CI5223-1 Diseño de Albañilería Estructural Facultad de Ciencias Físicas y Matemáticas Universidad de Chile

Diseño de Fundaciones

Memoria de cálculo

Grupo: N°1

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Diseño de fundaciones

$$\sigma_{suelo_estatico} := 8 \frac{\textit{kgf}}{\textit{cm}^2}$$

$$\sigma_{suelo_estatico} := 8 \frac{kgf}{cm^2}$$
 $\sigma_{suelo_sismico} := 10 \frac{kgf}{cm^2}$

1. Dimensiones elementos

Propiedades y esfuerzos de muro:

Dimensiones zapata:

$$L_{muro} \coloneqq 6.76 \ \boldsymbol{m}$$

$$L_{zap} = 90 \ cm + L_{muro} + 90 \ cm = 8.56 \ m$$

$$e_{muro} = 25$$
 cm

$$B_{zap} \coloneqq 200 \ cm$$

$$B_{zap} \coloneqq 200 \ \emph{cm}$$
 $\gamma_{H} \coloneqq 2.5 \ \dfrac{\emph{tonnef}}{\emph{m}^{3}}$ $H_{zap} \coloneqq 200 \ \emph{cm}$

$$H_{zap} \coloneqq 200 \ cm$$

$$N_{zan} := \gamma_H \cdot B_{zan} \cdot L_{zan} \cdot H_{zan} = 85.6$$
 tonnef

2. Esfuerzos de ETABS

$$N_{PP} = -455.244 \ tonnef$$

$$N_{PP}\coloneqq -455.244 \; \textit{tonnef} \qquad \qquad M_{PP}\coloneqq -112.8124 \; \textit{tonnef} \cdot \textit{m} \qquad V_{PP}\coloneqq 5.8048 \; \textit{tonnef}$$

$$V_{DD} = 5.8048 \ tonnef$$

$$N_{SC} = -118.0962$$
 tonnef

$$N_{SC} \coloneqq -118.0962 \ \textit{tonnef}$$
 $M_{SC} \coloneqq -20.3411 \ \textit{tonnef} \cdot \textit{m}$ $V_{SC} \coloneqq -1.0577 \ \textit{tonnef}$

$$V_{SC} = -1.0577 \ tonnef$$

$$N_{SX} = 216.7196$$
 tonnef

$$N_{SX} \coloneqq 216.7196 \ \textit{tonnef}$$
 $M_{SX} \coloneqq 522.4481 \ \textit{tonnef} \cdot \textit{m}$ $V_{SX} \coloneqq 27.6026 \ \textit{tonnef}$

$$V_{SY} = 27.6026 \ tonnef$$

$$N_{SV} = 157.9424 \ tonnef$$

$$N_{SY} \coloneqq 157.9424 \ \textit{tonnef}$$
 $M_{SY} \coloneqq 59.8586 \ \textit{tonnef} \cdot \textit{m}$ $V_{SY} \coloneqq 8.2291 \ \textit{tonnef}$

$$V_{SV} = 8.2291 \ tonnef$$

3. Combinaciones

3.1. Combinaciones

estáticas

Combinación 1 (PP)

$$N_{est1} \coloneqq N_{zap} + \left| N_{PP} \right| = 540.844$$
 tonnef $V_{est1} \coloneqq V_{PP} = 5.805$ tonnef

$$V_{est1} = V_{PP} = 5.805$$
 tonnef

$$M_{est1}\!\coloneqq\!M_{PP}\!=\!-112.812~\textbf{tonnef}\boldsymbol{\cdot}\boldsymbol{m}$$

$$l := \frac{L_{zap}}{6} = 1.427 \ m$$

$$e \coloneqq \left| \frac{M_{est1}}{N_{cot1}} \right| = 0.209 \text{ m}$$

$$\begin{split} M_{est1} \coloneqq & M_{PP} = -112.812 \; \textit{tonnef} \cdot \textit{m} \\ l \coloneqq & \frac{L_{zap}}{6} = 1.427 \; \textit{m} \qquad e \coloneqq \left| \frac{M_{est1}}{N_{est1}} \right| = 0.209 \; \textit{m} \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 12.214 \; \textit{m} \\ \sigma_{est1} \coloneqq & \text{if} \; e < l \qquad \qquad \left| \max \left(\frac{N_{est1}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{est1}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{est1}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{est1}}{B_{zap} \cdot L_{zap}^2} \right) \right| = 3.621 \; \frac{\textit{kgf}}{\textit{cm}^2} \end{split}$$

$$egin{aligned} & \max \left(rac{N_e}{B_{zap}}
ight) \ & ext{else if } e = l \ & \left\| rac{2 \; N_{est1}}{B_{zap} \cdot L_{zap}}
ight. \end{aligned}$$

$$\left\| rac{2 \ N_{est1}}{B_{zap} {m \cdot} L'}
ight.$$

Factores de seguridad

$$\mu = 0.4$$

$$F_D := V_{oct1} = 5.805 \ tonnef$$

$$F_D \coloneqq V_{est1} = 5.805$$
 tonnef $F_R \coloneqq N_{est1} \cdot \mu = 216.338$ tonnef

$$FS_D := \frac{|F_R|}{|F_D|} = 37.269$$

$$M_{V} \coloneqq \left| M_{est1} \right| + \left| V_{est1} \boldsymbol{\cdot} H_{zap} \right| = 124.422 \ \boldsymbol{tonnef \cdot m}$$

$$M_R \!\coloneqq \! \left| N_{est1} \! \cdot \! \frac{L_{zap}}{2} \right| \! + \! \left| M_{est1} \right| \! = \! 2427.625 \, \, \boldsymbol{tonnef \cdot m}$$

$$FS_V := \frac{|M_R|}{|M_V|} = 19.511$$

 $chequeo(FS_D) = "CUMPLE"$

 $chequeo(FS_V) = "CUMPLE"$

Combinación 2 (PP+SC)

$$N_{est2} \coloneqq N_{zap} + \left| N_{PP} \right| + \left| N_{SC} \right| = 658.94 \ \textit{tonnef}$$
 $V_{est2} \coloneqq V_{PP} + V_{SC} = 4.747 \ \textit{tonnef}$

$$V_{est2} = V_{PP} + V_{SC} = 4.747$$
 tonnet

$$M_{est2} := M_{PP} + M_{SC} = -133.154 \ tonnef \cdot m$$

$$l := \frac{L_{zap}}{6} = 1.427 \ m$$

$$e \coloneqq \left| \frac{M_{est2}}{N_{est2}} \right| = 0.202 \text{ m}$$

$$l \coloneqq \frac{L_{zap}}{6} = 1.427 \ \boldsymbol{m} \qquad e \coloneqq \left| \frac{M_{est2}}{N_{est2}} \right| = 0.202 \ \boldsymbol{m} \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 12.234 \ \boldsymbol{m}$$

$$\sigma_{est2} \coloneqq \text{if } e < l \\ \left\| \max \left(\frac{N_{est2}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{est2}}{B_{zap} \cdot L_{zap}^{2}}, \frac{N_{est2}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{est2}}{B_{zap} \cdot L_{zap}^{2}} \right) \right\| = 4.394 \frac{\textit{kgf}}{\textit{cm}^{2}}$$

$$\text{else if } e = l \\ \left\| \frac{2 N_{est2}}{B_{zap} \cdot L_{zap}} \right\|$$

$$\text{else} \\ \left\| \frac{2 N_{est2}}{B_{zap} \cdot L'} \right\|$$

$$\sigma_{est} \coloneqq \max \left(\sigma_{est1}, \sigma_{est2}\right) = 4.394 \frac{\textit{kgf}}{\textit{cm}^2}$$

 $resistencia (\sigma_{suelo\ estatico}, \sigma_{est}) = \text{"CUMPLE"}$

Factores de seguridad

$$\mu = 0.4$$

$$F_D := V_{est2} = 4.747$$
 tonnef

$$F_D \coloneqq V_{est2} = 4.747 \ \textit{tonnef}$$
 $F_R \coloneqq N_{est2} \cdot \mu = 263.576 \ \textit{tonnef}$

$$FS_D := \frac{|F_R|}{|F_D|} = 55.524$$

$$M_{V} \coloneqq \left| M_{est2} \right| + \left| V_{est2} \boldsymbol{\cdot} H_{zap} \right| = 142.648 \ \boldsymbol{tonnef \cdot m}$$

$$M_R \coloneqq \left| N_{est2} \cdot \frac{L_{zap}}{2} \right| + \left| M_{est2} \right| = 2953.418 \ extbf{tonnef} \cdot extbf{m}$$

$$FS_V \coloneqq \frac{|M_R|}{|M_V|} = 20.704$$

 $chequeo(FS_D) = "CUMPLE"$

 $chequeo(FS_V) = "CUMPLE"$

3.2. Combinaciones

sísmicas

Combinación 3,1 (PP+SX)

$$N_{sis} \coloneqq N_{zap} + \left| N_{PP} \right| + N_{SX} = 757.564 \ \textit{tonnef}$$
 $V_{sis} \coloneqq V_{PP} + V_{SX} = 33.407 \ \textit{tonnef}$

$$M_{sis} = M_{PP} + M_{SX} = 409.636$$
 tonnef·m

$$\begin{split} l \coloneqq & \frac{L_{zap}}{6} = 1.427 \; \boldsymbol{m} \qquad e \coloneqq \left| \frac{M_{sis}}{N_{sis}} \right| = 0.541 \; \boldsymbol{m} \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 11.218 \; \boldsymbol{m} \\ \sigma_{sis31} \coloneqq & \text{if } e < l \\ & \left\| \max \left(\frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right\| = 6.102 \; \frac{\boldsymbol{kgf}}{\boldsymbol{cm}^2} \\ & \text{else if } e = l \\ & \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L_{zap}} \right\| \\ & \text{else} \\ & \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L'} \right\| \end{split}$$

Factores de seguridad

$$\mu = 0.4$$

$$F_D \coloneqq V_{sis} = 33.407 \ \textit{tonnef}$$
 $F_R \coloneqq N_{sis} \cdot \mu = 303.025 \ \textit{tonnef}$

$$F_R := N_{sis} \cdot \mu = 303.025$$
 tonnef

$$FS_D := \frac{|F_R|}{|F_D|} = 9.071$$

$$M_V \coloneqq |M_{sis}| + |V_{sis} \cdot H_{zap}| = 476.451$$
 tonnef · m

$$M_R\!\coloneqq\!\left|N_{sis}\!\boldsymbol{\cdot}\!\frac{L_{zap}}{2}\right|\!+\!\left|M_{sis}\right|\!=\!3652.008~\textit{tonnef}\!\boldsymbol{\cdot}\!\textit{m}$$

$$FS_V := \frac{|M_R|}{|M_V|} = 7.665$$

 $chequeo(FS_D) = "CUMPLE"$

 $chequeo(FS_V) = "CUMPLE"$

Combinación 3,2 (PP-SX)

$$\begin{split} N_{sis} \coloneqq & N_{zap} + \left| N_{PP} \right| - N_{SX} = 324.124 \ \textit{tonnef} \qquad V_{sis} \coloneqq V_{PP} - V_{SX} = -21.798 \ \textit{tonnef} \\ M_{sis} \coloneqq & M_{PP} - M_{SX} = -635.261 \ \textit{tonnef} \cdot \textit{m} \\ l \coloneqq & \frac{L_{zap}}{6} = 1.427 \ \textit{m} \qquad e \coloneqq \left| \frac{M_{sis}}{N_{sis}} \right| = 1.96 \ \textit{m} \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 6.96 \ \textit{m} \\ \sigma_{sis32} \coloneqq & \text{if } e < l \qquad \qquad \left| \max \left(\frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right| = 4.657 \ \frac{\textit{kgf}}{\textit{cm}^2} \\ & \text{else if } e = l \qquad \qquad \left| \frac{2 \ N_{sis}}{B_{zap} \cdot L_{zap}} \right| \\ & \text{else} \qquad \left| \frac{2 \ N_{sis}}{B_{zap} \cdot L'} \right| \end{aligned}$$

Factores de seguridad

$$\mu = 0.4$$

$$F_D \coloneqq V_{sis} = -21.798$$
 tonnef $F_R \coloneqq N_{sis} \cdot \mu = 129.65$ tonnef

$$F_R \coloneqq N_{sis} \cdot \mu = 129.65$$
 tonnef

$$M_{V}\!\coloneqq\!\left|M_{sis}\right|\!+\!\left|V_{sis}\!\cdot\!H_{zap}\right|\!=\!678.856~\textbf{tonnef}\!\cdot\!\textbf{m}$$

$$M_R\!\coloneqq\!\left|N_{sis}\!\cdot\!\frac{L_{zap}}{2}\right|\!+\!\left|M_{sis}\right|\!=\!2022.513~\textit{tonnef}\!\cdot\!\textit{m}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 5.948$$

$$FS_V \coloneqq \frac{|M_R|}{|M_V|} = 2.979$$

 $chequeo(FS_D) = "CUMPLE"$

chequeo (FS_V) = "CUMPLE"

Combinación 4,1 (PP+SC+S)

$$N_{sis} = N_{zap} + |N_{PP}| + |N_{SC}| + N_{SX} = 875.66$$
 tonnef

$$M_{sis} := M_{PP} + M_{SC} + M_{SX} = 389.295 \ tonnef \cdot m$$

$$V_{sis} \coloneqq V_{PP} + V_{SC} + V_{SX} = 32.35$$
 tonnef

$$\begin{aligned} l &\coloneqq \frac{L_{zap}}{6} = 1.427 \; \boldsymbol{m} \qquad e \coloneqq \left| \frac{M_{sis}}{N_{sis}} \right| = 0.445 \; \boldsymbol{m} \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 11.506 \; \boldsymbol{m} \\ \sigma_{sis41} &\coloneqq \text{if } e < l \\ \left\| \max \left(\frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right\| = 6.709 \; \frac{\boldsymbol{kgf}}{\boldsymbol{cm}^2} \end{aligned}$$

$$\text{else if } e = l \quad \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L_{zap}} \right\|$$

$$\text{else} \quad \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L'} \right\|$$

Factores de seguridad

$$\mu = 0.4$$

$$F_D := V_{sis} = 32.35$$
 tonnef

$$F_D \coloneqq V_{sis} = 32.35 \ \textit{tonnef}$$
 $F_R \coloneqq N_{sis} \cdot \mu = 350.264 \ \textit{tonnef}$

$$FS_D := \frac{|F_R|}{|F_D|} = 10.827$$

$$M_{V}\!\coloneqq\!\left|M_{sis}\right|\!+\!\left|V_{sis}\!\cdot\!H_{zap}\right|\!=\!453.994~\textbf{tonnef}\!\cdot\!\textbf{m}$$

$$M_R\!\coloneqq\!\left|N_{sis}\!\boldsymbol{\cdot}\frac{L_{zap}}{2}\right|\!+\!\left|M_{sis}\right|\!=\!4137.119~\boldsymbol{tonnef}\!\boldsymbol{\cdot}\boldsymbol{m}$$

$$FS_V := \frac{|M_R|}{|M_V|} = 9.113$$

 $chequeo(FS_D) = "CUMPLE"$

 $chequeo(FS_V) = "CUMPLE"$

Combinación 4,2 (PP+SC-S)

$$N_{sis} := N_{zap} + |N_{PP}| + |N_{SC}| - N_{SX} = 442.221$$
 tonnef

$$M_{sis} := M_{PP} + M_{SC} - M_{SX} = -655.602 \ tonnef \cdot m$$

$$V_{sis} \coloneqq V_{PP} + V_{SC} - V_{SX} = -22.856$$
 tonnef

$$\begin{split} l \coloneqq & \frac{L_{zap}}{6} = 1.427 \; \textit{m} \qquad e \coloneqq \left| \frac{M_{sis}}{N_{sis}} \right| = 1.483 \; \textit{m} \qquad \qquad L' \coloneqq 3 \cdot \left(\frac{L_{zap}}{2} - e \right) = 8.392 \; \textit{m} \\ \sigma_{sis42} \coloneqq & \text{if } e < l \\ & \left\| \max \left(\frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right\| = 5.269 \; \frac{\textit{kgf}}{\textit{cm}^2} \\ & \text{else if } e = l \\ & \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L_{zap}} \right\| \\ & \text{else} \\ & \left\| \frac{2 \; N_{sis}}{B_{zap} \cdot L'} \right\| \end{split}$$

Factores de seguridad

$$\mu = 0.4$$

$$F_D \coloneqq V_{sis} = -22.856$$
 tonnef

$$F_D \coloneqq V_{sis} = -22.856 \ \textit{tonnef}$$
 $F_R \coloneqq N_{sis} \cdot \mu = 176.888 \ \textit{tonnef}$

$$FS_D := \frac{|F_R|}{|F_D|} = 7.739$$

$$M_{V} \coloneqq \left| M_{sis} \right| + \left| V_{sis} \cdot H_{zap} \right| = 701.313 \ \textit{tonnef} \cdot \textit{m}$$

$$M_R\!\coloneqq\!\left|N_{sis}\!\cdot\!\frac{L_{zap}}{2}\right|\!+\!\left|M_{sis}\right|\!=\!2548.306~\textit{tonnef}\!\cdot\!\textit{m}$$

$$FS_V \coloneqq \frac{|M_R|}{|M_V|} = 3.634$$

 $chequeo\left(FS_{D}\right)=$ "CUMPLE"

 $chequeo(FS_V) = "CUMPLE"$

$$\sigma_{sis} \coloneqq \max \left(\sigma_{sis31}, \sigma_{sis32}, \sigma_{sis41}, \sigma_{sis42}\right) = 6.709 \frac{\textit{kgf}}{\textit{cm}^2}$$

 $resistencia (\sigma_{suelo_estatico}, \sigma_{est}) = "CUMPLE"$

4. Chequeo parrilla

Momento lado corto

$$M1 \coloneqq \frac{\sigma_{sis} \cdot \left(\frac{B_{zap}}{2}\right)^2 \cdot 1 \ m}{2} = 33.544 \ \textit{tonnef} \cdot m \qquad M2 \coloneqq$$

Momento Lado Largo

$$M2 \coloneqq \frac{\sigma_{sis} \cdot \left(\frac{L_{zap} - L_{muro}}{2}\right)^2 \cdot 1 \ m}{2} = 27.17 \ \textit{tonnef} \cdot m$$

Propiedad de la Sección de **Zapata**

$$W := \frac{1}{6} \cdot 1 \ \boldsymbol{m} \cdot H_{zap}^2 = 0.667 \ \boldsymbol{m}^3$$

$$\frac{M1}{W} = 5.032 \frac{kgf}{cm^2}$$

if
$$\frac{M1}{W} < 7 \frac{kgf}{cm^2}$$
 = "No necesita parrilla" else | "Necesita Parrilla"

Propiedad de la Sección de Zapata

$$W \coloneqq \frac{1}{6} \cdot 1 \ \boldsymbol{m} \cdot H_{zap}^{2} = 0.667 \ \boldsymbol{m}^{3}$$

$$\frac{M1}{W} = 5.032 \frac{\textit{kgf}}{\textit{cm}^2}$$

$$\text{if } \frac{M1}{W} < 7 \frac{\textit{kgf}}{\textit{cm}^2}$$

$$\parallel \text{"No necesita parrilla"} = \text{"No necesita parrilla"}$$

$$\text{else}$$

$$\parallel \text{"Necesita Parrilla"} = \text{"No necesita parrilla"}$$

$$\text{else}$$

$$\parallel \text{"Necesita Parrilla"}$$