

Lecture 3

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Steady-State Equilibria

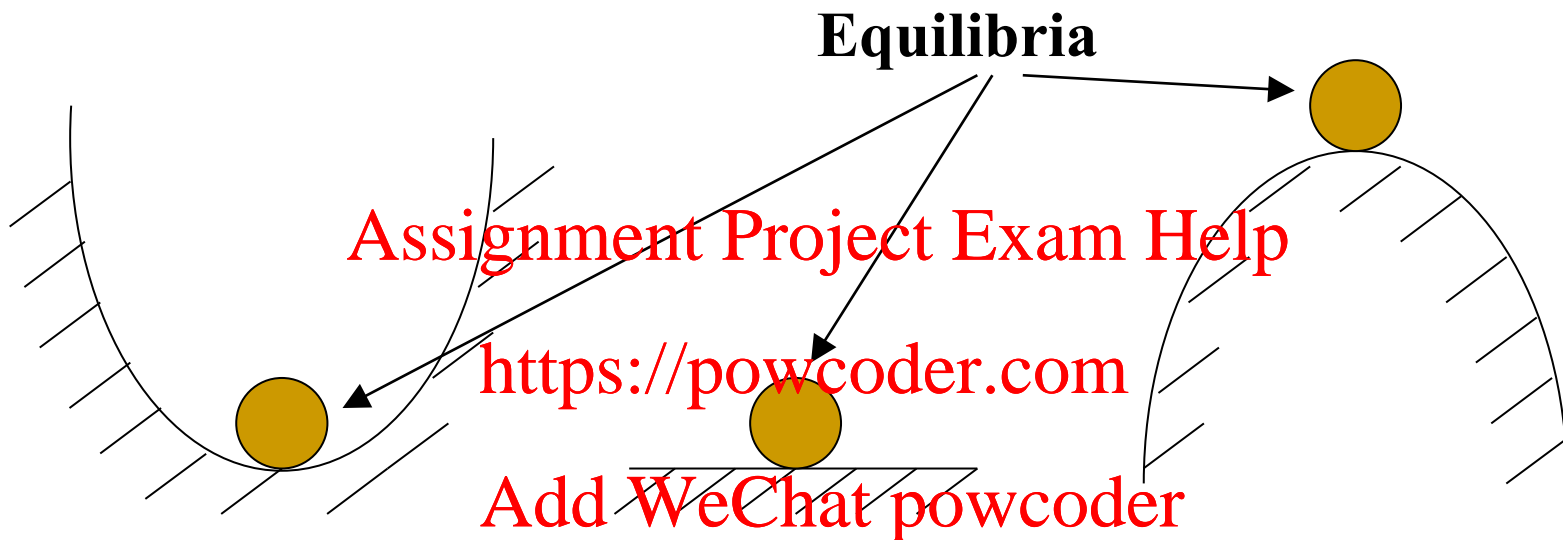
Modeling from first principles

Linearisation

What do we want in control?

- **Stability:** With no disturbances and constant input, output should approach a desired, constant equilibrium, even if initial conditions change slightly from nominal values
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- **Transient performance:** quick but “graceful” transition from initial value to steady-state.
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- **Robustness:** Steady-state behaviour doesn't change dramatically with uncertainties, disturbances or noise.

What is an equilibrium?



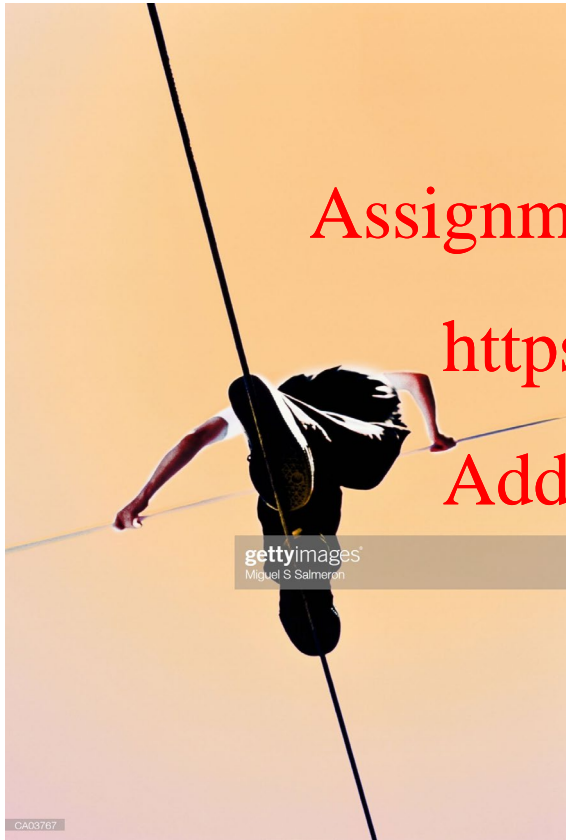
When a system is exactly at an equilibrium point,
nothing changes over time.

Can either be stable, marginally stable, or unstable

Why Go for Equilibria?

- Equilibria are “sweet spots”. When system input and output variables start from an equilibrium point, they remain there forever if no disturbances and noises.
- Nominal operating conditions should be chosen to be equilibrium points.
- In terms of the whole control system, we want to operate near equilibrium points that are stable.

On Unstable Equilibria



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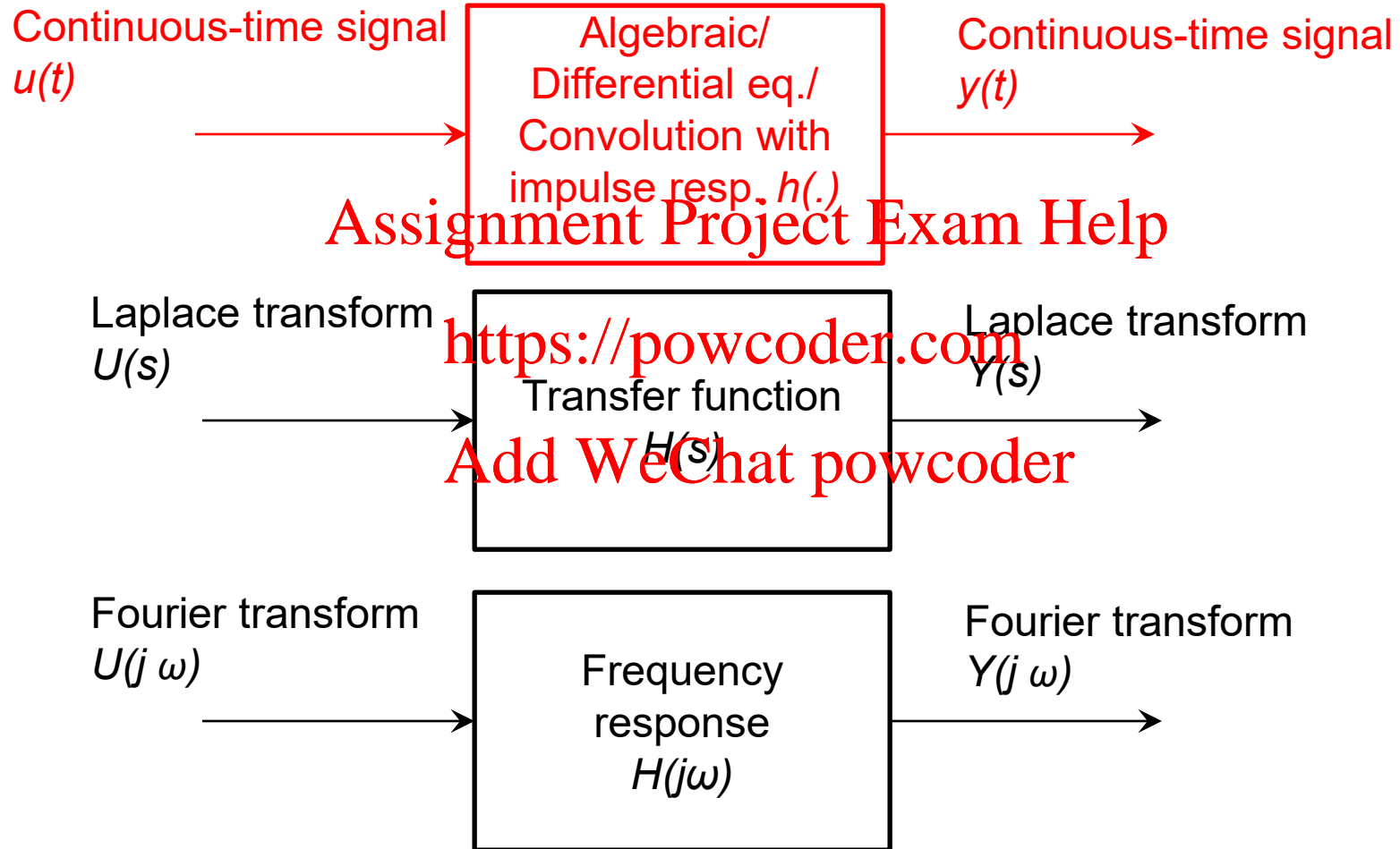
However when we consider just the plant, we sometimes operate at plant equilibria that are unstable.

We render these points stable by interconnecting the plant with a feedback controller.

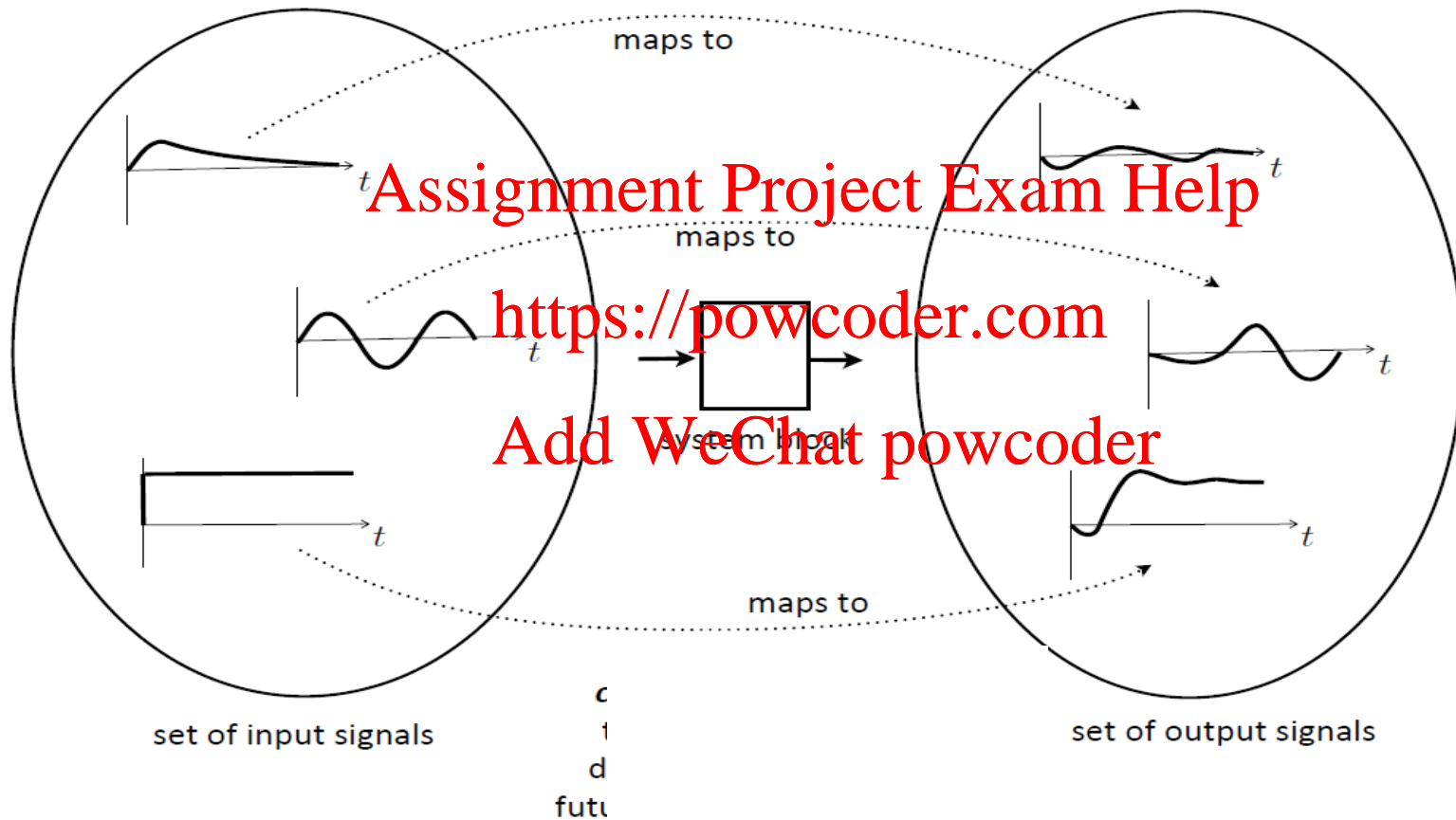
Preview of Techniques

- Stability at equilibrium studied using Laplace transforms, i.e. s-domain, after linearisation
- Transient performance examined in s-domain or frequency domain (Fourier transforms)
- Performance and robustness will be investigated in freq. domain. System freq. response typically needs
 - Good tracking of low freq. references
 - Good damping of disturbances and high freq. noise

System models



System = Mapping between Signal Spaces



How to construct a model

- From first principles (i.e. laws of nature), often followed by
 - Linearisation
 - Model reduction (e.g. neglecting small coefficients)
- Collecting lots of empirical data about input-output signal values over time and then fitting a convenient model (system identification, machine learning)

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On models

All models are wrong, but some are useful.

- G. Box (statistician)

A model should be as simple as possible, but no simpler.

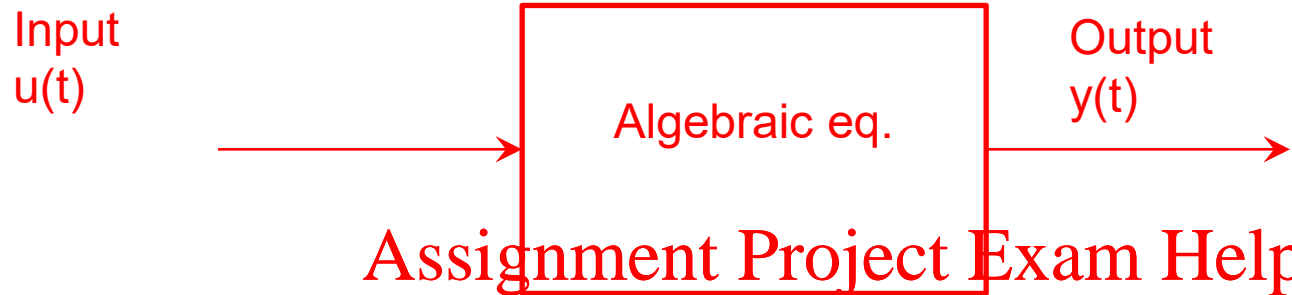
- A. Einstein (...)

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Simple models of the plant are often more useful than complex ones, even if they're less accurate:

- Each model parameter easier to estimate and interpret from empirical data
- Well-designed feedback law attenuates the effect of the modelling error

Static models



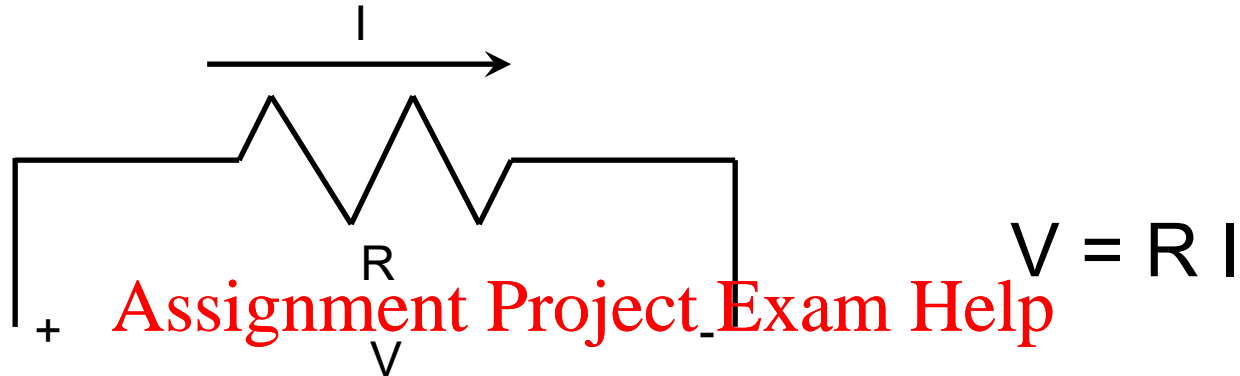
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Property: If $u(t) = u(t')$ then $y(t) = y(t')$

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Example:

$$y = 10u^2 + 2u$$

Example: Ohm's law for resistor



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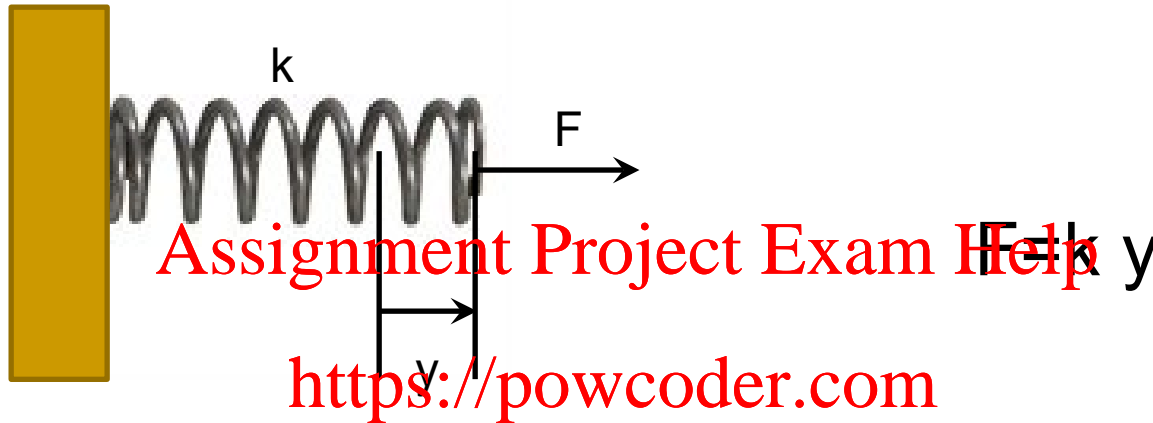
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Assumptions:

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- Resistor is made of "Ohmic" material
- Temperature is constant
- The current is sufficiently small
- Ageing is ignored, etc.

Example: Hooke's law for spring



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- The deflections are sufficiently small so that the material stays within its linear elasticity region (linearization!).

Differential equation models



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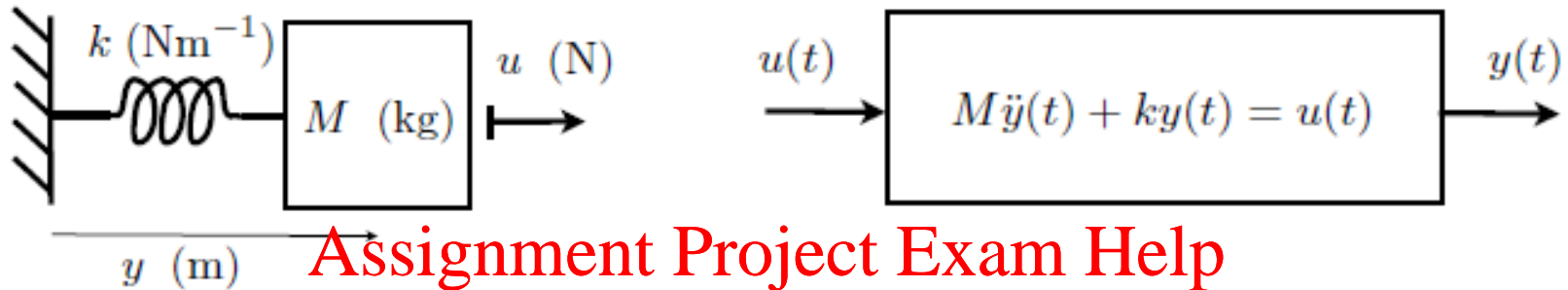
Property : $y(t)$ not necessarily $= y(t')$ when $u(t) = u(t')$.
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Example: $\dot{y} = u$

$$y(t) = y(0) + \int_0^t u(s) ds$$

Example (mass with spring)

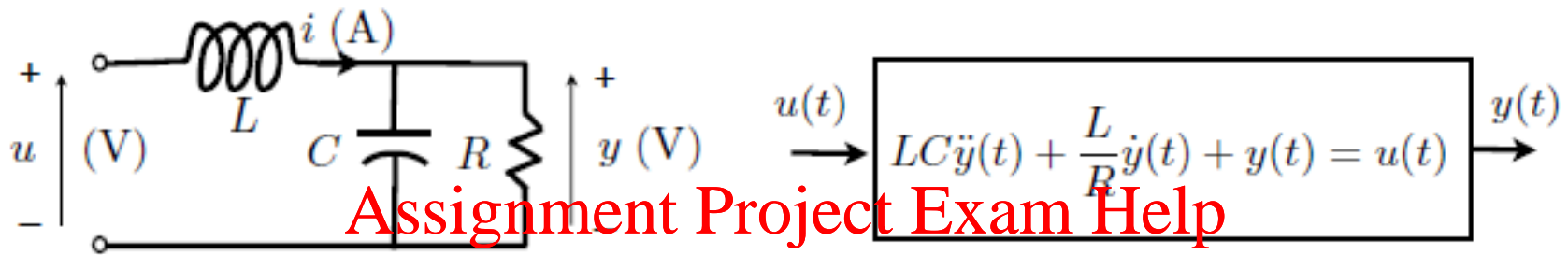


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Assumptions: <https://powcoder.com>

- Hooke's law
 - Newton's second law
 - No friction
 - No damping
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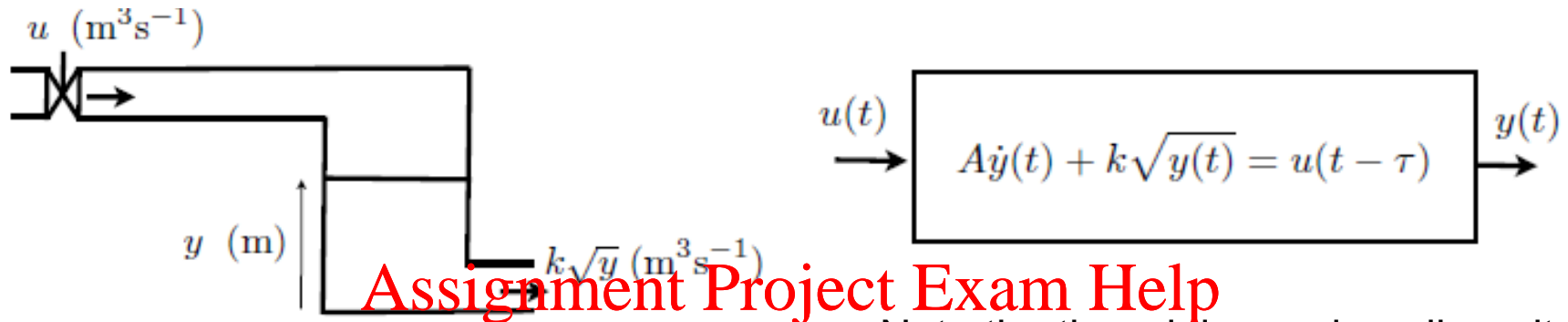
Example (electrical):



Assumptions: <https://powcoder.com>

- Ohm's law [Add WeChat powcoder](#)
- Ideal capacitor
- Ideal inductor
- Kirchhoff's current and voltage laws

Example (fluid flow):

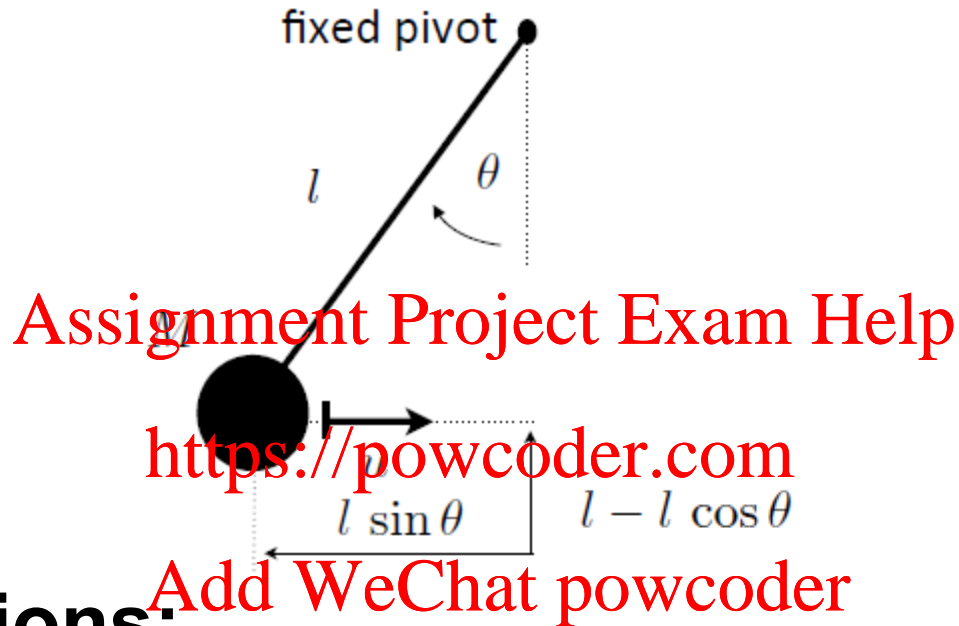


Note the time delay and nonlinearity!

Assumptions: <https://powcoder.com>

- Law of conservation of mass
- Constant cross section A
- Atmospheric pressure above water and at the outlet, and so on.

Example (pendulum):

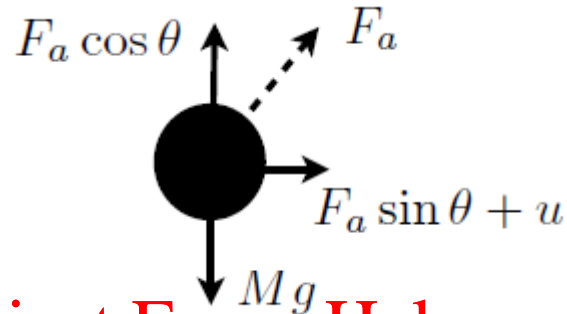


Assumptions:

- Bob is a point mass
- Arm is rigid but massless
- No friction, etc

Example (pendulum)

- Free body diagram:



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- Newton's second law (horizontal):

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$$-F_a \sin \theta - u = M \frac{d^2}{dt^2}(l \sin \theta) = M l \frac{d}{dt}(\dot{\theta} \cos \theta) = M l (\ddot{\theta} \cos \theta - \dot{\theta}^2 \sin \theta)$$

- Newton's second law (vertical)

$$F_a \cos \theta - M g = M \frac{d^2}{dt^2}(l - l \cos \theta) = M l \frac{d}{dt}(\dot{\theta} \sin \theta) = M l (\ddot{\theta} \sin \theta + \dot{\theta}^2 \cos \theta)$$

Example (pendulum)

- Eliminating the force in the arm yields:

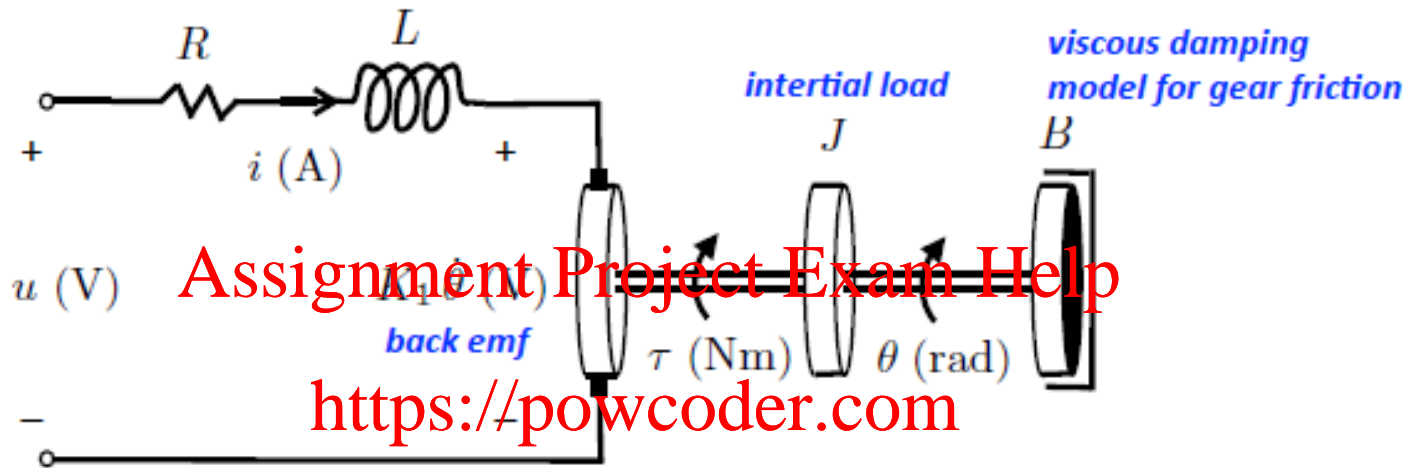
$$Ml\ddot{\theta} + mg \sin \theta = 0$$

- Note that this model is nonlinear!

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- We will revisit this model when we talk about equilibria and linearisation.

Example (DC motor):



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(Linearized) Motor: $\tau(t) = K_2 i(t)$

Newton's second law: $J\ddot{\theta}(t) = \tau(t) - B\dot{\theta}(t)$

Kirchoff's voltage law: $u(t) = Ri(t) + L\frac{di}{dt}(t) + K_1\dot{\theta}(t)$

Finding Equilibria

- Consider an input-output differential model

$$\ell\left(\frac{d^n y}{dt^n}(t), \dots, \frac{dy}{dt}(t), y(t), \frac{d^n u}{dt^n}(t), \dots, \frac{du}{dt}(t), u(t)\right) = 0$$

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- A signal pair $(y(\cdot), u(\cdot))$ is an equilibrium if

$$\frac{d^k y}{dt^k}(t) = 0, \frac{d^k u}{dt^k}(t) = 0 \text{ for } k = 1, \dots, n \text{ and all times } t$$

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- Equilibria can be computed by solving the static equation

$$\ell(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u}) = 0$$

Example (pendulum)

- Consider the pendulum equation

$$M\ddot{\theta} + u \cos \theta + Mg \sin \theta = 0$$

where we think of θ as the output.

- Equilibria satisfy:

$$\bar{\theta}(t) = \bar{\theta} = \text{const.} \Rightarrow \ddot{\bar{\theta}} = 0$$

$$\bar{u}(t) = \bar{u} = \text{const.}$$

$$\bar{u} \cos \bar{\theta} + Mg \sin \bar{\theta} = 0$$

Example (pendulum)

- If we are interested only in equilibria with

$$\bar{u} = 0$$

then, we have

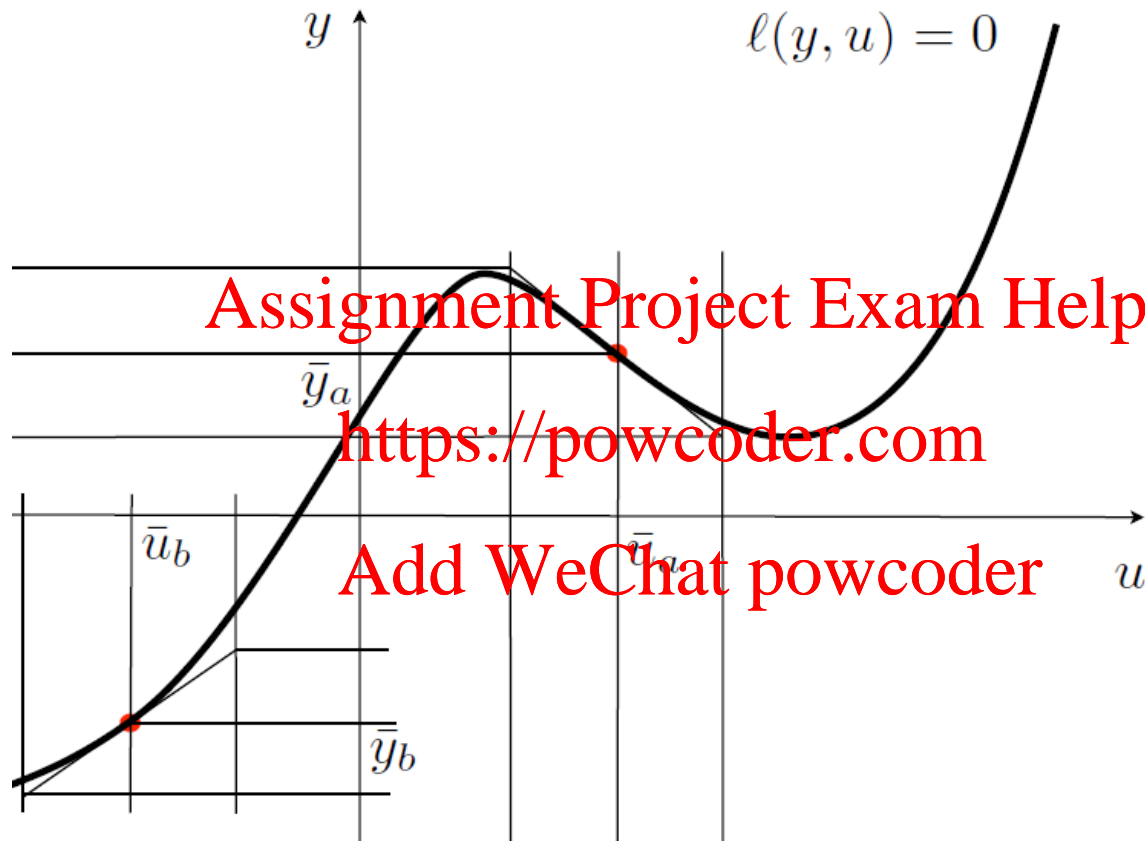
$$\{\bar{\theta} : \sin \bar{\theta} = 0\} = \{\bar{\theta} : \bar{\theta} = 2k\pi\}$$

- When mass is down: $(\bar{u}, \bar{\theta}) = (0, 0)$
- When mass is up: $(\bar{u}, \bar{\theta}) = (0, \pi)$

Why Think Linear?

- Often your plant model is already linear time-invariant (LTI).
- But sometimes, you'll get a nonlinear model
→ Difficult to fully analyse and control
- In the philosophy of starting simple, your first step should be to *linearise* the plant model around an equilibrium of interest.
- If disturbances are not too big, this will often yield satisfactory linear controller designs

Linearising a function



NOTE: linearisation of the same function around different points is different!

Comments:

- Linearizing a nonlinear function means approximating it **around a chosen operating point** by its tangent line
- Yields a good approximation valid near this point
- Linearisation is different around different points, because the tangent lines will be different

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Taylor series expansion

- To linearise a function near a point a , find its Taylor series

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$$f(x) = f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \frac{f'''(a)}{3!}(x-a)^3 + \dots$$

then ignore the 2nd and higher order terms

- Yields a good approximation for small deviation

$$\delta_x := x - a$$

Linearization

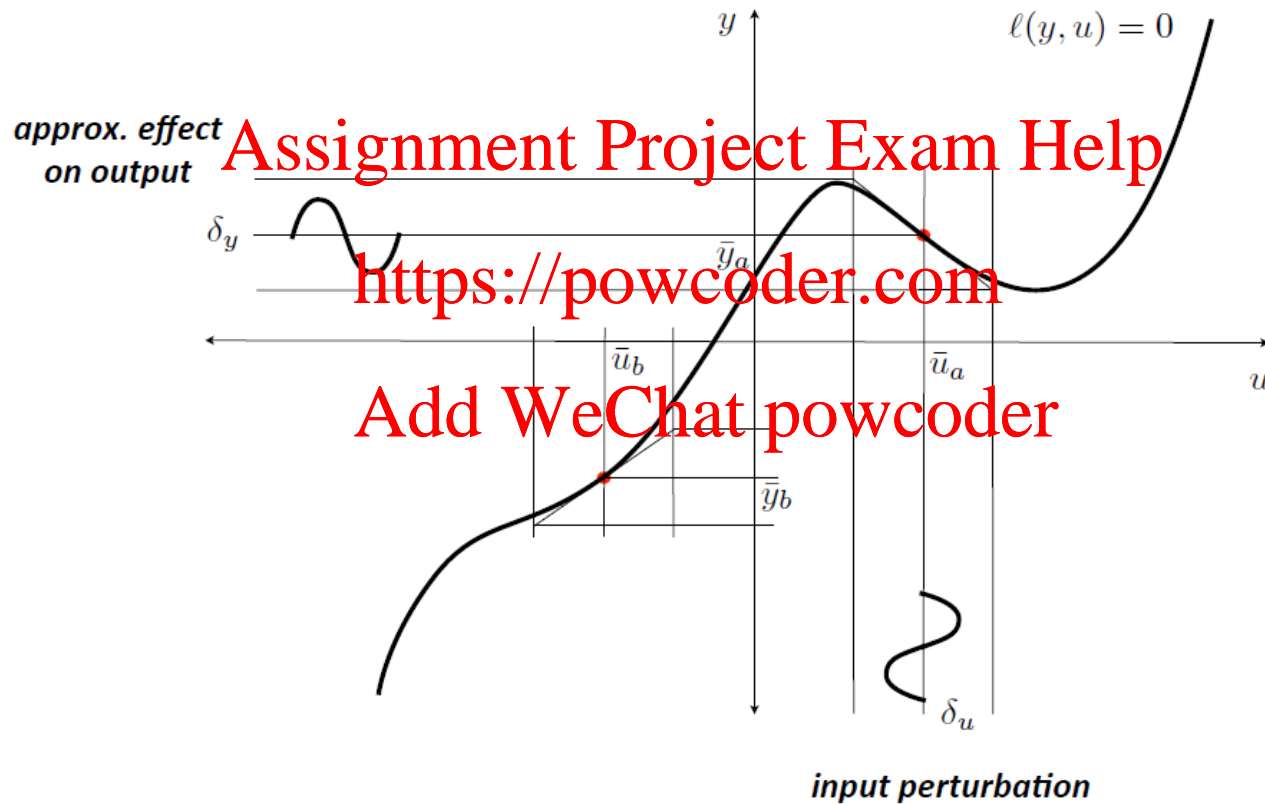
- Linearization of this function around $x=a$ is:

$$f(x) \approx f(a) + f'(a) \underbrace{(x-a)}_{\delta_x}$$

$$f(a) = 0 \Rightarrow f(x) \approx f'(a) \delta_x$$

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Graphical representation



Linearising a scalar (and static) input-output system

- Suppose output and input signals satisfy $l(y(t), u(t)) = 0$.
- We first select an equilibrium of interest (\bar{y}, \bar{u})
- Then find Taylor series around this equilibrium, keeping only 1st order terms

$$\underbrace{\ell(\bar{y}, \bar{u})}_{=0} + \left. \frac{\partial \ell}{\partial y} \right|_{(\bar{y}, \bar{u})} \delta_y + \left. \frac{\partial \ell}{\partial u} \right|_{(\bar{y}, \bar{u})} \delta_u = 0$$

$$\delta_u := u - \bar{u}; \quad \delta_y := y - \bar{y}$$

Linearised Scalar Static System

- Linearised model is

$$\delta_y = K \delta_u, \quad K := \frac{\frac{\partial \ell}{\partial u} \Big|_{(\bar{y}, \bar{u})}}{\frac{\partial \ell}{\partial y} \Big|_{(\bar{y}, \bar{u})}}$$

- Note that linearized model is different for different equilibria.
- Note that the following model is *affine*, not strictly linear:

$$y = Ku + c, \quad c \neq 0$$

Note: we assume that the derivative w.r.t. y does not vanish at equilibrium.

Multivariable Linearization

- We consider the multivariate function

$$\ell(y_n, \dots, y_1, y_0, u_n, \dots, u_1, u_0) = 0$$

(each subscript denotes time-derivative of that order in the relevant signal) <https://powcoder.com>

We find its 1st order Taylor series around

$$y_n = 0, \dots, y_1 = 0, y_0 = \bar{y}, u_n = 0, \dots, u_1 = 0, u_0 = \bar{u}$$

$$\begin{aligned} \ell_{\text{lin}}(y_n, \dots, y_1, y_0, u_n, \dots, u_1, u_0) \\ \doteq \ell(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u}) + \frac{\partial \ell}{\partial y_n} \Big|_{(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u})} (y_n - 0) + \dots + \frac{\partial \ell}{\partial y_0} \Big|_{(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u})} (y_0 - \bar{y}) \\ + \frac{\partial \ell}{\partial u_n} \Big|_{(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u})} (u_n - 0) + \dots + \frac{\partial \ell}{\partial u_0} \Big|_{(0, \dots, 0, \bar{y}, 0, \dots, 0, \bar{u})} (u_0 - \bar{u}) \end{aligned}$$

- This is a good approximation for small

$$y_n, \dots, (y_0 - \bar{y}), u_n, \dots, (u_0 - \bar{u})$$

- Linearized ODE is a map:

$$\delta_u = (u - \bar{u}) \mapsto \delta_y = (y - \bar{y})$$

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that is obtained by noting

$$\begin{aligned} \frac{d^k \delta_y}{dt^k} &= \frac{d^k y}{dt^k} \\ \frac{d^k \delta_u}{dt^k} &= \frac{d^k u}{dt^k} \end{aligned}$$

$$\ell_{\text{lin}}\left(\frac{d^n \delta_y}{dt^n}, \dots, \frac{d\delta_y}{dt}, (\delta_y + \bar{y}), \frac{d^n \delta_u}{dt^n}, \dots, \frac{d\delta_u}{dt}, (\delta_u + \bar{u})\right) = 0$$

Example (pendulum)

- From the differential equation, we see

$$\ell(\theta_2, \theta_1, \theta_0, u_0) = Ml\theta_2 + u_0 \cos \theta_0 + Mg \sin \theta_0$$

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- We linearise the function around an eq. $(\bar{u}, \bar{\theta})$

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$$\ell(\theta_2, \theta_1, \theta_0, u_0) = Ml\theta_2 + u_0 \cos \theta_0 + Mg \sin \theta_0$$

by definition

$$\approx \ell(0, 0, \bar{\theta}, \bar{u}) + \frac{\partial \ell}{\partial \theta_2} \Big|_{(0,0,\bar{\theta},\bar{u})} (\theta_2 - 0) + \frac{\partial \ell}{\partial \theta_1} \Big|_{(0,0,\bar{\theta},\bar{u})} (\theta_1 - 0)$$

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$$+ \frac{\partial \ell}{\partial \theta_0} \Big|_{(0,0,\bar{\theta},\bar{u})} (\theta_0 - \bar{\theta}) + \frac{\partial \ell}{\partial u_0} \Big|_{(0,0,\bar{\theta},\bar{u})} (u_0 - \bar{u})$$

$$= 0 + Ml(\theta_2 - 0) + 0(\theta_1 - 0) + (-\bar{u} \sin \bar{\theta} + Mg \cos \bar{\theta})(\theta_0 - \bar{\theta}) + \cos \bar{\theta} (u_0 - \bar{u})$$

$$= \ell_{\text{lin}}(\theta_2, \theta_1, \theta_0, u_0)$$

Example (pendulum)

- We define incremental input and output

$$\delta_u = u - \bar{u}, \quad \delta_\theta = \theta - \bar{\theta}, \quad \dot{\delta}_\theta = \dot{\theta} - \dot{\bar{\theta}}, \quad \ddot{\delta}_\theta = \ddot{\theta}$$

and obtain a linear incremental ODE model:

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$$M l \ddot{\delta}_\theta + (M g \cos \bar{\theta} - \bar{u} \sin \bar{\theta}) \delta_\theta + \cos \bar{\theta} \delta_u = 0$$

- Exercise: what are linearisations around

$$(\bar{u}, \bar{\theta}) = (0, 0) \quad \text{and} \quad (\bar{u}, \bar{\theta}) = (0, \pi)$$

Summary

- Equilibria can be obtained by solving an algebraic equation.
- A system can have multiple equilibria.
- The system can be approximated by a linear system around an equilibrium.
- Linearisation is different around different equilibria.

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