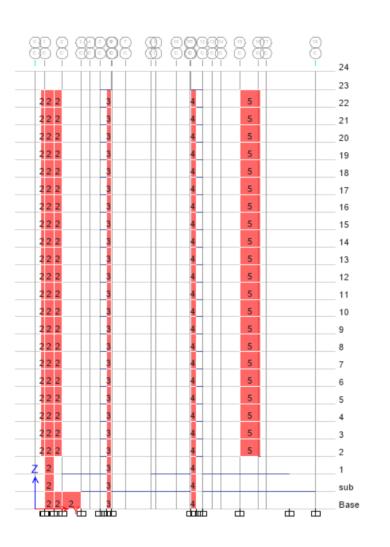
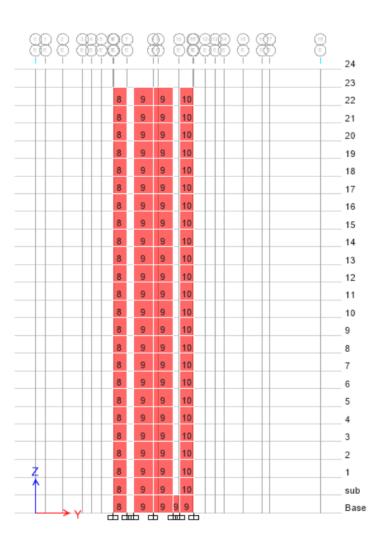


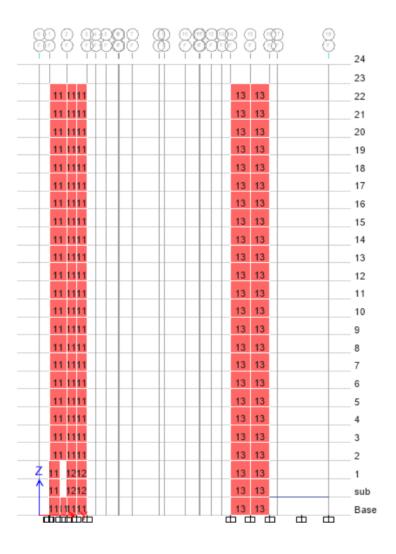
PROYECTO DE HORMIGÓN CI5206-2

AUXILIAR N°7

Piers



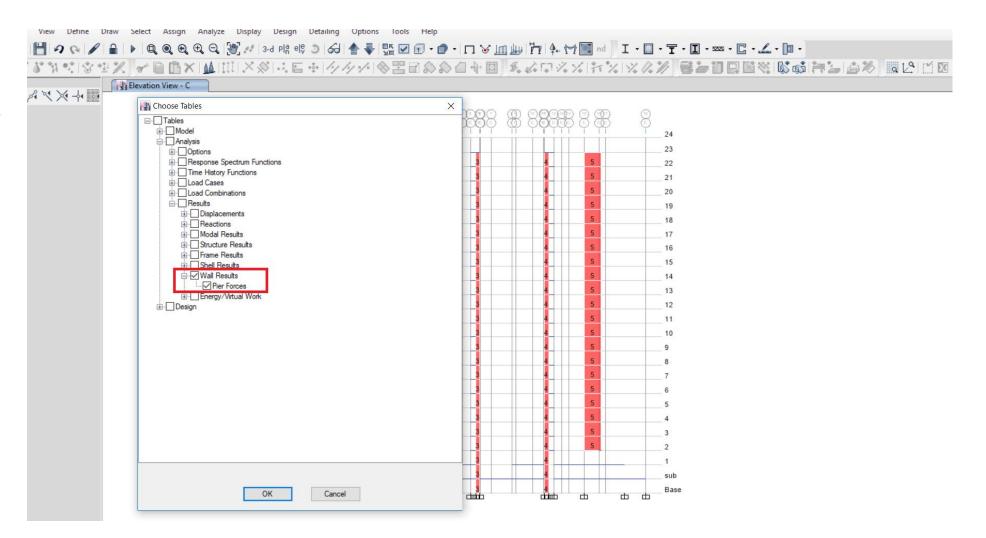




Piers

Display ->Show Tables

• P, V2, M3



Piers

-		▶ ▶ Reloa	- 117		_					
	Story	Pier	Load Case/Combo	Location	P tonf	V2 tonf	V3 tonf	T tonf-m	M2 tonf-m	M3 tonf-n
	12	10	PP	Тор	-77,15	0,2586	-0,3837	0,1175	0,4733	-0,2751
	12	10	PP	Bottom	-79,4775	0,2586	-0,3837	0,1175	-0,4666	0,3583
	12	10	SC	Тор	-18,2892	0,517	-0,1049	0,0305	0,129	-0,6328
	12	10	SC	Bottom	-18,2892	0,517	-0.1049	0.0305	-0,1281	0,6339
	12	10	SX Max	Тор	27,8711	14,6814	3,4145	0,8204	4,1391	17,954
	12	10	SX Max	Bottom	27,8711	14,6814	3,4145	0.8204	4,2267	18,0784
	12	10	SY Max	Тор	22,3012	24,7747	0,6614	0,0966	0,8078	30,5252
	12	10	SY Max	Bottom	22,3012	24,7747	0,6614	0,0966	0,8127	30,2428
	12	10	PPSC	Тор	-95,4392	0,7756	-0,4886	0,148	0,6023	-0,908
	12	10	PPSC	Bottom	-97,7667	0,7756	-0,4886	0.148	-0,5948	0,9922
	12	10	C1	Тор	-108,01	0,362	-0,5371	0,1645	0,6626	-0,3852
	12	10	C1	Bottom	-111,2685	0,362	-0,5371	0,1645	-0,6533	0,5017
	12	10	C2	Тор	-121,8428	1,1375	-0,6283	0,1898	0,7743	-1,3427
	12	10	C2	Bottom	-124,6358	1,1375	-0.6283	0,1898	-0.765	1,4442
	12	10	C3 Max	Тор	-30,4155	20,7866	4,4351	1,2543	6,2207	24,888
	12	10	C3 Max	Bottom	-32,5102	20,7866	4,4351	1,2543	5,4974	25,6323
	12	10	C3 Min	Тор	-108,4545	-20,3212	-5,1257	-1,0427	-5,3687	-25,3833
	12	10	C3 Min	Bottom	-110,5492	-20,3212	-5,1257	-1,0427	-6,3373	-24,9873
	12	10	C4 Max	Тор	-30,4155	20,7866	4,4351	1,2543	6,2207	24,888
	12	10	C4 Max	Bottom	-32,5102	20,7866	4,4351	1,2543	5,4974	25,6323
	12	10	C4 Min	Тор	-108,4545	-20,3212	-5,1257	-1,0427	-5,3687	-25,3833
	12	10	C4 Min	Bottom	-110,5492	-20,3212	-5,1257	-1,0427	-6,3373	-24,9873
	12	10	C5 Max	Тор	-38,2133	34,9173	0,5807	0,241	1,5569	42,4877
	12	10	C5 Max	Bottom	-40,308	34,9173	0,5807	0,241	0,7178	42,6625

VIGAS

Vigas Estáticas:

- Se estima cargas muertas (Peso de losa + PP adicional) y cargas vivas (SC)
 - → Carga distribuida
- Se calcula el área tributaria sobre cada viga
- El área tributaria se multiplica por el valor de la carga distribuida
- Se agrega el peso propio de la sección propuesta para la viga

Vigas Sísmicas:

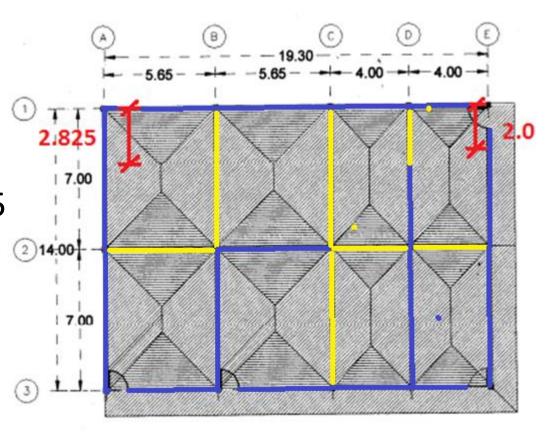
 Se agregan además de las cargas para vigas estáticas, los esfuerzos sísmicos de Etabs.

VIGAS

• Lado Apoyado - Apoyado: 45° y 45°

• Lado Apoyado - Empotrado: 30° y 60°

• Lado Empotrado - Empotrado: 45° y 45



• PP Losa e=15 cm: 0.375 ton/m²

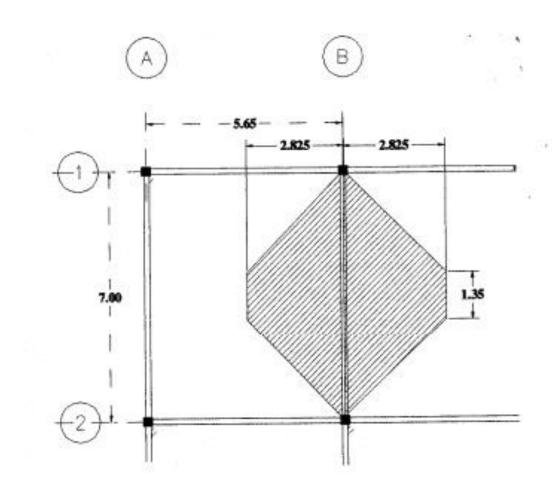
• PP adicional: 0.125 ton/m²

 \Rightarrow PP total: 0.5 ton/m²

• SC: 0.2 ton/m^2

Viga Propuesta: V30/50 H30

 \Rightarrow PP viga: 0.375 ton/m



- Carga Lineal:
- PP total: $0.5 \text{ ton/m}^2 \times 2.825 \text{ m} = 1.4125$

ton/m

- SC: $0.2 \text{ ton/m}^2 \times 2.825 \text{ m}$
- =0.565 ton/m
- Carga Lineal Última:
- $1.2 \times 1.4125 + 1.6 \times 0.565 = 2.6 \text{ ton/m}$

Carga Lineal:

PP total: $0.5 \text{ ton/m}^2 \times 2.825 \text{ m} = 1.4125 \text{ ton/m}$

SC: $0.2 \text{ ton/m}^2 \times 2.825 \text{ m}$

=0.565 ton/m

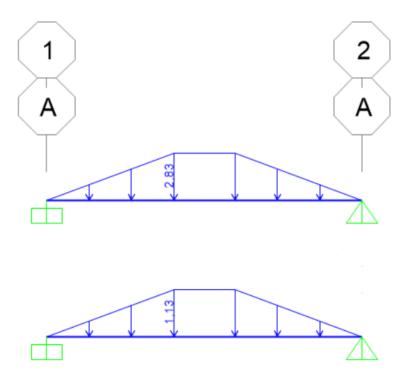
• Carga Lineal Última:

 $1.2 \times 1.4125 + 1.6 \times 0.565 = 2.6 \text{ ton/m}$

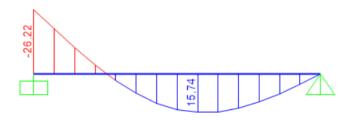
Por carga igual a ambos lados qu= 5.2 ton/m

Por carga igual a ambos lados qu= 5.2 ton/m

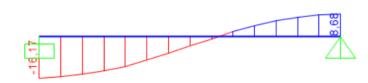
Viga en SAP2000:



Momento [Tonf-m]



Corte [Tonf]



- Para Mu (-)= 26.22 tonf-m se requiere 17.2 cm2
- \Rightarrow Se usan 2 φ 25

Para Mu (+)= 15.74 tonf-m se requiere 9,7 cm2

 \Rightarrow Se usan 2 φ 25

Para Vu=16.17 tonf se requiere estribos mínimos

 \Rightarrow Se usa φ 10 @ 20

Se Agregan barras Laterales L:1+1 φ 10

$$f_c := 250 \frac{\text{kgf}}{\text{cm}^2}$$

$$f_y := 4200 \frac{\text{kgf}}{\text{cm}^2}$$
 $\varepsilon_{\text{cu}} := 0.003$ $\varepsilon_y := 0.0021$

$$\varepsilon_{\mathbf{y}} := 0.0021$$

rec := 40mm

Ancho de viga

1. Flexión

 $M_{ij} := 26.22 tonf \cdot m$

$$\beta_1 := \begin{cases} 0.85 & \text{if } f_c < 30 \text{MPa} \\ 0.65 & \text{if } f_c > 55 \text{MPa} \end{cases}$$

$$0.85 - 0.008 \cdot \left(\frac{f_c}{\text{MPa}} - 30 \right) & \text{otherwise}$$

Given

$$\rho := 0.001$$
 $\phi := 0.9$

$$\frac{M_u}{h \cdot d^2} = \phi \cdot \rho \cdot f_y \cdot \left(1 - 0.588 \cdot \rho \cdot \frac{f_y}{f_c}\right) \qquad NL := Find(\rho) \qquad \rho := NL \qquad \rho = 0.012$$

$$\rho_{min} := max \left(\frac{0.25 \sqrt{f_c \cdot MPa}}{f_y}, \frac{1.4 \cdot MPa}{f_y} \right) \qquad \qquad \rho_{min} = 3.399 \times 10^{-3}$$

$$\rho_b := 0.85 \cdot \beta_1 \cdot \frac{f_c}{f_v} \cdot \frac{\varepsilon_{cu}}{\varepsilon_{cu} + \varepsilon_v} \qquad \rho_b = 0.025 \qquad \rho_{max} := 0.75 \cdot \rho_b \qquad \rho_{max} = 0.019$$

$$\rho_{\text{max}} := 0.75 \cdot \rho_{\text{b}}$$

$$\rho_{req} \coloneqq \text{max} \big(\text{min} \big(\rho, \rho_{max} \big), \rho_{min} \big) \qquad \qquad \rho_{req} = 0.012 \qquad \qquad A_{sreq} \coloneqq \rho_{req} \cdot b \cdot d$$

$$A_{sreq} := \rho_{req} \cdot b \cdot d$$

$$A_{sreq} = 17.196 \cdot cm^2$$

2. Corte

$$V_{11} := 16.17 ton$$

$$f_{vt} := 420MPa$$

$$V_c := 0.53 \cdot \sqrt{f_c \cdot \frac{kgf}{cm^2}} \cdot b \cdot d$$
 $V_c = 11.564 \cdot tonf$ (S. 11.1.3, Corte a Flexión pura)

$$\frac{\left(\frac{V_{\mathbf{u}}}{\phi} - V_{\mathbf{c}}\right)}{\left(\mathbf{f}_{\mathbf{yt}} \cdot \mathbf{d}\right)} = 5.074 \cdot \frac{\mathrm{cm}^2}{\mathrm{m}}$$

$$\phi_v := 10 \text{mr}$$

$$n := 2$$

$$\phi_{v} := 10 \text{mm}$$
 $n := 2$ $A_{v} := n \cdot \frac{{\phi_{v}}^{2} \cdot \pi}{4}$ $A_{v} = 1.571 \cdot \text{cm}^{2}$

$$A_v = 1.571 \cdot cm^2$$

$$V_{\text{S}} := \text{min}\!\!\left(\frac{A_{\text{V}} \cdot f_{\text{yt}} \cdot d}{\text{s}}, 0.66 \cdot \sqrt{f_{\text{C}} \cdot MP} a \cdot b \cdot d\right)$$

$$V_n := V_c + V_s$$
 $V_n = 27.038 \cdot tonf$

$$\phi \cdot V_n = 20.278 \cdot tonf$$

V_s = 15.473-tonf