

## Diseño de fundaciones

MURO: F4X

$$\sigma_{suelo\_estatico} := 8 \frac{kgf}{cm^2} \quad \sigma_{suelo\_sismico} := 10 \frac{kgf}{cm^2}$$

### 1. Dimensiones elementos

Propiedades y esfuerzos de muro:

$$L_{muro} := 6.76 \text{ m}$$

$$e_{muro} := 25 \text{ cm}$$

Dimensiones zapata:

$$L_{zap} := 60 \text{ cm} + L_{muro} + 60 \text{ cm} = 7.96 \text{ m}$$

$$B_{zap} := 140 \text{ cm}$$

$$H_{zap} := 200 \text{ cm}$$

$$\gamma_H := 2.5 \frac{tonnef}{m^3}$$

$$N_{zap} := \gamma_H \cdot B_{zap} \cdot L_{zap} \cdot H_{zap} = 55.72 \text{ tonnef}$$

### 2. Esfuerzos de ETABS

$$N_{PP} := -415.9831 \text{ tonnef}$$

$$M_{PP} := -176.3241 \text{ tonnef} \cdot m$$

$$V_{PP} := 26.6489 \text{ tonnef}$$

$$N_{SC} := -118.0962 \text{ tonnef}$$

$$M_{SC} := -20.3411 \text{ tonnef} \cdot m$$

$$V_{SC} := -1.0577 \text{ tonnef}$$

$$N_{SX} := 216.7196 \text{ tonnef}$$

$$M_{SX} := 522.4481 \text{ tonnef} \cdot m$$

$$V_{SX} := 27.6026 \text{ tonnef}$$

$$N_{SY} := 157.9424 \text{ tonnef}$$

$$M_{SY} := 59.8586 \text{ tonnef} \cdot m$$

$$V_{SY} := 8.2291 \text{ tonnef}$$

### 3. Combinaciones

#### 3.1. Combinaciones estáticas

Combinación 1 (PP)

$$N_{est1} := N_{zap} + |N_{PP}| = 471.703 \text{ tonnef}$$

$$V_{est1} := V_{PP} = 26.649 \text{ tonnef}$$

$$M_{est1} := M_{PP} = -176.324 \text{ tonnef} \cdot m$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m}$$

$$e := \left| \frac{M_{est1}}{N_{est1}} \right| = 0.374 \text{ m}$$

$$L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 10.819 \text{ m}$$

$$\sigma_{est1} := \begin{cases} \text{if } e < l \\ \left\| \max \left( \frac{N_{est1}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{est1}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{est1}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{est1}}{B_{zap} \cdot L_{zap}^2} \right) \right\| \\ \text{else if } e = l \\ \left\| \frac{2 N_{est1}}{B_{zap} \cdot L_{zap}} \right\| \\ \text{else} \\ \left\| \frac{2 N_{est1}}{B_{zap} \cdot L'} \right\| \end{cases} = 5.425 \frac{kgf}{cm^2}$$

Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{est1} = 26.649 \text{ tonnef}$$

$$F_R := N_{est1} \cdot \mu = 188.681 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 7.08$$

$$M_V := M_{est1} + V_{est1} \cdot H_{zap} = -123.026 \text{ tonnef} \cdot m$$

$$M_R := N_{est1} \cdot \frac{L_{zap}}{2} + M_{est1} = 1701.054 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 13.827$$

chequeo ( $FS_D$ ) = "CUMPLE"

chequeo ( $FS_V$ ) = "CUMPLE"

Combinación 2 (PP+SC)

$$N_{est2} := N_{zap} + |N_{PP}| + |N_{SC}| = 589.799 \text{ tonnef}$$

$$V_{est2} := V_{PP} + V_{SC} = 25.591 \text{ tonnef}$$

$$M_{est2} := M_{PP} + M_{SC} = -196.665 \text{ tonnef} \cdot m$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m}$$

$$e := \left| \frac{M_{est2}}{N_{est2}} \right| = 0.333 \text{ m}$$

$$L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 10.94 \text{ m}$$

$$\sigma_{est2} := \begin{cases} \text{if } e < l \\ \left\| \max \left( \frac{N_{est2}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{est2}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{est2}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{est2}}{B_{zap} \cdot L_{zap}^2} \right) \right\| \\ \text{else if } e = l \\ \left\| \frac{2 N_{est2}}{B_{zap} \cdot L_{zap}} \right\| \\ \text{else} \\ \left\| \frac{2 N_{est2}}{B_{zap} \cdot L'} \right\| \end{cases} = 6.623 \frac{\text{kgf}}{\text{cm}^2}$$

$$\sigma_{est} := \max(\sigma_{est1}, \sigma_{est2}) = 6.623 \frac{\text{kgf}}{\text{cm}^2}$$

resistencia ( $\sigma_{suelo\_estatico}, \sigma_{est}$ ) = "CUMPLE"

Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{est2} = 25.591 \text{ tonnef}$$

$$F_R := N_{est2} \cdot \mu = 235.92 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 9.219$$

$$M_V := M_{est2} + V_{est2} \cdot H_{zap} = -145.483 \text{ tonnef} \cdot m$$

$$M_R := N_{est2} \cdot \frac{L_{zap}}{2} + M_{est2} = 2150.736 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 14.783$$

chequeo ( $FS_D$ ) = "CUMPLE"

chequeo ( $FS_V$ ) = "CUMPLE"

### 3.2. Combinaciones

#### sísmicas

##### Combinación 3.1 (PP+SX)

$$N_{sis} := N_{zap} + |N_{PP}| + N_{SX} = 688.423 \text{ tonnef} \quad V_{sis} := V_{PP} + V_{SX} = 54.252 \text{ tonnef}$$

$$M_{sis} := M_{PP} + M_{SX} = 346.124 \text{ tonnef} \cdot m$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m} \quad e := \left| \frac{M_{sis}}{N_{sis}} \right| = 0.503 \text{ m} \quad L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 10.432 \text{ m}$$

$$\sigma_{sis31} := \begin{cases} \text{if } e < l \\ \left| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right| \\ \text{else if } e = l \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right| \\ \text{else} \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right| \end{cases} = 8.519 \frac{\text{kgf}}{\text{cm}^2}$$

##### Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{sis} = 54.252 \text{ tonnef} \quad F_R := N_{sis} \cdot \mu = 275.369 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 5.076$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = 454.627 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = 3086.046 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 6.788$$

chequeo ( $FS_D$ ) = "CUMPLE"

chequeo ( $FS_V$ ) = "CUMPLE"

### Combinación 3.2 (PP-SX)

$$N_{sis} := N_{zap} + |N_{PP}| - N_{SX} = 254.984 \text{ tonnef}$$

$$V_{sis} := V_{PP} - V_{SX} = -0.954 \text{ tonnef}$$

$$M_{sis} := M_{PP} - M_{SX} = -698.772 \text{ tonnef} \cdot m$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m}$$

$$e := \left| \frac{M_{sis}}{N_{sis}} \right| = 2.74 \text{ m}$$

$$L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 3.719 \text{ m}$$

$$\sigma_{sis32} := \begin{cases} \text{if } e < l \\ \left\| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right\| \\ \text{else if } e = l \\ \left\| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right\| \\ \text{else} \\ \left\| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right\| \end{cases} = 9.796 \frac{\text{kgf}}{\text{cm}^2}$$

### Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{sis} = -0.954 \text{ tonnef}$$

$$F_R := N_{sis} \cdot \mu = 101.993 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 106.945$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = -700.68 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = 316.062 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 0.451$$

*chequeo* ( $FS_D$ ) = "CUMPLE"

*chequeo* ( $FS_V$ ) = "REDISEÑAR"

#### Combinación 4.1 (PP+0.75(SC+S))

$$N_{sis} := N_{zap} + |N_{PP}| + 0.75 \cdot |N_{SC}| + 0.75 \cdot N_{SX} = 722.815 \text{ tonnef}$$

$$M_{sis} := M_{PP} + 0.75 \cdot M_{SC} + 0.75 \cdot M_{SX} = 200.256 \text{ tonnef} \cdot m$$

$$V_{sis} := V_{PP} + 0.75 \cdot (V_{SC} + V_{SX}) = 46.558 \text{ tonnef}$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m} \quad e := \left| \frac{M_{sis}}{N_{sis}} \right| = 0.277 \text{ m} \quad L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 11.109 \text{ m}$$

$$\sigma_{sis41} := \begin{cases} \text{if } e < l \\ \left\| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right\| \\ \text{else if } e = l \\ \left\| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right\| \\ \text{else} \\ \left\| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right\| \end{cases} = 7.841 \frac{\text{kgf}}{\text{cm}^2}$$

#### Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{sis} = 46.558 \text{ tonnef} \quad F_R := N_{sis} \cdot \mu = 289.126 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 6.21$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = 293.371 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = 3077.06 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 10.489$$

$$\text{chequeo}(FS_D) = \text{"CUMPLE"}$$

$$\text{chequeo}(FS_V) = \text{"CUMPLE"}$$

#### Combinación 4.2 (PP+0.75(SC-S))

$$N_{sis} := N_{zap} + |N_{PP}| + 0.75 \cdot |N_{SC}| - 0.75 \cdot N_{SX} = 397.736 \text{ tonnef}$$

$$M_{sis} := M_{PP} + 0.75 \cdot M_{SC} - 0.75 \cdot M_{SX} = -583.416 \text{ tonnef} \cdot m$$

$$V_{sis} := V_{PP} + 0.75 \cdot (V_{SC} - V_{SX}) = 5.154 \text{ tonnef}$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m} \quad e := \left| \frac{M_{sis}}{N_{sis}} \right| = 1.467 \text{ m} \quad L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 7.539 \text{ m}$$

$$\sigma_{sis42} := \text{if } e < l \quad \left| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right| = 7.536 \frac{\text{kgf}}{\text{cm}^2}$$
$$\text{else if } e = l \quad \left| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right|$$
$$\text{else} \quad \left| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right|$$

#### Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{sis} = 5.154 \text{ tonnef} \quad F_R := N_{sis} \cdot \mu = 159.094 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 30.87$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = -573.109 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = 999.571 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 1.744$$

$\text{chequeo}(FS_D) = \text{"CUMPLE"}$

$\text{chequeo}(FS_V) = \text{"CUMPLE"}$

Combinación 5.1 (0.6PP  
+SX)

$$N_{sis} := 0.6 N_{zap} + 0.6 |N_{PP}| + N_{SX} = 499.741 \text{ tonnef}$$

$$M_{sis} := 0.6 M_{PP} + M_{SX} = 416.654 \text{ tonnef} \cdot m$$

$$V_{sis} := 0.6 \cdot V_{PP} + V_{SX} = 43.592 \text{ tonnef}$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m} \quad e := \left| \frac{M_{sis}}{N_{sis}} \right| = 0.834 \text{ m} \quad L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = 9.439 \text{ m}$$

$$\sigma_{sis51} := \begin{cases} \text{if } e < l \\ \left| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right| \\ \text{else if } e = l \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right| \\ \text{else} \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right| \end{cases} = 7.303 \frac{\text{kgf}}{\text{cm}^2}$$

Factores de seguridad

$$\mu := 0.4$$

$$F_D := V_{sis} = 43.592 \text{ tonnef} \quad F_R := N_{sis} \cdot \mu = 199.897 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 4.586$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = 503.838 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = 2405.625 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 4.775$$

*chequeo* ( $FS_D$ ) = "CUMPLE"

*chequeo* ( $FS_V$ ) = "CUMPLE"

### Combinación 5,2 (0.6PP-SX)

$$N_{sis} := 0.6 N_{zap} + 0.6 |N_{PP}| - N_{SX} = 66.302 \text{ tonnef}$$

$$M_{sis} := 0.6 M_{PP} - M_{SX} = -628.243 \text{ tonnef} \cdot m$$

$$V_{sis} := 0.6 \cdot V_{PP} - V_{SX} = -11.613 \text{ tonnef}$$

$$l := \frac{L_{zap}}{6} = 1.327 \text{ m} \quad e := \left| \frac{M_{sis}}{N_{sis}} \right| = 9.475 \text{ m} \quad L' := 3 \cdot \left( \frac{L_{zap}}{2} - e \right) = -16.486 \text{ m}$$

$$\sigma_{sis52} := \begin{cases} \text{if } e < l \\ \left| \max \left( \frac{N_{sis}}{B_{zap} \cdot L_{zap}} + \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2}, \frac{N_{sis}}{B_{zap} \cdot L_{zap}} - \frac{6 \cdot M_{sis}}{B_{zap} \cdot L_{zap}^2} \right) \right| \\ \text{else if } e = l \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L_{zap}} \right| \\ \text{else} \\ \left| \frac{2 N_{sis}}{B_{zap} \cdot L'} \right| \end{cases} = -0.575 \frac{kgf}{cm^2}$$

$$\text{Factores de seguridad} \quad \mu := 0.4$$

$$F_D := V_{sis} = -11.613 \text{ tonnef} \quad F_R := N_{sis} \cdot \mu = 26.521 \text{ tonnef}$$

$$FS_D := \frac{|F_R|}{|F_D|} = 2.284$$

$$M_V := M_{sis} + V_{sis} \cdot H_{zap} = -651.469 \text{ tonnef} \cdot m$$

$$M_R := N_{sis} \cdot \frac{L_{zap}}{2} + M_{sis} = -364.36 \text{ tonnef} \cdot m$$

$$FS_V := \frac{|M_R|}{|M_V|} = 0.559$$

$$\text{chequeo}(FS_D) = \text{“CUMPLE”}$$

$$\text{chequeo}(FS_V) = \text{“REDISEÑAR”}$$

$$\sigma_{sis} := \max(\sigma_{sis31}, \sigma_{sis32}, \sigma_{sis41}, \sigma_{sis42}, \sigma_{sis51}, \sigma_{sis52}) = 9.796 \frac{kgf}{cm^2}$$

$$\text{resistencia}(\sigma_{suelo\_estatico}, \sigma_{est}) = \text{“CUMPLE”}$$



#### 4. Chequeo parrilla

Momento lado corto

$$M1 := \frac{\sigma_{sis} \cdot \left( \frac{B_{zap}}{2} \right)^2 \cdot 1 \text{ m}}{2} = 23.999 \text{ tonnef} \cdot \text{m}$$

Momento Lado Largo

$$M2 := \frac{\sigma_{sis} \cdot \left( \frac{L_{zap} - L_{muro}}{2} \right)^2 \cdot 1 \text{ m}}{2} = 17.632 \text{ tonnef} \cdot \text{m}$$

Propiedad de la Sección de Zapata

$$W := \frac{1}{6} \cdot 1 \text{ m} \cdot H_{zap}^2 = 0.667 \text{ m}^3$$

Propiedad de la Sección de Zapata

$$W := \frac{1}{6} \cdot 1 \text{ m} \cdot H_{zap}^2 = 0.667 \text{ m}^3$$

$$\frac{M1}{W} = 3.6 \frac{\text{kgf}}{\text{cm}^2}$$

if  $\frac{M1}{W} < 7 \frac{\text{kgf}}{\text{cm}^2}$  | = “No necesita parrilla”  
|| “No necesita parrilla”  
else  
|| “Necesita Parrilla”

$$\frac{M2}{W} = 2.645 \frac{\text{kgf}}{\text{cm}^2}$$

if  $\frac{M2}{W} < 7 \frac{\text{kgf}}{\text{cm}^2}$  | = “No necesita parrilla”  
|| “No necesita parrilla”  
else  
|| “Necesita Parrilla”