

10.1

(a) Let V_s increase by a positive increment. This will cause the drain current of Q_1 to increase. The increase in I_{d1} will be fed to the Q_3 - Q_4 mirror, which will provide a corresponding increase in the drain current of Q_4 . The latter current will cause the voltage at the output node to rise. A fraction of the increase in V_O is applied through the divider (R_1 , R_2) to the gate of Q_2 . The increase in the voltage of the gate of Q_2 will subtract from the initially assumed increase of the voltage of the gate of Q_1 , resulting in a smaller increase in the differential voltage applied to the (Q_1 , Q_2) pair. Thus, the feedback counter acts the originally assumed change, verifying that it is negative.

(b) The negative feedback will cause the dc voltage at the gate of Q_2 to be approximately equal to the dc voltage at the gate of Q_1 , that is zero. Now, with $V_{G2} = 0$, the dc current in R_2 will be zero and similarly the dc current in R_1 will be zero, resulting in $V_O = 0$ V dc.

(c) Figure 1 shows the A circuit. It also shows how the loading effect of the β network on the A circuit, namely R_{11} and R_{22} , are found. The gain of the A circuit can be written by inspection as:

$$A = g_{m1,2}(r_{o2} || r_{o4} || R_{22}) \text{ where: } g_{m1,2} = \frac{2I_{D1,2}}{V_{OV1,2}} = \frac{2 \times 0.1}{0.2} = 1 \text{ mA/V}$$

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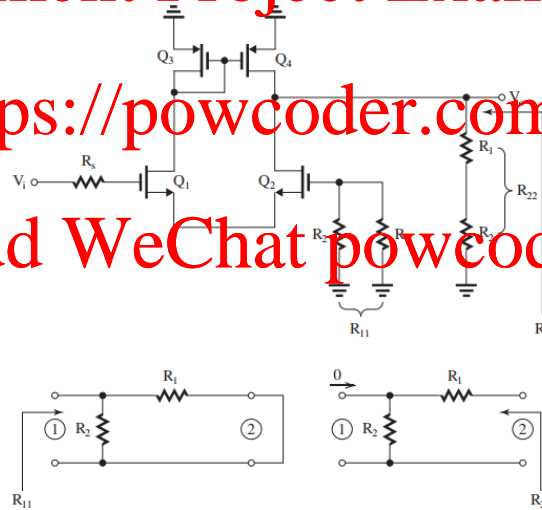


Figure 1

$$r_{o2} = r_{o4} = \frac{|V_A|}{I_{D3,4}} = \frac{10}{0.1} = 100 \text{ k}\Omega$$

$$R_{22} = R_1 + R_2 = 1 \text{ M}\Omega$$

$$A = 1(100 || 100 || 1000) = 47.62 \text{ V/V}$$

(d)

$$\frac{V_o}{V_s} = A_f = \frac{A}{1 + A\beta} \rightarrow 5 = \frac{47.62}{1 + 47.62\beta} \rightarrow \beta = 0.179$$

$$\text{Thus, } \frac{R_2}{R_1 + R_2} = 0.179 \rightarrow R_2 = 0.179 \text{ M}\Omega = 179 \text{ k}\Omega$$

$$R_1 = 1000 - 179 = 821 \text{ k}\Omega$$

(e) Refer to fig. 1:

$$R_o = R_{22} || r_{o2} || r_{o4} = 1000 || 100 || 100 = 47.62 \text{ k}\Omega$$

$$R_{out} = \frac{R_o}{1 + A\beta} = \frac{47.62}{1 + 47.62 \times 0.179} = 5 \text{ k}\Omega$$

(f) With $R_L = 10 \text{ k}\Omega$,

$$\frac{V_o}{V_s} = 5 \times \frac{R_L}{R_L + R_{out}} = 5 \times \frac{10}{10 + 5} = 3.33 \frac{\text{V}}{\text{V}}$$

(g)

With $R_L = 10 \text{ k}\Omega$:

$$A = g_{m1,2}(R_L || R_{22} || r_{o2} || r_{o4}) = 1(10 || 1000 || 100 || 100) = 8.26 \text{ V/V}$$

Using $\beta = 0.179$, we obtain:

$$A_f = \frac{8.26}{1 + 8.26 \times 0.179} = 3.33 \text{ V/V}$$

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10.2:

(a) If V_s increases, the output of A_1 will decrease and this will cause the output of A_2 to increase. This, in turn, causes the output of A_3 which is V_o , to increase. A portion of the positive increment in V_o is fed back to the positive input terminal of A_1 through the voltage divider (R_2 , R_1), the increased voltage at the positive input terminal of A_1 counteracts the originally assumed increase at the negative input terminal, verifying that the feedback is negative.

(b) $A_f = \frac{1}{\beta}$; where: $\beta = \frac{R_1}{R_1 + R_2}$

Thus, to obtain an ideal closed-loop gain of 5 V/V we need $\beta = 0.2 \rightarrow 0.2 = \frac{20}{20 + R_2} \rightarrow R_2 = 80 \text{ k}\Omega$

(c)

Figure 1 shows the small signal equivalent circuit of the feedback amplifier.

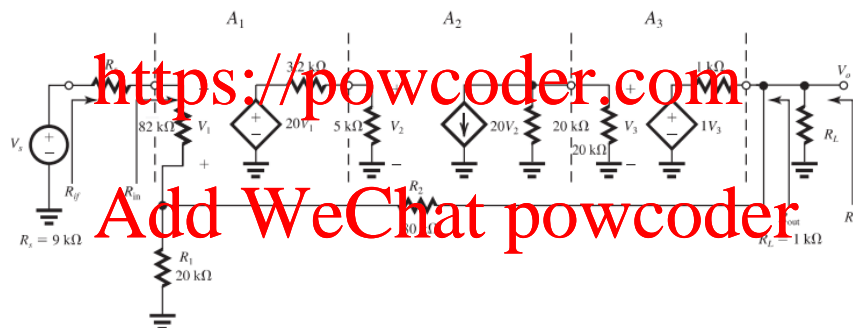


Figure 1

(d)

Figure 2 shows the A circuit and the β circuit together with the determination of its loading effects, R_{11} and R_{22} .

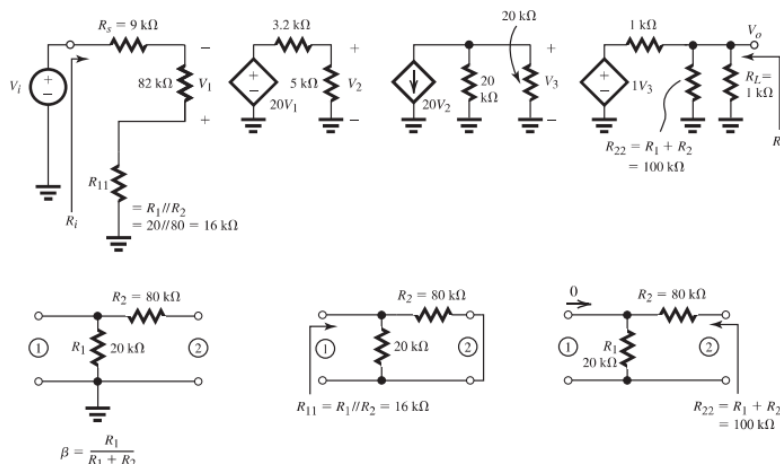


Figure 2

We can write:

$$\frac{V_1}{V_i} = -\frac{82}{82 + 9 + 16} = -0.766 \frac{V}{V}$$

$$V_2 = 20V_1 \times \frac{5}{3.2 + 5} = 12.195V_1$$

$$V_3 = -20V_2(20||20) = -200V_2$$

$$V_o = V_3 \frac{1||100}{(1||100) + 1} = 0.497V_3$$

Thus,

$$A \equiv \frac{V_o}{V_i} = 0.497 \times -200 \times 12.195 \times -0.766 = 925.5 \text{ V/V}$$

(e) $\beta = \frac{20}{20+5} = 0.2 \frac{V}{V}$, $1 + A\beta = 1 + 925.5 \times 0.2 = 186.7$

(f) $A_f = \frac{V_o}{V_i} = \frac{A}{1 + A\beta} = \frac{925.5}{186.7} = 4.97 \frac{V}{V}$

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From the A circuit:

$$R_i = 9 + 82 + 16 = 107 \text{ k}\Omega$$

$$R_{if} = R_i(1 + A\beta) = 107 \times 186.7 = 19.98 \text{ M}\Omega$$

$$R_{in} = R_{if} - R_s = 19.98 \text{ M}\Omega$$

(h) From the A circuit:

$$R_o = R_L || R_{22} || 1\text{k}\Omega = 1 || 100 || 1 = 497.5 \Omega$$

$$R_{of} = \frac{R_o}{1 + A\beta} = \frac{497.5}{186.7} = 2.66 \Omega$$

$$R_{of} = R_{out} || R_L \rightarrow R_{out} || 1000 = 2.66 \Omega \rightarrow R_{out} = 2.66 \Omega$$

(i) $f_{Hf} = f_H(1 + A\beta) = 100 \times 186.7 = 18.67 \text{ kHz}$

(j) if A_1 drops to half its nominal value, A will drop to half its nominal value:

$$A = \frac{1}{2} \times 928.5 = 464.25$$

And A_f becomes:

$$A_f = \frac{464.25}{1 + 464.25 \times 0.2} = 4.947 \text{ V/V}$$

Thus, the percentage change in A_f is

$$= \frac{4.947 - 4.97}{4.97} = -0.47\%$$

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