### **University of Manchester**

**ECON61001: Econometric Methods** 

### **Final Exam**

### January 2021

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#### Instructions:

- You must answer all five questions in Section A and two out of the four questions in Section Bir you answer more questions than the equired and do not indicate which answers should be ignored, we will mark the requisite number of answers in the order in which they appear in your answer submission: answers beyond that intropycill not become indicated. COM
- Your answers could be typed or hand-written (and scanned to a single pdf file that can be submitted) or a combination of a typed answer with included images of algebra or record
- Where relevant, questions include word limits. These are limits, not targets. Excellent answers can be shorter than the word limit. If you go beyond the word limit the additional text will be ignored. Where a question includes a word limit you HAVE to include a word count for your answer (excluding formulae). You could use https://wordcounter.net to obtain word counts.
- Candidates are advised that the examiners attach considerable importance to the clarity with which answers are expressed.
- You must correctly enter your registration number and the course code on your answer.

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### **SECTION A**

1. Suppose a researcher is interested in the following linear regression model

$$y_i = x_i' \beta_0 + u_i, \quad i = 1, 2, \dots N,$$

where  $x_i=(1,x_{2,i},x_{3,i},x_{4,i})'$  and  $\beta_0=(\beta_{0,1},\beta_{0,2},\beta_{0,3},\beta_{0,4})'$ . Given the context, the researcher is able to assume that  $\{u_i,x_i'\}_{i=1}^N$  form a sequence of independently and identically distributed random vectors with  $E[x_ix_i']=Q$ , a finite, positive definite matrix of constants,  $E[u_i|x_i]=0$  and  $Var[u_i|x_i]=\sigma_0^2$ . Therefore, she estimates the model via Ordinary Least Squares (OLS), obtaining the following estimated equation

$$\hat{y}_i = \underset{(0.1416)}{1.0213} - \underset{(0.0005)}{0.0020} x_{2,i} - \underset{(0.0080)}{0.0208} x_{3,i} + \underset{(0.0088)}{0.0095} x_{4,i},$$

where the number in parenthesis is the conventional OLS standard error for the coefficient in question. The Objectimator of  $\sigma_{\rm c}^2$  in this model is  $\hat{\sigma}_{\rm c}^2=0.0081$ . Given these results, the researcher concludes that  $\beta_{0,4}=0$  and so decides to

Given these results, the researcher concludes that  $\beta_{0,4}=0$  and so decides to estimate the model via OLS with  $x_{4,i}$  excluded, obtaining the following estimated equation

https://powcoder.com. (1)

Given that the sample size is N=108 in both estimations, calculate the OLS estimator of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimations, calculate the OLS estimator in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of from the estimation in (1). Be sure to carefully explain you chalculated a culture of the error variance of the estimation in (1).

- 2. Suppose it is desired to predict  $z_t$  using  $\hat{z}_t = w_t' \gamma$  where  $w_t$  is a vector of observable variables and  $\gamma$  is a vector of constants that needs to be specified. The choice of  $\gamma$  associated with the linear projection of  $z_t$  on  $w_t$  is  $\gamma_0$  where  $E[(z_t w_t' \gamma_0) w_t] = 0$ .
  - (a) What optimality property does  $\hat{z}^o_t = w'_t \gamma_0$  possess? (Word limit: 50) [1 mark]
  - (b) Now consider the regression model  $z_t = w_t' \gamma_0 + v_t$ . Is  $w_t$  contemporaneously exogenous or strictly exogenous for estimation of  $\gamma_0$  in this model? Justify your answer. (Word limit: 150) [4 marks]
  - (c) Suppose the model in part (b) is dynamically complete. What optimality property does  $\hat{z}_t^o$  possess? Briefly justify your answer. (Word limit: 150) [3 marks]

### **SECTION A continued**

- 3.(a) Let A be  $n \times n$  nonsingular symmetric matrix. Show that if A is positive definite then  $A^{-1}$  is positive definite. Hint:  $AA^{-1} = I_n$ . [4 marks]
- 3.(b) Consider the classical linear regression model

$$y = X\beta_0 + u, (2)$$

where X is the  $T \times k$  observable data matrix that is fixed in repeated samples with rank(X) = k, and u is a  $T \times 1$  vector with E[u] = 0 and  $Var[u] = \sigma_0^2 I_T$  where  $\sigma_0^2$ is an unknown positive finite constant. Let  $\hat{\beta}_T$  be the OLS estimator of  $\beta_0$  based on (2) and  $\hat{\beta}_{R,T}$  be the Restricted Least Squares (RLS) estimator of  $\beta_0$  based on (2) subject to the restrictions  $R\beta_0 = r$  where R is a  $n_r \times k$  matrix of specified constants with  $rank(R) = n_r$  and r is a specified  $n_r \times 1$  vector of constants. Assuming the restrictions are correct, prove that  $\hat{\beta}_{R,T}$  is at least as efficient as  $\hat{\beta}_T$ . Hint: you may quote the formula for the variance-covariance matrix of the OLS and RLS estimators without proof; you may also take advantage of the stated result in part (a) ent Project Exam Help [4 marks]

4. Consider the linear regression model

of unknown regression coefficients. Assume that X is fixed in repeated sam-constant. Let or denote the maximum likelihood estimator of the unknown parameter vector  $\theta_0 = (\beta_0', \sigma_0^2)'$ . Derive the information matrix for this model. *Hint:* you may state the form of the log likelihood function and score function for this model without proof. [8 marks]

5. Consider the model

$$y_i = x_i' \beta_0 + u_i, \qquad i = 1, 2, \dots, N,$$

where  $\beta_0$  is the  $k \times 1$  vector of unknown regression coefficients,  $\{(x_i', u_i)\}_{i=1}^N$ is a sequence of independently and identically distributed random vectors with  $E[u_i|x_i]=0$ ,  $Var[u_i|x_i]=\sigma_0^2$ , an unknown finite positive constant and  $E[x_ix_i']=0$ Q, a finite positive definite matrix of constants. Let  $\hat{\sigma}_N^2$  be the OLS estimator of  $\sigma_0^2$ . Show that  $N^{1/2}(\hat{\sigma}_N^2-\sigma_0^2)\stackrel{d}{\to} N(0,\,\mu_4-\sigma_0^2)$  where  $\mu_4=E[u_i^4]$ . Hint: You may assume that:  $N^{-1}\sum_{i=1}^N x_i x_i' \stackrel{p}{\to} Q$ ; (ii)  $N^{-1/2}\sum_{i=1}^N v_i \stackrel{d}{\to} N(0,\Omega)$ 

where  $v_i = (u_i^2 - \sigma_0^2, x_i' u_i)'$ , and  $\Omega = Var[v_i]$  is a finite, positive definite  $(k+1) \times (k+1)$  matrix whose elements you must specify as needed to develop your answer. [8 marks]

### **SECTION B**

6. Consider the regression model

$$y_i = x_i' \beta_0 + u_i, \quad i = 1, 2, \dots, N,$$

where  $\beta_0$  is the  $k \times 1$  vector of unknown regression coefficients,  $\{(x_i', u_i)\}_{i=1}^N$ is a sequence of independently and identically distributed random vectors with  $E[u_i|x_i]=0$ ,  $Var[u_i|x_i]=\sigma_0^2$ , an unknown finite positive constant and  $E[x_ix_i']=0$ Q, a finite positive definite matrix of constants. You may further assume that: (i)  $N^{-1} \sum_{i=1}^{N} x_i x_i' \xrightarrow{p} Q$ ; (ii)  $N^{-1/2} \sum_{i=1}^{N} x_i u_i \xrightarrow{d} N(0, \sigma_0^2 Q)$ .

Let  $\hat{\beta}_{R,N}$  denote the RLS estimator based on the linear restrictions  $R\beta = r$  where R is a  $n_r \times k$  matrix of pre-specified constants with rank equal to  $n_r$  and r is a  $n_r \times 1$  vector of pre-specified constants, and let  $\hat{\lambda}_N$  be the vector of Lagrange Multipliers associated with this RLS estimation. Assuming  $R\beta_0 = r$ , answer the following sugginsment Project Exam Help (a) Show that  $N^{1/2}(\hat{\beta}_{R,N}-\beta_0)\overset{a}{\to}N(0,V_R)$  where

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Hint: you may quote the formulae for  $\hat{\beta}_{R,N}$  and  $\hat{\beta}_{N}$ , the Ordinary Least Squares estimator of  $\beta_0$ , without proof. [10 marks]

(b) A colleague proposes testing  $H_0$ :  $H_$ decision rule of the form: reject  $H_0$  at the (approximate)  $100\alpha\%$  significance level if

$$\hat{\lambda}'_N M_N \hat{\lambda}_N > c_{n_r} (1 - \alpha)$$

where  $c_{n_r}(1-\alpha)$  is the  $100(1-\alpha)^{th}$  percentile of the  $\chi^2_{n_r}$  distribution. However, your colleague is unsure what the matrix  $M_N$  should be in order that this decision rule has the properties implied by the stated significance level. Provide a suitable choice of  $M_N$ , being sure to justify your choice carefully. Hint: you may quote without proof: (i) the formulae for  $\hat{\lambda}_N$  and  $\hat{\beta}_N$ ; (ii) that both the OLS and RLS estimators of  $\sigma_0^2$  are consistent under the conditions of the question. [20 marks]

Continued over

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### **SECTION B continued**

7.(a) Let  $\{v_t\}_{t=-3}^T$  be a weakly stationary time series process. Consider the following statistic,

$$\hat{\rho}_{4,T} = \frac{\sum_{t=1}^{T} v_t v_{t-4}}{\sum_{t=1}^{T} v_t^2}.$$

Let  $\{\varepsilon_t\}_{t=-\infty}^{\infty}$  denote a sequence of independently and identically distributed (i.i.d.) random variables with mean zero and variance  $\sigma_{\varepsilon}^2$ .

- (i) Assume that  $v_t = \varepsilon_t$ . Show that  $T^{1/2}\hat{\rho}_{4,T} \stackrel{d}{\to} N(0,1)$ . [6 marks]
- (ii) Assume that

$$v_t = \theta_4 v_{t-4} + \varepsilon_t$$

where  $|\theta_4| < 1$ . What is the probability limit of  $\hat{\rho}_{4,T}$  as  $T \to \infty$ ? Be sure to justify your answer carefully. Hint:  $v_t$  has the following representation,

### A signment Project Exam Help [9 marks]

7.(b) A researcher wishes to test the simple efficient-markets hypothesis in the foreign exchange market. Let  $s_t = ln(S_t)$  and  $f_{t,n} = ln[F_{t,n}]$ , where  $S_t$  and  $F_{t,n}$  are the levels of the spbt p shange of the wind the condition of forward exchange rate at time t. The simple efficient-markets hypothesis is that  $f_{t,n} = E[s_{t+n} \mid \mathcal{I}_t]$  where  $\mathcal{I}_t$  is the information set at time t which for the purposes of this question can be taken to be  $\mathcal{I}_t = V_t / f_t /$ 

$$y_{t+n} = x_t' \beta_0 + u_{t,n},$$
 (3)

where  $y_{t+n} = s_{t+n} - f_{t,n}$ ,  $x_t$  is the  $3 \times 1$  vector given by

$$x'_{t} = (1, s_{t} - f_{t-n,n}, s_{t-1} - f_{t-1-n,n}),$$

n=30 and  $u_{t,n}$  is the error term. If the simple efficient markets hypothesis holds in this foreign exchange market then  $E[u_{t,n}\,|\,\mathcal{I}_t]=0$  and the regression coefficients in (3) satisfy a set of restrictions denoted here by  $g(\beta_0)=0$  where  $g(\,\cdot\,)$  is  $n_q\times 1$  vector.

(i) What is  $g(\beta_0)$ ? Briefly justify your answer. (Word limit: 75) [4 marks]

### **SECTION B continued**

### 7.(b) continued

(ii) The researcher tests  $H_0: g(\beta_0)=0$  versus  $H_1: g(\beta_0)\neq 0$  using the test statistic

$$S_T = Tg(\hat{\beta}_T)' \left( G(\hat{\beta}_T) \hat{V}_{\beta} G(\hat{\beta}_T)' \right)^{-1} g(\hat{\beta}_T), \tag{4}$$

where  $G(\hat{\beta}_T) = \partial g(\beta)/\partial \beta \big|_{\beta = \hat{\beta}_T}$ . Assuming  $T^{1/2}(\hat{\beta}_T - \beta_0) \stackrel{d}{\to} N(0, V_\beta)$  and  $\hat{V}_{\beta} \stackrel{p}{\to} V_{\beta}$ , write down a suitable decision rule for this test. If  $S_T = 8.2$  then what is the outcome of the test? [3 marks]

(iii) Since the  $y_{t+n}$  is a financial variable, the researcher is concerned that the errors may exhibit autoregressive conditional heteroscedasticity and so has calculated  $\hat{V}_{\beta}$  in (4) using White's heteroscedasticity robust estimator. Given this information, do you have any concerns about the test in part (ii)? If so Then explain your conder is and how you would madify the tast to address these concerns. (Word limit: 350)

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### **SECTION B continued**

8. Consider the linear regression model

$$y_{1,i} = \gamma_0 y_{2,i} + z'_{1,i} \delta_0 + u_{1,i} = x'_i \beta_0 + u_{1,i},$$

where  $x_i' = (y_{2,i}, z_{1,i}'), \beta_0 = (\gamma_0, \delta_0')'$  and assume that

$$y_{2,i} = z_i' \eta_0 + u_{2,i}, \tag{5}$$

where  $y_{1,i}$  and  $y_{2,i}$  are observable random variables,  $z_i = (z'_{1,i}, z'_{2,i})'$  is a random vector of observable variables,  $u_{1,i}$  and  $u_{2,i}$  are the error terms (unobservable scalar random variables),  $\gamma_0$  is an unknown scalar parameter, and  $\delta_0$ , and  $\eta_0$  are vectors of unknown parameters. Suppose there is a sample of N observations, and let  $\hat{y}_{2,i}$  denote the predicted value of  $y_{2,i}$  based on Ordinary Least Squares (OLS) estimation of (5). Define  $\hat{x}_i = (\hat{y}_{2,i}, z'_{1,i})'$ . Let X be the  $N \times k$  matrix with  $i^{th}$ row X,  $\hat{X}$  be the  $N \times 1$  vector with  $i^{th}$  row  $i^t$ ,  $i^t$  be the  $i^t$  row  $i^t$  and  $i^t$  be the  $i^t$  vector with  $i^t$  element  $i^t$ . Consider the following three estimators of  $\beta_0$ :

- $\hat{\beta}_1 = (\hat{X}_1 \hat{X}_2) \hat{P}_2 \hat{Y}_2 \hat$

- $\hat{\beta}_3 = \{X'Z(Z'Z)^{-1}Z'X\}^{-1}X'Z(Z'Z)^{-1}Z'y_1.$ (a) Show that  $\hat{\beta}_1 = \hat{\beta}_2 = \hat{\beta}_3$ . We Chat powcoder

[15 marks]

(b) Let  $\hat{\phi}=(\hat{\beta}',\hat{\theta})'$  be the OLS estimator of  $\phi_0=(\beta_0',\theta_0)'$  based on the model

$$y_{1,i} = x_i' \beta_0 + \theta \hat{u}_{2,i} + \text{"error"}$$

where  $\hat{u}_{2,i}$  is the  $i^{th}$  element of  $\hat{u}_2$ , the  $N \times 1$  vector of residual from OLS estimation of (5). Via an application of the Frisch-Waugh-Lovell Theorem or otherwise, show that  $\hat{\beta} = \hat{\beta}_1$ .

[15 marks]

### **SECTION B continued**

9.(a) Let  $\{(y_i, x_i')\}_{i=1}^N$  be a sequence of independently and identically distributed (i.i.d.) random vectors. Suppose that  $y_i$  is a dummy variable and so has a sample space of  $\{0, 1\}$ . Consider the model

$$y_i = x_i' \beta_0 + u_i.$$

- (i) Assume that  $E[u_i|x_i]=0$ . Derive the Generalized Least Squares (GLS) estimator of  $\beta_0$  in this model? Hint: you may quote the generic formula for the GLS estimator that is,  $\hat{\beta}_{GLS}=(X'\Sigma^{-1}X)^{-1}X'\Sigma^{-1}y$ , but you must derive  $\Sigma$  for this model. [6 marks]
- (ii) Is your answer to part (i) a feasible or infeasible GLS estimator? If infeasible then suggest a feasible GLS estimator. Do you foresee any potential problems in implementing your proposed Feasible GLS estimator? [4 marks]
- (b) Let  $\{V_i\}_{i=1}$  be a sequence of i.i.d. Bernoulli random variables with  $P(V_i=1)=\theta_0$ . We assume here that  $\theta_0\in(0,1)$  and that our sample size is large enough for both outcomes to occur.
  - (i) Derive the ward, Likelihood Katlo and Lagrange Multiplier statistics for testing  $H_0: \theta_0 = \theta_*$  against  $H_1: \theta_0 \neq \theta_*$ . Hint: you may quote the form of the log likelihood function, the score equation and the formula for the maximum likelihood efficatory the movel with move [16 marks]
  - (ii) Given that N=100 and the sample contains 55 outcomes that are one, use your statistics in part (i) to test the hypothesis  $H_0: \theta_0=0.5$  against  $H_1: \theta_0 \neq 0.5$  at the 5% significance level. [4 marks]

**END OF EXAMINATION** 

### 1 Table 1: Percentage Points for the t distribution

| Student's t Distribution Function for Selected Probabilities The table provides values of $t_{\alpha,v}$ where $\Pr(T \leq t_{\alpha,v}) = \alpha$ and $T \sim t_v$ |       |                |                    |       |               |                    |                        |                     |                |                |  |
|---|-------|----------------|--------------------|-------|---------------|--------------------|------------------------|---------------------|----------------|----------------|--|
| $\alpha$  | 0.750 | 0.800          | 0.900              | 0.950 | 0.975         | 0.990              | $\frac{-0.995}{0.995}$ | 0.9975              | 0.999          | 0.9995         |  |
| $\nu$   |       |                |                    |       | Value         | es of $t_{lpha,v}$ |                        |                     |                |                |  |
| 1   | 1.000 | 1.376          | 3.078              | 6.314 | 12.706        | 31.821             | 63.657                 |                     |                |                |  |
| 2   | 0.816 | 1.061          | 1.886              | 2.920 | 4.303         | 6.965              | 9.925                  |                     |                |                |  |
| 3   | 0.765 | 0.978          | 1.638              | 2.353 | 3.182         | 4.541              | 5.841                  |                     |                |                |  |
| 4   | 0.741 | 0.941          | 1.533              | 2.132 | 2.776         | 3.747              | 4.604                  |                     |                |                |  |
| 5   | 0.727 | 0.920          | 1.476              | 2.015 | 2.571         | 3.365              | 4.032                  | 4.773               |                |                |  |
| 6   | 0.718 | 0.906          | 1.440              | 1.943 | 2.447         | 3.143              | 3.707                  | 4.317               | 5.208          |                |  |
| 7   | 0.711 | 0.896          | 1.415              | 1.895 | 2.365         | 2.998              | 3.499                  | 4.029               | 4.785          | 5.408          |  |
| 8   | 0.706 | 0.889          | 1.397              | 1.860 | 2.306         | 2.896              | 3.355                  | 3.833               | 4.501          | 5.041          |  |
| 9   | 0.703 | 0.883          | 1.383              | 1.833 | 2.262         | 2.821              | 3.250                  | 3.690               | 4.297          | 4.781          |  |
| 10  | 0.700 | 0.879          | 1.372              | 1.812 | 2.228         | 2.764              | 3.169                  | 3.581               | 4.144          | 4.587          |  |
| 11  | 0.697 | 0.876          | 1.363              | 1.796 | 2.201         | 2.718              | 3.106                  | 3.497               | 4.025          | 4.437          |  |
| 12  | 0.695 | 0.873          | 1.356              | 1.782 | 2.179         | 2.681              | 3.055                  | 3.428               | 3.930          | 4.318          |  |
| 13  | 0.694 | 0.870          | 1.350              | 1.771 | 2.160         | 2.650              | 3.012                  | 3.372               | 3.852          | 4.221          |  |
| 14  |       | 0.868          | 1 <del>134</del> 5 | 176P  |               | 2.924              | 3977                   | H-326               | 3.787          | 4.140          |  |
| 15  |       | 9.8            | 14.84              | 1.755 | T SABA        | 2.602              |                        | 3.286               | 3.733          | 4.073          |  |
| 16  | 0.690 | 0.865          | 1.337              | 1.746 | 2.120         | 2.583              | 2.921                  | 3.252               | 3.686          | 4.015          |  |
| 17  | 0.689 | 0.863          | 1.333              | 1,740 | 2.110         | 2.567              | 2.898                  | 3.222               | 3.646          | 3.965          |  |
| 18  | 0.688 |                | tps:               |       | <b>W</b> .000 |                    |                        | 3.197               | 3.610          | 3.922          |  |
| 19  | 0.688 | 0.861          | 1.328              | 1.729 | 2.093         | 2.539              | 2.861                  | 3.174               | 3.579          | 3.883          |  |
| 20<br>21  | 0.687 | 0.860          | 1.325              | 1.725 | 2.086         | 2.528              | 2.845                  | 3.153               | 3.552          | 3.850          |  |
| 22  | 0.686 | 0.858<br>0.858 |                    | W/AX  | 2.030         | <b>p</b> 2518      | CZZZ                   | 21 <sup>3.135</sup> | 3.527<br>3.505 | 3.819<br>3.792 |  |
| 23  | 0.685 | 0.858          | 1.321<br>1.319     | 1.717 | 2.074         | 2.508              | 2.807                  | 3.119               | 3.485          | 3.768          |  |
| 24  | 0.685 | 0.857          | 1.318              | 1.714 | 2.069         | 2.492              | 2.797                  | 3.091               | 3.467          | 3.745          |  |
| 25  | 0.684 | 0.856          | 1.316              | 1.708 | 2.060         | 2.485              | 2.787                  | 3.078               | 3.450          | 3.725          |  |
| 26  | 0.684 | 0.856          | 1.315              | 1.706 | 2.056         | 2.479              | 2.779                  | 3.067               | 3.435          | 3.707          |  |
| 27  | 0.684 | 0.855          | 1.314              |       | 2.052         | 2.473              | 2.771                  | 3.057               | 3.421          | 3.690          |  |
| 28  | 0.683 | 0.855          | 1.313              | 1.701 | 2.048         | 2.467              | 2.763                  | 3.047               | 3.408          | 3.674          |  |
| 29  | 0.683 | 0.854          | 1.311              | 1.699 | 2.045         | 2.462              | 2.756                  | 3.038               | 3.396          | 3.659          |  |
| 30  | 0.683 | 0.854          | 1.310              | 1.697 | 2.042         | 2.457              | 2.750                  | 3.030               | 3.385          | 3.646          |  |
| 40  | 0.681 | 0.851          | 1.303              | 1.684 | 2.021         | 2.423              | 2.704                  | 2.971               | 3.307          | 3.551          |  |
| 50  | 0.679 | 0.849          | 1.299              | 1.676 | 2.009         | 2.403              | 2.678                  | 2.937               | 3.261          | 3.496          |  |
| 60  | 0.679 | 0.848          | 1.296              | 1.671 | 2.000         | 2.390              | 2.660                  | 2.915               | 3.232          | 3.460          |  |
| 70  | 0.678 | 0.847          | 1.294              | 1.667 | 1.994         | 2.381              | 2.648                  | 2.899               | 3.211          | 3.435          |  |
| 80  | 0.678 | 0.846          | 1.292              | 1.664 | 1.990         | 2.374              | 2.639                  | 2.887               | 3.195          | 3.416          |  |
| 90  | 0.677 | 0.846          | 1.291              | 1.662 | 1.987         | 2.368              | 2.632                  | 2.878               | 3.183          | 3.402          |  |
| 100   | 0.677 | 0.845          | 1.290              | 1.660 | 1.984         | 2.364              | 2.626                  | 2.871               | 3.174          | 3.390          |  |
| 110   | 0.677 | 0.845          | 1.289              | 1.659 | 1.982         | 2.361              | 2.621                  | 2.865               | 3.166          | 3.381          |  |
| 120   | 0.677 | 0.845          | 1.289              | 1.658 | 1.980         | 2.358              | 2.617                  | 2.860               | 3.160          | 3.373          |  |
| $\infty$  | 0.674 | 0.842          | 1.282              | 1.645 | 1.960         | 2.326              | 2.576                  | 2.808               | 3.090          | 3.297          |  |

### 2 Table 2: Percentage Points for the $\chi^2$ distribution

| The $\chi^2$ Distribution Function for Selected Probabilities |   |                |                |                      |                             |                |                |                |                |                |                |  |  |
|---|---|----------------|----------------|----------------------|-----------------------------|----------------|----------------|----------------|----------------|----------------|----------------|--|--|
|   | The table provides values of $\chi^2_{\alpha,v}$ where $\Pr(\chi^2 \leq \chi^2_{\alpha,v}) = \alpha$ and $\chi^2 \sim \chi^2_v$ |                |                |                      |                             |                |                |                |                |                |                |  |  |
| $\alpha$  | 0.005   | 0.01           | 0.025          | 0.05                 | 0.1                         | 0.5            | 0.9            | 0.95           | 0.975          | 0.99           | 0.995          |  |  |
| v   |   |                |                |                      | Va                          | lues of $\chi$ |                |                |                |                |                |  |  |
| 1   | 0.000   | 0.000          | 0.001          | 0.004                | 0.016                       | 0.455          | 2.706          | 3.841          | 5.024          | 6.635          | 7.879          |  |  |
| 2   | 0.010   | 0.020          | 0.051          | 0.103                | 0.211                       | 1.386          | 4.605          | 5.991          | 7.378          | 9.210          | 10.60          |  |  |
| 3   | 0.072   | 0.115          | 0.216          | 0.352                | 0.584                       | 2.366          | 6.251          | 7.815          | 9.348          | 11.34          | 12.84          |  |  |
| 4   | 0.207   | 0.297          | 0.484          | 0.711                | 1.064                       | 3.357          | 7.779          | 9.488          | 11.14          | 13.28          | 14.86          |  |  |
| 5   | 0.412   | 0.554          | 0.831          | 1.145                | 1.610                       | 4.351          | 9.236          | 11.07          | 12.83          | 15.09          | 16.75          |  |  |
| 6   | 0.676   | 0.872          | 1.237          | 1.635                | 2.204                       | 5.348          | 10.64          | 12.59          | 14.45          | 16.81          | 18.55          |  |  |
| 7   | 0.989   | 1.239          | 1.690          | 2.167                | 2.833                       | 6.346          | 12.02          | 14.07          | 16.01          | 18.48          | 20.28          |  |  |
| 8   | 1.344   | 1.646          | 2.180          | 2.733                | 3.490                       | 7.344          | 13.36          | 15.51          | 17.53          | 20.09          | 21.95          |  |  |
| 9   | 1.735   | 2.088          | 2.700          | 3.325                | 4.168                       | 8.343          | 14.68          | 16.92          | 19.02          | 21.67          | 23.59          |  |  |
| 10  | 2.156   | 2.558          | 3.247          | 3.940                | 4.865                       | 9.342          | 15.99          | 18.31          | 20.48          | 23.21          | 25.19          |  |  |
| 11  | 2.603   | 3.053          | 3.816          | 4.575                | 5.578                       | 10.34          | 17.28          | 19.68          | 21.92          | 24.72          | 26.76          |  |  |
| 12  | 3.074   | 3.571          | 4.404          | 5.226                | 6.304                       | 11.34          | 18.55          | 21.03          | 23.34          | 26.22          | 28.30          |  |  |
| 13  | 3.565   | 4.107          | 5.009          | 5.892                | 7.042                       | 12.34          | 19.81          | 22.36          | 24.74          | 27.69          | 29.82          |  |  |
| 14  | /   | \$ 669         |                | 1967P                | 1171                        | 13:34          | ', <b>X</b>    |                | ert?           | 29.14          | 31.32          |  |  |
| 15  | 4.601   | 5.229          | 6.262          | 7.261                | 8.547                       | 14.34          | 22.31          | 25.00          | 27 49          | 30.58          | 32.80          |  |  |
| 16  | 5.142   | 5.812          | 6.908          | 7.962                | 9.312                       | 15.34          | 23.54          | 26.30          | 28.85          | 32.00          | 34.27          |  |  |
| 17  | 5.697   |                | 7.564          | 8,672                | 10.09                       | 16.34          | 24.77          | 27.59          | 30.19          | 33.41          | 35.72          |  |  |
| 18  | 6.265   |                |                |                      |                             |                |                |                | 31.53          | 34.81          | 37.16          |  |  |
| 19  | 6.844<br>7.434  | 7.633<br>8.260 | 8.907<br>9.591 | 10.12                | 11.65                       | 18.34<br>19.34 | 27.20<br>28.41 | 30.14<br>31.41 | 32.85          | 36.19<br>37.57 | 38.58          |  |  |
| 20<br>21  | 8.034   | 8.89           |                | 10.85<br><b>W 59</b> | 12.44<br><b>1</b> 3.241     |                |                | -              | 34.17<br>35.48 | 38.93          | 40.00<br>41.40 |  |  |
| 22  | 8.643   | 9.542          | 10.98          | 12.34                | <b>-  12  2  </b><br> 14.04 | <b>17.34</b>   | <b>1</b> 30.81 | <b>deg7</b>    | 36.78          | 40.29          | 42.80          |  |  |
| 23  | 9.260   | 10.20          | 11.69          | 13.09                | 14.85                       | 22.34          | 32.01          | 35.17          | 38.08          | 41.64          | 44.18          |  |  |
| 24  | 9.886   | 10.26          | 12.40          | 13.85                | 15.66                       | 23.34          | 33.20          | 36.42          | 39.36          | 42.98          | 45.56          |  |  |
| 25  | 10.52   | 11.52          | 13.12          | 14.61                | 16.47                       | 24.34          | 34.38          | 37.65          | 40.65          | 44.31          | 46.93          |  |  |
| 26  | 11.16   | 12.20          | 13.84          | 15.38                | 17.29                       | 25.34          | 35.56          | 38.89          | 41.92          | 45.64          | 48.29          |  |  |
| 27  | 11.81   |                | 14.57          | 16.15                |                             | 26.34          | 36.74          | 40.11          |                | 46.96          | 49.64          |  |  |
| 28  | 12.46   | 13.56          | 15.31          | 16.93                | 18.94                       | 27.34          | 37.92          | 41.34          | 44.46          | 48.28          | 50.99          |  |  |
| 29  | 13.12   | 14.26          | 16.05          | 17.71                | 19.77                       | 28.34          | 39.09          | 42.56          | 45.72          | 49.59          | 52.34          |  |  |
| 30  | 13.79   | 14.95          | 16.79          | 18.49                | 20.60                       | 29.34          | 40.26          | 43.77          | 46.98          | 50.89          | 53.67          |  |  |
| 35  | 17.19   | 18.51          | 20.57          | 22.47                | 24.80                       | 34.34          | 46.06          | 49.80          | 53.20          | 57.34          | 60.27          |  |  |
| 40  | 20.71   | 22.16          | 24.43          | 26.51                | 29.05                       | 39.34          | 51.81          | 55.76          | 59.34          | 63.69          | 66.77          |  |  |
| 45  | 24.31   | 25.90          | 28.37          | 30.61                | 33.35                       | 44.34          | 57.51          | 61.66          | 65.41          | 69.96          | 73.17          |  |  |
| 50  | 27.99   | 29.71          | 32.36          | 34.76                | 37.69                       | 49.33          | 63.17          | 67.50          | 71.42          | 76.15          | 79.49          |  |  |
| 60  | 35.53   | 37.48          | 40.48          | 43.19                | 46.46                       | 59.33          | 74.40          | 79.08          | 83.30          | 88.30          | 91.95          |  |  |
| 70  | 43.28   | 45.44          | 48.76          | 51.74                | 55.33                       | 69.33          | 85.53          | 90.53          | 95.02          | 100.4          | 104.2          |  |  |
| 80  | 51.17   | 53.54          | 57.15          | 60.39                | 64.28                       | 79.33          | 96.58          | 101.9          | 106.6          | 112.3          | 116.3          |  |  |
| 90  | 59.20   | 61.75          | 65.65          | 69.13                | 73.29                       | 89.33          | 107.6          | 113.1          | 118.1          | 124.1          | 128.3          |  |  |
| 100   | 67.33   | 70.06          | 74.22          | 77.93                | 82.36                       | 99.33          | 118.5          | 124.3          | 129.6          | 135.8          | 140.2          |  |  |
| 150   | 109.1   | 112.7          | 118.0          | 122.7                | 128.3                       | 149.3          | 172.6          | 179.6          | 185.8          | 193.2          | 198.4          |  |  |
| 200   | 152.2   | 156.4          | 162.7          | 168.3                | 174.8                       | 199.3          | 226.0          | 234.0          | 241.1          | 249.4          | 255.3          |  |  |

# 3 Table 3: Upper 5% percentage points for the F distribution

| The $F$ Distribution Function for $\alpha=0.05$ |   |       |        |       |               |            |              |        |              |              |               |      |
|---|---|-------|--------|-------|---------------|------------|--------------|--------|--------------|--------------|---------------|------|
| The   | The table provides values of $F_{\alpha,v_1,v_2}$ where $\Pr(F \geq F_{\alpha,v_1,v_2}) = 0.05$ and $F \sim F(v_1,v_2)$ |       |        |       |               |            |              |        |              |              |               |      |
|   | $v_1 \rightarrow$   |       |        |       |               |            |              |        |              |              |               |      |
| $v_2 \downarrow$                                | 1   | 2     | 3      | 4     | 5             | 6          | 7            | 8      | 9            | 10           | 12            | 15   |
| 5   | 6.61  | 5.79  | 5.41   | 5.19  | 5.05          | 4.95       | 4.88         | 4.82   | 4.77         | 4.74         | 4.68          | 4.62 |
| 6   | 5.99  | 5.14  | 4.76   | 4.53  | 4.39          | 4.28       | 4.21         | 4.15   | 4.10         | 4.06         | 4.00          | 3.94 |
| 7   | 5.59  | 4.74  | 4.35   | 4.12  | 3.97          | 3.87       | 3.79         | 3.73   | 3.68         | 3.64         | 3.57          | 3.51 |
| 8   | 5.32  | 4.46  | 4.07   | 3.84  | 3.69          | 3.58       | 3.50         | 3.44   | 3.39         | 3.35         | 3.28          | 3.22 |
| 9   | 5.12  | 4.26  | 3.86   | 3.63  | 3.48          | 3.37       | 3.29         | 3.23   | 3.18         | 3.14         | 3.07          | 3.01 |
| 10  | 4.96  | 4.10  | 3.71   | 3.48  | 3.33          | 3.22       | 3.14         | 3.07   | 3.02         | 2.98         | 2.91          | 2.85 |
| 11  | 4.84  | 3.98  | 3.59   | 3.36  | 3.20          | 3.09       | 3.01         | 2.95   | 2.90         | 2.85         | 2.79          | 2.72 |
| 12  | 4.75  | 3.89  | 3.49   | 3.26  | 3.11          | 3.00       | 2.91         | 2.85   | 2.80         | 2.75         | 2.69          | 2.62 |
| 13  | 4.67  | 3.81  | 3.41   | 3.18  | 3.03          | 2.92       | 2.83         | 2.77   | 2.71         | 2.67         | 2.60          | 2.53 |
| 14  | 4.60  | 3.74  | 3.34   | 3.11  | 2.96          | 2.85       | 2.76         | 2.70   | 2.65         | 2.60         | 2.53          | 2.46 |
| 15  | 4.54  | 3.68  | 3.29   | 3.06  | 2.90          | 2.79       | 2.71         | 2.64   | 2.59         | 2.54         | 2.48          | 2.40 |
| 16  | 4.49  | 3.63  | 3.24   | 3.01  | 2.85          | 2.74       | 2.66         | 2.59   | 2.54         | 2.49         | 2.42          | 2.35 |
| 17  | 4.45  | 34590 | r β120 | 12991 | 28h           | <b>478</b> | <b>21</b> 61 | -12x55 | 12:149       | <b>-</b> 245 | <b>13</b> .38 | 2.31 |
| 18  | 4.41  | 3.55  | 3.16   | 2.93  | 2.77          | 2.66       | 2.58         | 2.51   | 2.46         | 2.41         | 2.34          | 2.27 |
| 19  | 4.38  | 3.52  | 3.13   | 2.90  | 2.74          | 2.63       | 2.54         | 2.48   | 2.42         | 2.38         | 2.31          | 2.23 |
| 20  | 4.35  | 3.49  | 3,10   | 2,87/ | 2.71          | 2.60       | 2.51         | 2.45   | 2.39         | 2.35         | 2.28          | 2.20 |
| 21  | 4.32  | 3.47  |        | _     | <b>2.68</b> V |            | 2.19         |        | <b>2.3</b> 7 | 2.32         | 2.25          | 2.18 |
| 22  | 4.30  | 3.44  | 3.05   | 2.82  | 2.66          | 2.55       | 2.46         | 2.40   | 2.34         | 2.30         | 2.23          | 2.15 |
| 23  | 4.28  | 3.42  | 3.03   | 2.80  | 2.64          | 2.53       | 2.44         | 2.37   | 2.32         | 2.27         | 2.20          | 2.13 |
| 24  | 4.26  | 4     | 3010   | 2.⊽8∕ | <b>2.62</b>   | rat        | PO           | W. 66( | <b>Me</b>    | 2.25         | 2.18          | 2.11 |
| 25  | 4.24  | 3.39  | 2.99   | 2.76  | 2.60          | 2.49       | 2.40         | 2.34   | 2.28         | 2.24         | 2.16          | 2.09 |
| 30  | 4.17  | 3.32  | 2.92   | 2.69  | 2.53          | 2.42       | 2.33         | 2.27   | 2.21         | 2.16         | 2.09          | 2.01 |
| 35  | 4.12  | 3.27  | 2.87   | 2.64  | 2.49          | 2.37       | 2.29         | 2.22   | 2.16         | 2.11         | 2.04          | 1.96 |
| 40  | 4.08  | 3.23  | 2.84   | 2.61  | 2.45          | 2.34       | 2.25         | 2.18   | 2.12         | 2.08         | 2.00          | 1.92 |
| 45  | 4.06  | 3.20  | 2.81   | 2.58  | 2.42          | 2.31       | 2.22         | 2.15   | 2.10         | 2.05         | 1.97          | 1.89 |
| 50  | 4.03  | 3.18  | 2.79   | 2.56  | 2.40          | 2.29       | 2.20         | 2.13   | 2.07         | 2.03         | 1.95          | 1.87 |
| 55  | 4.02  | 3.16  | 2.77   |       |               | 2.27       | 2.18         | 2.11   | 2.06         | 2.01         | 1.93          | 1.85 |
| 60  | 4.00  | 3.15  | 2.76   | 2.53  | 2.37          | 2.25       | 2.17         |        | 2.04         | 1.99         | 1.92          | 1.84 |
| 70  | 3.98  | 3.13  | 2.74   | 2.50  | 2.35          | 2.23       | 2.14         | 2.07   | 2.02         | 1.97         | 1.89          | 1.81 |
| 80  | 3.96  | 3.11  | 2.72   | 2.49  | 2.33          | 2.21       | 2.13         | 2.06   | 2.00         | 1.95         | 1.88          | 1.79 |
| 90  | 3.95  | 3.10  | 2.71   | 2.47  | 2.32          | 2.20       | 2.11         | 2.04   | 1.99         | 1.94         | 1.86          | 1.78 |
| 100   | 3.94  | 3.09  | 2.70   | 2.46  | 2.31          | 2.19       | 2.10         | 2.03   | 1.97         | 1.93         | 1.85          | 1.77 |
| 110   | 3.93  | 3.08  | 2.69   | 2.45  | 2.30          | 2.18       | 2.09         | 2.02   | 1.97         | 1.92         | 1.84          | 1.76 |
| 120   | 3.92  | 3.07  | 2.68   | 2.45  | 2.29          | 2.18       | 2.09         | 2.02   | 1.96         | 1.91         | 1.83          | 1.75 |
| 150   | 3.90  | 3.06  | 2.66   | 2.43  | 2.27          | 2.16       | 2.07         | 2.00   | 1.94         | 1.89         | 1.82          | 1.73 |

# 4 Table 4: Upper 1% percentage points for the F distribution

| The $F$ Distribution Function for $lpha=0.01$   |                   |       |          |               |                   |                |      |              |            |               |               |      |
|---|-------------------|-------|----------|---------------|-------------------|----------------|------|--------------|------------|---------------|---------------|------|
| The table provides values of $F_{\alpha,v_1,v_2}$ where $\Pr(F \geq F_{\alpha,v_1,v_2}) = 0.01$ and $F \sim F(v_1,v_2)$ |                   |       |          |               |                   |                |      |              |            |               |               |      |
|   | $v_1 \rightarrow$ |       |          |               |                   |                |      |              |            |               |               |      |
| $v_2 \downarrow$  | 1                 | 2     | 3        | 4             | 5                 | 6              | 7    | 8            | 9          | 10            | 12            | 15   |
| 5   | 16.3              | 13.3  | 12.1     | 11.4          | 11.0              | 10.7           | 10.5 | 10.3         | 10.2       | 10.1          | 9.89          | 9.72 |
| 6   | 13.7              | 10.9  | 9.78     | 9.15          | 8.75              | 8.47           | 8.26 | 8.10         | 7.98       | 7.87          | 7.72          | 7.56 |
| 7   | 12.2              | 9.55  | 8.45     | 7.85          | 7.46              | 7.19           | 6.99 | 6.84         | 6.72       | 6.62          | 6.47          | 6.31 |
| 8   | 11.3              | 8.65  | 7.59     | 7.01          | 6.63              | 6.37           | 6.18 | 6.03         | 5.91       | 5.81          | 5.67          | 5.52 |
| 9   | 10.6              | 8.02  | 6.99     | 6.42          | 6.06              | 5.80           | 5.61 | 5.47         | 5.35       | 5.26          | 5.11          | 4.96 |
| 10  | 10.0              | 7.56  | 6.55     | 5.99          | 5.64              | 5.39           | 5.20 | 5.06         | 4.94       | 4.85          | 4.71          | 4.56 |
| 11  | 9.65              | 7.21  | 6.22     | 5.67          | 5.32              | 5.07           | 4.89 | 4.74         | 4.63       | 4.54          | 4.40          | 4.25 |
| 12  | 9.33              | 6.93  | 5.95     | 5.41          | 5.06              | 4.82           | 4.64 | 4.50         | 4.39       | 4.30          | 4.16          | 4.01 |
| 13  | 9.07              | 6.70  | 5.74     | 5.21          | 4.86              | 4.62           | 4.44 | 4.30         | 4.19       | 4.10          | 3.96          | 3.82 |
| 14  | 8.86              | 6.51  | 5.56     | 5.04          | 4.69              | 4.46           | 4.28 | 4.14         | 4.03       | 3.94          | 3.80          | 3.66 |
| 15  | 8.68              | 6.36  | 5.42     | 4.89          | 4.56              | 4.32           | 4.14 | 4.00         | 3.89       | 3.80          | 3.67          | 3.52 |
| 16  | 8.53              | 6.23  | 5.29     | 4.77          | 4.44              | 4.20           | 4.03 | 3.89         | 3.78       | 3.69          | 3.55          | 3.41 |
| 17  | 8.40              | SQ110 | T for to | <b>.</b> 6971 | 4 <mark>34</mark> | (418           | 3193 | <b>⊣3</b> 79 | 13.68      | <b>-\$5</b> 9 | <b>13</b> .46 | 3.31 |
| 18  | 8.29              | 6.01  | 5.09     | 4.58          | 4.25              | 4.01           | 3.84 | 3.71         | 3.60       | 3.51          | 3.37          | 3.23 |
| 19  | 8.18              | 5.93  | 5.01     | 4.50          | 4.17              | 3.94           | 3.77 | 3.63         | 3.52       | 3.43          | 3.30          | 3.15 |
| 20  | 8.10              | 5.85  | 4,94     | 4.48/         | 4.10              | 3.87           | 3.70 | 3.56         | 3.46       | 3.37          | 3.23          | 3.09 |
| 21  | 8.02              | 5.78  | 14.87    | <b>4.37</b>   | 4.04              | <b>V</b> 3.8 U | 3.54 | 3.50         | 3.40       | 3.31          | 3.17          | 3.03 |
| 22  | 7.95              | 5.72  | 4.82     | 4.31          | 3.99              | 3.76           | 3.59 | 3.45         | 3.35       | 3.26          | 3.12          | 2.98 |
| 23  | 7.88              | 5.66  | 4.76     | 4.26          | 3.94              | 3.71           | 3.54 | 3.41         | 3.30       | 3.21          | 3.07          | 2.93 |
| 24  | 7.82              | 5.61  | 407      | 4.92          | <b>9.00</b>       | rat            | 1979 | W 66(        | <b>STE</b> | <b>1</b> 3.17 | 3.03          | 2.89 |
| 25  | 7.77              | 5.57  | 4.68     | 4.18          | 3.85              | 3.63           | 3.46 | 3.32         | 3.22       | 3.13          | 2.99          | 2.85 |
| 30  | 7.56              | 5.39  | 4.51     | 4.02          | 3.70              | 3.47           | 3.30 | 3.17         | 3.07       | 2.98          | 2.84          | 2.70 |
| 35  | 7.42              | 5.27  | 4.40     | 3.91          | 3.59              | 3.37           | 3.20 | 3.07         | 2.96       | 2.88          | 2.74          | 2.60 |
| 40  | 7.31              | 5.18  | 4.31     | 3.83          | 3.51              | 3.29           | 3.12 | 2.99         | 2.89       | 2.80          | 2.66          | 2.52 |
| 45  | 7.23              | 5.11  | 4.25     | 3.77          | 3.45              | 3.23           | 3.07 | 2.94         | 2.83       | 2.74          | 2.61          | 2.46 |
| 50  | 7.17              | 5.06  | 4.20     | 3.72          | 3.41              | 3.19           | 3.02 | 2.89         | 2.78       | 2.70          | 2.56          | 2.42 |
| 55  | 7.12              | 5.01  | 4.16     | 3.68          | 3.37              | 3.15           | 2.98 | 2.85         | 2.75       | 2.66          | 2.53          | 2.38 |
| 60  | 7.08              | 4.98  | 4.13     | 3.65          | 3.34              | 3.12           | 2.95 | 2.82         | 2.72       | 2.63          | 2.50          | 2.35 |
| 70  | 7.01              | 4.92  | 4.07     | 3.60          | 3.29              | 3.07           | 2.91 | 2.78         | 2.67       | 2.59          | 2.45          | 2.31 |
| 80  | 6.96              | 4.88  | 4.04     | 3.56          | 3.26              | 3.04           | 2.87 | 2.74         | 2.64       | 2.55          | 2.42          | 2.27 |
| 90  | 6.93              | 4.85  | 4.01     | 3.53          | 3.23              | 3.01           | 2.84 | 2.72         | 2.61       | 2.52          | 2.39          | 2.24 |
| 100   | 6.90              | 4.82  | 3.98     | 3.51          | 3.21              | 2.99           | 2.82 | 2.69         | 2.59       | 2.50          | 2.37          | 2.22 |
| 110   | 6.87              | 4.80  | 3.96     | 3.49          | 3.19              | 2.97           | 2.81 | 2.68         | 2.57       | 2.49          | 2.35          | 2.21 |
| 120   | 6.85              | 4.79  | 3.95     | 3.48          | 3.17              | 2.96           | 2.79 | 2.66         | 2.56       | 2.47          | 2.34          | 2.19 |
| 150   | 6.81              | 4.75  | 3.91     | 3.45          | 3.14              | 2.92           | 2.76 | 2.63         | 2.53       | 2.44          | 2.31          | 2.16 |