A generally applicable atomic-charge dependent London dispersion correction

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Part I: Additional theory, parameters, and timings

A. Classical partial charges

Classical electronegativity equilibration (EEQ) partial charges are determined by minimizing the following energy expression

$$E_{\text{IES}} = \sum_{i=1}^{N} \left(\chi_i q_i + \frac{1}{2} \left(J_{ii} + \frac{2\gamma_{ii}}{\sqrt{\pi}} \right) q_i^2 \right) + \frac{1}{2} \sum_{i=1}^{N} \sum_{\substack{j=1\\i \neq j}}^{N} q_i q_j \frac{\text{erf}(\gamma_{ij} R_{ij})}{R_{ij}}$$
(1)

where γ_{ij} is given as $(a_i^2 + a_j^2)^{-\frac{1}{2}}$ with a_i beeing the van der Waals radius of atom i. For a more compact representation we rewrite the above expression in matrix notation

$$E_{\rm IES} = \mathbf{q}^{\top} (\frac{1}{2} A \mathbf{q} - \mathbf{X}) \tag{2}$$

where we define the A matrix and the X vector by

$$X_{i} = -\chi_{i} \quad \text{and} \quad A_{ij} = \begin{cases} J_{ii} + \frac{\sqrt{2}\gamma_{ii}}{\sqrt{\pi}} & i = j\\ \frac{\text{erf}(\gamma_{ij}R_{ij})}{R_{ij}} & \text{otherwise} \end{cases}$$
(3)

Note that the choice of **X** is defined according to the work of Goedecker *et al.* in 2015 [1], and we keep the original notation to aid comparability. To obtain EEQ partial charges from this equations, under the constraint that the partial charges conserve the total charge q_{total} of the system, the method of constrained Lagrangian optimization is used as

$$L = E_{\text{IES}} + \lambda \left(\sum_{k=1}^{N} q_k - q_{\text{total}} \right) \quad \text{with} \quad \frac{\partial L}{\partial \mathbf{q}} = \mathbf{0} \ \land \ \frac{\partial L}{\partial \lambda} = \sum_{i=1}^{N} q_i - q_{\text{total}} = 0$$
 (4)

which leads to the following set of (N+1) linear equations

$$\begin{pmatrix} A & \mathbf{1} \\ \mathbf{1}^{\top} & 0 \end{pmatrix} \cdot \begin{pmatrix} \mathbf{q} \\ \lambda \end{pmatrix} = \begin{pmatrix} \mathbf{X} \\ q_{\text{total}} \end{pmatrix}$$
 (5)

In contrast to Goedecker's approach we determine χ_i not by a neural network but use a modified variant of the coordination number (mCN) similarly as in the DFT-D3 model [2]. For this EEQ charge model we suggest

$$\chi_i = EN_i - \kappa_i \sqrt{mCN_i}$$
 (6)

where EN_i is the electronegativity, κ_i is a scaling factor for the geometry dependency, and mCN_i is the coordination number defined as

$$\mathrm{mCN}_{i} = \sum_{\substack{j=1\\j\neq i}}^{N} \frac{1}{2} \cdot \left(1 + \mathrm{erf}\left(-k_{1} \cdot \left(\frac{R_{ij}}{R_{ij}^{\mathrm{cov}}} - 1 \right) \right) \right)$$
 (7)

where k_1 is an ad-hoc parameter which is set to 7.5 to reproduce the short range behaviour of the original DFT-D3 CN as close as possible while having a better long-range behaviour. $R_{ij}^{\text{cov}} = R_i^{\text{cov}} + R_j^{\text{cov}}$ are the covalent radii published by Pyykkö $et\ al.$ in 2010 [3] which are

used to be consistent with the DFT-D3 CN. As we arrived at a stationary point in the constrained optimization we can derive the expression needed to calculate the analytical partial charge derivative by

$$\frac{\partial L}{\partial q_k} = 0 \implies 0 = \frac{d}{d\mathbf{R}_j} \frac{\partial L}{\partial q_k} = \frac{\partial^2 L}{\partial q_k \partial \mathbf{R}_j} + \frac{\partial^2 L}{\partial q_k^2} \cdot \frac{\partial q_k}{\partial \mathbf{R}_j}
\iff \frac{\partial^2 L}{\partial q_k^2} \cdot \frac{\partial q_k}{\partial \mathbf{R}_j} = -\frac{\partial^2 L}{\partial q_k \partial \mathbf{R}_j}$$
(8)

Plugging in the expression for L from equation 4 we get

$$\frac{\partial^{2} L}{\partial \mathbf{R}_{j} \partial \mathbf{q}} = \begin{pmatrix} \frac{\partial A}{\partial \mathbf{R}_{j}} & \mathbf{0} \\ \mathbf{0}^{\top} & 0 \end{pmatrix} \cdot \begin{pmatrix} \mathbf{q} \\ \lambda \end{pmatrix} + \begin{pmatrix} A & \mathbf{1} \\ \mathbf{1}^{\top} & 0 \end{pmatrix} \cdot \begin{pmatrix} \frac{\partial \mathbf{q}}{\partial \mathbf{R}_{j}} \\ \frac{\partial \lambda}{\partial \mathbf{R}_{j}} \end{pmatrix} - \begin{pmatrix} \frac{\partial \mathbf{X}}{\partial \mathbf{R}_{j}} \\ 0 \end{pmatrix}$$
(9)

we do the same to obtain the electronic Hessian from equation 4

$$\frac{\partial^2 L}{\partial \mathbf{q}^2} = \begin{pmatrix} A & \mathbf{1} \\ \mathbf{1}^\top & 0 \end{pmatrix} \tag{10}$$

Plugging everything back into equation 8 we get

$$\begin{pmatrix}
\frac{\partial \mathbf{q}}{\partial \mathbf{R}_{j}} \\
\frac{\partial \lambda}{\partial \mathbf{R}_{j}}
\end{pmatrix} = \begin{pmatrix} A & \mathbf{1} \\ \mathbf{1}^{\top} & 0 \end{pmatrix}^{-1} \cdot \left(-\begin{pmatrix} \frac{\partial A}{\partial \mathbf{R}_{j}} & \mathbf{0} \\ \mathbf{0}^{\top} & 0 \end{pmatrix} \cdot \begin{pmatrix} \mathbf{q} \\ \lambda \end{pmatrix} + \begin{pmatrix} \frac{\partial \mathbf{X}}{\partial \mathbf{R}_{j}} \\ 0 \end{pmatrix} \right) \tag{11}$$

To invert the indefinite but symmetric (N+1) matrix we apply a Bunch–Kaufman factorization. Overall four parameter are fitted for each element i: EN_i , J_{ii} , κ_i , and a_i (namely the atomic electronegativity, atomic hardness terms, element specific scaling parameters, and atomic van der Waals radii).

Table A1: Atomic electronegativities EN, element-dependent atomic hardness terms J, element specific scaling parameters κ , and atomic van der Waals radii a for all elements up to radon (Z=86).

| Atomic number | EN_i | J_{ii} | κ_i | a_i |
|---------------|------------|-------------|-------------|------------|
| 1 | 1.23695041 | -0.35015861 | 0.04916110 | 0.55159092 |
| 2 | 1.26590957 | 1.04121227 | 0.10937243 | 0.66205886 |
| 3 | 0.54341808 | 0.09281243 | -0.12349591 | 0.90529132 |
| 4 | 0.99666991 | 0.09412380 | -0.02665108 | 1.51710827 |
| 5 | 1.26691604 | 0.26629137 | -0.02631658 | 2.86070364 |
| 6 | 1.40028282 | 0.19408787 | 0.06005196 | 1.88862966 |
| 7 | 1.55819364 | 0.05317918 | 0.09279548 | 1.32250290 |
| 8 | 1.56866440 | 0.03151644 | 0.11689703 | 1.23166285 |
| 9 | 1.57540015 | 0.32275132 | 0.15704746 | 1.77503721 |
| 10 | 1.15056627 | 1.30996037 | 0.07987901 | 1.11955204 |
| 11 | 0.55936220 | 0.24206510 | -0.10002962 | 1.28263182 |
| 12 | 0.72373742 | 0.04147733 | -0.07712863 | 1.22344336 |
| 13 | 1.12910844 | 0.11634126 | -0.02170561 | 1.70936266 |

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|-----------------|------------|-------------|-------------|------------|
| Atomic number | EN_i | J_{ii} | κ_i | a_i |
| 14 | 1.12306840 | 0.13155266 | -0.04964052 | 1.54075036 |
| 15 | 1.52672442 | 0.15350650 | 0.14250599 | 1.38200579 |
| 16 | 1.40768172 | 0.15250997 | 0.07126660 | 2.18849322 |
| 17 | 1.48154584 | 0.17523529 | 0.13682750 | 1.36779065 |
| 18 | 1.31062963 | 0.28774450 | 0.14877121 | 1.27039703 |
| 19 | 0.40374140 | 0.42937314 | -0.10219289 | 1.64466502 |
| 20 | 0.75442607 | 0.01896455 | -0.08979338 | 1.58859404 |
| 21 | 0.76482096 | 0.07179178 | -0.08273597 | 1.65357953 |
| 22 | 0.98457281 | -0.01121381 | -0.01754829 | 1.50021521 |
| 23 | 0.96702598 | -0.03093370 | -0.02765460 | 1.30104175 |
| 24 | 1.05266584 | 0.02716319 | -0.02558926 | 1.46301827 |
| 25 | 0.93274875 | -0.01843812 | -0.08010286 | 1.32928147 |
| 26 | 1.04025281 | -0.15270393 | -0.04163215 | 1.02766713 |
| 27 | 0.92738624 | -0.09192645 | -0.09369631 | 1.02291377 |
| 28 | 1.07419210 | -0.13418723 | -0.03774117 | 0.94343886 |
| 29 | 1.07900668 | -0.09861139 | -0.05759708 | 1.14881311 |
| 30 | 1.04712861 | 0.18338109 | 0.02431998 | 1.47080755 |
| 31 | 1.15018618 | 0.08299615 | -0.01056270 | 1.76901636 |
| 32 | 1.15388455 | 0.11370033 | -0.02692862 | 1.98724061 |
| 33 | 1.36313743 | 0.19005278 | 0.07657769 | 2.41244711 |
| 34 | 1.36485106 | 0.10980677 | 0.06561608 | 2.26739524 |
| 35 | 1.39801837 | 0.12327841 | 0.08006749 | 2.95378999 |
| 36 | 1.18695346 | 0.25345554 | 0.14139200 | 1.20807752 |
| 37 | 0.36273870 | 0.58615231 | -0.05351029 | 1.65941046 |
| 38 | 0.58797255 | 0.16093861 | -0.06701705 | 1.62733880 |
| 39 | 0.71961946 | 0.04548530 | -0.07377246 | 1.61344972 |
| 40 | 0.96158233 | -0.02478645 | -0.02927768 | 1.63220728 |
| 41 | 0.89585296 | 0.01909943 | -0.03867291 | 1.60899928 |
| 42 | 0.81360499 | 0.01402541 | -0.06929825 | 1.43501286 |
| 43 | 1.00794665 | -0.03595279 | -0.04485293 | 1.54559205 |
| 44 | 0.92613682 | 0.01137752 | -0.04800824 | 1.32663678 |
| 45 | 1.09152285 | -0.03697213 | -0.01484022 | 1.37644152 |
| 46 | 1.14907070 | 0.08009416 | 0.07917502 | 1.36051851 |
| 47 | 1.13508911 | 0.02274892 | 0.06619243 | 1.23395526 |
| 48 | 1.08853785 | 0.12801822 | 0.02434095 | 1.65734544 |
| 49 | 1.11005982 | -0.02078702 | -0.01505548 | 1.53895240 |
| 50 | 1.12452195 | 0.05284319 | -0.03030768 | 1.97542736 |
| 51 | 1.21642129 | 0.07581190 | 0.01418235 | 1.97636542 |
| 52 | 1.36507125 | 0.09663758 | 0.08953411 | 2.05432381 |
| 53 | 1.40340000 | 0.09547417 | 0.08967527 | 3.80138135 |
| 54 | 1.16653482 | 0.07803344 | 0.07277771 | 1.43893803 |
| 55 | 0.34125098 | 0.64913257 | -0.02129476 | 1.75505957 |
| 56 | 0.58884173 | 0.15348654 | -0.06188828 | 1.59815118 |
| 57 | 0.68441115 | 0.05054344 | -0.06568203 | 1.76401732 |
| | | | | |

Table A1: Atomic electronegativities EN, element-dependent atomic hardness terms J, element specific scaling parameters κ , and atomic van der Waals radii a for all elements up to radon (Z=86).

| Atomic number | EN_i | J_{ii} | κ_i | a_i |
|---------------|------------|-------------|-------------|------------|
| 58 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 59 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 60 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 61 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 62 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 63 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 64 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 65 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 66 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 67 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 68 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 69 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 70 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 71 | 0.56999999 | 0.11000000 | -0.11000000 | 1.63999999 |
| 72 | 0.87936784 | -0.02786741 | -0.03585873 | 1.47055223 |
| 73 | 1.02761808 | 0.01057858 | -0.03132400 | 1.81127084 |
| 74 | 0.93297476 | -0.03892226 | -0.05902379 | 1.40189963 |
| 75 | 1.10172128 | -0.04574364 | -0.02827592 | 1.54015481 |
| 76 | 0.97350071 | -0.03874080 | -0.07606260 | 1.33721475 |
| 77 | 1.16695666 | -0.03782372 | -0.02123839 | 1.57165422 |
| 78 | 1.23997927 | -0.07046855 | 0.03814822 | 1.04815857 |
| 79 | 1.18464453 | 0.09546597 | 0.02146834 | 1.78342098 |
| 80 | 1.14191734 | 0.21953269 | 0.01580538 | 2.79106396 |
| 81 | 1.12334192 | 0.02522348 | -0.00894298 | 1.78160840 |
| 82 | 1.01485321 | 0.15263050 | -0.05864876 | 2.47588882 |
| 83 | 1.12950808 | 0.08042611 | -0.01817842 | 2.37670734 |
| 84 | 1.30804834 | 0.01878626 | 0.07721851 | 1.76613217 |
| 85 | 1.33689961 | 0.08715453 | 0.07936083 | 2.66172302 |
| 86 | 1.27465977 | 0.10500484 | 0.05849285 | 2.82773085 |

The quality of those classical partial charges can be seen in Figure 1 and in Figure 2 where we correlate PBE0/def2-TZVP Hirshfeld partial charges with classical EEQ charges and with GFN2-xTB charges. As can be seen from the Table A2, GFN2-xTB converges in some cases to the wrong electronic solution, so that huge deviations can occur (maximum deviation is 19.92 e⁻). The EEQ model on the other hand proves to be quite robust and can convince with a maximum deviation of $0.56~{\rm e^-}$ on more than 20000 calculated data points for the Z=1-86 case.

Table A2: Statistical measures calculated for the comparison between calculated partial charges and reference PBE0/def2-TZVP Hirshfeld partial charges. Deviations are given in e⁻.

| Measure | EEQ(Z = 1 - 86) | GFN2-xTB(Z = 1 - 86) | EEQ(Z = 1 - 17) | GFN2-xTB(Z = 1 - 17) |
|---------|-----------------|----------------------|-----------------|----------------------|
| MAD | 0.04 | 0.13 | 0.03 | 0.18 |
| MD | 0.00 | 0.00 | 0.00 | -0.01 |
| SD | 0.06 | 0.36 | 0.05 | 0.65 |
| AMAX | 0.56 | 19.27 | 0.33 | 19.92 |

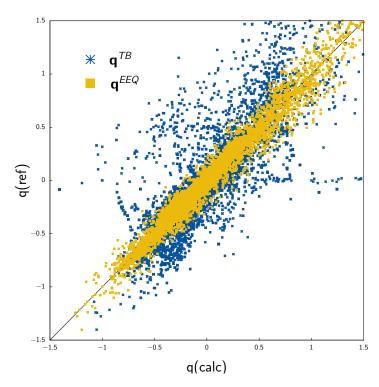


Figure 1: EEQ versus GFN2-xTB partial charges in direct correlation with Hirshfeld partial charges calculated at the PBE0/def2-TZVP level of theory for all elements with Z=1-86.

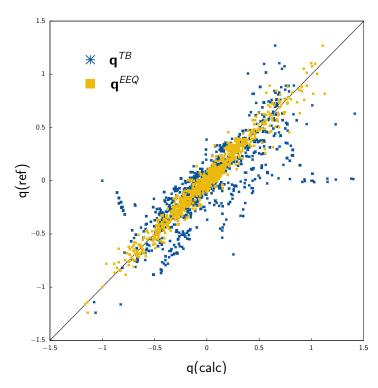


Figure 2: EEQ versus GFN2-xTB partial charges in direct correlation with Hirshfeld partial charges calculated at the PBE0/def2-TZVP level of theory for all elements with Z=1-17 (excluding helium and neon).

B. Many-body dispersion theory

Tkatchenko et al. [4] have shown that the dispersion energy can be written as

$$E_{\text{disp}}^{(n),MBD} = \int_{0}^{\infty} \frac{d\omega}{2\pi} \operatorname{Tr} \left\{ \ln \left(\mathbf{1} - \mathbf{A}(i\omega) \mathbf{T} \right) \right\}, \tag{12}$$

when neglecting intra-oscillator interactions [5] within the matrix formulation ($\operatorname{Tr} \{ \mathbf{A}(i\omega) \mathbf{T} \} = 0$). In DFT-D4, the frequency-dependent polarizability matrix $\mathbf{A}(i\omega)$ is obtained from the previously generated atom-in-molecule dynamic polarizabilities

$$A_{KP}^{\beta\gamma}(i\omega) = \alpha^K(i\omega)\delta_{KP}\delta_{\gamma\beta}$$

= $\alpha^K(i\omega, z^K, CN^K)\delta_{KP}\delta_{\gamma\beta}.$ (13)

In equation 13, K and P label atoms, and β and γ refer to the Cartesian components of their internuclear distance. The use of D4 atom-in-molecule dynamic polarizabilities offers advantages. Different from the TS-based polarizabilites, the D4 polarizabilites already contain information about the molecular environment and no self-consistent screening needs to be performed, which can jeopardize the stability of the method [6]. The generation of the D4 polarizabilities is simple and robust, since only the geometry and atomic partial charges are needed and no additional information from DFT is required. \mathbf{T} is the interaction tensor describing the coupling between the oscillators. The matrix elements of the damped interaction tensor \mathbf{T} are given by

$$T_{KP}^{\beta\gamma} = \sqrt{f_{\rm BJD}^{(6)}} \frac{\partial}{\partial R_{KP}^{\beta}} \frac{\partial}{\partial R_{KP}^{\gamma}} \left(\frac{1}{R_{KP}}\right). \tag{14}$$

It should be noted that the BJ-damping function is used here as well to screen the elements of the tensor. A motivation for this choice is given below. The MBD energy can be viewed as a series of n-body dipole-dipole terms, and hence, the n-body energy can be obtained directly via a Casimir-Polder similar integration of the coupled atom-in-molecule polarizabilities. Because the contributions of the terms in the series tend to oscillate and it converges slowly with n, the value of the limit of the series is used here as computed in equation 12. The astute reader will note that the evaluation of the logarithmic trace in equation 12 is not directly possible since the product $\mathbf{A}(i\omega)\mathbf{T}$ is a trace-less matrix. To obtain the logarithmic trace, the matrix created by subtraction $(\mathbf{1} - \mathbf{A}(i\omega)\mathbf{T})$ is diagonalized and the sum of the eigenvalues is used to calculate all many-body dispersion terms. Furthermore, splitting the diagonal polarizability matrix $\mathbf{A}(i\omega)$ into the product of its square roots, which is possible due to the invariance regarding cyclic permutation, simplifies the problem to symmetrical matrices only, which makes the calculation of eigenvalues much simpler

$$\left(\mathbf{1} - \mathbf{A}^{1/2}(i\omega)\mathbf{T}\mathbf{A}^{1/2}(i\omega)\right)\mathbf{U} = \mathbf{U}\boldsymbol{\Lambda}.$$
 (15)

Here, Λ represents the matrix of eigenvalues with elements λ . The eigenvalues are then used analogously to equation 12, and hence the final expression for the MBD energy reads

$$E_{disp}^{(n),MBD} = \int_{0}^{\infty} \frac{d\omega}{2\pi} \ln\left(\prod_{l=1}^{3N} \lambda_l\right). \tag{16}$$

Semi-local DFAs already include short-ranged electron correlation within the exchange-correlation functional. Along with avoiding singularities, this is why the dispersion energy is always damped

at short range. Likewise, the interaction tensor in the MBD model needs to be damped. Ideally, the second order term of the MBD energy should be exactly equivalent to the D4 two-body dipole-dipole energy, i.e.,

$$E_{\text{disp}}^{(6),MBD} = -\int_{0}^{\infty} \frac{d\omega}{2\pi} \operatorname{Tr} \left\{ \frac{1}{2} \left(\mathbf{A}(i\omega) \mathbf{T} \right)^{2} \right\}$$

$$= -\int_{0}^{\infty} \frac{d\omega}{2\pi} \frac{1}{2} \sum_{K}^{N} \sum_{P}^{N} \frac{\alpha^{K}(i\omega)\alpha^{P}(i\omega)}{R_{KP}^{10}} f_{damp}^{2}$$

$$\times \sum_{\beta}^{3} \sum_{\gamma}^{3} \left(3R_{KP}^{\beta} R_{KP}^{\gamma} - \delta_{\beta\gamma} R_{KP}^{2} \right)^{2}$$

$$= -\frac{1}{2} \sum_{K}^{N} \sum_{P}^{N} \frac{C_{6}^{KP}}{R_{KP}^{6}} f_{damp}^{2}$$

$$\stackrel{!}{=} -\frac{1}{2} \sum_{K}^{N} \sum_{P}^{N} \frac{C_{6}^{KP}}{R_{KP}^{6}} f_{BJD}^{(6)} = E_{disp}^{(6)}.$$
(17)

Hence, the square root of the BJ-damping function is used to damp the MBD interaction tensor. Nevertheless, it should be noted that for higher interaction orders (higher exponentiation of f_{damp}), the respective MBD energy contributions become damped more strongly also in the mid-range distance regime. However, this peculiarity is considered to be small, since the higher-order (n > 2) MBD energies represent a smaller fraction of the total dispersion energy (usually one to two magnitudes less than two-body contributions).

The final D4-MBD dispersion energy expression consists of two parts. The first compose the two-body dipole-dipole and dipole-quadrupole interaction (denoted as $E_{disp}^{(6,8)}$). The second part includes all dipole-dipole interactions up to infinite order, $E_{disp}^{(n),MBD}$ ($n=6,9,12,15,\ldots,\infty$). To avoid double counting of the two-body dipole-dipole energy, it is removed explicitly from the MBD energy according to

$$E_{disp}^{D4-MBD} = E_{disp}^{(6,8)} + \left(E_{disp}^{(n),MBD} - E_{disp}^{(6),MBD}\right). \tag{18}$$

Exploiting that $E_{disp}^{(6)} = E_{disp}^{(6),MBD}$ and re-arranging to $E_{disp}^{D4-MBD} = E_{disp}^{(n),MBD} + E_{disp}^{(8)}$ is not possible in the general case, as for double hybrid density functionals (abbreviated as DHDF) $s_6 \neq 1$, whereas this scaling cannot be applied to an individual term in the infinite-order MBD energy. Hence, the dispersion energy in DFT-D4-MBD is always calculated as shown in Eq. 18.

Similar to Figure 16 of Ref.[7], the contributions to the dispersion energy considered in D4 are put into context with other correction schemes in Figure 3.

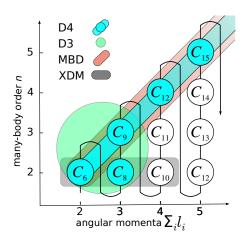


Figure 3: Asymptotic dispersion coefficients from different many-body orders and increasing number of terms in the multipole expansion. The contributions covered by the D3 (including ATM term), D4-MBD, MBD, and XDM methods are highlighted. This Figure is generated in analogy to Figure 16 in Ref.[7].

C. Tight-binding two-body dispersion potential (GFN2-xTB)

We developed the GFN2-xTB dispersion potential in terms of density fluctuations (see Ref. [8])

$$\frac{\partial}{\partial c_{\nu i}} \left[E_{\text{disp}}^{(6,8)} - \sum_{j} n_{j} \varepsilon_{j} \left(\sum_{A,B} \sum_{\kappa \in A} \sum_{\lambda \in B} c_{\kappa j} c_{\lambda j} S_{\kappa \lambda} - 1 \right) \right] = 0$$

Take the derivative of $E_{disp}^{(6,8)}$ with respect to the AO coefficient

$$\begin{split} & \frac{\partial E_{\text{disp}}^{(l)ap}}{\partial c_{\text{tot}}} = \frac{\partial}{\partial c_{\text{tot}}} \frac{1}{2} \sum_{A} \sum_{A, \text{ref}}^{A, \text{ref}} \sum_{B} \sum_{B, \text{ref}}^{B, \text{ref}} \frac{\zeta(z^{A}, z^{A, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{B}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{B}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{B}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{A}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref}})}{\zeta_{B}^{B, \text{ref}}} \frac{\zeta(z^{B}, z^{B, \text{ref$$

Which leads to the two-body DFT-D4 potential used within the GFN2-xTB method

$$F_{\kappa\lambda}^{\mathrm{D4}} = \frac{1}{2} S_{\kappa\lambda} (d_A + d_B), \forall \kappa \in A, \lambda \in B$$

D. Double hybrid density functionals

In the following we give the construction scheme to build the double hybrid density functionals (DHDF) as

$$E_{\rm DHDF} = (1 - a_x^{\rm Fock}) E_x^{\rm DFT} + a_x^{\rm Fock} + a_c^{\rm DFT} E_c^{\rm DFT} + a_c^{\rm PT2,\,OS} E_{c,\rm OS}^{\rm PT2} + a_c^{\rm PT2,\,SS} E_{c,\rm SS}^{\rm PT2}.$$

Table A3: Double hybrid functional definitions as given in the literature.

| Name | Exchange | Correlation | a_x^{Fock} | a_c^{DFT} | $a_c^{\mathrm{PT2,OS}}$ | $a_c^{\mathrm{PT2,SS}}$ | Ref. |
|------------|----------|-------------|-----------------------|----------------------|-------------------------|-------------------------|------|
| B2PLYP | B88 | LYP | 0.5300 | 0.7300 | 0.2700 | 0.2700 | [9] |
| mPW2PLYP | mPW | LYP | 0.5500 | 0.7500 | 0.2500 | 0.2500 | [10] |
| PWPB95 | PW | B95 | 0.5000 | 0.7310 | 0.2690 | 0.0000 | [11] |
| DSD-BLYP | B88 | LYP | 0.6900 | 0.5400 | 0.4600 | 0.3700 | [12] |
| DSD-PBE | PBE | PBE | 0.6800 | 0.4900 | 0.5500 | 0.1300 | [13] |
| DSD-PBEB95 | PBE | B95 | 0.6600 | 0.5500 | 0.4600 | 0.0900 | [13] |
| DSD-PBEP86 | PBE | P86 | 0.7000 | 0.4300 | 0.5300 | 0.2500 | [13] |
| DSD-SVWN | Slater | VWN5 | 0.7200 | 0.3300 | 0.5900 | 0.1200 | [13] |
| DOD-BLYP | B88 | LYP | 0.6500 | 0.5800 | 0.5300 | 0.0000 | [13] |
| DOD-PBE | PBE | PBE | 0.6400 | 0.5400 | 0.4200 | 0.0000 | [13] |
| DOD-PBEB95 | PBE | B95 | 0.6400 | 0.5700 | 0.4600 | 0.0000 | [13] |
| DOD-PBEP86 | PBE | P86 | 0.6500 | 0.4700 | 0.5400 | 0.0000 | [13] |
| DOD-SVWN | Slater | VWN5 | 0.6900 | 0.3400 | 0.5800 | 0.0000 | [13] |
| PBE0-2 | PBE | PBE | 0.7937 | 0.5000 | 0.5000 | 0.5000 | [14] |
| PBE0-DH | PBE | PBE | 0.5000 | 0.8750 | 0.1250 | 0.1250 | [15] |

Within this section we neglect explicit notation for EEQ charges and denote GFN2-xTB Mulliken-type charges as "TB".

E. BJ-damping parameters

Different parametrizations are created for the application of either ATM or MBD for higher-order dipole-dipole interactions within the DFT-D4 treatment.

Table A4: BJ-damping parameter (DFT-D4-ATM, **default model** also abbreviated as DFT-D4) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| DFA | s_6 | s_8 | a_1 | a_2 |
|-----------------|--------|--------------|--------------|--------------|
| B1B95 | 1.0000 | 1.27701162 | 0.40554715 | 4.63323074 |
| B1LYP | 1.0000 | 1.98553711 | 0.39309040 | 4.55465145 |
| B1P | 1.0000 | 3.36115015 | 0.48665293 | 5.05219572 |
| B1PW | 1.0000 | 3.02227550 | 0.47396846 | 4.49845309 |
| B2PLYP | 0.6400 | 1.16888646 | 0.44154604 | 4.73114642 |
| B3LYP | 1.0000 | 2.02929367 | 0.40868035 | 4.53807137 |
| B3P | 1.0000 | 3.08822155 | 0.47324238 | 4.98682134 |
| B3PW | 1.0000 | 2.88364295 | 0.46990860 | 4.51641422 |
| B97 | 1.0000 | 0.87854260 | 0.29319126 | 4.51647719 |
| BHLYP | 1.0000 | 1.65281646 | 0.27263660 | 5.48634586 |
| BLYP | 1.0000 | 2.34076671 | 0.44488865 | 4.09330090 |
| BPBE | 1.0000 | 3.64405246 | 0.52905620 | 4.11311891 |
| BP | 1.0000 | 3.35497927 | 0.43645861 | 4.92406854 |
| BPW | 1.0000 | 3.24571506 | 0.50050454 | 4.12346483 |
| CAMB3LYP | 1.0000 | 1.66041301 | 0.40267156 | 5.17432195 |
| DODBLYP | 0.4700 | 1.31146043 | 0.43407294 | 4.27914360 |
| DODPBEB95 | 0.5600 | 0.01574635 | 0.43745720 | 3.69180763 |
| DODPBE | 0.4800 | 0.92051454 | 0.43037052 | 4.38067238 |
| DODPBEP86 | 0.4600 | 0.71405681 | 0.42408665 | 4.52884439 |
| DODSVWN | 0.4200 | 0.94500207 | 0.47449026 | 5.05316093 |
| DSDBLYP | 0.5400 | 0.63018237 | 0.47591835 | 4.73713781 |
| DSDPBEB95 | 0.5400 | -0.14668670 | 0.46394587 | 3.64913860 |
| DSDPBE | 0.4500 | 0.70584116 | 0.45787085 | 4.44566742 |
| DSDPBEP86 | 0.4700 | 0.37586675 | 0.53698768 | 5.13022435 |
| DSDSVWN | 0.4100 | 0.72914436 | 0.51347412 | 5.11858541 |
| GLYP | 1.0000 | 4.23798924 | 0.38426465 | 4.38412863 |
| $_{ m HF}$ | 1.0000 | 1.61679827 | 0.44959224 | 3.35743605 |
| LB94 | 1.0000 | 2.59538499 | 0.42088944 | 3.28193223 |
| LCBLYP | 1.0000 | 1.60344180 | 0.45769839 | 7.86924893 |
| Lh07s-SVWN | 1.0000 | 3.16675531 | 0.35965552 | 4.31947614 |
| Lh07t-SVWN | 1.0000 | 2.09333001 | 0.35025189 | 4.34166515 |
| Lh12ct-SsifPW92 | 1.0000 | 2.684 676 10 | 0.341 904 16 | 3.910 396 66 |
| Lh12ct-SsirPW92 | 1.0000 | 2.48973402 | 0.34026075 | 3.969 480 81 |
| Lh14t-calPBE | 1.0000 | 1.28130770 | 0.38822021 | 4.92501211 |
| M06 | 1.0000 | 0.16366729 | 0.53456413 | 6.06192174 |

Table A4: BJ-damping parameter (DFT-D4-ATM, **default model** also abbreviated as DFT-D4) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| DFA | s_6 | s_8 | a_1 | a_2 |
|---------------------------------|--------|--------------|------------|--------------|
| M06L | 1.0000 | 0.59493760 | 0.71422359 | 6.35314182 |
| mPW1B95 | 1.0000 | 0.50093024 | 0.41585097 | 4.991 548 69 |
| mPW1LYP | 1.0000 | 1.155 911 53 | 0.25603493 | 5.320 838 95 |
| mPW1PW | 1.0000 | 1.808 417 16 | 0.42961819 | 4.68892341 |
| mPW2PLYP | 0.7500 | 0.45788846 | 0.42997704 | 5.07650682 |
| mPWB1K | 1.0000 | 0.57338313 | 0.44687975 | 5.21266777 |
| mPWLYP | 1.0000 | 1.25842942 | 0.25773894 | 5.02319542 |
| mPWPW | 1.0000 | 1.82596836 | 0.34526745 | 4.84620734 |
| O3LYP | 1.0000 | 1.75762508 | 0.10348980 | 6.16233282 |
| OLYP | 1.0000 | 2.74836820 | 0.60184498 | 2.53292167 |
| OPBE | 1.0000 | 3.06917417 | 0.68267534 | 2.22849018 |
| PBE0-2 | 0.5000 | 0.64299082 | 0.76542115 | 5.78578675 |
| PBE0 | 1.0000 | 1.20065498 | 0.40085597 | 5.02928789 |
| PBE0-DH | 0.8750 | 0.96811578 | 0.47592488 | 5.08622873 |
| PBE | 1.0000 | 0.95948085 | 0.38574991 | 4.80688534 |
| PW1PW | 1.0000 | 0.96850170 | 0.42427511 | 5.02060636 |
| PW6B95 | 1.0000 | -0.31926054 | 0.04142919 | 5.84655608 |
| PW86PBE | 1.0000 | 1.21362856 | 0.40510366 | 4.66737724 |
| PW91 | 1.0000 | 0.77283111 | 0.39581542 | 4.93405761 |
| PWP1 | 1.0000 | 0.60492565 | 0.46855837 | 5.76921413 |
| PWPB95 | 0.8200 | -0.34639127 | 0.41080636 | 3.83878274 |
| PWP | 1.0000 | 0.32801227 | 0.35874687 | 6.05861168 |
| revPBE0 | 1.0000 | 1.57185414 | 0.38705966 | 4.11028876 |
| revPBE0-DH | 0.8750 | 1.24456037 | 0.36730560 | 4.71126482 |
| revPBE38 | 1.0000 | 1.66597472 | 0.39476833 | 4.39026628 |
| revPBE | 1.0000 | 1.74676530 | 0.53634900 | 3.07261485 |
| revTPSS0 | 1.0000 | 1.54664499 | 0.45890964 | 4.78426405 |
| revTPSS | 1.0000 | 1.53089454 | 0.44880597 | 4.64042317 |
| revTPSSH | 1.0000 | 1.52740307 | 0.45161957 | 4.70779483 |
| RPBE | 1.0000 | 1.31183787 | 0.46169493 | 3.15711757 |
| RPW86PBE | 1.0000 | 1.12624034 | 0.38151218 | 4.75480472 |
| SCAN | 1.0000 | 1.46126056 | 0.62930855 | 6.31284039 |
| TPSS0 | 1.0000 | 1.62438102 | 0.40329022 | 4.80537871 |
| TPSS | 1.0000 | 1.76596355 | 0.42822303 | 4.54257102 |
| TPSSH | 1.0000 | 1.85897750 | 0.44286966 | 4.60230534 |
| $\omega \mathrm{B}97$ | 1.0000 | 6.55792598 | 0.76666802 | 8.36027334 |
| $\omega \mathrm{B}97\mathrm{X}$ | 1.0000 | -0.07519516 | 0.45094893 | 6.78425255 |
| X3LYP | 1.0000 | 1.54701429 | 0.20318443 | 5.61852648 |
| XLYP | 1.0000 | 1.62972054 | 0.11268673 | 5.40786417 |

Table A5: BJ-damping parameter (DFT-D4-MBD) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| | ` - | 0], 522x3 [17], NCID | • • • • | |
|-------------------------------|------------------|----------------------------|----------------------------|-------------------------|
| DFA | s_6 | s_8 | a_1 | a_2 |
| B1B95 | 1.0000 | 1.19549420 | 0.39241474 | 4.60397611 |
| B1LYP | 1.0000 | 1.94609514 | 0.38643351 | 4.54135968 |
| B1P | 1.0000 | 3.38693011 | 0.48478615 | 5.04361224 |
| B1PW | 1.0000 | 2.98402204 | 0.46862950 | 4.48637849 |
| B2PLYP | 0.6400 | 1.15117773 | 0.42666167 | 4.73635790 |
| B3LYP | 1.0000 | 2.00246246 | 0.40276191 | 4.52778320 |
| B3P | 1.0000 | 3.14456298 | 0.47187947 | 4.98624258 |
| B3PW | 1.0000 | 2.85656268 | 0.46491801 | 4.50601452 |
| B97 | 1.0000 | 0.81171211 | 0.28461283 | 4.48691468 |
| BHLYP | 1.0000 | 1.68082973 | 0.26835837 | 5.48847218 |
| BLYP | 1.0000 | 2.33971306 | 0.44733688 | 4.06583931 |
| BPBE | 1.0000 | 3.65322996 | 0.49933501 | 4.24294852 |
| BP | 1.0000 | 3.33728176 | 0.43220330 | 4.91443061 |
| BPW | 1.0000 | 3.23137432 | 0.49955226 | 4.10411084 |
| CAMB3LYP | 1.0000 | 1.74407961 | 0.40137870 | 5.18731225 |
| DODBLYP | 0.4700 | 1.17809956 | 0.40252428 | 4.25096555 |
| DODPBEB95 | 0.5400 | -0.15702803 | 0.30629389 | 3.69170956 |
| DODPBE | 0.4800 | 0.83908332 | 0.40655901 | 4.33601239 |
| DODPBEP86 | 0.4600 | 0.68309910 | 0.40600975 | 4.50011772 |
| DODSVWN | 0.4200 | 1.01890345 | 0.46167459 | 5.11121382 |
| DSDBLYP | 0.5400 | 0.65438817 | 0.46549574 | 4.73449899 |
| DSDPBEB95 | 0.5400 | -0.24336862 | 0.32697409 | 3.69767540 |
| DSDPBE | 0.4500 | 0.66116783 | 0.43565915 | 4.41110670 |
| DSDPBEP86 | 0.4700 | 0.51157821 | 0.53889789 | 5.18645943 |
| DSDSVWN | 0.4100 | 0.900 844 57 | 0.51106529 | 5.224 901 48 |
| GLYP | 1.0000 | 3.838 615 84 | 0.36343954 | 4.328 751 83 |
| HF | 1.0000 | 1.460 011 46 | 0.431 869 01 | 3.341 160 14 |
| LB94 | 1.0000 | 2.364 615 24 | 0.415 183 79 | 3.193 654 71 |
| LCBLYP | 1.0000 | 2.401 099 62 | 0.478 674 38 | 8.010 384 24 |
| Lh07s-SVWN | 1.0000 | 2.924 984 06 | 0.34173988 | 4.284 049 51 |
| Lh07t-SVWN | 1.0000 | 1.953 893 00 | 0.335 115 15 | 4.318 539 58 |
| Lh12ct-SsifPW92 | 1.0000 | 2.413 566 07 | 0.313 913 16 | 3.889 357 69 |
| Lh12ct-SsirPW92 | 1.0000 | 2.249 171 62 | 0.31446575 | 3.950 709 25 |
| Lh14t-calPBE | 1.0000 | 1.27677253 | 0.381 286 70 | 4.916 988 83 |
| M06 | 1.0000 | 0.229 482 74 | $0.52927285 \ 0.69611405$ | 6.065 167 82 |
| M06L | 1.0000 | 0.40077779 | | 6.290 920 87 |
| ${ m mPW1B95} \ { m mPW1LYP}$ | 1.0000 | $0.53791835 \\ 1.19986100$ | $0.41016913 \\ 0.25502469$ | 4.99284176 5.32301304 |
| mPW1PW | 1.0000 | 1.80656973 | 0.25502409 0.42456967 | 4.68132317 |
| mPW2PLYP | 1.0000 0.7500 | 0.611 611 79 | 0.42430907 0.43748316 | 5.125 403 64 |
| mPWB1K | | 0.62221146 | 0.43746316 0.44216745 | 5.213 246 59 |
| mPWLYP | 1.0000 1.0000 | 1.18243337 | 0.44210745 0.38968985 | 4.30835285 |
| mPWPW | 1.0000 | 1.79674014 | 0.33870479 | 4.834 422 13 |
| O3LYP | 1.0000 | 1.79074014 1.77793802 | 0.099 617 45 | 6.16089304 |
| OLYP | 1.0000 | 2.58717041 | 0.59759271 | 2.48760353 |
| OLII | 1.0000 | 2.00111041 | 0.001 002 11 | 2.401 000 00 |

Table A5: BJ-damping parameter (DFT-D4-MBD) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| DFA | s_6 | s_8 | a_1 | a_2 |
|---------------------------------|--------|-------------|------------|------------|
| OPBE | 1.0000 | 2.93544102 | 0.67903933 | 2.19810071 |
| PBE0-2 | 0.5000 | 0.98834859 | 0.77911062 | 5.90389569 |
| PBE0 | 1.0000 | 1.26829475 | 0.39907098 | 5.03951304 |
| PBE0-DH | 0.8750 | 1.19306002 | 0.46106784 | 5.25210480 |
| PBE | 1.0000 | 0.99924614 | 0.38142528 | 4.81839284 |
| PW1PW | 1.0000 | 1.09759050 | 0.42759830 | 5.04559572 |
| PW6B95 | 1.0000 | -0.31629935 | 0.03999357 | 5.83690254 |
| PW86PBE | 1.0000 | 1.22842987 | 0.39998824 | 4.66739111 |
| PW91 | 1.0000 | 0.81406882 | 0.34094706 | 5.18568823 |
| PWP1 | 1.0000 | 0.95936222 | 0.48552982 | 5.84956411 |
| PWPB95 | 0.8200 | -0.46453780 | 0.29884136 | 3.87641255 |
| PWP | 1.0000 | 0.66056055 | 0.37768052 | 6.14787138 |
| revPBE0 | 1.0000 | 1.47198256 | 0.37471756 | 4.08904369 |
| revPBE0-DH | 0.8750 | 1.22494188 | 0.35904781 | 4.70216012 |
| revPBE38 | 1.0000 | 1.60423529 | 0.38938475 | 4.35557832 |
| revPBE | 1.0000 | 1.62543693 | 0.54031831 | 2.97965648 |
| revTPSS0 | 1.0000 | 1.55321888 | 0.45355319 | 4.77588598 |
| revTPSS | 1.0000 | 1.51858035 | 0.44243222 | 4.62881620 |
| revTPSSH | 1.0000 | 1.52542064 | 0.44570207 | 4.69883717 |
| RPBE | 1.0000 | 1.11793696 | 0.44632488 | 3.08890917 |
| RPW86PBE | 1.0000 | 1.13795871 | 0.37636536 | 4.75236384 |
| SCAN | 1.0000 | 1.75408315 | 0.63571334 | 6.35690748 |
| TPSS0 | 1.0000 | 1.66752698 | 0.40074746 | 4.80927196 |
| TPSS | 1.0000 | 1.91130849 | 0.43332851 | 4.56986797 |
| TPSSH | 1.0000 | 1.88783525 | 0.43968167 | 4.60342700 |
| $\omega \mathrm{B}97$ | 1.0000 | 7.11022468 | 0.76423345 | 8.44559334 |
| $\omega \mathrm{B}97\mathrm{X}$ | 1.0000 | 0.38815338 | 0.47448629 | 6.91367384 |
| X3LYP | 1.0000 | 1.55067492 | 0.19818545 | 5.61262748 |
| XLYP | 1.0000 | 1.51577878 | 0.10026585 | 5.37506460 |

Table A6: BJ-damping parameter (DFT-D4(TB)-MBD) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| | data (S66x8 | [16], S22x5 [17], NCII | BLIND10 [18]). | |
|----------|-------------|------------------------|----------------|------------|
| DFA | s_6 | s_8 | a_1 | a_2 |
| HF | 1.0000 | 1.45828683 | 0.44712742 | 3.26487734 |
| BLYP | 1.0000 | 2.08117058 | 0.41711642 | 4.03955128 |
| BPBE | 1.0000 | 3.64259175 | 0.47063878 | 4.34712279 |
| BP | 1.0000 | 3.11112473 | 0.40995387 | 4.91005330 |
| BPW | 1.0000 | 2.52744727 | 0.40402782 | 4.22084057 |
| LB94 | 1.0000 | 2.091 418 91 | 0.301 280 51 | 3.45788060 |
| MPWLYP | 1.0000 | 1.36460200 | 0.28610246 | 4.91028062 |
| MPWPW | 1.0000 | 1.73130752 | 0.32547973 | 4.81372663 |
| OLYP | 1.0000 | 2.30187644 | 0.54154721 | 2.53287278 |
| OPBE | 1.0000 | 2.47862243 | 0.59805792 | 2.26671322 |
| PBE | 1.0000 | 0.95159605 | 0.40436318 | 4.65010856 |
| RPBE | 1.0000 | 1.05401423 | 0.42599648 | 3.10146307 |
| REVPBE | 1.0000 | 1.52850098 | 0.49314034 | 3.10441225 |
| PW86PBE | 1.0000 | 1.46497296 | 0.42635774 | 4.67070001 |
| RPW86PBE | 1.0000 | 1.23782981 | 0.39785399 | 4.69412260 |
| PW91 | 1.0000 | 0.89648532 | 0.39592418 | 4.96320977 |
| PWP | 1.0000 | 0.63806944 | 0.47390787 | 5.66515208 |
| XLYP | 1.0000 | 1.50994082 | 0.09051215 | 5.36205296 |
| B97 | 1.0000 | 0.89799738 | 0.30819088 | 4.44324265 |
| TPSS | 1.0000 | 1.88901638 | 0.42775015 | 4.55379980 |
| REVTPSS | 1.0000 | 1.50883062 | 0.43017530 | 4.65783611 |
| SCAN | 1.0000 | 0.46990209 | 0.61436450 | 5.89911495 |
| B1LYP | 1.0000 | 1.83074938 | 0.38493543 | 4.45592640 |
| B3LYP | 1.0000 | 1.93642773 | 0.40445381 | 4.45704639 |
| BHLYP | 1.0000 | 1.51896770 | 0.28192218 | 5.29427469 |
| B1P | 1.0000 | 3.41675121 | 0.48253511 | 5.03389354 |
| B3P | 1.0000 | 3.18279035 | 0.46992325 | 4.97650253 |
| B3PW | 1.0000 | 2.72363274 | 0.44377256 | 4.52215574 |
| O3LYP | 1.0000 | 1.73874942 | 0.10638982 | 6.04981736 |
| REVPBE0 | 1.0000 | 1.49890714 | 0.35819541 | 4.15947955 |
| REVPBE38 | 1.0000 | 1.57382508 | 0.37838702 | 4.35632432 |
| PBE0 | 1.0000 | 1.19661978 | 0.41734308 | 4.88432030 |
| PWP1 | 1.0000 | 0.64888926 | 0.55564809 | 5.32212639 |
| PW1PW | 1.0000 | 1.18364244 | 0.46953724 | 4.88272276 |
| MPW1PW | 1.0000 | 1.62788471 | 0.41557675 | 4.59973489 |
| MPW1LYP | 1.0000 | 1.33170909 | 0.29830906 | 5.17345035 |
| PW6B95 | 1.0000 | -0.16443919 | 0.07904989 | 5.94439646 |
| TPSSH | 1.0000 | 2.16468907 | 0.45254189 | 4.65553922 |
| TPSS0 | 1.0000 | 1.25285163 | 0.38223499 | 4.61593529 |
| X3LYP | 1.0000 | 1.50562853 | 0.21152728 | 5.47901628 |
| M06L | 1.0000 | 0.01347697 | 0.70834664 | 6.03315516 |
| M06 | 1.0000 | 0.50785008 | 0.58953157 | 5.97317057 |
| M062X | 1.0000 | 0.04672618 | 0.87098156 | 7.32988630 |
| WB97 | 1.0000 | 1.12736363 | 0.75396590 | 7.31052961 |
| WB97X | 1.0000 | 0.35040501 | 0.56974796 | 6.44327794 |

Table A6: BJ-damping parameter (DFT-D4(TB)-MBD) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| DFA | s_6 | s_8 | a_1 | a_2 |
|----------------|--------|-------------|------------|--------------|
| CAMB3LYP | 1.0000 | 1.65213437 | 0.42676206 | 4.99450582 |
| LCBLYP | 1.0000 | 1.67459038 | 0.64772566 | 7.02691022 |
| LH07TSVWN | 1.0000 | 1.64716468 | 0.36027550 | 3.948 840 94 |
| LH07SSVWN | 1.0000 | 2.54773475 | 0.37196719 | 3.89864094 |
| LH12CTSSIRPW92 | 1.0000 | 1.90023851 | 0.33513581 | 3.53724635 |
| LH12CTSSIFPW92 | 1.0000 | 2.04371641 | 0.33238788 | 3.47234711 |
| LH14TCALPBE | 1.0000 | 0.96217113 | 0.40809799 | 4.53911955 |
| B2PLYP | 0.7800 | 0.97090085 | 0.41849225 | 4.59286243 |
| MPW2PLYP | 0.7500 | 0.55506801 | 0.48148834 | 4.88179316 |
| PWPB95 | 0.8200 | -0.02640853 | 0.43744768 | 4.53884724 |
| DSDBLYP | 0.5400 | 0.62642144 | 0.45589598 | 4.73062294 |
| DSDPBE | 0.4500 | 0.69229105 | 0.41584408 | 4.52896960 |
| DSDPBEB95 | 0.5400 | -0.02535683 | 0.43117570 | 4.31724907 |
| DSDPBEP86 | 0.4700 | 0.40437239 | 0.52692625 | 5.08678249 |
| DSDSVWN | 0.4100 | 0.73668521 | 0.50541252 | 5.06078930 |
| DODBLYP | 0.4700 | 1.04384962 | 0.37001761 | 4.22041649 |
| DODPBE | 0.4800 | 0.80824428 | 0.38386476 | 4.37573221 |
| DODPBEB95 | 0.5600 | 0.02781676 | 0.38100406 | 4.18729280 |
| DODPBEP86 | 0.4600 | 0.71163846 | 0.40907164 | 4.51396886 |
| DODSVWN | 0.4200 | 0.82959503 | 0.45957776 | 4.89671368 |
| PBE0-2 | 0.5000 | 0.12481539 | 0.66150525 | 5.70164463 |
| PBE0-DH | 0.8750 | 0.65674732 | 0.47131118 | 4.82816982 |

Table A7: BJ-damping parameter (DFT-D4(TB)-ATM) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| | ` . | [16], S22x5 [17], NCII | • | |
|----------|--------|------------------------|---|--------------|
| DFA | s_6 | s_8 | a_1 | a_2 |
| HF | 1.0000 | 1.55736644 | 0.44217952 | 3.32410441 |
| BLYP | 1.0000 | 2.19020080 | 0.42913071 | 4.05110479 |
| BPBE | 1.0000 | 3.62974920 | 0.47179311 | 4.34832782 |
| BP | 1.0000 | 3.08647246 | 0.41162112 | 4.91954319 |
| BPW | 1.0000 | 2.85109094 | 0.45463214 | 4.14345106 |
| LB94 | 1.0000 | 2.39809364 | 0.36347155 | 3.34195390 |
| MPWLYP | 1.0000 | 1.36395783 | 0.28602441 | 4.91054588 |
| MPWPW | 1.0000 | 1.73185625 | 0.32534435 | 4.81318452 |
| OLYP | 1.0000 | 2.30087126 | 0.54144859 | 2.53332300 |
| OPBE | 1.0000 | 2.70962530 | 0.61800352 | 2.27621123 |
| PBE | 1.0000 | 0.93625094 | 0.40790049 | 4.65135944 |
| RPBE | 1.0000 | 1.05164427 | 0.42592627 | 3.10037133 |
| REVPBE | 1.0000 | 1.61138201 | 0.51215200 | 3.04718355 |
| PW86PBE | 1.0000 | 1.19254614 | 0.39745489 | 4.66150128 |
| RPW86PBE | 1.0000 | 1.22289266 | 0.39946065 | 4.70231415 |
| PW91 | 1.0000 | 0.78221005 | 0.39097390 | 4.94408451 |
| PWP | 1.0000 | 0.61218826 | 0.47778963 | 5.64605664 |
| XLYP | 1.0000 | 1.50968143 | 0.09056306 | 5.36223975 |
| B97 | 1.0000 | 0.89818005 | 0.30891258 | 4.44379503 |
| TPSS | 1.0000 | 2.22336684 | 0.44903931 | 4.65080532 |
| REVTPSS | 1.0000 | 1.49374036 | 0.43199183 | 4.66405759 |
| SCAN | 1.0000 | 0.45775648 | 0.61669342 | 5.90523468 |
| B1LYP | 1.0000 | 1.82819641 | 0.38561062 | 4.46105123 |
| B3LYP | 1.0000 | 1.93077774 | 0.40520781 | 4.46255249 |
| BHLYP | 1.0000 | 1.50655502 | 0.28355060 | 5.30354638 |
| B1P | 1.0000 | 3.39400623 | 0.48389119 | 5.03982146 |
| B3P | 1.0000 | 3.16190735 | 0.47103271 | 4.98137363 |
| B3PW | 1.0000 | 2.71273965 | 0.44631895 | 4.52517962 |
| O3LYP | 1.0000 | 1.72321198 | 0.10802598 | 6.06126661 |
| REVPBE0 | 1.0000 | 1.50046346 | 0.35837424 | 4.15979987 |
| REVPBE38 | 1.0000 | 1.61994900 | 0.38456295 | 4.37487340 |
| PBE0 | 1.0000 | 1.18497326 | 0.419 185 88 | 4.891 700 85 |
| PWP1 | 1.0000 | 0.61368682 | 0.556 828 03 | 5.332 668 14 |
| PW1PW | 1.0000 | 1.16002822 | 0.470 785 18 | 4.892 430 94 |
| MPW1PW | 1.0000 | 1.619 913 31 | 0.417 097 90 | 4.607 283 22 |
| MPW1LYP | 1.0000 | 1.325 394 33 | 0.301 234 36 | 5.175 749 56 |
| PW6B95 | 1.0000 | -0.24364276 | 0.068 613 69 | 5.893 703 10 |
| TPSSH | 1.0000 | 1.816 993 05 | 0.437 085 55 | 4.576 793 51 |
| TPSS0 | 1.0000 | 1.469 388 02 | 0.397 514 11 | 4.710 147 42 |
| X3LYP | 1.0000 | 1.494 935 75 | 0.213 108 66 | 5.487 460 09 |
| M06L | 1.0000 | 0.02539965 | 0.711 107 72 | 6.050 635 04 |
| M06 | 1.0000 | 0.50295755 | 0.588 756 42 | 5.965 574 87 |
| M062X | 1.0000 | -0.12770286 | 0.862 899 08 | 7.30761622 |
| WB97 | 1.0000 | 1.26204557 | 0.754 376 95 | 7.315 277 80 |
| WB97X | 1.0000 | 0.34783580 | 0.57488291 | 6.41921802 |

Table A7: BJ-damping parameter (DFT-D4(TB)-ATM) for various DFAs as derived by fitting to reference data (S66x8 [16], S22x5 [17], NCIBLIND10 [18]).

| | \ | L 3/ | L 1/ | |
|----------------|--------|-------------|------------|------------|
| DFA | s_6 | s_8 | a_1 | a_2 |
| CAMB3LYP | 1.0000 | 1.63966917 | 0.42427808 | 5.03109815 |
| LCBLYP | 1.0000 | 1.67838379 | 0.64705435 | 7.02883375 |
| LH07TSVWN | 1.0000 | 3.40858218 | 0.53218598 | 3.55068620 |
| LH07SSVWN | 1.0000 | 2.01742030 | 0.49983199 | 3.53449278 |
| LH12CTSSIRPW92 | 1.0000 | 2.46688356 | 0.56783603 | 2.83126177 |
| LH12CTSSIFPW92 | 1.0000 | 2.70376807 | 0.58623258 | 2.72103381 |
| LH14TCALPBE | 1.0000 | 1.23827287 | 0.43537537 | 4.63938635 |
| B2PLYP | 0.7800 | 1.00468553 | 0.42737183 | 4.62624158 |
| MPW2PLYP | 0.7500 | 0.54318070 | 0.48472756 | 4.89674342 |
| PWPB95 | 0.8200 | -0.35342155 | 0.37278086 | 4.03580081 |
| DSDBLYP | 0.5400 | 0.60151254 | 0.46091302 | 4.75348449 |
| DSDPBE | 0.4500 | 0.69865539 | 0.42508371 | 4.56518930 |
| DSDPBEB95 | 0.5400 | -0.05097431 | 0.42967019 | 4.32398958 |
| DSDPBEP86 | 0.4700 | 0.38271706 | 0.53397308 | 5.11687101 |
| DSDSVWN | 0.4100 | 0.50904643 | 0.49413232 | 4.92092377 |
| DODBLYP | 0.4700 | 1.17101452 | 0.39833737 | 4.25809811 |
| DODPBE | 0.4800 | 0.80761267 | 0.38873738 | 4.40171191 |
| DODPBEB95 | 0.5600 | 0.00959016 | 0.38866713 | 4.09462693 |
| DODPBEP86 | 0.4600 | 0.71327951 | 0.41631367 | 4.53851973 |
| DODSVWN | 0.4200 | 0.62186246 | 0.45590032 | 4.74298602 |
| PBE0-2 | 0.5000 | 0.10740034 | 0.66706819 | 5.73936118 |
| PBE0-DH | 0.8750 | 0.74864713 | 0.47598257 | 4.90910090 |

F. Timings of energy and gradient calls

We compare timings for energy and gradient calls between DFT–D4 and DFT–D3(BJ)-ATM for the Tetrakis(isonitrile)rhodium(I) dimer with 106 atoms (doubly positively charged) and a diamond chunk with 430 atoms (286 carbon atoms and 144 hydrogen atoms) derived at four Intel(R) Core(TM) i7-6700 CPU (3.40 GHz).

| Property | CPU time(DFT–D4) / s | CPU time (DFT–D3(BJ)-ATM) / s | | | | | | |
|-------------------------------------|-------------------------------|----------------------------------|--|--|--|--|--|--|
| Tetra | akis(isonitrile)rhodium(I) di | mer (106 atoms, charge +2) | | | | | | |
| single-point | 0.01 | 0.03 | | | | | | |
| gradient | 0.01 | 0.03 | | | | | | |
| Diamond chunk (430 atoms, charge 0) | | | | | | | | |
| single-point | 0.34 | 0.41 | | | | | | |
| gradient | 0.51 | 1.02 | | | | | | |

Part II: Statistical measures and evaluations

G. Extendet statistical measures

As statistical measure for a set $\{x_1, \dots, x_n\}$ of data points with references $\{r_1, \dots, r_n\}$ we use

- Average : $\overline{x} = \frac{1}{n} \sum_{i} x_i$
- Mean deviation (MD): $MD = \frac{1}{n} \sum_{i} (\mathbf{x}_i \mathbf{r}_i)$
- Mean absolute deviation (MAD): $MAD = \frac{1}{n} \sum_{i} |\mathbf{x}_i \mathbf{r}_i|$
- Root mean square deviation (RMSD) : RMSD = $\sqrt{\frac{1}{n}\sum_{i=1}^{n}}x_i^2$
- Bessel corrected variance (Var): $Var = \frac{1}{n-1} \sum_{i=1}^{n} (x_i \overline{x})^2$
- Bessel corrected standard deviation (SD): $SD = \sqrt{\frac{1}{n-1} \sum_{i} (\mathbf{x}_i \mathbf{r}_i MD)^2}$
- Maximum deviation (Max): $Max = \max\{x_i r_i\}$
- Minimum deviation (Min): $Min = \min\{x_i r_i\}$

H. Statistical evaluation: S30L

Table A8: Extendet statistical evaluation of the S30L [19] benchmark set for various different DFAs. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4-ATM (abbreviated as D4) corrected values given in kcal mol⁻¹. For further details please check Ref. [20, 21]. We follow the numberation of the systems regarding Ref. [19]

| | DLPNO- | PV | V6B95 | S | CAN | I | PBE |
|-----|-----------------|--------|--------|--------|--------|--------|--------|
| # | $CCSD(T)/CBS^*$ | D4 | D3 | D4 | D3 | D4 | D3 |
| 1 | -31.0 | -28.2 | -30.1 | -30.2 | -29.7 | -29.6 | -28.0 |
| 2 | -20.7 | -19.0 | -20.4 | -19.8 | -19.4 | -19.6 | -18.2 |
| 3 | -23.3 | -19.1 | -19.2 | -22.5 | -21.5 | -20.8 | -18.0 |
| 4 | -18.6 | -20.9 | -20.3 | -21.4 | -21.0 | -20.7 | -18.6 |
| 5 | -27.9 | -31.6 | -32.9 | -33.2 | -32.2 | -32.7 | -28.7 |
| 6 | -25.2 | -21.2 | -22.8 | -25.6 | -25.2 | -24.8 | -22.2 |
| 7 | -31.0 | -32.1 | -33.4 | -33.2 | -33.2 | -34.8 | -29.9 |
| 8 | -35.6 | -36.9 | -38.7 | -38.1 | -38.0 | -40.2 | -34.5 |
| 9 | -33.7 | -31.6 | -32.7 | -33.6 | -29.4 | -35.1 | -27.0 |
| 10 | -35.0 | -30.5 | -32.0 | -34.7 | -30.2 | -36.2 | -27.8 |
| 11 | -35.8 | -32.8 | -36.7 | -40.1 | -34.2 | -42.5 | -32.5 |
| 12 | -36.9 | -33.6 | -37.5 | -40.1 | -34.1 | -42.5 | -32.4 |
| 13 | -27.3 | -24.2 | -25.7 | -27.1 | -25.5 | -24.0 | -22.9 |
| 14 | -28.6 | -24.2 | -26.7 | -28.3 | -26.6 | -25.6 | -23.9 |
| 15 | -17.5 | -17.3 | -18.1 | -21.8 | -21.9 | -21.2 | -21.1 |
| 16 | -21.6 | -21.4 | -23.9 | -24.2 | -24.2 | -25.3 | -24.7 |
| 17 | -34.3 | -32.6 | -31.7 | -36.0 | -35.9 | -33.4 | -32.3 |
| 18 | -22.8 | -20.8 | -20.4 | -24.4 | -24.0 | -22.5 | -21.3 |
| 19 | -15.3 | -14.4 | -14.7 | -17.0 | -16.1 | -15.4 | -15.3 |
| 20 | -18.5 | -17.2 | -17.9 | -20.1 | -19.1 | -18.0 | -18.2 |
| 21 | -28.0 | -22.8 | -24.9 | -27.3 | -25.1 | -23.9 | -23.5 |
| 22 | -35.3 | -35.2 | -33.9 | -38.6 | -38.8 | -39.5 | -38.7 |
| 23 | -62.1 | -63.0 | -61.8 | -66.5 | -66.9 | -68.7 | -68.1 |
| 24 | -136.3 | -130.3 | -133.1 | -138.0 | -134.7 | -126.9 | -126.5 |
| 25 | -28.7 | -27.4 | -31.2 | -30.2 | -28.9 | -29.8 | -27.1 |
| 26 | -28.6 | -26.4 | -30.3 | -27.9 | -26.5 | -29.8 | -27.1 |
| 27 | -83.4 | -80.6 | -82.0 | -84.3 | -83.5 | -80.6 | -80.7 |
| 28 | -80.0 | -77.4 | -78.7 | -80.7 | -80.1 | -77.2 | -77.4 |
| 29 | -52.8 | -56.0 | -54.2 | -58.1 | -58.2 | -55.8 | -54.2 |
| 30 | -49.6 | -51.1 | -49.9 | -53.6 | -53.4 | -51.5 | -49.7 |
| MD | | 1.5 | 0.3 | -1.7 | -0.4 | -0.8 | 1.8 |
| MA | D | 2.5 | 1.8 | 2.0 | 2.3 | 2.9 | 3.1 |
| RM | SD | 2.9 | 2.2 | 2.6 | 2.7 | 3.6 | 3.8 |
| SD | | 13.3 | 11.7 | 10.5 | 14.8 | 19.5 | 18.4 |
| Var | | 6.1 | 4.7 | 3.8 | 7.6 | 13.1 | 11.7 |
| Max | X. | 6.0 | 4.1 | 0.9 | 4.8 | 9.4 | 9.8 |
| Min | | -3.7 | -5.0 | -5.3 | -5.4 | -6.7 | -6.0 |
| AM | ax | 6.0 | 5.0 | 5.3 | 5.4 | 9.4 | 9.8 |

Table A9: Extendet statistical evaluation of the S30L [19] benchmark set for various different DFAs. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4-MBD (abbreviated as D4) corrected values given in kcal mol⁻¹. For further details please check Ref. [20, 21]. We follow the numberation of the systems regarding Ref. [19]

| | DLPNO- | PV | V6B95 | S | CAN | I | PBE |
|-----|--------------|--------|--------|--------|--------|--------|--------|
| # | CCSD(T)/CBS* | D4 | D3 | D4 | D3 | D4 | D3 |
| 1 | -31.0 | -29.8 | -30.1 | -30.1 | -29.7 | -30.2 | -28.0 |
| 2 | -20.7 | -20.2 | -20.4 | -19.7 | -19.4 | -20.0 | -18.2 |
| 3 | -23.3 | -20.8 | -19.2 | -22.6 | -21.5 | -21.8 | -18.0 |
| 4 | -18.6 | -21.5 | -20.3 | -21.5 | -21.0 | -21.1 | -18.6 |
| 5 | -27.9 | -33.4 | -32.9 | -33.2 | -32.2 | -33.4 | -28.7 |
| 6 | -25.2 | -22.9 | -22.8 | -25.6 | -25.2 | -25.5 | -22.2 |
| 7 | -31.0 | -33.2 | -33.4 | -33.3 | -33.2 | -35.2 | -29.9 |
| 8 | -35.6 | -38.2 | -38.7 | -38.1 | -38.0 | -40.5 | -34.5 |
| 9 | -33.7 | -35.2 | -32.7 | -34.1 | -29.4 | -37.3 | -27.0 |
| 10 | -35.0 | -34.6 | -32.0 | -35.3 | -30.2 | -38.6 | -27.8 |
| 11 | -35.8 | -38.7 | -36.7 | -40.9 | -34.2 | -46.0 | -32.5 |
| 12 | -36.9 | -39.4 | -37.5 | -40.9 | -34.1 | -45.9 | -32.4 |
| 13 | -27.3 | -26.4 | -25.7 | -27.0 | -25.5 | -25.3 | -22.9 |
| 14 | -28.6 | -26.8 | -26.7 | -28.2 | -26.6 | -27.0 | -23.9 |
| 15 | -17.5 | -17.9 | -18.1 | -21.9 | -21.9 | -21.6 | -21.1 |
| 16 | -21.6 | -22.4 | -23.9 | -24.3 | -24.2 | -25.9 | -24.7 |
| 17 | -34.3 | -33.3 | -31.7 | -36.0 | -35.9 | -33.9 | -32.3 |
| 18 | -22.8 | -21.6 | -20.4 | -24.4 | -24.0 | -23.1 | -21.3 |
| 19 | -15.3 | -15.6 | -14.7 | -17.1 | -16.1 | -16.3 | -15.3 |
| 20 | -18.5 | -19.0 | -17.9 | -20.2 | -19.1 | -19.3 | -18.2 |
| 21 | -28.0 | -25.9 | -24.9 | -27.3 | -25.1 | -25.9 | -23.5 |
| 22 | -35.3 | -35.5 | -33.9 | -38.7 | -38.8 | -39.8 | -38.7 |
| 23 | -62.1 | -63.0 | -61.8 | -66.6 | -66.9 | -68.8 | -68.1 |
| 24 | -136.3 | -135.9 | -133.1 | -138.5 | -134.7 | -130.8 | -126.5 |
| 25 | -28.7 | -30.4 | -31.2 | -30.2 | -28.9 | -31.0 | -27.1 |
| 26 | -28.6 | -29.5 | -30.3 | -27.8 | -26.5 | -31.0 | -27.1 |
| 27 | -83.4 | -82.8 | -82.0 | -84.3 | -83.5 | -81.9 | -80.7 |
| 28 | -80.0 | -79.1 | -78.7 | -80.6 | -80.1 | -78.2 | -77.4 |
| 29 | -52.8 | -55.9 | -54.2 | -58.1 | -58.2 | -55.8 | -54.2 |
| 30 | -49.6 | -51.3 | -49.9 | -53.6 | -53.4 | -51.6 | -49.7 |
| MD | 1 | -0.5 | 0.3 | -1.8 | -0.4 | -1.9 | 1.8 |
| MA | D | 1.5 | 1.8 | 2.1 | 2.3 | 3.1 | 3.1 |
| RM | SD | 1.9 | 2.2 | 2.7 | 2.7 | 3.9 | 3.8 |
| SD | | 10.2 | 11.7 | 10.8 | 14.8 | 18.8 | 18.4 |
| Var | | 3.6 | 4.7 | 4.0 | 7.6 | 12.2 | 11.7 |
| Ma | X | 2.5 | 4.1 | 1.0 | 4.8 | 5.5 | 9.8 |
| Mir | l | -5.5 | -5.0 | -5.3 | -5.4 | -10.2 | -6.0 |
| AM | ax | 5.5 | 5.0 | 5.3 | 5.4 | 10.2 | 9.8 |

Table A10: Extendet statistical evaluation of the S30L [19] benchmark set for various different DFAs. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4(TB)-ATM (abbreviated as D4) corrected values given in kcal mol⁻¹. For further details please check Ref. [20, 21]. We follow the numberation of the systems regarding Ref. [19]

| | DLPNO- | PV | V6B95 | S | CAN | | PBE |
|----------------------|------------------|--------|--------|--------|--------|--------|--------|
| # | $CCSD(T)/CBS^*$ | D4 | D3 | D4 | D3 | D4 | D3 |
| 1 | -31.0 | -29.0 | -30.1 | -29.5 | -29.7 | -29.6 | -28.0 |
| 2 | -20.7 | -19.5 | -20.4 | -19.3 | -19.4 | -19.4 | -18.2 |
| 3 | -23.3 | -19.5 | -19.2 | -21.9 | -21.5 | -20.6 | -18.0 |
| 4 | -18.6 | -20.9 | -20.3 | -21.1 | -21.0 | -20.5 | -18.6 |
| 5 | -27.9 | -32.1 | -32.9 | -32.4 | -32.2 | -31.9 | -28.7 |
| 6 | -25.2 | -21.5 | -22.8 | -24.9 | -25.2 | -24.0 | -22.2 |
| 7 | -31.0 | -32.5 | -33.4 | -32.3 | -33.2 | -33.8 | -29.9 |
| 8 | -35.6 | -37.4 | -38.7 | -37.0 | -38.0 | -38.9 | -34.5 |
| 9 | -33.7 | -31.7 | -32.7 | -31.3 | -29.4 | -33.2 | -27.0 |
| 10 | -35.0 | -30.8 | -32.0 | -32.3 | -30.2 | -34.2 | -27.8 |
| 11 | -35.8 | -33.3 | -36.7 | -37.0 | -34.2 | -40.1 | -32.5 |
| 12 | -36.9 | -34.2 | -37.5 | -36.9 | -34.1 | -40.1 | -32.4 |
| 13 | -27.3 | -25.5 | -25.7 | -26.7 | -25.5 | -24.8 | -22.9 |
| 14 | -28.6 | -25.4 | -26.7 | -27.6 | -26.6 | -26.0 | -23.9 |
| 15 | -17.5 | -17.6 | -18.1 | -21.5 | -21.9 | -21.1 | -21.1 |
| 16 | -21.6 | -22.0 | -23.9 | -23.8 | -24.2 | -25.0 | -24.7 |
| 17 | -34.3 | -32.3 | -31.7 | -35.5 | -35.9 | -32.9 | -32.3 |
| 18 | -22.8 | -20.6 | -20.4 | -23.8 | -24.0 | -22.1 | -21.3 |
| 19 | -15.3 | -14.8 | -14.7 | -16.6 | -16.1 | -15.7 | -15.3 |
| 20 | -18.5 | -18.0 | -17.9 | -19.6 | -19.1 | -18.7 | -18.2 |
| 21 | -28.0 | -25.4 | -24.9 | -27.1 | -25.1 | -26.6 | -23.5 |
| 22 | -35.3 | -35.0 | -33.9 | -38.3 | -38.8 | -39.4 | -38.7 |
| 23 | -62.1 | -62.5 | -61.8 | -66.3 | -66.9 | -68.4 | -68.1 |
| 24 | -136.3 | -132.4 | -133.1 | -136.7 | -134.7 | -128.6 | -126.5 |
| 25 | -28.7 | -28.3 | -31.2 | -29.2 | -28.9 | -29.1 | -27.1 |
| 26 | -28.6 | -27.3 | -30.3 | -26.8 | -26.5 | -29.0 | -27.1 |
| 27 | -83.4 | -81.5 | -82.0 | -84.1 | -83.5 | -81.2 | -80.7 |
| 28 | -80.0 | -78.0 | -78.7 | -80.4 | -80.1 | -77.5 | -77.4 |
| 29 | -52.8 | -56.2 | -54.2 | -58.3 | -58.2 | -56.3 | -54.2 |
| 30 | -49.6 | -51.4 | -49.9 | -53.5 | -53.4 | -52.0 | -49.7 |
| MD | | 1.0 | 0.3 | -0.9 | -0.4 | -0.5 | 1.8 |
| MAI | | 2.0 | 1.8 | 1.8 | 2.3 | 2.4 | 3.1 |
| RMS | $^{\mathrm{SD}}$ | 2.4 | 2.2 | 2.3 | 2.7 | 3.0 | 3.8 |
| SD | | 11.8 | 11.7 | 11.5 | 14.8 | 16.1 | 18.4 |
| Var | | 4.8 | 4.7 | 4.6 | 7.6 | 9.0 | 11.7 |
| Max | | 4.2 | 4.1 | 2.7 | 4.8 | 7.7 | 9.8 |
| Min | | -4.2 | -5.0 | -5.5 | -5.4 | -6.3 | -6.0 |
| AMa | X | 4.2 | 5.0 | 5.5 | 5.4 | 7.7 | 9.8 |

I. Statistical evaluation: L7

Table A11: Extended statistical evaluations of different DFAs with respect to DLPNO-CCSD(T)/CBS* data. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4-ATM (abbreviated as D4) corrected values given in kcal mol⁻¹. We follow the numberation of the systems regarding Ref. [22].

| | DLPNO- PW6B95 | | V6B95 | P | BE0 | Т | PSS |
|--------|-----------------|-------|-------|-------|-------|-------|-------|
| # | $CCSD(T)/CBS^*$ | D4 | D3 | D4 | D3 | D4 | D3 |
| СВН | -11.6 | -8.2 | -9.0 | -10.8 | -11.7 | -10.8 | -11.6 |
| C2C2PD | -21.3 | -18.8 | -20.4 | -20.1 | -18.3 | -23.9 | -20.1 |
| C3A | -17.0 | -14.7 | -14.9 | -16.0 | -14.4 | -18.4 | -15.3 |
| C3GC | -29.1 | -26.2 | -26.6 | -27.0 | -24.2 | -31.1 | -25.9 |
| GCGC | -12.8 | -13.5 | -12.4 | -14.1 | -12.1 | -15.8 | -12.5 |
| GGG | -1.9 | -1.8 | -1.4 | -2.1 | -1.3 | -3.0 | -1.6 |
| PHE | -23.0 | -23.7 | -23.7 | -25.4 | -25.3 | -24.2 | -23.9 |
| MD | | 1.4 | 1.2 | 0.2 | 1.3 | -1.5 | 0.8 |
| MAD | | 1.8 | 1.4 | 1.3 | 2.0 | 1.7 | 1.1 |
| RMSD | | 2.2 | 1.7 | 1.5 | 2.6 | 1.9 | 1.5 |
| SD | | 4.3 | 3.1 | 3.9 | 5.8 | 3.1 | 3.3 |
| Var | | 3.1 | 1.6 | 2.5 | 5.7 | 1.6 | 1.8 |
| Max | | 3.4 | 2.6 | 2.1 | 4.9 | 0.8 | 3.2 |
| Min | | -0.7 | -0.7 | -2.4 | -2.3 | -3.0 | -0.9 |
| AMax | | 3.4 | 2.6 | 2.4 | 4.9 | 3.0 | 3.2 |

Table A12: Extended statistical evaluations of different DFAs with respect to DLPNO-CCSD(T)/CBS* data. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4-MBD (abbreviated as D4) corrected values given in kcal mol⁻¹. We follow the numberation of the systems regarding Ref. [22].

| | DLPNO- | PV | V6B95 | P | BE0 | Т | PSS |
|--------|-----------------|-------|-------|-------|-------|-------|-------|
| # | $CCSD(T)/CBS^*$ | D4 | D3 | D4 | D3 | D4 | D3 |
| СВН | -11.6 | -8.6 | -9.0 | -11.0 | -11.7 | -10.8 | -11.6 |
| C2C2PD | -21.3 | -20.5 | -20.4 | -20.3 | -18.3 | -23.6 | -20.1 |
| C3A | -17.0 | -15.6 | -14.9 | -16.1 | -14.4 | -18.1 | -15.3 |
| C3GC | -29.1 | -27.8 | -26.6 | -27.2 | -24.2 | -30.7 | -25.9 |
| GCGC | -12.8 | -13.9 | -12.4 | -14.1 | -12.1 | -15.6 | -12.5 |
| GGG | -1.9 | -2.0 | -1.4 | -2.1 | -1.3 | -2.8 | -1.6 |
| PHE | -23.0 | -24.0 | -23.7 | -25.6 | -25.3 | -24.3 | -23.9 |
| MD | | 0.6 | 1.2 | 0.1 | 1.3 | -1.3 | 0.8 |
| MAD | | 1.2 | 1.4 | 1.2 | 2.0 | 1.5 | 1.1 |
| RMSD | | 1.5 | 1.7 | 1.4 | 2.6 | 1.7 | 1.5 |
| SD | | 3.6 | 3.1 | 3.7 | 5.8 | 2.8 | 3.3 |
| Var | | 2.1 | 1.6 | 2.3 | 5.7 | 1.3 | 1.8 |
| Max | | 3.0 | 2.6 | 1.9 | 4.9 | 0.8 | 3.2 |
| Min | | -1.1 | -0.7 | -2.6 | -2.3 | -2.8 | -0.9 |
| AMax | | 3.0 | 2.6 | 2.6 | 4.9 | 2.8 | 3.2 |

Table A13: Extended statistical evaluations of different DFAs with respect to DLPNO-CCSD(T)/CBS* data. For each functional we directly compare DFT-D3 (BJ)-ATM (abbreviated as D3) corrected values with DFT-D4(TB)-ATM (abbreviated as D4) corrected values given in kcal mol⁻¹. We follow the numberation of the systems regarding Ref. [22].

| | DLPNO- | PW | V6B95 | P | BE0 | 7 | TPSS |
|--------|--------------|-------|-------|-------|-------|-------|-------|
| # | CCSD(T)/CBS* | | D3 | D4 | D3 | D4 | D3 |
| СВН | -11.6 | -9.0 | -9.0 | -11.8 | -11.7 | -12.1 | -11.6 |
| C2C2PD | -21.3 | -18.7 | -20.4 | -20.0 | -18.3 | -23.7 | -20.1 |
| C3A | -17.0 | -14.6 | -14.9 | -16.0 | -14.4 | -18.3 | -15.3 |
| C3GC | -29.1 | -26.2 | -26.6 | -26.9 | -24.2 | -31.0 | -25.9 |
| GCGC | -12.8 | -13.4 | -12.4 | -14.1 | -12.1 | -15.7 | -12.5 |
| GGG | -1.9 | -1.8 | -1.4 | -2.2 | -1.3 | -3.0 | -1.6 |
| PHE | -23.0 | -23.8 | -23.7 | -25.6 | -25.3 | -24.4 | -23.9 |
| MD | | 1.3 | 1.2 | 0.0 | 1.3 | -1.7 | 0.8 |
| MAD | | 1.7 | 1.4 | 1.2 | 2.0 | 1.7 | 1.1 |
| RMSD | | 2.0 | 1.7 | 1.5 | 2.6 | 1.8 | 1.5 |
| SD | | 4.1 | 3.1 | 4.0 | 5.8 | 2.0 | 3.3 |
| Var | | 2.8 | 1.6 | 2.6 | 5.7 | 0.7 | 1.8 |
| Max | | 2.9 | 2.6 | 2.2 | 4.9 | -0.5 | 3.2 |
| Min | | -0.8 | -0.7 | -2.6 | -2.3 | -2.9 | -0.9 |
| AMax | | 2.9 | 2.6 | 2.6 | 4.9 | 2.9 | 3.2 |

J. Statistical evaluation: MOR41

We follow the numberation of the systems regarding Ref. [23].

Table A14: Extendet statistical evaluations of : DOD-PBE and DSD-PBE in $kcal\,mol^{-1}$. We abbreviate D3(BJ)-ATM by D3.

| # Ref. D4-ATM D4-MBD D3 D4-ATM D4-MBD D3 1 -43.1 | | | | | | | | |
|---|-----|-------|-----------|---------|-------|-----------|---------|-------|
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | ,, | D. C | D.4. ATDA | DOD-PBE | De | D.4. ATTM | DSD-PBE | Do |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | # | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| 7 -16.2 -14.3 -14.2 -14.5 -14.8 -14.8 -13.3 8 -17.2 -13.5 -13.7 -14.0 -13.2 -13.3 -13.3 9 -18.8 -14.5 -14.6 -15.0 -14.2 -14.3 -13.2 10 -22.6 -21.9 -22.1 -22.1 -23.3 -23.4 -24.6 11 27.0 24.7 24.7 24.5 23.0 23.0 21.4 12 -29.8 -33.4 -33.5 -33.6 -35.5 -35.6 -35.2 13 -43.2 -45.8 -46.0 -46.0 -47.7 -47.8 -49.2 14 -52.0 -53.7 -54.0 -54.5 -55.1 -55.4 -56.7 15 -4.1 7.5 7.3 7.3 11.8 11.6 12.1 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.7 17 -16.1 | | | | | | | | |
| 8 -17.2 -13.5 -13.7 -14.0 -13.2 -13.3 -13.3 9 -18.8 -14.5 -14.6 -15.0 -14.2 -14.3 -13.2 10 -22.6 -21.9 -22.1 -22.1 -23.3 -23.4 -24.6 11 27.0 24.7 24.7 24.5 23.0 23.0 21.4 12 -29.8 -33.4 -33.5 -33.6 -35.5 -35.6 -35.2 13 -43.2 -45.8 -46.0 -46.0 -47.7 -47.8 -49.2 14 -52.0 -53.7 -54.0 -54.5 -55.1 -55.4 -56.7 15 -4.1 7.5 7.3 7.3 11.8 11.6 12.1 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.9 16 -39.8 -40.3 -40.8 -33.7 -33.9 -36.2 19 -40.1 -39.9 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<> | | | | | | | | |
| 9 -18.8 | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | -14.0 | -13.2 | -13.3 | -13.3 |
| 11 27.0 24.7 24.7 24.5 23.0 23.0 21.4 12 -29.8 -33.4 -33.5 -33.6 -35.5 -35.6 -35.2 13 -43.2 -45.8 -46.0 -46.0 -47.7 -47.8 -49.2 14 -52.0 -53.7 -54.0 -54.5 -55.1 -55.4 -56.7 15 -4.1 7.5 7.3 7.3 11.8 11.6 12.1 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.7 17 -16.1 -13.9 -14.0 -14.0 -14.0 -14.1 -11.8 18 -34.2 -34.0 -34.4 -34.8 -33.7 -33.9 -36.2 19 -40.1 -39.9 -40.3 -40.7 -39.4 -39.9 -41.9 20 -30.2 -29.5 -29.8 -30.1 -28.8 -28.9 -30.9 21 -15.1 < | | | | | | | | |
| 12 -29.8 -33.4 -33.5 -33.6 -35.5 -35.6 -35.2 13 -43.2 -45.8 -46.0 -46.0 -47.7 -47.8 -49.2 14 -52.0 -53.7 -54.0 -54.5 -55.1 -55.4 -56.7 15 -4.1 7.5 7.3 7.3 11.8 11.6 12.1 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.7 17 -16.1 -13.9 -14.0 -14.0 -14.0 -14.1 -11.8 18 -34.2 -34.0 -34.4 -34.8 -33.7 -33.9 -36.2 19 -40.1 -39.9 -40.3 -40.7 -39.4 -39.6 -41.9 20 -30.2 -29.5 -29.8 -30.1 -28.8 -28.9 -30.9 21 -15.1 -17.2 -17.7 -18.1 -15.8 -16.1 -17.3 22 -35.9 | | | | | | | | |
| 13 -43.2 -45.8 -46.0 -46.0 -47.7 -47.8 -49.2 14 -52.0 -53.7 -54.0 -54.5 -55.1 -55.4 -56.7 15 -4.1 7.5 7.3 7.3 11.8 11.6 12.1 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.7 17 -16.1 -13.9 -14.0 -14.0 -14.1 -11.8 18 -34.2 -34.0 -34.8 -33.7 -33.9 -36.2 19 -40.1 -39.9 -40.3 -40.7 -39.4 -39.6 -41.9 20 -30.2 -29.5 -29.8 -30.1 -28.8 -28.9 -30.9 21 -15.1 -17.2 -17.7 -18.1 -15.8 -16.1 -17.3 22 -35.9 -39.0 -39.4 -39.9 -40.3 -40.6 -42.6 23 -55.0 -55.1 -55.6 | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | -46.0 | -46.0 | -47.7 | | -49.2 |
| 16 -39.8 -40.3 -40.8 -41.1 -40.3 -40.8 -41.7 17 -16.1 -13.9 -14.0 -14.0 -14.1 -11.8 18 -34.2 -34.0 -34.4 -34.8 -33.7 -33.9 -36.2 19 -40.1 -39.9 -40.3 -40.7 -39.4 -39.6 -41.9 20 -30.2 -29.5 -29.8 -30.1 -28.8 -28.9 -30.9 21 -15.1 -17.2 -17.7 -18.1 -15.8 -16.1 -17.3 22 -35.9 -39.0 -39.4 -39.9 -40.3 -40.6 -42.6 23 -55.0 -55.1 -55.6 -56.1 -54.8 -55.1 -57.9 24 -41.6 -40.2 -41.1 -41.4 -39.9 -40.7 -42.7 25 -45.9 -45.2 -46.3 -46.4 -45.4 -46.3 -48.1 26 -36.4 -34 | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | -34.2 | -34.0 | | | | | -36.2 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | -40.1 | -39.9 | -40.3 | -40.7 | -39.4 | -39.6 | -41.9 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 20 | -30.2 | -29.5 | -29.8 | -30.1 | -28.8 | -28.9 | -30.9 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 21 | -15.1 | -17.2 | -17.7 | -18.1 | -15.8 | -16.1 | -17.3 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 22 | -35.9 | -39.0 | -39.4 | -39.9 | -40.3 | -40.6 | -42.6 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 23 | -55.0 | -55.1 | -55.6 | -56.1 | | -55.1 | -57.9 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | -41.6 | -40.2 | -41.1 | -41.4 | -39.9 | -40.7 | -42.7 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 25 | -45.9 | -45.2 | -46.3 | -46.4 | -45.4 | -46.3 | -48.1 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | -36.4 | -34.9 | | -35.3 | -33.3 | -33.5 | -34.7 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | -21.8 | | | -21.3 | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | -36.3 | -35.9 | | | -34.6 | -34.7 | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | -28.3 | -28.7 | | -28.8 | -27.9 | -28.0 | -29.2 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | -29.4 | -29.8 | -30.1 | -28.6 | -28.9 | -30.1 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | -2.0 | -2.0 | -1.9 | -2.3 | | -2.1 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | -10.7 | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
| 38 -64.4 -68.1 -68.6 -69.0 -67.4 -67.9 -74.0 39 -63.9 -63.9 -64.5 -63.7 -64.0 -66.3 40 -65.8 -65.2 -65.4 -65.5 -64.9 -65.0 -67.7 41 -3.2 -2.4 -2.3 -2.4 -2.1 -2.1 -0.7 MD 0.1 -0.2 -0.3 0.2 0.0 -0.9 | | | | | | | | |
| 39 -63.9 -63.3 -63.9 -64.5 -63.7 -64.0 -66.3 40 -65.8 -65.2 -65.4 -65.5 -64.9 -65.0 -67.7 41 -3.2 -2.4 -2.3 -2.4 -2.1 -2.1 -0.7 MD 0.1 -0.2 -0.3 0.2 0.0 -0.9 | 37 | -14.0 | -16.9 | -17.4 | -17.3 | -16.0 | -16.4 | -16.6 |
| 40 -65.8 -65.2 -65.4 -65.5 -64.9 -65.0 -67.7 41 -3.2 -2.4 -2.3 -2.4 -2.1 -2.1 -0.7 MD 0.1 -0.2 -0.3 0.2 0.0 -0.9 | 38 | | -68.1 | -68.6 | -69.0 | -67.4 | -67.9 | -74.0 |
| 41 -3.2 -2.4 -2.3 -2.4 -2.1 -2.1 -0.7 MD 0.1 -0.2 -0.3 0.2 0.0 -0.9 | 39 | | | | | | | |
| MD 0.1 -0.2 -0.3 0.2 0.0 -0.9 | 40 | -65.8 | -65.2 | -65.4 | -65.5 | -64.9 | -65.0 | -67.7 |
| | 41 | -3.2 | -2.4 | -2.3 | -2.4 | -2.1 | -2.1 | -0.7 |
| MAD 2.1 2.1 2.2 2.9 2.9 3.7 | MD |) | 0.1 | -0.2 | -0.3 | 0.2 | 0.0 | -0.9 |
| | MA | .D | 2.1 | 2.1 | 2.2 | 2.9 | 2.9 | 3.7 |
| RMSD 3.1 3.1 4.3 4.3 5.0 | RM | SD | 3.1 | 3.1 | 3.1 | 4.3 | 4.3 | 5.0 |
| SD 19.7 19.9 20.0 27.5 27.6 31.8 | SD | | 19.7 | 19.9 | 20.0 | 27.5 | 27.6 | 31.8 |
| Var 9.7 9.9 10.0 18.9 19.0 25.3 | Var | | 9.7 | 9.9 | 10.0 | 18.9 | 19.0 | 25.3 |
| Max 11.5 11.4 11.4 15.8 15.7 16.2 | Max | X | 11.5 | 11.4 | 11.4 | 15.8 | 15.7 | 16.2 |
| Min -8.2 -8.4 -8.4 -11.8 -11.9 -12.7 | Min | 1 | -8.2 | -8.4 | -8.4 | -11.8 | -11.9 | -12.7 |
| AMax 11.5 11.4 11.4 15.8 15.7 16.2 | AM | lax | 11.5 | 11.4 | 11.4 | 15.8 | 15.7 | 16.2 |

Table A15: Extendet statistical evaluations of : B3LYP and PBE0 in kcal $\mathrm{mol^{-1}}$. We abbreviate D3(BJ)-ATM by D3.

| | - () - | 11M by D5. | | | | | |
|-----|---------|------------|--------|-------|-----------|--------|-------|
| ,, | D 4 | D (100) | B3LYP | ъ. | D (100 f | PBE0 | D.o. |
| # | Ref. | D4-ATM | D4-MBD | D3 | D4-ATM | D4-MBD | D3 |
| 1 | -43.1 | -40.5 | -40.6 | -40.7 | -44.6 | -44.6 | -44.7 |
| 2 | -46.6 | -41.9 | -42.0 | -42.0 | -47.4 | -47.4 | -47.4 |
| 3 | -27.6 | -22.8 | -22.9 | -22.8 | -26.4 | -26.5 | -26.4 |
| 4 | -62.5 | -66.2 | -66.4 | -66.5 | -71.3 | -71.4 | -71.4 |
| 5 | 3.7 | -0.1 | -0.1 | -0.2 | -2.6 | -2.7 | -2.4 |
| 6 | -23.1 | -17.4 | -17.4 | -17.5 | -21.0 | -21.0 | -20.3 |
| 7 | -16.2 | -12.1 | -12.0 | -12.8 | -15.7 | -15.6 | -15.3 |
| 8 | -17.2 | -12.8 | -12.9 | -13.3 | -16.0 | -16.0 | -15.3 |
| 9 | -18.8 | -14.3 | -14.3 | -15.1 | -16.1 | -16.1 | -15.0 |
| 10 | -22.6 | -16.4 | -16.6 | -16.4 | -19.4 | -19.4 | -19.1 |
| 11 | 27.0 | 30.0 | 30.1 | 29.8 | 30.9 | 30.9 | 30.2 |
| 12 | -29.8 | -24.6 | -24.6 | -24.7 | -29.9 | -29.9 | -28.9 |
| 13 | -43.2 | -38.0 | -38.1 | -37.9 | -43.9 | -43.9 | -43.6 |
| 14 | -52.0 | -43.8 | -44.0 | -44.7 | -50.9 | -51.1 | -50.5 |
| 15 | -4.1 | -5.0 | -5.1 | -5.1 | -4.8 | -4.9 | -4.4 |
| 16 | -39.8 | -39.3 | -39.8 | -39.9 | -40.4 | -40.7 | -40.0 |
| 17 | -16.1 | -14.5 | -14.6 | -14.5 | -13.7 | -13.7 | -11.2 |
| 18 | -34.2 | -31.8 | -32.0 | -31.9 | -33.3 | -33.4 | -32.8 |
| 19 | -40.1 | -37.2 | -37.4 | -37.3 | -38.7 | -38.7 | -38.0 |
| 20 | -30.2 | -29.2 | -29.4 | -29.3 | -28.6 | -28.6 | -27.8 |
| 21 | -15.1 | -18.5 | -18.8 | -19.0 | -18.7 | -18.8 | -17.1 |
| 22 | -35.9 | -32.3 | -32.6 | -32.6 | -33.5 | -33.7 | -32.1 |
| 23 | -55.0 | -51.2 | -51.4 | -51.3 | -52.6 | -52.8 | -52.3 |
| 24 | -41.6 | -40.8 | -41.7 | -41.5 | -41.3 | -42.0 | -41.7 |
| 25 | -45.9 | -45.4 | -46.4 | -46.0 | -45.6 | -46.4 | -45.6 |
| 26 | -36.4 | -42.4 | -42.6 | -42.5 | -38.5 | -38.7 | -39.0 |
| 27 | -21.8 | -26.8 | -27.0 | -27.1 | -25.1 | -25.3 | -25.5 |
| 28 | -36.3 | -41.7 | -41.9 | -41.8 | -39.2 | -39.4 | -39.5 |
| 29 | -28.3 | -32.8 | -33.0 | -32.6 | -30.0 | -30.1 | -30.0 |
| 30 | -14.9 | -21.8 | -22.1 | -21.6 | -16.3 | -16.6 | -16.1 |
| 31 | -29.9 | -32.8 | -33.2 | -33.5 | -29.4 | -29.8 | -29.7 |
| 32 | -1.9 | 0.1 | 0.1 | 0.5 | 0.2 | 0.2 | 0.7 |
| 33 | -10.7 | -18.9 | -19.0 | -19.1 | -9.4 | -9.5 | -8.8 |
| 34 | -25.6 | -30.3 | -30.5 | -30.6 | -25.1 | -25.2 | -25.0 |
| 35 | -30.9 | -34.6 | -34.7 | -34.9 | -29.8 | -29.9 | -29.9 |
| 36 | -39.8 | -39.4 | -39.5 | -39.7 | -34.9 | -34.9 | -35.3 |
| 37 | -14.0 | -33.0 | -33.4 | -33.4 | -23.3 | -23.5 | -23.4 |
| 38 | -64.4 | -72.2 | -72.6 | -72.6 | -69.1 | -69.4 | -71.8 |
| 39 | -63.9 | -58.2 | -58.5 | -59.0 | -60.7 | -60.9 | -59.5 |
| 40 | -65.8 | -66.4 | -66.5 | -66.3 | -69.0 | -69.1 | -69.2 |
| 41 | -3.2 | -6.3 | -6.3 | -6.6 | -3.0 | -3.0 | -3.4 |
| MD |) | -0.1 | -0.3 | -0.4 | -0.3 | -0.4 | 0.0 |
| MA | | 4.2 | 4.2 | 4.2 | 2.3 | 2.3 | 2.6 |
| RM | | 5.3 | 5.3 | 5.2 | 3.1 | 3.1 | 3.4 |
| SD | | 33.7 | 33.9 | 33.5 | 19.7 | 19.8 | 21.8 |
| Var | | 28.3 | 28.8 | 28.0 | 9.7 | 9.8 | 11.9 |
| Max | | 8.2 | 7.9 | 7.3 | 5.0 | 4.9 | 4.9 |
| Mir | | -19.0 | -19.4 | -19.3 | -9.2 | -9.5 | -9.4 |
| AM | | 19.0 | 19.4 | 19.3 | 9.2 | 9.5 | 9.4 |
| | | | | | <u> </u> | | |

Table A16: Extendet statistical evaluations of : PW6B95 and CAM-B3LYP in kcal $\rm mol^{-1}$. We abbreviate D3(BJ)-ATM by D3.

| | | | PW6R05 | PW6B95 | | | |
|-----|-------|--------|--------|--------|--------|---------------------|-------|
| # | Ref. | D4-ATM | D4-MBD | D3 | D4-ATM | CAM-B3LYI D4-MBD | D3 |
| 1 | -43.1 | -41.8 | -41.8 | -41.8 | -40.1 | -40.1 | -40.1 |
| 2 | -46.6 | -42.9 | -43.0 | -42.9 | -42.7 | -42.8 | -42.7 |
| 3 | -27.6 | -22.6 | -22.6 | -22.5 | -23.2 | -23.2 | -23.1 |
| 4 | -62.5 | -63.0 | -63.0 | -63.0 | -64.4 | -64.4 | -64.2 |
| 5 | 3.7 | 1.0 | 1.1 | 1.1 | 2.7 | 2.7 | 3.0 |
| 6 | -23.1 | -19.8 | -19.7 | -19.7 | -19.5 | -19.4 | -18.6 |
| 7 | -16.2 | -16.5 | -16.0 | -16.0 | -14.1 | -14.1 | -13.4 |
| 8 | -17.2 | -12.2 | -12.4 | -12.6 | -15.8 | -15.8 | -14.8 |
| 9 | -18.8 | -12.5 | -12.3 | -12.2 | -17.8 | -17.8 | -16.5 |
| 10 | -22.6 | -15.5 | -15.6 | -15.6 | -15.8 | -15.9 | -15.3 |
| 11 | 27.0 | 32.8 | 33.0 | 32.7 | 33.6 | 33.7 | 33.1 |
| 12 | -29.8 | -28.4 | -28.2 | -28.2 | -24.3 | -24.3 | -23.0 |
| 13 | -43.2 | -40.9 | -40.7 | -40.7 | -38.4 | -38.4 | -37.9 |
| 14 | -52.0 | -47.9 | -48.1 | -48.6 | -44.1 | -44.3 | -43.5 |
| 15 | -4.1 | -3.9 | -4.0 | -3.8 | -9.6 | -9.7 | -9.1 |
| 16 | -39.8 | -40.0 | -40.5 | -40.8 | -39.0 | -39.3 | -38.2 |
| 17 | -16.1 | -15.2 | -15.2 | -15.0 | -16.2 | -16.3 | -13.1 |
| 18 | -34.2 | -29.4 | -29.3 | -31.0 | -30.2 | -30.3 | -29.8 |
| 19 | -40.1 | -34.5 | -34.5 | -36.2 | -36.4 | -36.5 | -35.9 |
| 20 | -30.2 | -27.1 | -26.9 | -27.8 | -28.2 | -28.3 | -27.3 |
| 21 | -15.1 | -16.0 | -16.1 | -17.5 | -14.4 | -14.6 | -12.8 |
| 22 | -35.9 | -26.1 | -26.6 | -29.1 | -27.4 | -27.6 | -26.5 |
| 23 | -55.0 | -46.8 | -46.7 | -49.2 | -49.0 | -49.1 | -49.2 |
| 24 | -41.6 | -39.7 | -41.2 | -42.0 | -40.7 | -41.3 | -41.0 |
| 25 | -45.9 | -43.0 | -44.7 | -45.4 | -45.0 | -45.6 | -44.7 |
| 26 | -36.4 | -33.5 | -34.2 | -34.8 | -42.1 | -42.3 | -42.9 |
| 27 | -21.8 | -21.4 | -22.1 | -22.7 | -27.4 | -27.5 | -28.2 |
| 28 | -36.3 | -34.3 | -34.9 | -35.6 | -41.8 | -41.9 | -42.6 |
| 29 | -28.3 | -26.1 | -26.7 | -27.0 | -32.1 | -32.2 | -32.4 |
| 30 | -14.9 | -9.9 | -10.6 | -11.0 | -17.4 | -17.7 | -17.7 |
| 31 | -29.9 | -25.4 | -26.4 | -26.8 | -33.3 | -33.6 | -34.1 |
| 32 | -1.9 | -1.2 | -1.1 | -1.2 | 0.5 | 0.5 | 0.8 |
| 33 | -10.7 | -10.5 | -10.7 | -10.7 | -18.5 | -18.6 | -18.1 |
| 34 | -25.6 | -24.1 | -24.4 | -24.9 | -28.6 | -28.7 | -28.8 |
| 35 | -30.9 | -28.7 | -29.0 | -30.0 | -32.7 | -32.9 | -33.3 |
| 36 | -39.8 | -33.5 | -33.5 | -35.2 | -36.5 | -36.6 | -37.7 |
| 37 | -14.0 | -19.6 | -20.2 | -19.6 | -26.7 | -26.9 | -26.9 |
| 38 | -64.4 | -59.6 | -60.5 | -61.7 | -67.0 | -67.3 | -70.0 |
| 39 | -63.9 | -61.0 | -61.2 | -62.4 | -60.8 | -60.9 | -59.8 |
| 40 | -65.8 | -66.2 | -66.2 | -66.8 | -65.9 | -66.0 | -66.2 |
| 41 | -3.2 | -1.0 | -1.4 | -1.4 | -5.9 | -6.0 | -6.6 |
| MD |) | 2.7 | 2.4 | 1.9 | 0.5 | 0.4 | 0.7 |
| MA | | 3.2 | 3.0 | 2.6 | 3.7 | 3.7 | 4.3 |
| RM | | 4.0 | 3.8 | 3.3 | 4.6 | 4.6 | 5.0 |
| SD | | 18.9 | 19.1 | 17.2 | 28.9 | 29.1 | 31.4 |
| Var | | 8.9 | 9.1 | 7.4 | 21.0 | 21.2 | 24.7 |
| Max | | 9.8 | 9.2 | 7.1 | 8.5 | 8.3 | 9.3 |
| Min | | -5.6 | -6.2 | -5.6 | -12.7 | -12.8 | -12.8 |
| AM | | 9.8 | 9.2 | 7.1 | 12.7 | 12.8 | 12.8 |
| | | | | | | | |

Table A17: Extendet statistical evaluations of : revPBE and M06L in kcal $\rm mol^{-1}$. We abbreviate D3(BJ)-ATM by D3.

| | - () - | 11M by D5. | | | | | |
|-----|---------|------------|--------|-------|----------|----------|----------|
| | | | revPBE | | | M06L | _ |
| _# | Ref. | D4-ATM | D4-MBD | D3 | D4-ATM | D4-MBD | D3 |
| 1 | -43.1 | -44.5 | -44.6 | -45.0 | -41.0 | -41.0 | -40.7 |
| 2 | -46.6 | -47.6 | -47.6 | -48.0 | -45.1 | -45.1 | -44.9 |
| 3 | -27.6 | -29.0 | -29.1 | -29.2 | -27.1 | -27.1 | -26.9 |
| 4 | -62.5 | -73.6 | -73.8 | -74.5 | -64.9 | -64.9 | -64.7 |
| 5 | 3.7 | -6.8 | -6.7 | -7.1 | -2.7 | -2.7 | -2.5 |
| 6 | -23.1 | -17.9 | -17.9 | -18.1 | -18.1 | -18.1 | -18.1 |
| 7 | -16.2 | -12.9 | -12.9 | -13.3 | -16.8 | -16.8 | -16.8 |
| 8 | -17.2 | -14.2 | -14.3 | -15.3 | -7.7 | -7.7 | -7.5 |
| 9 | -18.8 | -14.0 | -13.8 | -15.0 | -7.2 | -7.2 | -8.2 |
| 10 | -22.6 | -24.6 | -24.7 | -25.0 | -13.2 | -13.2 | -12.7 |
| 11 | 27.0 | 24.2 | 24.5 | 23.9 | 30.7 | 30.7 | 31.3 |
| 12 | -29.8 | -30.6 | -30.4 | -30.9 | -24.7 | -24.7 | -24.3 |
| 13 | -43.2 | -44.8 | -44.7 | -45.0 | -39.8 | -39.8 | -39.4 |
| 14 | -52.0 | -51.2 | -51.3 | -52.9 | -50.0 | -50.0 | -49.2 |
| 15 | -4.1 | 1.9 | 1.7 | 1.6 | 5.4 | 5.4 | 5.5 |
| 16 | -39.8 | -41.7 | -42.0 | -43.0 | -42.3 | -42.3 | -40.6 |
| 17 | -16.1 | -14.8 | -14.9 | -14.7 | -18.2 | -18.2 | -17.7 |
| 18 | -34.2 | -34.8 | -34.5 | -35.7 | -24.7 | -24.7 | -23.9 |
| 19 | -40.1 | -39.0 | -38.5 | -39.9 | -28.8 | -28.8 | -27.7 |
| 20 | -30.2 | -31.2 | -30.9 | -31.9 | -24.6 | -24.6 | -23.6 |
| 21 | -15.1 | -23.9 | -23.7 | -25.2 | -13.7 | -13.7 | -12.7 |
| 22 | -35.9 | -37.5 | -37.1 | -38.5 | -21.8 | -21.7 | -20.7 |
| 23 | -55.0 | -52.2 | -51.6 | -53.4 | -40.8 | -40.8 | -39.8 |
| 24 | -41.6 | -39.1 | -40.0 | -41.0 | -39.0 | -38.9 | -36.8 |
| 25 | -45.9 | -43.5 | -44.7 | -45.3 | -44.0 | -43.9 | -41.1 |
| 26 | -36.4 | -35.5 | -35.6 | -36.1 | -33.7 | -33.7 | -33.0 |
| 27 | -21.8 | -21.5 | -21.7 | -22.2 | -22.2 | -22.2 | -22.1 |
| 28 | -36.3 | -36.0 | -36.2 | -36.6 | -33.9 | -33.9 | -33.5 |
| 29 | -28.3 | -28.9 | -29.1 | -28.8 | -25.7 | -25.7 | -25.4 |
| 30 | -14.9 | -23.2 | -23.2 | -22.9 | -12.4 | -12.4 | -12.2 |
| 31 | -29.9 | -28.0 | -28.4 | -29.3 | -23.8 | -23.8 | -23.9 |
| 32 | -1.9 | -0.5 | -0.3 | 0.2 | 1.4 | 1.4 | 1.4 |
| 33 | -10.7 | -10.5 | -10.6 | -10.4 | -12.1 | -12.1 | -11.8 |
| 34 | -25.6 | -25.1 | -25.1 | -25.5 | -22.1 | -22.1 | -21.7 |
| 35 | -30.9 | -29.1 | -29.0 | -29.8 | -23.6 | -23.5 | -23.2 |
| 36 | -39.8 | -33.6 | -33.2 | -34.5 | -29.8 | -29.8 | -29.6 |
| 37 | -14.0 | -29.7 | -30.4 | -30.5 | -26.4 | -26.5 | -26.1 |
| 38 | -64.4 | -73.0 | -73.0 | -74.4 | -59.1 | -59.1 | -57.4 |
| 39 | -63.9 | -56.7 | -56.8 | -59.0 | -56.1 | -56.1 | -55.6 |
| 40 | -65.8 | -66.7 | -66.5 | -66.9 | -65.0 | -65.0 | -64.7 |
| 41 | -3.2 | -1.3 | -1.4 | -1.4 | -4.7 | -4.7 | -4.9 |
| MD |) | -0.6 | -0.6 | -1.3 | 3.6 | 3.6 | 4.2 |
| MA | | 3.3 | 3.3 | 3.2 | 5.1 | 5.1 | 5.4 |
| RM | | 4.8 | 4.9 | 4.9 | 6.4 | 6.4 | 6.8 |
| SD | | 30.7 | 31.0 | 30.5 | 34.1 | 34.1 | 34.5 |
| Var | | 23.6 | 24.1 | 23.3 | 29.1 | 29.1 | 29.7 |
| Max | | 7.2 | 7.2 | 5.7 | 14.2 | 14.2 | 15.2 |
| Min | | -15.7 | -16.3 | -16.5 | -12.4 | -12.5 | -12.1 |
| AM | | 15.7 | 16.3 | 16.5 | 14.2 | 14.2 | 15.2 |
| | | | | _0.0 | - | - | - |

Table A18: Extendet statistical evaluations of : PBE and RPBE in kcal $\rm mol^{-1}$. We abbreviate D3(BJ)-ATM by D3.

| | | | DDE | | | DDDD | |
|------|-------|--------|---------------|-------|--------|----------------|-------|
| # | Ref. | D4-ATM | PBE D4-MBD | D3 | D4-ATM | RPBE D4-MBD | D3 |
| 1 | -43.1 | -46.7 | -46.8 | -46.7 | -44.4 | -44.6 | -49.0 |
| 2 | -46.6 | -50.0 | -50.0 | -50.0 | -47.3 | -47.6 | -51.6 |
| 3 | -27.6 | -31.5 | -31.5 | -31.4 | -28.8 | -29.0 | -31.8 |
| 4 | -62.5 | -75.1 | -75.2 | -75.2 | -74.0 | -74.5 | -76.4 |
| 5 | 3.7 | -7.4 | -7.4 | -7.4 | -7.2 | -7.2 | -8.6 |
| 6 | -23.1 | -20.4 | -20.4 | -20.4 | -17.7 | -17.8 | -11.6 |
| 7 | -16.2 | -14.9 | -14.8 | -15.3 | -12.1 | -11.7 | -4.3 |
| 8 | -17.2 | -14.4 | -14.5 | -14.7 | -14.1 | -14.4 | -13.6 |
| 9 | -18.8 | -16.0 | -15.9 | -16.4 | -15.3 | -15.2 | -10.5 |
| 10 | -22.6 | -24.5 | -24.6 | -24.4 | -24.6 | -24.9 | -28.1 |
| 11 | 27.0 | 25.0 | 25.0 | 25.0 | 24.4 | 24.9 | 18.2 |
| 12 | -29.8 | -30.8 | -30.7 | -30.6 | -30.8 | -30.8 | -26.0 |
| 13 | -43.2 | -45.2 | -45.2 | -45.0 | -44.9 | -45.1 | -48.9 |
| 14 | -52.0 | -52.3 | -52.5 | -52.6 | -51.2 | -51.5 | -55.5 |
| 15 | -4.1 | 1.2 | 1.1 | 1.1 | 1.2 | 0.8 | 3.8 |
| 16 | -39.8 | -39.5 | -39.9 | -39.7 | -40.5 | -41.0 | -42.2 |
| 17 | -16.1 | -14.4 | -14.5 | -14.4 | -14.6 | -14.6 | -2.1 |
| 18 | -34.2 | -32.5 | -32.6 | -32.1 | -36.0 | -36.0 | -44.7 |
| 19 | -40.1 | -36.3 | -36.4 | -35.8 | -39.9 | -39.9 | -48.6 |
| 20 | -30.2 | -28.1 | -28.1 | -27.7 | -32.2 | -32.1 | -38.0 |
| 21 | -15.1 | -20.4 | -20.6 | -20.3 | -25.2 | -25.3 | -28.0 |
| 22 | -35.9 | -35.2 | -35.4 | -34.7 | -38.5 | -38.6 | -48.8 |
| 23 | -55.0 | -50.2 | -50.3 | -49.6 | -53.8 | -53.6 | -65.6 |
| 24 | -41.6 | -36.8 | -37.6 | -37.2 | -38.1 | -39.4 | -47.5 |
| 25 | -45.9 | -41.4 | -42.3 | -41.7 | -41.6 | -43.3 | -50.6 |
| 26 | -36.4 | -34.9 | -35.1 | -34.9 | -35.6 | -35.9 | -41.8 |
| 27 | -21.8 | -21.9 | -22.1 | -22.1 | -21.8 | -22.3 | -30.1 |
| 28 | -36.3 | -35.5 | -35.7 | -35.5 | -36.3 | -36.8 | -44.2 |
| 29 | -28.3 | -27.7 | -27.8 | -27.5 | -29.0 | -29.4 | -35.5 |
| 30 | -14.9 | -19.9 | -20.1 | -19.7 | -23.6 | -23.8 | -28.7 |
| 31 | -29.9 | -26.6 | -26.9 | -27.0 | -28.9 | -29.6 | -36.5 |
| 32 | -1.9 | 0.9 | 0.9 | 1.2 | -0.5 | -0.4 | -0.4 |
| 33 | -10.7 | -9.5 | -9.6 | -9.7 | -10.1 | -10.1 | -5.2 |
| 34 | -25.6 | -23.8 | -23.9 | -23.8 | -25.0 | -25.0 | -27.0 |
| 35 | -30.9 | -28.1 | -28.2 | -28.1 | -29.2 | -29.2 | -34.1 |
| 36 | -39.8 | -32.8 | -32.9 | -32.7 | -34.3 | -34.0 | -41.5 |
| 37 | -14.0 | -29.8 | -30.0 | -30.0 | -30.3 | -31.3 | -31.1 |
| 38 | -64.4 | -68.5 | -68.8 | -68.4 | -73.9 | -74.3 | -99.4 |
| 39 | -63.9 | -57.0 | -57.2 | -57.1 | -58.6 | -59.5 | -68.8 |
| 40 | -65.8 | -68.4 | -68.5 | -68.2 | -67.4 | -67.5 | -79.4 |
| 41 | -3.2 | -2.8 | -2.9 | -3.2 | -1.1 | -1.0 | 2.6 |
| MD | | -0.1 | -0.3 | -0.1 | -0.9 | -1.1 | -4.7 |
| MA | D | 3.5 | 3.4 | 3.5 | 3.4 | 3.4 | 8.3 |
| RMSD | | 4.8 | 4.7 | 4.8 | 5.0 | 5.1 | 10.1 |
| SD | | 30.5 | 30.4 | 30.6 | 31.4 | 31.7 | 57.5 |
| Var | | 23.3 | 23.0 | 23.4 | 24.6 | 25.2 | 82.6 |
| Max | | 7.0 | 6.9 | 7.1 | 5.5 | 5.9 | 14.0 |
| Min | | -15.7 | -16.0 | -16.0 | -16.2 | -17.3 | -35.0 |
| AM | ax | 15.7 | 16.0 | 16.0 | 16.2 | 17.3 | 35.0 |

K. Statistical evaluation: SCONF

Table A19: Reference values are calculated on a DLPNO-CCSD(T)/TightPNO/CBS(aug-cc-pVTZ/aug-cc-pVQZ) level of theory. We follow the nomenclature of the GMTKN55 [24] database. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | DSF | BLYP | R3 | LYP | PW | 6B95 | ī | PBE |
|--------|------|------|------|------|------|------|------|------|------|
| # | Ref. | D4 | D3 | D4 | D3 | D4 | D3 | D4 | D3 |
| | | | ANGC | L15 | | | | | |
| C1-C2 | 0.9 | 0.9 | 0.9 | 0.8 | 0.8 | 0.9 | 0.9 | 0.8 | 0.8 |
| C1-C3 | 2.3 | 2.2 | 2.2 | 2.5 | 2.6 | 2.5 | 2.5 | 3.2 | 3.2 |
| C1-C4 | 3.1 | 3.1 | 3.1 | 3.2 | 3.3 | 3.3 | 3.3 | 3.9 | 3.9 |
| C1-C5 | 4.6 | 4.5 | 4.5 | 4.5 | 4.4 | 4.7 | 4.7 | 5.1 | 5.1 |
| C1-C6 | 4.9 | 4.8 | 4.8 | 4.7 | 4.7 | 5.1 | 5.1 | 5.4 | 5.4 |
| C1-C7 | 4.2 | 4.2 | 4.2 | 4.6 | 4.5 | 4.3 | 4.2 | 5.3 | 5.3 |
| C1-C8 | 4.4 | 4.3 | 4.3 | 4.7 | 4.5 | 4.4 | 4.3 | 5.3 | 5.2 |
| C1-C9 | 6.2 | 6.2 | 6.1 | 6.2 | 6.0 | 6.4 | 6.3 | 6.8 | 6.6 |
| C1-C10 | 6.2 | 6.1 | 6.1 | 6.3 | 6.1 | 6.5 | 6.4 | 7.1 | 6.9 |
| C1-C11 | 5.7 | 5.6 | 5.6 | 5.9 | 5.7 | 5.8 | 5.7 | 6.5 | 6.4 |
| C1-C12 | 5.6 | 5.6 | 5.6 | 6.0 | 5.8 | 5.8 | 5.7 | 6.7 | 6.6 |
| C1-C13 | 5.9 | 5.8 | 5.8 | 6.0 | 5.7 | 6.7 | 6.5 | 6.8 | 6.7 |
| C1-C14 | 6.3 | 6.3 | 6.3 | 6.4 | 6.2 | 6.5 | 6.4 | 6.8 | 6.7 |
| C1-C15 | 6.2 | 6.3 | 6.2 | 6.5 | 6.0 | 6.2 | 6.0 | 6.8 | 6.5 |
| | | | GLC | C4 | | | | | |
| G1-G2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 |
| G1-G3 | 6.2 | 6.2 | 6.3 | 5.3 | 5.6 | 4.8 | 5.0 | 4.6 | 4.8 |
| G1–G4 | 5.5 | 5.1 | 5.2 | 3.5 | 3.8 | 4.8 | 5.0 | 2.6 | 2.8 |
| MD | | 0.0 | 0.0 | -0.1 | -0.1 | 0.0 | 0.0 | 0.3 | 0.3 |
| MAD | | 0.1 | 0.1 | 0.3 | 0.3 | 0.3 | 0.2 | 0.9 | 0.8 |
| RMSD | | 0.1 | 0.1 | 0.6 | 0.5 | 0.4 | 0.4 | 1.1 | 1.0 |
| SD | | 0.5 | 0.4 | 2.4 | 1.9 | 1.8 | 1.6 | 4.3 | 3.9 |
| Var | | 0.0 | 0.0 | 0.3 | 0.2 | 0.2 | 0.2 | 1.1 | 0.9 |
| Max | | 0.1 | 0.1 | 0.4 | 0.3 | 0.7 | 0.6 | 1.2 | 1.1 |
| Min | | -0.4 | -0.4 | -2.1 | -1.7 | -1.3 | -1.2 | -3.0 | -2.7 |
| AMax | | 0.4 | 0.4 | 2.1 | 1.7 | 1.3 | 1.2 | 3.0 | 2.7 |

L. Statistical evaluation: PCONF21

Table A20: The reference energies were generated on the DLPNO-CCSD(T)/TightPNO/CBS(aug-cc-pVTZ/aug-cc-pVQZ) level of theory while the original geometries were kept. We follow the nomenclature of the GMTKN55 [24] database. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | DSI | BLYP | В3 | LYP | PW | 6B95 |] | PBE |
|------------------|------|------------|---------|------|------|------|------|------|------|
| # | Ref. | D4 | D3 | D4 | D3 | D4 | D3 | D4 | D3 |
| | | Tripe | eptides | | | | | | |
| 99-444 | 0.0 | 0.2^{-1} | 0.1 | -0.3 | -0.7 | 0.9 | 0.7 | -2.2 | -2.5 |
| 99-357 | 1.0 | 1.0 | 0.8 | 0.9 | 0.1 | 0.9 | 0.6 | -1.0 | -1.5 |
| 99-366 | 0.7 | 1.1 | 1.0 | 1.2 | 1.1 | 1.7 | 1.7 | 0.6 | 0.5 |
| 99 - 215 | 0.8 | 1.1 | 0.9 | 0.6 | 0.2 | 1.6 | 1.4 | -1.2 | -1.4 |
| 99-300 | 0.8 | 1.3 | 1.2 | 1.5 | 1.2 | 1.6 | 1.5 | 0.8 | 0.6 |
| 99–114 | 1.9 | 1.8 | 1.6 | 1.7 | 1.1 | 1.6 | 1.3 | 0.1 | -0.3 |
| 99-412 | 2.2 | 2.2 | 2.1 | 2.0 | 1.9 | 2.1 | 2.1 | 1.4 | 1.4 |
| 99-691 | 1.6 | 1.9 | 1.8 | 1.9 | 1.8 | 2.3 | 2.3 | 1.1 | 1.1 |
| 99 - 470 | 1.9 | 2.0 | 1.9 | 2.3 | 1.7 | 2.6 | 2.3 | 1.4 | 1.0 |
| 99-224 | 2.1 | 1.8 | 1.7 | 1.2 | 1.0 | 2.9 | 2.8 | -0.2 | -0.4 |
| | | C | LY | | | | | | |
| GLY_ab-GLY_aR | 1.1 | 1.1 | 1.2 | 0.9 | 1.3 | 1.2 | 1.4 | 1.3 | 1.6 |
| GLY_ab-GLY_pII | 1.2 | 1.5 | 1.5 | 1.8 | 1.9 | 2.2 | 2.3 | 2.3 | 2.4 |
| GLY_ab-GLY_aL | 2.4 | 2.5 | 2.7 | 2.4 | 3.0 | 2.2 | 2.5 | 2.8 | 3.2 |
| GLY_ab-GLY_b | 2.1 | 1.8 | 1.9 | 1.8 | 1.8 | 2.1 | 2.1 | 1.3 | 1.3 |
| | | | ER | | | | | | |
| SER_ab-SER_aR | 1.5 | 1.6 | 1.6 | 1.6 | 1.9 | 1.6 | 1.7 | 2.0 | 2.2 |
| SER_ab-SER_pII | 2.8 | 3.1 | 3.2 | 3.2 | 3.5 | 3.6 | 3.7 | 3.9 | 4.0 |
| SER_ab-SER_aL | 2.3 | 2.7 | 2.8 | 2.6 | 3.2 | 1.8 | 2.1 | 3.4 | 3.7 |
| SER_ab-SER_b | 2.7 | 2.5 | 2.6 | 2.5 | 2.5 | 2.9 | 2.9 | 2.3 | 2.3 |
| MD | | 0.1 | 0.1 | 0.0 | 0.0 | 0.4 | 0.3 | -0.5 | -0.5 |
| MAD | | 0.2 | 0.2 | 0.3 | 0.5 | 0.5 | 0.5 | 1.0 | 1.2 |
| RMSD | | 0.3 | 0.3 | 0.4 | 0.6 | 0.6 | 0.6 | 1.2 | 1.4 |
| SD | | 1.0 | 1.2 | 1.7 | 2.6 | 2.0 | 2.0 | 4.8 | 5.7 |
| Var | | 0.1 | 0.1 | 0.2 | 0.4 | 0.2 | 0.2 | 1.4 | 1.9 |
| Max | | 0.5 | 0.6 | 0.7 | 0.9 | 1.0 | 1.0 | 1.1 | 1.5 |
| Min | | -0.3 | -0.4 | -0.9 | -1.1 | -0.5 | -0.6 | -2.3 | -2.5 |
| AMax | | 0.5 | 0.6 | 0.9 | 1.1 | 1.0 | 1.0 | 2.3 | 2.5 |

M. Statistical evaluation: ICONF

Table A21: Reference energies are obtained with the W1–F12 protocol on TPSS-D3(BJ)/def2-TZVP optimised geometries without spin–orbit and DBOC. We follow the nomenclature of the GMTKN55 [24] database. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | DSDBLYP | | | B3 | LYP | PW | 6B95 | F | PBE | |
|-----------------------|---------|------|------|------|------|------|------|------|------|--|
| # | Ref. | D4 | D3 | D4 | D3 | D4 | D3 | D4 | D3 | |
| N3H5_1-N3H5_2 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | |
| N3H5_1-N3H5_3 | 5.3 | 5.3 | 5.4 | 5.2 | 5.3 | 5.2 | 5.2 | 5.6 | 5.6 | |
| $N4H6_{-}1-N4H6_{-}2$ | 0.1 | 0.5 | 0.5 | 0.6 | 0.6 | 0.8 | 0.9 | 0.4 | 0.4 | |
| N4H6_1-N4H6_3 | 2.3 | 2.7 | 2.7 | 3.0 | 3.1 | 3.2 | 3.2 | 3.0 | 3.0 | |
| N3P3H12_1-N3P3H12_2 | 12.2 | 12.5 | 12.5 | 12.2 | 12.3 | 12.2 | 12.2 | 11.9 | 11.9 | |
| $SI5H12_1 - SI5H12_2$ | 0.1 | -0.1 | 0.0 | 0.1 | 0.2 | -0.1 | 0.0 | 0.1 | 0.2 | |
| SI5H12_1-SI5H12_3 | 1.0 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | |
| $SI5H12_1-SI5H12_4$ | 3.5 | 3.7 | 3.7 | 3.3 | 3.3 | 3.5 | 3.4 | 3.1 | 3.1 | |
| SI6H12_1-SI6H12_2 | 1.7 | 1.8 | 1.8 | 1.7 | 1.5 | 1.4 | 1.4 | 1.6 | 1.4 | |
| $P7H7_{-}1-P7H7_{-}2$ | 1.4 | 1.6 | 1.6 | 1.6 | 1.6 | 1.5 | 1.6 | 1.2 | 1.2 | |
| S4O4_1-S4O4_2 | 4.4 | 4.5 | 4.5 | 4.2 | 4.3 | 3.8 | 3.9 | 5.0 | 5.0 | |
| S8_1-S8_2 | 9.2 | 9.1 | 9.1 | 9.4 | 9.1 | 9.1 | 9.2 | 10.3 | 10.0 | |
| H2S2O7_1-H2S2O7_2 | 0.6 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | |
| H2S2O7_1-H2S2O7_3 | 3.5 | 3.2 | 3.2 | 3.1 | 3.2 | 3.6 | 3.6 | 3.1 | 3.2 | |
| H4P2O7_1-H4P2O7_2 | 1.3 | 1.4 | 1.4 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | |
| H4P2O7_1-H4P2O7_3 | 3.7 | 3.4 | 3.4 | 3.0 | 3.0 | 3.6 | 3.6 | 3.8 | 3.8 | |
| H4P2O7_1-H4P2O7_4 | 4.3 | 3.7 | 3.7 | 3.2 | 3.4 | 4.5 | 4.4 | 4.2 | 4.3 | |
| MD | | 0.0 | 0.0 | -0.1 | -0.1 | 0.0 | 0.0 | 0.1 | 0.1 | |
| MAD | | 0.2 | 0.2 | 0.3 | 0.3 | 0.2 | 0.2 | 0.3 | 0.3 | |
| RMSD | | 0.3 | 0.3 | 0.4 | 0.4 | 0.3 | 0.3 | 0.4 | 0.4 | |
| SD | | 1.1 | 1.1 | 1.7 | 1.6 | 1.4 | 1.4 | 1.6 | 1.5 | |
| Var | | 0.1 | 0.1 | 0.2 | 0.2 | 0.1 | 0.1 | 0.2 | 0.1 | |
| Max | | 0.4 | 0.4 | 0.7 | 0.8 | 0.8 | 0.9 | 1.1 | 0.8 | |
| Min | | -0.7 | -0.6 | -1.1 | -1.0 | -0.6 | -0.5 | -0.4 | -0.4 | |
| AMax | | 0.7 | 0.6 | 1.1 | 1.0 | 0.8 | 0.9 | 1.1 | 0.8 | |

N. Statistical evaluation: UPU23

Table A22: Reference values are obtained at the DLPNO-CCSD(T)/CBS*//TPSS-D3(BJ)/def2-TZVP(COSMO) level of theory. We follow the nomenclature of the GMTKN55 [24] database. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | DSD | BLYP | В3 | LYP | PW | 6B95 | I | PBE |
|---------------------------------|------|------|------|------|------|------|------|------|------|
| # | Ref. | D4 | D3 | D4 | D3 | D4 | D3 | D4 | D3 |
| 2p-1a | 4.9 | 5.4 | 5.5 | 5.6 | 6.0 | 6.0 | 6.1 | 5.5 | 5.7 |
| 2p-1b | 3.0 | 3.7 | 3.8 | 3.6 | 4.1 | 4.2 | 4.3 | 4.0 | 4.2 |
| 2p-1c | 8.9 | 9.4 | 9.6 | 9.7 | 10.1 | 10.4 | 10.6 | 9.6 | 9.8 |
| 2p-1g | 2.2 | 2.6 | 2.6 | 2.7 | 2.7 | 3.2 | 3.2 | 2.9 | 2.9 |
| 2p-1p | 2.0 | 2.7 | 2.8 | 2.4 | 2.7 | 3.0 | 3.0 | 2.5 | 2.6 |
| 2p-2a | 3.1 | 3.0 | 3.0 | 3.5 | 3.5 | 2.9 | 2.9 | 3.1 | 3.1 |
| 2p-5z | 0.6 | 0.2 | 0.4 | -0.3 | 0.1 | 0.9 | 0.9 | 0.8 | 1.0 |
| 2p-6p | 3.3 | 3.2 | 3.2 | 3.1 | 3.2 | 3.0 | 3.1 | 2.9 | 2.9 |
| 2p-7a | 7.3 | 8.4 | 8.4 | 8.8 | 8.8 | 8.4 | 8.4 | 8.9 | 8.9 |
| 2p–aa | 4.0 | 4.4 | 4.4 | 4.8 | 4.9 | 4.2 | 4.2 | 5.0 | 5.2 |
| $2\mathrm{p}	ext{-}1\mathrm{e}$ | 11.1 | 11.8 | 11.8 | 11.8 | 12.0 | 12.2 | 12.3 | 11.7 | 11.9 |
| 2p-0a | 4.8 | 5.9 | 6.0 | 6.0 | 6.2 | 5.7 | 5.8 | 5.6 | 5.7 |
| 2p-1f | 14.4 | 14.1 | 14.1 | 14.3 | 14.4 | 14.1 | 14.2 | 13.8 | 13.9 |
| 2p-9a | 5.2 | 5.5 | 5.5 | 5.8 | 5.7 | 5.5 | 5.4 | 5.7 | 5.7 |
| 2p-4b | 5.5 | 5.6 | 5.6 | 5.5 | 5.6 | 5.7 | 5.7 | 5.3 | 5.4 |
| 2p-3a | 6.8 | 7.2 | 7.2 | 7.3 | 7.3 | 7.6 | 7.6 | 6.7 | 6.7 |
| 2p-7p | 3.9 | 3.7 | 3.7 | 3.6 | 3.6 | 3.5 | 3.5 | 3.5 | 3.5 |
| 2p-8d | 6.4 | 6.4 | 6.5 | 6.7 | 6.8 | 6.4 | 6.5 | 6.5 | 6.6 |
| 2p-3d | 5.4 | 5.5 | 5.5 | 5.7 | 5.8 | 5.7 | 5.8 | 5.6 | 5.7 |
| 2p-0b | 6.7 | 6.5 | 6.5 | 6.1 | 6.2 | 6.3 | 6.3 | 5.9 | 6.0 |
| 2p-1m | 5.6 | 6.8 | 6.8 | 6.7 | 6.7 | 6.7 | 6.7 | 5.9 | 5.9 |
| 2p-2h | 10.4 | 10.9 | 10.9 | 11.5 | 11.4 | 10.7 | 10.8 | 10.4 | 10.4 |
| 2p-3b | 6.1 | 6.5 | 6.5 | 6.4 | 6.4 | 6.6 | 6.6 | 6.2 | 6.2 |
| MD | | 0.3 | 0.4 | 0.4 | 0.6 | 0.5 | 0.5 | 0.3 | 0.4 |
| MAD | | 0.4 | 0.5 | 0.6 | 0.7 | 0.6 | 0.7 | 0.5 | 0.6 |
| RMSD | | 0.6 | 0.6 | 0.7 | 0.8 | 0.8 | 0.8 | 0.6 | 0.7 |
| SD | | 2.1 | 2.2 | 2.7 | 2.8 | 2.8 | 2.9 | 2.8 | 2.9 |
| Var | | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.3 | 0.4 |
| Max | | 1.2 | 1.2 | 1.5 | 1.6 | 1.5 | 1.7 | 1.6 | 1.7 |
| Min | | -0.3 | -0.3 | -0.9 | -0.5 | -0.4 | -0.4 | -0.8 | -0.8 |
| AMax | | 1.2 | 1.2 | 1.5 | 1.6 | 1.5 | 1.7 | 1.6 | 1.7 |

O. Statistical evaluation: ROT34

Table A23: Statistical data for the results of the ROT34 test set for three DFAs using the def2–QZVP basis set. Anharmonic corrections have been performed at the HF/DZ level of theory as described in the literature [25]. All values are given in MHz. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | | | PBE0 | | PBE | | TPSS |
|-----|-----------------|--------|--------|--------|-----------------|--------|--------|--------|
| # | rot. const | Ref. | D3 | D4 | D3 | D4 | D3 | D4 |
| | A | 4293.9 | 4299.8 | 4298.1 | 4240.8 | 4238.8 | 4235.9 | 4235.8 |
| 1 | В | 1395.9 | 1400.7 | 1400.7 | 1383.9 | 1382.9 | 1384.5 | 1384.1 |
| | $^{\mathrm{C}}$ | 1130.2 | 1133.1 | 1132.9 | 1119.3 | 1118.3 | 1119.5 | 1119.1 |
| | A | 3322.5 | 3309.3 | 3307.7 | 3247.0 | 3247.8 | 3239.0 | 3240.4 |
| 2 | В | 719.8 | 718.8 | 719.0 | 707.2 | 707.5 | 709.5 | 709.4 |
| | $^{\mathrm{C}}$ | 698.0 | 697.0 | 697.2 | 686.0 | 686.0 | 687.7 | 687.6 |
| | A | 3071.1 | 3071.9 | 3071.3 | 3023.0 | 3022.8 | 3021.0 | 3022.3 |
| 3 | В | 1285.0 | 1289.9 | 1290.4 | 1271.9 | 1270.9 | 1271.1 | 1270.2 |
| | $^{\mathrm{C}}$ | 1248.7 | 1249.0 | 1249.3 | 1232.4 | 1231.7 | 1231.0 | 1230.7 |
| | A | 2755.9 | 2765.6 | 2765.8 | 2731.3 | 2731.7 | 2729.3 | 2730.3 |
| 4 | В | 2675.6 | 2689.5 | 2689.3 | 2652.4 | 2652.1 | 2653.3 | 2653.1 |
| | C | 2653.3 | 2666.5 | 2666.8 | 2631.5 | 2631.8 | 2633.1 | 2634.1 |
| 5 | A | 2336.9 | 2339.1 | 2339.9 | 2307.0 | 2306.5 | 2306.0 | 2307.1 |
| | A | 1464.2 | 1471.0 | 1471.1 | 1440.0 | 1439.7 | 1439.1 | 1439.9 |
| 6 | В | 768.2 | 767.6 | 768.3 | 756.4 | 757.1 | 762.1 | 763.0 |
| 0 | Č | 580.6 | 580.9 | 581.4 | 572.3 | 572.7 | 576.1 | 576.8 |
| | Ä | 1165.7 | 1170.2 | 1170.4 | 1152.1 | 1153.5 | 1154.6 | 1155.9 |
| 7 | В | 661.2 | 660.6 | 661.3 | 653.3 | 653.8 | 654.0 | 654.6 |
| • | Č | 454.0 | 454.6 | 454.9 | 448.9 | 449.4 | 449.6 | 450.2 |
| | Ä | 1166.3 | 1167.7 | 1168.3 | 1147.9 | 1148.4 | 1153.1 | 1155.3 |
| 8 | В | 767.6 | 766.4 | 767.0 | 752.7 | 753.0 | 754.3 | 755.0 |
| 0 | Č | 513.0 | 512.5 | 512.9 | 504.3 | 504.5 | 505.6 | 506.4 |
| | A | 862.5 | 865.9 | 866.0 | 852.4 | 852.4 | 853.2 | 853.8 |
| 9 | В | 754.2 | 752.8 | 752.8 | 741.8 | 741.7 | 742.6 | 742.9 |
| 3 | Č | 513.7 | 513.6 | 513.7 | 505.7 | 505.6 | 506.5 | 506.8 |
| | Ä | 3086.2 | 3101.0 | 3100.5 | 3060.2 | 3059.9 | 3061.3 | 3061.6 |
| 10 | В | 723.7 | 725.3 | 725.2 | 716.2 | 715.9 | 715.8 | 716.0 |
| 10 | C | 685.0 | 686.7 | 686.6 | 678.0 | 677.8 | 677.7 | 677.9 |
| | A | 1432.1 | 1436.0 | 1435.5 | 1416.5 | 1416.5 | 1418.6 | 1418.9 |
| 11 | В | 820.5 | 822.8 | 822.9 | 810.9 | 811.4 | 812.1 | 813.3 |
| 11 | C | 679.4 | 683.0 | 682.9 | 674.1 | 675.0 | 675.4 | 676.1 |
| | A | 1523.2 | 1523.3 | 1521.2 | 1496.3 | 1495.8 | 1497.2 | 1497.4 |
| 12 | В | 1070.5 | 1075.0 | 1076.0 | 1490.3 1059.8 | 1060.6 | 1060.9 | 1061.9 |
| 12 | С | 719.9 | 721.1 | 721.5 | 709.3 | 709.7 | 711.0 | 711.9 |
| | | 719.9 | | | | | | |
| MD | | | 2.6 | 2.7 | -18.1 | -18.1 | -17.6 | -17.0 |
| MAD | | | 3.8 | 3.9 | 18.1 | 18.1 | 17.6 | 17.0 |
| RMS | D | | 5.7 | 5.8 | 23.3 | 23.4 | 24.1 | 23.7 |
| SD | | | 29.4 | 30.0 | 85.5 | 86.5 | 96.5 | 95.9 |
| Var | | | 26.1 | 27.3 | 221.8 | 226.5 | 282.2 | 278.9 |
| Max | | | 14.8 | 14.3 | -5.1 | -4.4 | -4.0 | -3.3 |
| Min | | | -13.2 | -14.8 | -75.5 | -74.7 | -83.5 | -82.1 |
| AMa | x | | 14.8 | 14.8 | 75.5 | 74.7 | 83.5 | 82.1 |

Table A24: Statistical data for the results of the ROT34 test set for three DFAs using the def2–QZVP basis set. Anharmonic corrections have been performed at the HF/DZ level of theory as described in the literature [25]. All values are given in MHz. We abbreviate D3(BJ)-ATM by D3 and D4(TB)-ATM by D4.

| | | | | BE0 | | PBE | | PSS |
|-------------------------------|-------------|-----------------------------|--|---|---|---|---|---|
| # | rot. const | Ref. | D3 | D4 | D3 | D4 | D3 | D4 |
| 1 | A B C | 4293.9 1395.9 1130.2 | $4299.8 \\ 1400.7 \\ 1133.1$ | 4300.5 1400.3 1132.8 | 4240.8 1383.9 1119.3 | 4239.3 1383.6 1118.8 | 4235.9 1384.5 1119.5 | 4239.0 1384.9 1119.9 |
| 2 | A B C | 3322.5 719.8 698.0 | 3309.3 718.8 697.0 | 3308.4 718.9 697.1 | $3247.0 \\ 707.2 \\ 686.0$ | $3247.9 \\ 708.0 \\ 686.3$ | 3239.0 709.5 687.7 | 3243.4 710.5 688.3 |
| 3 | А В С | 3071.1 1285.0 1248.7 | 3071.9 1289.9 1249.0 | 3072.6 1290.0 1248.8 | 3023.0 1271.9 1232.4 | 3023.1 1271.9 1232.0 | 3021.0 1271.1 1231.0 | 3024.1 1272.3 1231.8 |
| 4 | А В С | 2755.9 2675.6 2653.3 | $2765.6 \\ 2689.5 \\ 2666.5$ | 2766.1 2689.8 2667.2 | $2731.3 \\ 2652.4 \\ 2631.5$ | $2732.3 \\ 2652.8 \\ 2632.2$ | 2729.3 2653.3 2633.1 | 2732.0 2654.7 2635.1 |
| 5 | A | 2336.9 | 2339.1 | 2339.1 | 2307.0 | 2307.1 | 2306.0 | 2308.6 |
| 6 | А В С | $1464.2 \\ 768.2 \\ 580.6$ | $1471.0 \\ 767.6 \\ 580.9$ | 1471.4 768.5 581.5 | $1440.0 \\ 756.4 \\ 572.3$ | 1440.2 757.3 572.8 | 1439.1 762.1 576.1 | $1440.7 \\ 764.5 \\ 577.9$ |
| 7 | А В С | $1165.7 \\ 661.2 \\ 454.0$ | $1170.2 \\ 660.6 \\ 454.6$ | $1170.1\\661.0\\454.8$ | $1152.1 \\ 653.3 \\ 448.9$ | $1153.4 \\ 653.8 \\ 449.4$ | $1154.6 \\ 654.0 \\ 449.6$ | $1156.2 \\ 654.7 \\ 450.2$ |
| 8 | А В С | 1166.3 767.6 513.0 | $1167.7 \\ 766.4 \\ 512.5$ | $ \begin{array}{c} 1168.3 \\ 766.9 \\ 512.8 \end{array} $ | 1147.9 752.7 504.3 | 1149.6 753.3 504.8 | $1153.1 \\ 754.3 \\ 505.6$ | $ \begin{array}{c} 1158.8 \\ 755.8 \\ 507.2 \end{array} $ |
| 9 | А В С | 862.5 754.2 513.7 | 865.9 752.8 513.6 | 866.0 752.8 513.7 | 852.4 741.8 505.7 | 852.6 741.9 505.8 | 853.2 742.6 506.5 | 854.7 743.6 507.3 |
| 10 | A B C | 3086.2 723.7 685.0 | 3101.0 725.3 686.7 | 3100.8 725.3 686.6 | 3060.2 716.2 678.0 | 3060.5 716.1 677.9 | 3061.3 715.8 677.7 | 3063.5 716.6 678.5 |
| 11 | A B C | $1432.1 \\ 820.5 \\ 679.4$ | $1436.0 \\ 822.8 \\ 683.0$ | $1435.6 \\ 822.6 \\ 682.7$ | 1416.5 810.9 674.1 | 1416.4 810.9 674.1 | $1418.6 \\ 812.1 \\ 675.4$ | $ \begin{array}{c} 1421.2 \\ 813.2 \\ 676.3 \end{array} $ |
| 12 | А В С | $1523.2 \\ 1070.5 \\ 719.9$ | $1523.3 \\ 1075.0 \\ 721.1$ | $1520.1 \\ 1076.4 \\ 721.5$ | $1496.3 \\ 1059.8 \\ 709.3$ | $1495.5 \\ 1060.6 \\ 710.1$ | 1497.2 1060.9 711.0 | $1499.0 \\ 1062.5 \\ 712.7$ |
| MD MAI RMS SD Var Max Min AMa | SD | | 2.6 3.8 5.7 29.4 26.1 14.8 -13.2 14.8 | 2.7 4.0 5.9 30.6 28.3 14.6 -14.1 14.6 | -18.1 18.1 23.3 85.5 221.8 -5.1 -75.5 75.5 | -17.8 17.8 23.1 86.0 224.3 -4.6 -74.6 74.6 | -17.6 17.6 24.1 96.5 282.2 -4.0 -83.5 83.5 | -15.8 15.8 22.4 92.7 260.3 -2.7 -79.1 79.1 |

P. Statistical evaluation: LMGB35

Table A25: The LMGB35 benchmark set contains of systems from the first and second row of the periodic system. All bond lengths are given in pm. Reference distances are taken from Ref. [26]. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | D | DD0 | Т | DE | TT: | TIDGG. | | |
|--|----------------|-------|-------|-------|-------|-------|-------|--------|--|--|
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | system(bond) | Ref. | | | | | | | | |
| $\begin{array}{c} H_2 \circ (HO) & 95.7 & 95.7 & 95.7 & 96.9 & 96.9 & 96.7 \\ HOF(OH) & 96.6 & 96.6 & 96.6 & 97.9 & 97.9 & 97.7 & 97.7 \\ OH(O-H) & 97.0 & 97.0 & 97.0 & 98.3 & 98.3 & 98.2 & 98.1 \\ NH_3 (N-H) & 101.2 & 101.1 & 101.1 & 102.1 & 102.1 & 101.9 & 101.8 \\ OH^+ (O-H) & 102.9 & 103.2 & 103.2 & 104.7 & 104.7 & 104.0 & 103.9 \\ NH(N-H) & 103.6 & 103.7 & 103.7 & 105.0 & 104.9 & 104.4 & 104.4 \\ C_2H_2 (C-H) & 106.2 & 106.4 & 106.4 & 107.0 & 107.0 & 106.5 & 106.5 \\ NO^+ (N-O) & 106.3 & 105.3 & 105.3 & 106.9 & 106.9 & 106.6 & 106.6 \\ HCN (H-C) & 106.5 & 106.8 & 106.8 & 107.5 & 107.5 & 107.0 & 107.0 \\ NH^+ (N-H) & 107.0 & 107.6 & 107.6 & 109.1 & 109.1 & 108.3 & 108.3 \\ C_2H_4 (C-H) & 108.1 & 108.3 & 108.3 & 109.1 & 109.1 & 108.6 & 108.6 \\ CH_4 (CH) & 108.6 & 108.8 & 108.8 & 109.5 & 109.5 & 109.1 & 109.1 \\ N_2 (N-N) & 109.8 & 108.9 & 108.9 & 110.2 & 110.2 & 109.9 & 109.9 \\ CH_2 O(O-H) & 109.9 & 110.7 & 110.7 & 111.7 & 111.7 & 111.0 & 111.0 \\ N_2^+ (N-N) & 111.6 & 110.1 & 110.1 & 111.4 & 111.4 & 111.2 & 111.2 \\ CH (C-H) & 112.0 & 112.4 & 112.4 & 113.6 & 113.6 & 112.9 & 112.9 \\ CO(C-O) & 112.8 & 112.2 & 112.2 & 113.5 & 113.5 & 113.3 & 113.3 \\ HCN (C-N) & 115.3 & 114.5 & 114.5 & 115.7 & 115.7 & 115.4 & 115.4 \\ C_2H_2 (C-C) & 120.3 & 119.6 & 119.6 & 120.6 & 120.6 & 120.2 & 120.2 \\ CH_2 (C-C) & 120.3 & 119.5 & 119.9 & 121.3 & 121.3 & 121.2 & 121.2 \\ O_2 (O-O) & 120.8 & 119.9 & 119.9 & 121.3 & 121.3 & 121.2 & 121.2 \\ O_2 (O-O) & 120.8 & 119.9 & 119.9 & 121.3 & 121.3 & 121.2 & 121.2 \\ O_2 (O-O) & 120.8 & 119.2 & 119.2 & 121.8 & 121.8 & 121.9 & 121.9 \\ OC(C-F) & 120.3 & 119.5 & 119.5 & 120.8 & 120.8 & 120.7 & 120.7 \\ BO(B-O) & 120.5 & 119.9 & 119.9 & 121.3 & 121.3 & 121.2 & 121.2 \\ O_2 (O-O) & 120.8 & 119.2 & 119.2 & 121.8 & 121.8 & 121.9 & 121.9 \\ O_2 (O-O) & 120.8 & 119.2 & 119.2 & 121.8 & 121.8 & 121.9 & 121.9 \\ OC(C-F) & 120.3 & 119.5 & 119.5 & 120.8 & 120.8 & 120.7 & 120.7 \\ OC(C-F) & 120.3 & 119.5 & 119.5 & 120.8 & 120.8 & 120.7 & 120.7 \\ OC(C-F) & 120.3 & 119.5 & 119.5 & 120.8 & 120.8 & 120.7 & 120.7 \\ OC(C-F) & 120.3 & 119.5 & 1$ | | 74.1 | 74.5 | 74.4 | | 75.0 | 74.3 | 74.2 | | |
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| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $O^{\pm}(O,O)$ | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $C_2H_2(C-C)$ | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 120.5 | 119.9 | 119.9 | 121.3 | | 121.2 | 121.2 | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $O_2(O-O)$ | 120.8 | 119.2 | 119.2 | 121.8 | 121.8 | 121.9 | 121.9 | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | BH(B-H) | 123.2 | 124.0 | 124.0 | 125.1 | 125.1 | 123.6 | 123.6 | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | BF(B-F) | 126.3 | | | 127.3 | | | 127.3 | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 131.7 | 130.3 | 130.3 | 132.7 | 132.7 | 133.3 | 133.3 | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | |
| B2(B-B) 159.0 161.3 161.3 161.8 161.8 161.9 161.9 MD -0.5 -0.6 1.0 1.0 0.7 0.7 MAD 0.9 0.9 1.0 1.0 0.8 0.8 RMSD 1.4 1.4 1.2 1.2 1.0 1.0 SD 7.8 7.7 4.0 3.9 3.9 3.9 Var 1.8 1.7 0.5 0.5 0.5 0.5 Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | | | | | | | | | | |
| MD | | | | | | | | | | |
| MAD 0.9 0.9 1.0 1.0 0.8 0.8 RMSD 1.4 1.4 1.2 1.2 1.0 1.0 SD 7.8 7.7 4.0 3.9 3.9 3.9 Var 1.8 1.7 0.5 0.5 0.5 0.5 Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | B2(B-B) | 159.0 | 161.3 | 161.3 | 161.8 | 161.8 | 161.9 | 161.9 | | |
| RMSD 1.4 1.4 1.2 1.2 1.0 1.0 SD 7.8 7.7 4.0 3.9 3.9 3.9 Var 1.8 1.7 0.5 0.5 0.5 0.5 Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | | | -0.5 | -0.6 | 1.0 | 1.0 | 0.7 | 0.7 | | |
| SD 7.8 7.7 4.0 3.9 3.9 3.9 Var 1.8 1.7 0.5 0.5 0.5 0.5 Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | | | | | | | | | | |
| Var 1.8 1.7 0.5 0.5 0.5 0.5 Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | | | | | | | | | | |
| Max 2.3 2.3 2.8 2.8 2.9 2.9 Min -5.0 -4.9 -0.6 -0.6 -0.5 -0.5 | | | | | | | | | | |
| Min -5.0 -4.9 -0.6 -0.5 -0.5 | | | | | | | | | | |
| | | | | | | | | | | |
| AMax 5.0 4.9 2.8 2.8 2.9 2.9 | | | | | | | | | | |
| | AMax | | 5.0 | 4.9 | 2.8 | 2.8 | 2.9 | 2.9 | | |

Table A26: The LMGB35 benchmark set contains of systems from the first and second row of the periodic system. All bond lengths are given in pm. Reference distances are taken from Ref. [26].We abbreviate D3(BJ)-ATM by D3 and D4(TB)-ATM by D4.

| | | P | BE0 | F | BE | T | TPSS | | |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|--|--|
| system(bond) | Ref. | D3 | D4 | D3 | D4 | D3 | D4 | | |
| $H_2(H-H)$ | 74.1 | 74.5 | 74.4 | 75.0 | 74.2 | 74.3 | 74.2 | | |
| HF(H-F) | 91.7 | 91.8 | 91.7 | 93.0 | 92.9 | 92.9 | 92.9 | | |
| $H_2O(HO)$ | 95.7 | 95.7 | 95.7 | 96.9 | 96.7 | 96.7 | 96.7 | | |
| HOF(OH) | 96.6 | 96.6 | 96.6 | 97.9 | 97.7 | 97.7 | 97.7 | | |
| OH(O-H) | 97.0 | 97.0 | 97.0 | 98.3 | 98.1 | 98.2 | 98.1 | | |
| $NH_3(N-H)$ | 101.2 | 101.1 | 101.1 | 102.1 | 101.9 | 101.9 | 101.9 | | |
| $OH^{+}(O-H)$ | 102.9 | 103.2 | 103.2 | 104.7 | 103.9 | 104.0 | 103.9 | | |
| NH(N-H) | 103.6 | 103.7 | 103.7 | 105.0 | 104.4 | 104.4 | 104.4 | | |
| $C_2H_2(C-H)$ | 106.2 | 106.4 | 106.4 | 107.0 | 106.5 | 106.5 | 106.5 | | |
| $NO^{+}(N-O)$ | 106.3 | 105.3 | 105.3 | 106.9 | 106.6 | 106.6 | 106.6 | | |
| HCN(H-C) | 106.5 | 106.8 | 106.8 | 107.5 | 107.0 | 107.0 | 107.0 | | |
| $NH^{+}(N-H)$ | 107.0 | 107.6 | 107.6 | 109.1 | 108.3 | 108.3 | 108.3 | | |
| $C_2H_4(C-H)$ | 108.1 | 108.3 | 108.3 | 109.1 | 108.6 | 108.6 | 108.6 | | |
| $CH_4(CH)$ | 108.6 | 108.8 | 108.8 | 109.5 | 109.1 | 109.1 | 109.1 | | |
| $N_2(N-N)$ | 109.8 | 108.9 | 108.9 | 110.2 | 109.9 | 109.9 | 109.9 | | |
| $CH_2O(O-H)$ | 109.9 | 110.7 | 110.7 | 111.7 | 111.0 | 111.0 | 111.0 | | |
| $N_{2}^{+}(N-N)$ | 111.6 | 110.1 | 110.1 | 111.4 | 111.2 | 111.2 | 111.2 | | |
| $O_2^{\uparrow}(O-O)$ | 111.6 | 109.8 | 109.8 | 112.1 | 112.0 | 112.0 | 112.0 | | |
| CH(C-H) | 112.0 | 112.4 | 112.4 | 113.6 | 112.9 | 112.9 | 112.9 | | |
| CO(C-O) | 112.8 | 112.2 | 112.2 | 113.5 | 113.3 | 113.3 | 113.3 | | |
| HCN(C-N) | 115.3 | 114.5 | 114.5 | 115.7 | 115.4 | 115.4 | 115.4 | | |
| $CO_2(C-O)$ | 116.0 | 115.6 | 115.6 | 117.0 | 116.8 | 116.8 | 116.8 | | |
| $C_2H_2(C-C)$ | 120.3 | 119.6 | 119.6 | 120.6 | 120.2 | 120.2 | 120.2 | | |
| $\mathrm{CH_2O(C-O)}$ | 120.3 | 119.5 | 119.5 | 120.8 | 120.7 | 120.7 | 120.7 | | |
| BO(B-O) | 120.5 | 119.9 | 119.9 | 121.3 | 121.2 | 121.2 | 121.2 | | |
| $O_2(O-O)$ | 120.8 | 119.2 | 119.2 | 121.8 | 121.9 | 121.9 | 121.9 | | |
| BH(B-H) | 123.2 | 124.0 | 124.0 | 125.1 | 123.6 | 123.6 | 123.6 | | |
| BF(B-F) | 126.3 | 125.9 | 125.9 | 127.3 | 127.3 | 127.3 | 127.3 | | |
| CF(C-F) | 127.2 | 126.7 | 126.7 | 128.5 | 128.9 | 128.9 | 128.9 | | |
| NF(N-F) | 131.7 | 130.3 | 130.3 | 132.7 | 133.3 | 133.3 | 133.3 | | |
| $F_2^+(F-F)$ | 132.2 | 127.2 | 127.3 | 131.6 | 131.7 | 131.7 | 131.7 | | |
| $C_2H_4(C-C)$ | 133.4 | 132.2 | 132.2 | 133.2 | 133.0 | 133.0 | 133.0 | | |
| $F_2(F-F)$ | 141.2 | 137.5 | 137.6 | 141.4 | 141.6 | 141.6 | 141.6 | | |
| HOF(O-F) | 143.5 | 140.5 | 140.6 | 144.5 | 145.0 | 145.0 | 145.0 | | |
| B2(B-B) | 159.0 | 161.3 | 161.3 | 161.8 | 161.9 | 161.9 | 161.9 | | |
| MD | | -0.5 | -0.6 | 1.0 | 0.7 | 0.7 | 0.7 | | |
| MAD | | 0.9 | 0.9 | 1.0 | 0.8 | 0.8 | 0.8 | | |
| RMSD | | 1.4 | 1.4 | 1.2 | 1.0 | 1.0 | 1.0 | | |
| SD | | 7.8 | 7.7 | 4.0 | 3.9 | 3.9 | 3.9 | | |
| Var | | 1.8 | 1.7 | 0.5 | 0.5 | 0.5 | 0.5 | | |
| Max | | 2.3 | 2.3 | 2.8 | 2.9 | 2.9 | 2.9 | | |
| Min | | -5.0 | -4.9 | -0.6 | -0.5 | -0.5 | -0.5 | | |
| AMax | | 5.0 | 4.9 | 2.8 | 2.9 | 2.9 | 2.9 | | |

Q. Statistical evaluation: HMGB11

Table A27: Experimental reference bond distances for 11 molecules from Ref. [27] containing third–row or higher main group elements. All distances are given in pm. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | P | BE0 | F | PBE | Т | PSS |
|--|-------|-------|-------|-------|-------|-------|-------|
| system(bond) | Ref. | D3 | D4 | D3 | D4 | D3 | D4 |
| Cl ₂ (Cl–Cl) | 198.8 | 197.9 | 197.9 | 200.4 | 200.5 | 200.8 | 200.8 |
| $S_2H_2(S-S)$ | 205.5 | 204.4 | 204.4 | 206.3 | 206.3 | 206.4 | 206.4 |
| $P_2(CH_3)_4(P-P)$ | 221.2 | 219.2 | 219.2 | 221.3 | 221.4 | 220.9 | 221.0 |
| $Br_2(Br-Br)$ | 228.1 | 227.8 | 227.8 | 230.8 | 230.8 | 230.5 | 230.5 |
| $Se_2H_2(Se-Se)$ | 234.6 | 232.4 | 232.4 | 235.0 | 235.0 | 234.4 | 234.4 |
| $Ge_2H_6(Ge-Ge)$ | 241.0 | 242.1 | 242.1 | 243.3 | 243.3 | 242.5 | 242.5 |
| $As_2(CH_3)_4(As-As)$ | 242.9 | 243.8 | 243.8 | 247.3 | 247.2 | 246.1 | 246.1 |
| $Te_2(CH_3)_2(Te-Te)$ | 268.6 | 267.3 | 267.3 | 269.7 | 269.6 | 268.5 | 269.1 |
| $\operatorname{Sn}_{2}(\operatorname{CH}_{3})_{6}(\operatorname{Sn-Sn})$ | 277.6 | 277.7 | 278.0 | 279.6 | 280.1 | 278.4 | 278.9 |
| $Sb_2(CH_3)_4(Sb-Sb)$ | 281.8 | 282.5 | 282.6 | 286.2 | 286.1 | 284.9 | 285.0 |
| $Pb_2(CH_3)_6(Pb-Pb)$ | 288.0 | 287.1 | 287.2 | 292.0 | 291.9 | 289.8 | 290.3 |
| MD | | -0.5 | -0.5 | 2.2 | 2.2 | 1.4 | 1.5 |
| MAD | | 1.0 | 1.1 | 2.2 | 2.2 | 1.5 | 1.6 |
| RMSD | | 1.2 | 1.2 | 2.6 | 2.6 | 1.8 | 1.9 |
| SD | | 3.6 | 3.6 | 4.9 | 4.8 | 4.0 | 3.8 |
| Var | | 1.3 | 1.3 | 2.4 | 2.3 | 1.6 | 1.5 |
| Max | | 1.1 | 1.1 | 4.4 | 4.3 | 3.2 | 3.2 |
| Min | | -2.2 | -2.2 | 0.1 | 0.2 | -0.3 | -0.2 |
| AMax | | 2.2 | 2.2 | 4.4 | 4.3 | 3.2 | 3.2 |

Table A28: Experimental reference bond distances for 11 molecules from Ref. [27] containing third—row or higher main group elements. All distances are given in pm. We abbreviate D3(BJ)-ATM by D3 and D4(TB)-ATM by D4.

| | | P | BE0 | P | BE | Т | PSS |
|--|-------|-------|-------|-------|-------|-------|-------|
| system(bond) | Ref. | D3 | D4 | D3 | D4 | D3 | D4 |
| Cl ₂ (Cl–Cl) | 198.8 | 197.9 | 197.9 | 200.4 | 200.5 | 200.8 | 200.8 |
| $S_2H_2(S-S)$ | 205.5 | 204.4 | 204.4 | 206.3 | 206.4 | 206.4 | 206.4 |
| $P_2(CH_3)_4(P-P)$ | 221.2 | 219.2 | 219.2 | 221.3 | 221.7 | 220.9 | 221.3 |
| $\mathrm{Br}_2(\mathrm{Br}\mathrm{-Br})$ | 228.1 | 227.8 | 227.8 | 230.8 | 230.8 | 230.5 | 230.6 |
| $Se_2H_2(Se-Se)$ | 234.6 | 232.4 | 232.4 | 235.0 | 235.0 | 234.4 | 234.5 |
| $Ge_2H_6(Ge-Ge)$ | 241.0 | 242.1 | 242.1 | 243.3 | 243.3 | 242.5 | 242.6 |
| $As_2(CH_3)_4(As-As)$ | 242.9 | 243.8 | 243.8 | 247.3 | 247.4 | 246.1 | 246.3 |
| $Te_2(CH_3)_2(Te-Te)$ | 268.6 | 267.3 | 267.3 | 269.7 | 269.8 | 268.5 | 269.2 |
| $\operatorname{Sn}_2(\operatorname{CH}_3)_6(\operatorname{Sn-Sn})$ | 277.6 | 277.7 | 278.0 | 279.6 | 280.7 | 278.4 | 279.3 |
| $Sb_2(CH_3)_4(Sb-Sb)$ | 281.8 | 282.5 | 282.6 | 286.2 | 286.8 | 284.9 | 285.5 |
| $Pb_2(CH_3)_6(Pb-Pb)$ | 288.0 | 287.1 | 287.2 | 292.0 | 292.7 | 289.8 | 291.0 |
| MD | | -0.5 | -0.5 | 2.2 | 2.4 | 1.4 | 1.8 |
| MAD | | 1.0 | 1.1 | 2.2 | 2.4 | 1.5 | 1.8 |
| RMSD | | 1.2 | 1.2 | 2.6 | 2.9 | 1.8 | 2.1 |
| SD | | 3.6 | 3.6 | 4.9 | 5.3 | 4.0 | 4.1 |
| Var | | 1.3 | 1.3 | 2.4 | 2.9 | 1.6 | 1.7 |
| Max | | 1.1 | 1.1 | 4.4 | 5.0 | 3.2 | 3.7 |
| Min | | -2.2 | -2.2 | 0.1 | 0.4 | -0.3 | -0.1 |
| AMax | | 2.2 | 2.2 | 4.4 | 5.0 | 3.2 | 3.7 |

R. Statistical evaluation: TMC32

Table A29: Diverse set of 32 metal complexes from the first transition row, for which precise gasphase geometries are known from electron diffraction or microwave spectroscopy. Compilation by Bühl *et al.* [28]. We abbreviate D3(BJ)-ATM by D3 and D4-ATM by D4.

| | | Д | BE0 | | BE | Т. | PSS |
|---|------------------|------------------|------------------|-----------------------|------------------|------------------|----------------|
| system(bond) | Ref. | D3 | D4 | D3 | D4 | D3 | rss D4 |
| Sc(acac) ₃ (Sc-O) | 207.6 | 209.0 | 208.8 | 210.4 | 210.3 | 210.0 | 209.8 |
| $\operatorname{TiCl_4(Ti-Cl)}$ | 216.9 | 209.0 216.4 | 208.8 216.4 | 210.4 | 210.3 218.2 | 210.0 218.3 | 218.3 |
| $Ti(CH_3)Cl_3(Ti-C)$ | 210.9 204.7 | 202.3 | 202.3 | 204.5 | 204.7 | 205.3 | 205.3 |
| Ti(CH ₃)Cl ₃ (Ti–Cl) | 218.5 | 218.0 | 217.9 | 219.3 | 219.2 | 219.5 | 219.4 |
| Ti(CH ₃) ₂ Cl ₂ (Ti–C) | 205.8 | 203.5 | 203.6 | 205.5 | 205.5 | 206.3 | 206.3 |
| Ti(CH ₃) ₂ Cl ₂ (Ti-Cl) | 219.6 | 219.6 | 219.6 | 220.5 | 220.4 | 220.7 | 220.6 |
| $Ti(BD_4)_3(Ti-B)$ | 217.5 | 214.3 | 214.3 | 214.7 | 214.6 | 214.9 | 214.8 |
| $Ti(BD_4)_3(Ti-D^{br})$ | 198.4 | 193.4 | 193.5 | 193.7 | 193.7 | 193.2 | 193.1 |
| $VOF_3(V=O)$ | 157.0 | 154.1 | 154.1 | 157.5 | 157.5 | 157.6 | 157.5 |
| $VOF_3(V-F)$ | 172.9 | 171.6 | 171.6 | 173.7 | 173.7 | 173.4 | 173.4 |
| $VF_5(V-F^{ax})$ | 173.4 | 173.5 | 173.5 | 176.4 | 176.4 | 175.9 | 175.9 |
| $VF_5(V-F^{eq})$ | 170.8 | 169.9 | 169.9 | 172.7 | 172.6 | 172.3 | 172.3 |
| VOCl ₃ (V=O) | 157.3 | 153.9 | 153.9 | 157.2 | 157.2 | 157.3 | 157.3 |
| $VOCl_3(V-Cl)$ | 213.8 | 213.0 | 213.0 | 215.0 | 214.9 | 214.9 | 214.9 |
| $V(N(CH_3)_2)_4(V-N)$ | 187.9 | 186.1 | 186.1 | 188.2 | 188.1 | 188.1 | 187.9 |
| $V(Cp)(CO)_4(V-C^{CO})$ $CrO_2F_2(Cr=O)$ | $196.3 \\ 157.4$ | 192.3 153.7 | 192.3 153.6 | $192.7 \\ 157.1$ | 192.7 157.1 | 194.4 157.0 | 194.3 157.0 |
| $CrO_2F_2(Cr=O)$ $CrO_2F_2(Cr-F)$ | 157.4 171.9 | 170.2 | 170.2 | 172.4 | 172.3 | 172.0 | 172.0 |
| $CrO_2Cl_2(Cr=O)$ | 157.7 | 153.8 | 153.8 | 157.2 | 172.3 157.2 | 172.0 157.2 | 157.1 |
| $CrO_2Cl_2(Cr-Cl)$ | 212.2 | 210.6 | 210.6 | 212.4 | 212.4 | 212.4 | 212.3 |
| $CrO_2(NO_3)_2(Cr=O)$ | 158.4 | 153.8 | 153.8 | 157.4 | 157.4 | 157.4 | 157.4 |
| $CrO_2(NO_3)_2(Cr-O)$ | 195.4 | 191.0 | 191.0 | 193.2 | 193.2 | 193.0 | 192.9 |
| $Cr(C_6H_6)_2(Cr-C)$ | 215.0 | 213.0 | 212.9 | 213.8 | 213.7 | 213.6 | 213.5 |
| $Cr(C_6H_6)(CO)_3(Cr-C^{Ar})$ | 220.8 | 219.1 | 219.2 | 221.0 | 221.1 | 220.2 | 220.2 |
| $\operatorname{Cr}(\operatorname{C}_6\operatorname{H}_6)(\operatorname{CO})_3(\operatorname{Cr-C}^{CO})$ | 186.3 | 183.8 | 183.8 | 183.9 | 183.9 | 185.2 | 185.0 |
| $Cr(NO)_4(Cr-N)$ | 175.0 | 171.5 | 171.5 | 174.1 | 174.1 | 174.1 | 174.0 |
| $MnO_3F(Mn=O)$ | 158.6 | 154.2 | 154.2 | 159.2 | 157.7 | 157.6 | 157.6 |
| $MnO_3F(Mn-F)$ | 172.4 | 170.1 | 170.1 | 171.0 | 172.0 | 171.6 | 171.6 |
| $MnCp(CO)_3(Mn-C^{Cp})$ | 214.7 | 213.7 | 213.7 | 215.2 | 215.1 | 214.3 | 214.2 |
| $MnCp(CO)_3(Mn-C^{CO})$ | 180.6 | 178.3 | 178.3 | 178.4 | 178.3 | 179.4 | 179.3 |
| $Fe(CO)_5(Fe-C)^{mean}$ | 182.9 | 179.7 | 179.7 | 180.2 | 180.1 | 181.0 | 180.9 |
| $Fe(CO)_3(tmm)(Fe-C^{CO})$ | 181.0 | 177.9 | 177.9 | 178.0 | 178.0 | 178.8 | 178.8 |
| $Fe(CO)_3(tmm)(Fe-C_{cont}^{cent})$ | 193.8 | 192.2 | 192.2 | 194.6 | 194.6 | 194.3 | 194.3 |
| $Fe(CO)_3(tmm)(Fe-C^{CH_2})$ | 212.3 | 209.8 | 209.9 | 213.1 | 213.2 | 212.0 | 212.2 |
| $Fe(CO)_2(NO)_2(Fe-C)^{mean}$ | 187.2 | 180.8 | 180.8 | 181.5 | 181.3 | 182.3 | 182.2 |
| $Fe(CO)_2(NO)_2(Fe-N)$ | 167.4 | 164.1 | 164.1 | 167.1 | 167.0 | 166.9 | 166.9 |
| $FeCp_2(Fe-C)$ | 206.4 | 204.2 | 204.2 | 204.0 | 204.1 | 203.7 | 203.5 |
| $\operatorname{Fe}(\operatorname{C}_{2}\operatorname{H}_{4})(\operatorname{CO})_{4}(\operatorname{Fe-C}^{et})$ | 211.7 | 209.7 | 216.2 | 213.0 | 216.7 | 212.3 | 216.7 |
| $\operatorname{Fe}(\operatorname{C}_2\operatorname{H}_4)(\operatorname{CO})_4(\operatorname{Fe}-\operatorname{C}^{ax})$ | 181.5 | 180.0 | 180.1 | 179.9 | 179.9 | $180.7 \\ 179.6$ | 180.7 |
| $Fe(C_2H_4)(CO)_4(Fe-C^{eq})$ $Fe(C_5(CH_3)_5)(P_5)(Fe-P)$ | $180.6 \\ 237.7$ | $178.1 \\ 235.7$ | $177.8 \\ 235.7$ | $178.9 \\ 236.3$ | $178.7 \\ 236.1$ | 234.9 | 179.3 234.7 |
| $CoH(CO)_4(Co-C^{eq})$ | 181.8 | 233.7 178.4 | 233.7 178.4 | $\frac{250.5}{179.0}$ | 179.0 | 179.5 | 234.7 179.5 |
| $Co(CO)_3(NO)(Co-N)$ | 165.8 | 162.9 | 162.9 | 166.1 | 166.1 | 165.8 | 165.8 |
| $C_0(CO)_3(NO)(Co-C)$ | 183.0 | 180.1 | 180.1 | 180.5 | 180.4 | 181.1 | 181.0 |
| Ni(CO) ₄ (Ni-C) | 182.5 | 182.1 | 182.0 | 182.3 | 182.2 | 182.7 | 182.6 |
| Ni(acac) ₂ (Ni–O) | 187.6 | 185.1 | 184.3 | 185.8 | 185.3 | 185.4 | 184.6 |
| Ni(PF ₃) ₄ (Ni–P) | 209.9 | 209.0 | 208.8 | 210.6 | 210.3 | 210.0 | 209.5 |
| $CuCH_3(Cu-C)$ | 188.4 | 190.1 | 190.1 | 189.3 | 189.4 | 189.6 | 189.6 |
| CuCN(Cu-C) | 183.2 | 184.3 | 184.3 | 182.0 | 182.0 | 182.3 | 182.3 |
| $Cu(acac)_2(Cu-O)$ | 191.4 | 191.9 | 191.8 | 194.3 | 194.2 | 193.2 | 193.1 |
| MD | | -2.1 | -2.0 | -0.6 | -0.5 | -0.6 | -0.5 |
| MAD | | 2.3 | 2.4 | 1.5 | 1.6 | 1.3 | 1.4 |
| RMSD | | 2.7 | 2.8 | 1.9 | 2.1 | 1.7 | 1.9 |
| SD | | 11.6 | 13.3 | 13.0 | 14.0 | 11.3 | 12.8 |
| Var | | 2.7 | 3.6 | 3.5 | 4.0 | 2.6 | 3.3 |
| Max | | 1.7 | 4.5 | 3.0 | 5.0 | 2.5 | 5.0 |
| Min | | -6.4 | -6.4 | -5.7 | -5.9 | -5.2 | -5.3 |
| AMax | | 6.4 | 6.4 | 5.7 | 5.9 | 5.2 | 5.3 |
| | | | | | | | |

Table A30: Diverse set of 32 metal complexes from the first transition row, for which precise gasphase geometries are known from electron diffraction or microwave spectroscopy. Compilation by Bühl *et al.* [28]. We abbreviate D3(BJ)-ATM by D3 and D4(TB)-ATM by D4.

| - | | D | BE0 | | BE | Т | PSS |
|---|------------------|------------------|------------------|------------------|------------------|------------------|---------------|
| system(bond) | Ref. | D3 | D4 | D3 | D4 | D3 | rss D4 |
| Sc(acac) ₃ (Sc-O) | 207.6 | 209.0 | 208.9 | 210.4 | 210.3 | 210.0 | 209.8 |
| $\operatorname{TiCl}_4(\operatorname{Ti-Cl})$ | 216.9 | 209.0 216.4 | 208.9 216.4 | 210.4 | 210.3 | 218.3 | 218.3 |
| $Ti(CH_3)Cl_3(Ti-C)$ | 210.9 204.7 | 202.3 | 202.3 | 204.5 | 204.5 | 205.3 | 205.4 |
| $Ti(CH_3)Cl_3(Ti-Cl)$ | 218.5 | 218.0 | 217.9 | 219.3 | 219.3 | 219.5 | 219.5 |
| $Ti(CH_3)_2Cl_2(Ti-C)$ | 205.8 | 203.5 | 203.6 | 205.5 | 205.5 | 206.3 | 206.4 |
| Ti(CH ₃) ₂ Cl ₂ (Ti-Cl) | 219.6 | 219.6 | 219.5 | 220.5 | 220.5 | 220.7 | 220.7 |
| $Ti(BD_4)_3(Ti-B)$ | 217.5 | 214.3 | 214.3 | 214.7 | 214.6 | 214.9 | 214.8 |
| $Ti(BD_4)_3(Ti-D^{br})$ | 198.4 | 193.4 | 193.4 | 193.7 | 193.7 | 193.2 | 193.1 |
| $VOF_3(V=O)$ | 157.0 | 154.1 | 154.1 | 157.5 | 157.5 | 157.6 | 157.5 |
| $VOF_3(V-F)$ | 172.9 | 171.6 | 171.6 | 173.7 | 173.7 | 173.4 | 173.4 |
| $VF_5(V-F^{ax})$ | 173.4 | 173.5 | 173.5 | 176.4 | 176.4 | 175.9 | 175.9 |
| $VF_5(V-F^{eq})$ | 170.8 | 169.9 | 169.8 | 172.7 | 172.6 | 172.3 | 172.4 |
| VOCl ₃ (V=O) | 157.3 | 153.9 | 153.9 | 157.2 | 157.2 | 157.3 | 157.3 |
| $VOCl_3(V-Cl)$ | 213.8 | 213.0 | 213.0 | 215.0 | 214.9 | 214.9 | 214.9 |
| $V(N(CH_3)_2)_4(V-N)$ | 187.9 | 186.1 | 186.2 | 188.2 | 188.1 | 188.1 | 188.0 |
| $V(Cp)(CO)_4(V-C^{CO})$ $CrO_2F_2(Cr=O)$ | $196.3 \\ 157.4$ | 192.3 153.7 | $192.3 \\ 153.7$ | $192.7 \\ 157.1$ | 192.7 157.1 | $194.4 \\ 157.0$ | 194.3 157.0 |
| $CrO_2F_2(Cr=O)$ $CrO_2F_2(Cr-F)$ | 157.4 171.9 | 170.2 | 170.2 | 172.4 | 172.4 | 172.0 | 172.0 |
| $CrO_2Cl_2(Cr=O)$ | 157.7 | 153.8 | 153.8 | 157.2 | 157.2 | 157.2 | 157.2 |
| $CrO_2Cl_2(Cr-Cl)$ | 212.2 | 210.6 | 210.6 | 212.4 | 212.4 | 212.4 | 212.4 |
| $CrO_2(NO_3)_2(Cr=O)$ | 158.4 | 153.8 | 153.8 | 157.4 | 157.4 | 157.4 | 157.4 |
| $CrO_2(NO_3)_2(Cr-O)$ | 195.4 | 191.0 | 191.0 | 193.2 | 193.2 | 193.0 | 192.9 |
| $Cr(C_6H_6)_2(Cr-C)$ | 215.0 | 213.0 | 213.0 | 213.8 | 213.7 | 213.6 | 213.6 |
| $Cr(C_6H_6)(CO)_3(Cr-C^{Ar})$ | 220.8 | 219.1 | 219.2 | 221.0 | 221.1 | 220.2 | 220.3 |
| $Cr(C_6H_6)(CO)_3(Cr-C^{CO})$ | 186.3 | 183.8 | 183.8 | 183.9 | 183.9 | 185.2 | 185.1 |
| $Cr(NO)_4(Cr-N)$ | 175.0 | 171.5 | 171.5 | 174.1 | 174.1 | 174.1 | 174.1 |
| $MnO_3F(Mn=O)$ | 158.6 | 154.2 | 154.2 | 159.2 | 157.7 | 157.6 | 157.6 |
| $MnO_3F(Mn-F)$ | 172.4 | 170.1 | 170.1 | 171.0 | 172.0 | 171.6 | 171.6 |
| $MnCp(CO)_3(Mn-C^{Cp})$ | 214.7 | 213.7 | 213.7 | 215.2 | 215.1 | 214.3 | 214.3 |
| $MnCp(CO)_3(Mn-C^{CO})$ | 180.6 | 178.3 | 178.3 | 178.4 | 178.4 | 179.4 | 179.4 |
| $Fe(CO)_5(Fe-C)^{mean}$ | 182.9 | 179.7 | 179.7 | 180.2 | 180.2 | 181.0 | 181.0 |
| $Fe(CO)_3(tmm)(Fe-C^{CO})$ | 181.0 | 177.9 | 177.9 | 178.0 | 178.0 | 178.8 | 178.8 |
| $Fe(CO)_3(tmm)(Fe-C_{cont}^{cent})$ | 193.8 | 192.2 | 192.2 | 194.6 | 194.7 | 194.3 | 194.4 |
| $Fe(CO)_3(tmm)(Fe-C^{CH_2})$ | 212.3 | 209.8 | 209.8 | 213.1 | 213.1 | 212.0 | 212.2 |
| $Fe(CO)_2(NO)_2(Fe-C)^{mean}$ | 187.2 | 180.8 | 180.7 | 181.5 | 181.4 | 182.3 | 182.3 |
| $Fe(CO)_2(NO)_2(Fe-N)$ | 167.4 | 164.1 | 164.2 | 167.1 | 167.1 | 166.9 | 166.9 |
| $FeCp_2(Fe-C)$ | 206.4 | 204.2 | 204.2 | 204.0 | 204.1 | 203.7 | 203.6 |
| $Fe(C_2H_4)(CO)_4(Fe-C^{et})$ | 211.7 | 209.7 | 209.9 | 213.0 | 213.1 | 212.3 | 212.6 |
| $\operatorname{Fe}(\operatorname{C}_2\operatorname{H}_4)(\operatorname{CO})_4(\operatorname{Fe}-\operatorname{C}^{ax})$ | 181.5 | 180.0 | 180.0 | 179.9 | 179.9 | $180.7 \\ 179.6$ | 180.7 |
| $Fe(C_2H_4)(CO)_4(Fe-C^{eq})$ $Fe(C_5(CH_3)_5)(P_5)(Fe-P)$ | $180.6 \\ 237.7$ | $178.1 \\ 235.7$ | $178.1 \\ 244.7$ | $178.9 \\ 236.3$ | $178.8 \\ 236.2$ | 234.9 | 179.6 234.8 |
| $CoH(CO)_4(Co-C^{eq})$ | 181.8 | 178.4 | 178.4 | 179.0 | 179.0 | 179.5 | 179.5 |
| $Co(CO)_3(NO)(Co-N)$ | 165.8 | 162.9 | 162.9 | 166.1 | 166.1 | 165.8 | 165.8 |
| $C_0(CO)_3(NO)(Co-C)$ | 183.0 | 180.1 | 180.1 | 180.5 | 180.5 | 181.1 | 181.1 |
| Ni(CO) ₄ (Ni-C) | 182.5 | 182.1 | 182.0 | 182.3 | 182.3 | 182.7 | 182.7 |
| Ni(acac) ₂ (Ni–O) | 187.6 | 185.1 | 184.3 | 185.8 | 185.3 | 185.4 | 184.6 |
| Ni(PF ₃) ₄ (Ni–P) | 209.9 | 209.0 | 208.4 | 210.6 | 209.8 | 210.0 | 209.1 |
| $CuCH_3(Cu-C)$ | 188.4 | 190.1 | 190.1 | 189.3 | 189.4 | 189.6 | 189.6 |
| CuCN(Cu-C) | 183.2 | 184.3 | 184.3 | 182.0 | 182.0 | 182.3 | 182.3 |
| $Cu(acac)_2(Cu-O)$ | 191.4 | 191.9 | 191.8 | 194.3 | 194.2 | 193.2 | 193.1 |
| MD | | -2.1 | -2.0 | -0.6 | -0.6 | -0.6 | -0.6 |
| MAD | | 2.3 | 2.5 | 1.5 | 1.5 | 1.3 | 1.3 |
| RMSD | | 2.7 | 2.9 | 1.9 | 1.9 | 1.7 | 1.7 |
| SD | | 11.6 | 14.7 | 13.0 | 12.9 | 11.3 | 11.5 |
| Var | | 2.7 | 4.4 | 3.5 | 3.4 | 2.6 | 2.7 |
| Max | | 1.7 | 7.0 | 3.0 | 3.0 | 2.5 | 2.5 |
| Min | | -6.4 | -6.5 | -5.7 | -5.8 | -5.2 | -5.3 |
| AMax | | 6.4 | 7.0 | 5.7 | 5.8 | 5.2 | 5.3 |
| | | | | | | | |

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