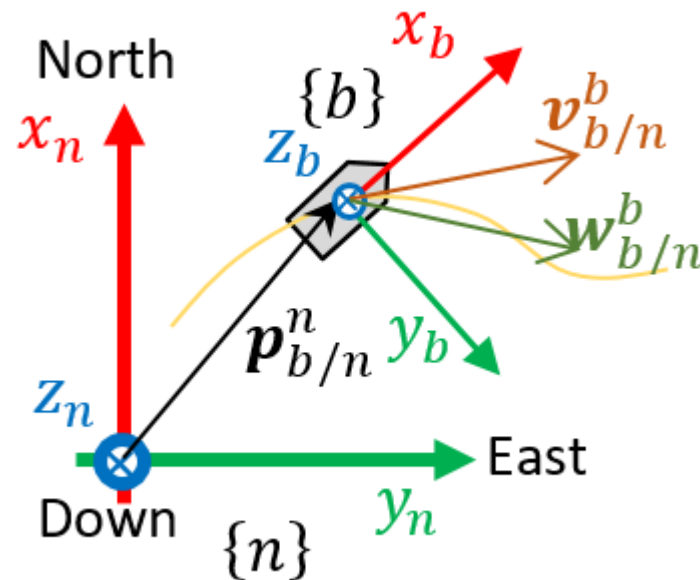
$$\mathbf{q} = (q_0, \vec{q}) = q_0\mathbf{1} + q_1\mathbf{i} + q_2\mathbf{j} + q_3\mathbf{k}$$

$$q_0 = \cos \frac{\theta}{2}$$

$$\vec{q} = \sin \frac{\theta}{2} \vec{\hat{n}}$$

$$\mathbf{R}_b^n(\mathbf{q})^{-1} = \mathbf{R}_b^n(\mathbf{q})^T$$

$$\mathbf{R}_b^n(\mathbf{q}) = \begin{bmatrix} 1 - 2(q_2^2 + q_3^2) & 2(q_1q_2 - q_3q_0) & 2(q_1q_3 + q_2q_0) \\ 2(q_1q_2 + q_3q_0) & 1 - 2(q_3^2 + q_1^2) & 2(q_2q_3 - q_1q_0) \\ 2(q_1q_3 - q_2q_0) & 2(q_2q_3 + q_1q_0) & 1 - 2(q_1^2 + q_2^2) \end{bmatrix}$$



Angular Velocity Transformation

$$\dot{\mathbf{R}}_b^n(\mathbf{q}) = \mathbf{R}_b^n(\mathbf{q})\mathbf{S}(\mathbf{w}_{b/n}^b) \Rightarrow \boxed{\dot{\mathbf{q}} = \mathbf{T}_q(\mathbf{q})\mathbf{w}_{b/n}^b}$$

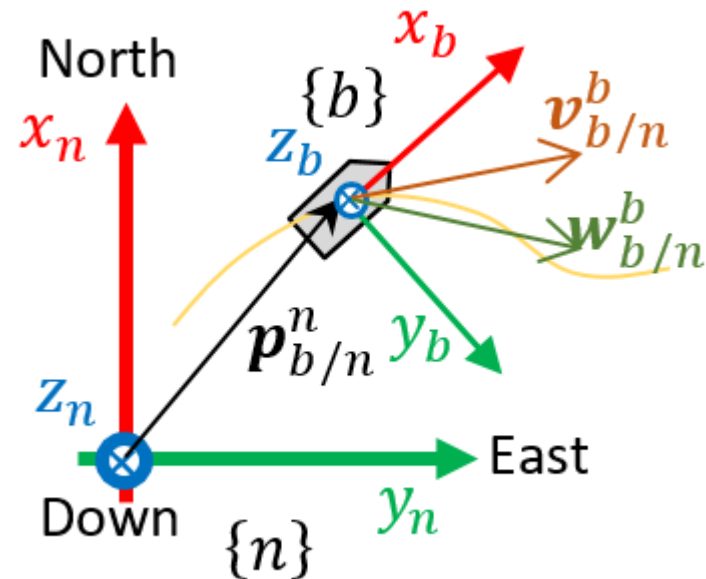
$$\mathbf{q} = (q_0, \vec{q}) = q_0\mathbf{1} + q_1\mathbf{i} + q_2\mathbf{j} + q_3\mathbf{k}$$

$$q_0 = \cos \frac{\theta}{2} \quad \mathbf{T}_q^T(\mathbf{q})\mathbf{T}_q(\mathbf{q}) = \frac{1}{4}\mathbf{I}_{3 \times 3}$$

$$\vec{q} = \sin \frac{\theta}{2} \vec{\hat{n}}$$

$$\mathbf{T}_q(\mathbf{q}) = \frac{1}{2} \begin{bmatrix} -\vec{q}^T \\ q_0\mathbf{I}_{3 \times 3} + \mathbf{S}(\vec{q}) \end{bmatrix}$$

$$\mathbf{T}_q(\mathbf{q}) = \frac{1}{2} \begin{bmatrix} -q_1 & -q_2 & -q_3 \\ q_0 & -q_3 & q_2 \\ q_3 & q_0 & -q_1 \\ -q_2 & q_1 & q_0 \end{bmatrix}$$



Angular Velocity Transformation

Quaternions

$$\mathbf{T}_q(\mathbf{q}) = \frac{1}{2} \begin{bmatrix} -q_1 & -q_2 & -q_3 \\ q_0 & -q_3 & q_2 \\ q_3 & q_0 & -q_1 \\ -q_2 & q_1 & q_0 \end{bmatrix}$$

Euler Angles

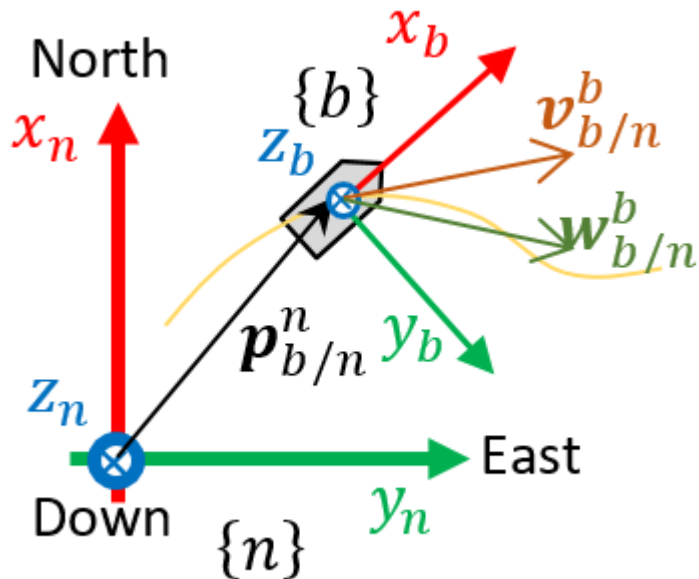
$$\mathbf{T}_\theta(\boldsymbol{\theta}_{nb}) = \begin{bmatrix} 1 & sRtP & cRtP \\ 0 & cR & -sR \\ 0 & sR/cP & cR/cP \end{bmatrix}$$

Singularity for $P = \pm 90^\circ$

6 DOF Kinematic Equations

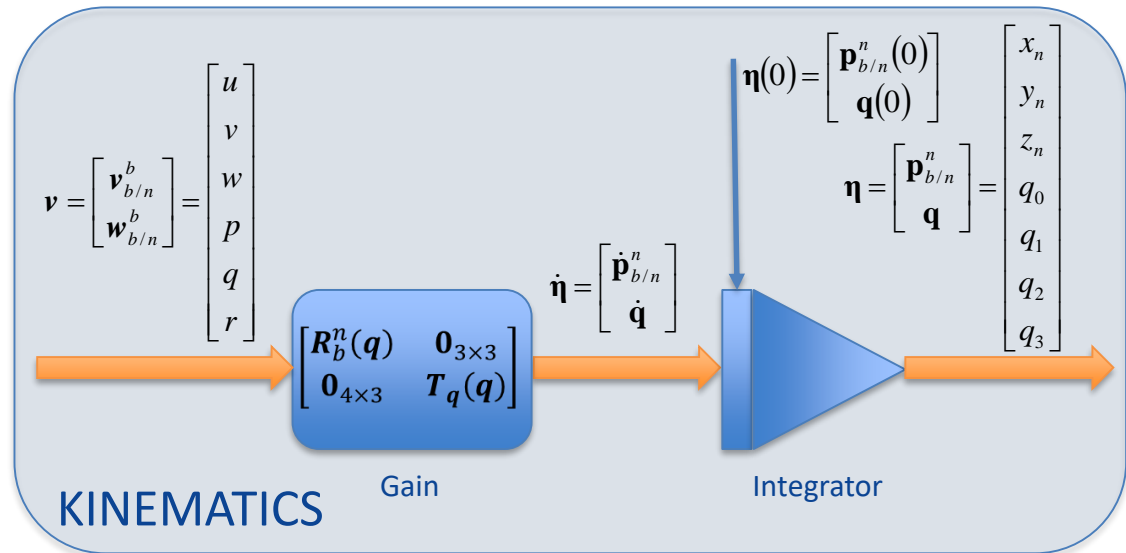
$$\begin{bmatrix} \dot{\mathbf{p}}_{b/n}^n \\ \dot{\mathbf{q}} \end{bmatrix} = \begin{bmatrix} \mathbf{R}_b^n(\mathbf{q}) & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{4 \times 3} & \mathbf{T}_q(\mathbf{q}) \end{bmatrix} \begin{bmatrix} \mathbf{v}_{b/n}^b \\ \mathbf{w}_{b/n}^b \end{bmatrix}$$

$$\dot{\boldsymbol{\eta}} = \mathbf{J}_q(\boldsymbol{\eta}) \mathbf{v}$$



Simulation Model

Attitude representation: **Quaternions**



Euler Angles \rightarrow Quaternions

$$\mathbf{q} = \begin{bmatrix} q_0 \\ q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} c(R/2)c(P/2)c(Y/2) + s(R/2)s(P/2)s(Y/2) \\ s(R/2)c(P/2)c(Y/2) - c(R/2)s(P/2)s(Y/2) \\ c(R/2)s(P/2)c(Y/2) + s(R/2)c(P/2)s(Y/2) \\ c(R/2)c(P/2)s(Y/2) - s(R/2)s(P/2)c(Y/2) \end{bmatrix}$$

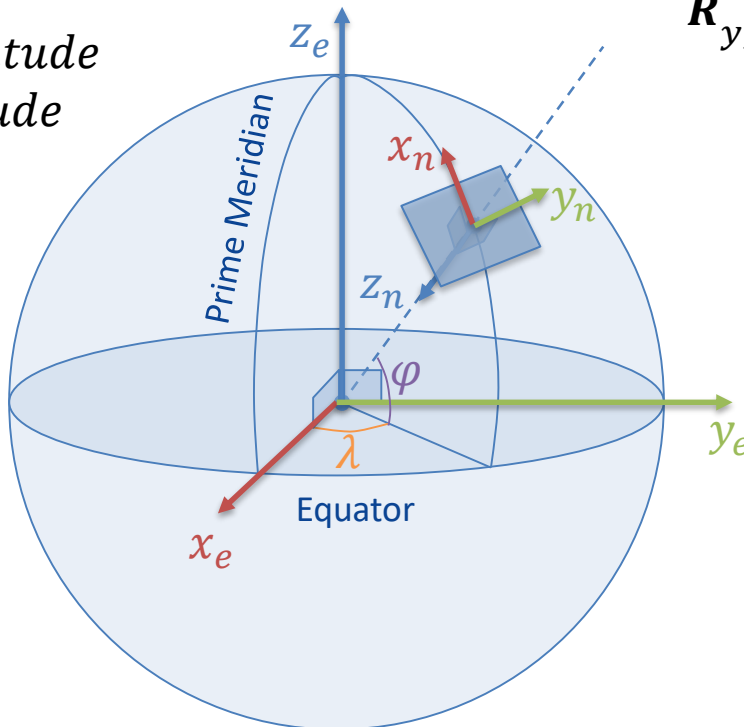
Quaternions \rightarrow Euler Angles

$$\theta_{nb} = \begin{bmatrix} R \\ P \\ Y \end{bmatrix} = \begin{bmatrix} \text{atan2} \left(2(q_2q_3 + q_1q_0), 1 - 2(q_1^2 + q_2^2) \right) \\ \text{asin} \left(2(q_0q_2 - q_3q_1) \right) \\ \text{atan2} \left(2(q_0q_3 + q_1q_2), 1 - 2(q_2^2 + q_3^2) \right) \end{bmatrix}$$

NED \rightarrow ECEF

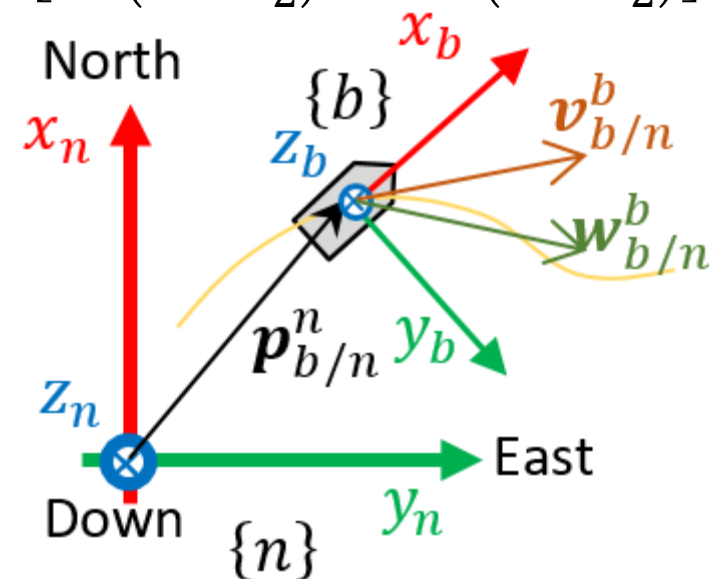
$$\underbrace{\dot{\mathbf{p}}_{b/e}^e}_{\{e\}} = \underbrace{\mathbf{R}_n^e(\boldsymbol{\theta}_{en})}_{\{e\}} \underbrace{\mathbf{R}_b^n(\boldsymbol{\theta}_{nb})}_{\{b\}} \underbrace{\mathbf{v}_{b/n}^b}_{\{b\}} = \underbrace{\mathbf{R}_{z,\lambda} \mathbf{R}_{y,-\varphi-\frac{\pi}{2}}}_{\mathbf{R}_n^e(\boldsymbol{\theta}_{en})} \dot{\mathbf{p}}_{b/n}^n$$

λ – Longitude
 φ – Latitude



$$\mathbf{R}_{z,Y} = \begin{bmatrix} c\lambda & -s\lambda & 0 \\ s\lambda & c\lambda & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{R}_{y,-\varphi-\frac{\pi}{2}} = \begin{bmatrix} c\left(-\varphi-\frac{\pi}{2}\right) & 0 & s\left(-\varphi-\frac{\pi}{2}\right) \\ 0 & 1 & 0 \\ -s\left(-\varphi-\frac{\pi}{2}\right) & 0 & c\left(-\varphi-\frac{\pi}{2}\right) \end{bmatrix}$$



NED \rightarrow ECEF

$$\underbrace{\dot{\mathbf{p}}_{b/e}^e}_{\text{ECEF}} = \mathbf{R}_n^e(\boldsymbol{\theta}_{en}) \underbrace{\dot{\mathbf{p}}_{b/n}^n}_{\text{NED}} = \underbrace{\begin{bmatrix} -c\lambda s\varphi & -s\lambda & -c\lambda c\varphi \\ -s\lambda s\varphi & c\lambda & -s\lambda c\varphi \\ c\varphi & 0 & -s\varphi \end{bmatrix}}_{\mathbf{R}_n^e(\boldsymbol{\theta}_{en})} \underbrace{\begin{bmatrix} \dot{x}_n \\ \dot{y}_n \\ \dot{z}_n \end{bmatrix}}_{\dot{\mathbf{p}}_{b/n}^n}$$

\dot{x}_n — North Velocity
 \dot{y}_n — East Velocity
 \dot{z}_n — Down Velocity

ECEF \rightarrow NED

$$\underbrace{\dot{\mathbf{p}}_{b/n}^n}_{\text{NED}} = \mathbf{R}_e^n(\boldsymbol{\theta}_{en}) \underbrace{\dot{\mathbf{p}}_{b/e}^e}_{\text{ECEF}} = \mathbf{R}_n^{eT}(\boldsymbol{\theta}_{en}) \dot{\mathbf{p}}_{b/e}^e = \underbrace{\begin{bmatrix} -c\lambda s\varphi & -s\lambda s\varphi & c\varphi \\ -s\lambda & c\lambda & 0 \\ -c\lambda c\varphi & -s\lambda c\varphi & -s\varphi \end{bmatrix}}_{\mathbf{R}_e^n(\boldsymbol{\theta}_{en})} \underbrace{\begin{bmatrix} \dot{x}_e \\ \dot{y}_e \\ \dot{z}_e \end{bmatrix}}_{\dot{\mathbf{p}}_{b/e}^e}$$

Speed & Heading

$$\text{Speed} = \sqrt{\dot{x}_n^2 + \dot{y}_n^2}$$

$$\text{Heading} = \tan^{-1} \frac{y_n}{x_n}$$

Geodetic Latitude vs Geocentric Latitude

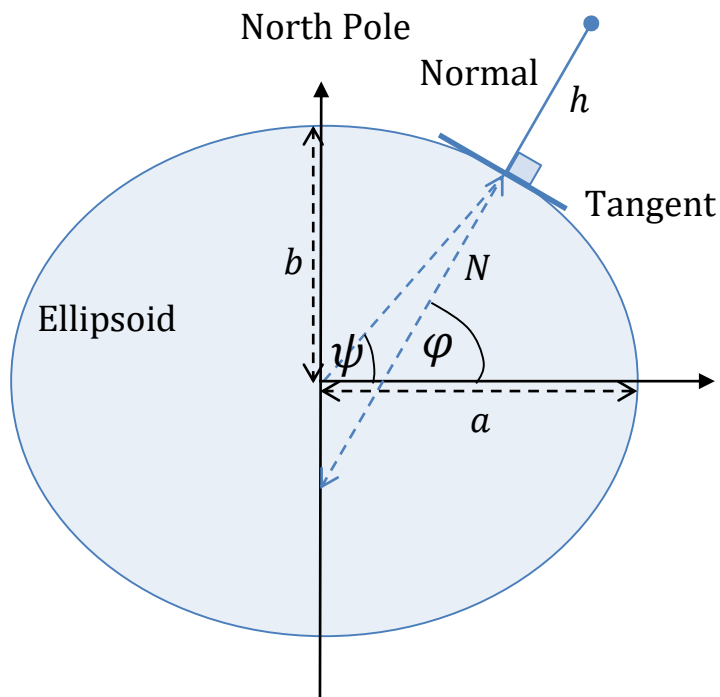
Raw GNSS (GPS, GLONASS and Galileo) output $\mathbf{p}_{b/e}^e$ is given in Cartesian ECEF frame.

It is presented to users in terms of longitude λ , latitude φ and height h relative to WGS-84 ellipsoid.

φ – Geodetic Latitude

ψ – Geocentric Latitude

$$\psi(\varphi) = \tan^{-1}((1 - e^2) \tan \varphi)$$



WGS-84 parameters:

$a = 6378137.0m$ (semi – major axis)

$b = 6356752.3142m$ (semi – minor axis)

$$e = \sqrt{\frac{a^2 - b^2}{a^2}} \text{ (eccentricity)}$$

$$e' = \sqrt{\frac{a^2 - b^2}{b^2}}$$

$f = (a - b)/a$ ("flattening" parameter)

$$e^2 = 2f - f^2$$

1. Mean Sea Level (MSL) Datum (height relative to geoid)
2. GPS height (height above WGS-84 ellipsoid)

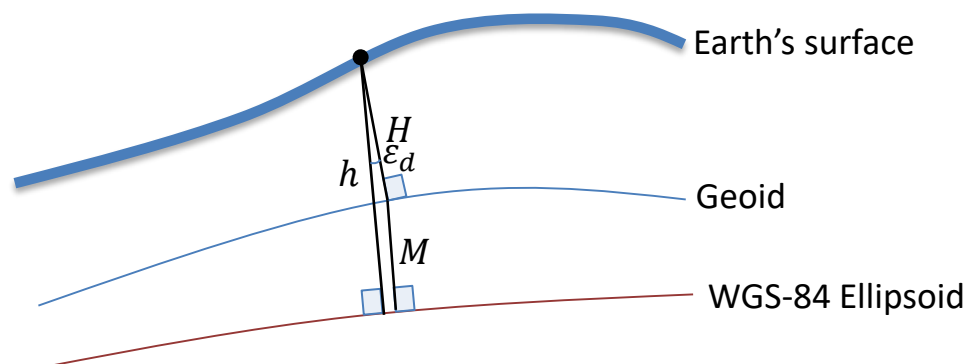
h – ellipsoidal height (geodetic)

H – orthometric height (MSL)

M – geoid separation (undulation) $|M| \leq 100\text{m}$

ε_d – deflection of the vertical ≈ 0

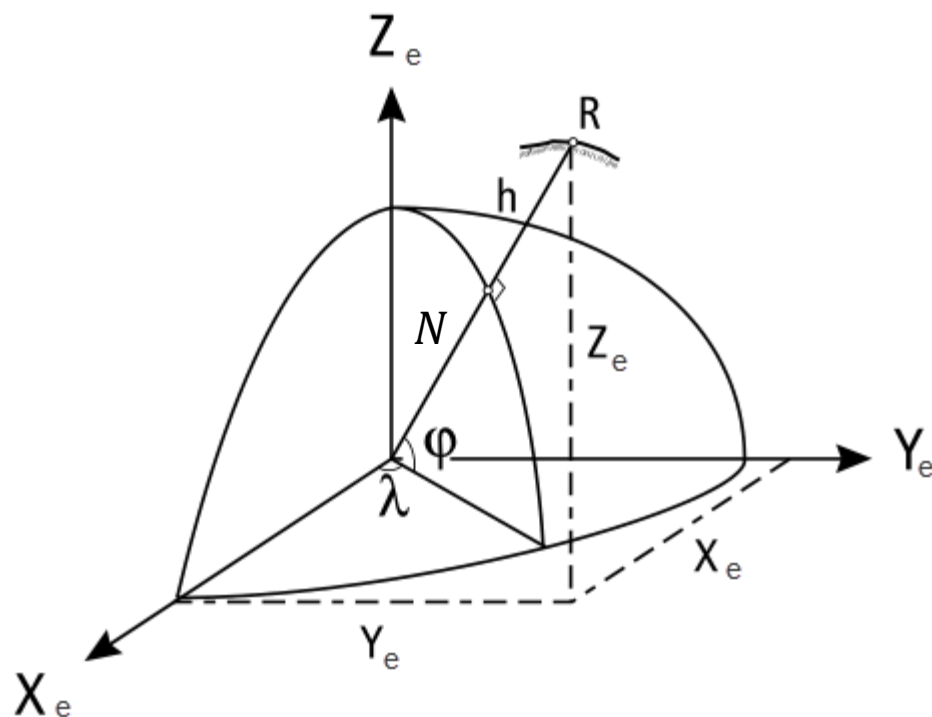
$$h \approx H + M$$



Lat-Lon → ECEF Coordinates

$$N = \frac{a^2}{\sqrt{(a^2 \cos^2 \varphi + b^2 \sin^2 \varphi)}} \quad (\text{Prime Vertical of Curvature (m)})$$

$$\mathbf{p}_{b/e}^e = \begin{bmatrix} x_e \\ y_e \\ z_e \end{bmatrix} = \begin{bmatrix} (N + h) \cos \varphi \cos \lambda \\ (N + h) \cos \varphi \sin \lambda \\ \left(\frac{b^2}{a^2} N + h \right) \sin \lambda \end{bmatrix}$$



ECEF Coordinates \rightarrow Lat-Lon

$$p = \sqrt{x_e^2 + y_e^2}$$

$$\theta = \tan^{-1} \frac{z_e a}{pb}$$

$$\lambda = \tan^{-1} \frac{y_e}{x_e}$$

$$\varphi = \tan^{-1} \frac{z_e + e'^2 b \sin^3 \theta}{p - e^2 a \cos^3 \theta}$$

$$h = \frac{p}{\cos \varphi} - N$$



EXCELLABUST
EXCELLING LABUST IN MARINE ROBOTICS



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