WECC Composite Load Flow Model

DIgSILENT PowerFactory 2019

16D170007 - Kumaresh Ramesh 16D170027 - Prabhat Ranjan

Dynamic Load Flow Modelling and WECC

Dynamic load models are used to simulate aggregate load responses to disturbances in the grid. The dynamic behaviour of the end-user load has a huge impact on the dynamic behaviour of the interconnected Bulk power system.

Considerable progress has been made in these fields from simple static load modelling to three-phase induction motor plus the ZIP model and then composite load model (CLM).

The WECC CLM guidelines are one of the state-of-art, due to the capability for representing the diversity in the composition and dynamic characteristics of end-use loads and the electrical distance between its end-use and substations.

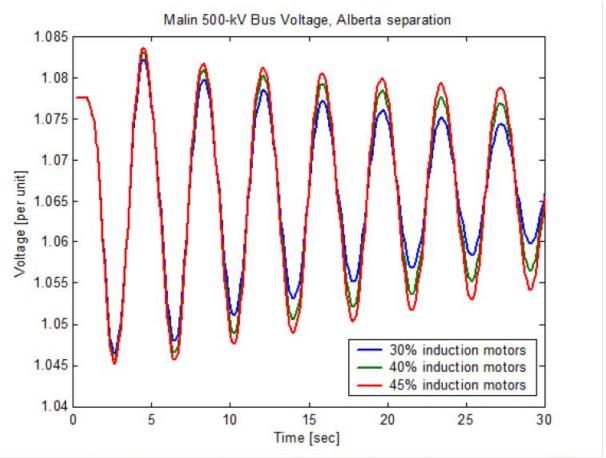
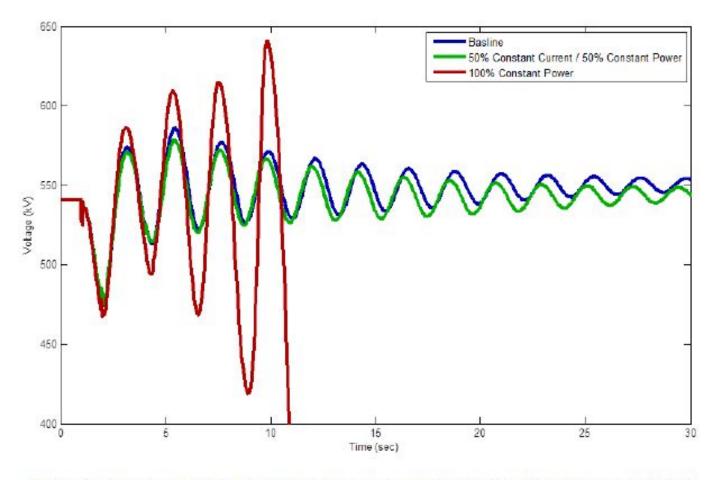


Figure 1.1: System Damping Sensitivity to Motor Load [Source: BPA]

Source NERC



Source NERC

Figure 2.1: Impact of Constant Power Load on Oscillatory Stability [Source: WECC]

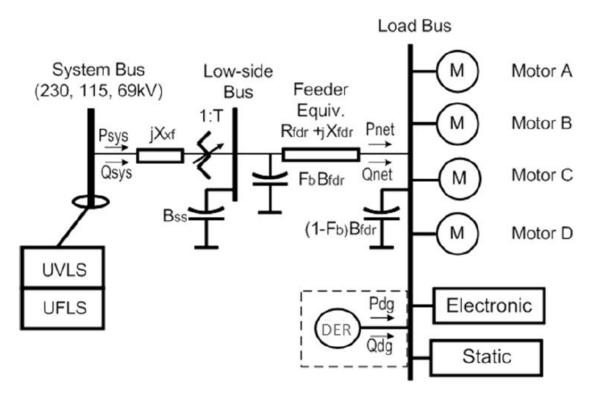
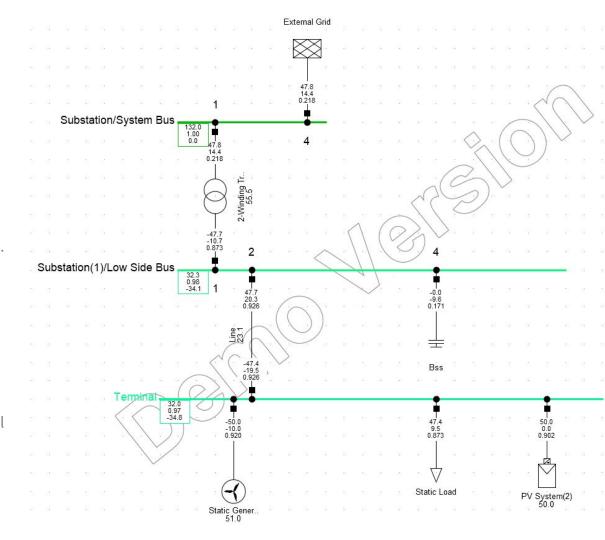


Figure 1.3: Composite Load Model Structure (CMPLDWG)

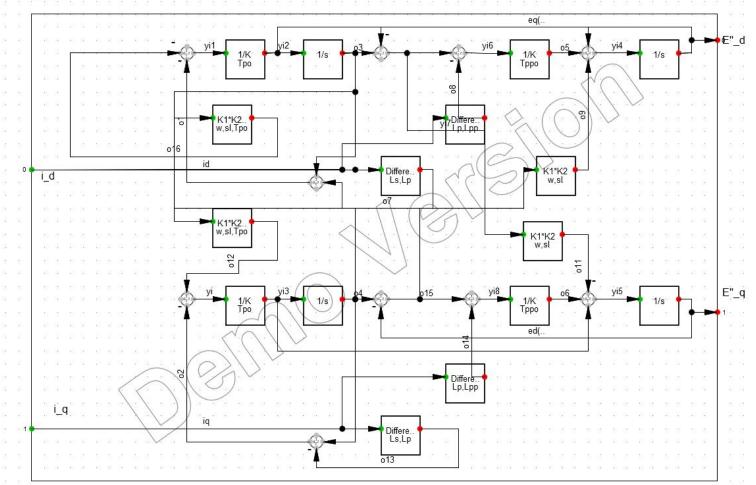
The WECC Composite Load Model

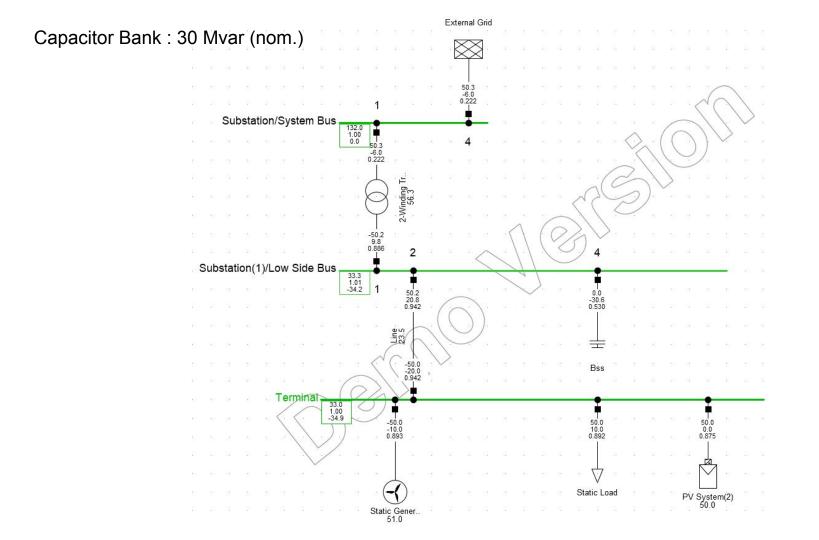
DIgSILENT Model

- Grid with a 132 kV 3-phase busbar system
- Transformer of 132/33 KV, 90 MVA rating. LV side of the transformer is connected to a transmission bus at 33 KV.
- The 33 kV load bus is connected through a transmission line of 1 km length with the resistance of 0.1 ohm and inductance of 1mH. (shunt capacitance is neglected)
- Variable capacitor bank for reactive power compensation.
- The PV system injects 50 MW into the system.
- The WECC modelled motor consumes 50 MW and 10 Mvar of active and reactive power respectively.
- Static load has been modelled as a ZIP-model with 70% constant impedance and 30% constant current load. The nominal power consumption of the load (rated at 33 kV) is 50 MW (active) and 10 Mvar (reactive).

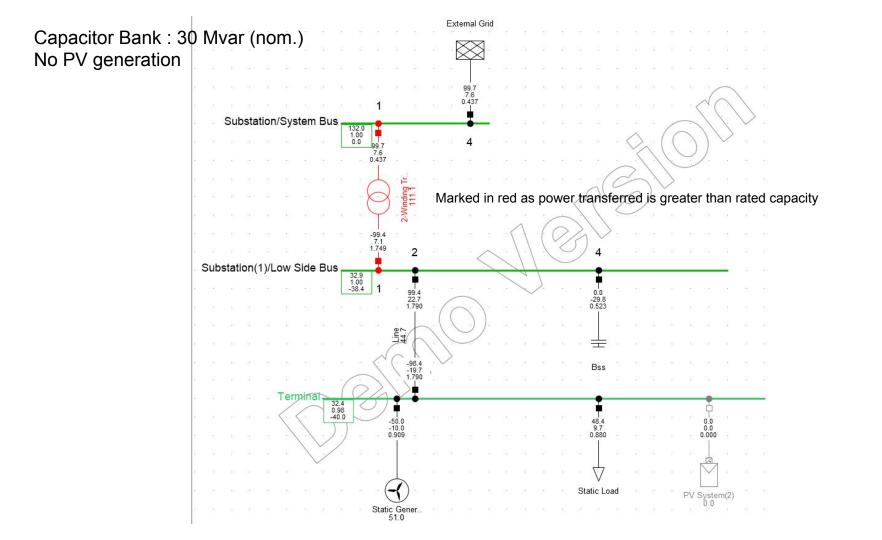


Motor:





Load Flow Calculation Bus													bars/Terminals				
AC Load Flow, balanced, positive sequence							!	Automatic Model Adaptation for Convergence						No			
Automatic tap adjustment of transformers Consider reactive power limits						1	Max. Acceptable Load Flow Error for Nodes Model Equations						1.00 kVA 0.10 %				
					No	1											
								nou		.10115					.10 %	5,056	
Grid: Grid System Stage: G				e: Grid		Stud	iy Case:	Study Case				/	1				
	rated				Active	Reactive	Power			I							
	The second second		100000000000000000000000000000000000000						Loading	11		Additio	nal Data				
	[kV]	[p.u.]	[kV]	[deg]	[MW]	[Mvar]	[-]	[kA]	[%]	E							
Substatio	n(1)									1						and the	
Low Sid	ie B.00	1.01	33.33	-34.19						1							
Cub_1	/Shnt	Bss			0.00	-30.60	0.00	0.53		1							
Cub_1		Line				20.83	Control of the Contro		23.55	Pv:	266.13 kV	CLod:	0.00 Mvar	L:	1.00	kı	
Cub_1	/Tr2	2-Wi	inding Tr	ansfor	-50.22	9.77	-0.98	0.89	56.33	Tap:	0.00	Min:	-9	Max:	6		
Substatio	n									i							
System	Bus.00	1.00	132.00	0.00						1							
Cub_1	/Xnet	Exte	ernal Gri	d	50.34	-5.97	0.99	0.22		Sk":	10000.00 M	/A					
Cub_1	/Tr2	2-Wi	inding Tr	ansfor	50.34	-5.97	0.99	0.22	56.33	Tap:	0.00	Min:	-9	Max:	6		
Terminal										Ĺ							
	33.00	1.00	32.98	-34.91						T							
Cub_10	(/Pvsys	PV S	System(2)		50.00	0.00	1.00	0.88	50.00	1							
the state of the s	/Lod		cic Load			9.99	0.98	0.89		P10:	50.00 MV	Q10:	10.00 Mvar				
		at Stat	tic Gener	ator	-50.00	-10.00	-0.98	0.89	50.99	1							
Cub_9	/Lne	Line	9		-49.95	-19.99	-0.93	0.94	23.55	Pv:	266.13 kV	CLod:	0.00 Mvar	L:	1.00	k	



Loa	d Flow	V Calcula	ation												Busb	ars/Te	rmina	als	
AC Load Flow, balanced, positive sequence Automatic tap adjustment of transformers Consider reactive power limits							No	Automatic Model Adaptation for Convergenc No Max. Acceptable Load Flow Error for							e No				
							No	1	Nodes					1.00 kVA					
 							I		el Equat							.10 %			
Grid: Grid System Stage: Grid							dy Case:							1					
		rated					Reactive				1							\$193	
		Voltage	Bu	s-voltage	e	Power	Power	Factor	Current	Loading	1		Addition	nal Dat	a				
		[kV]	[p.u.]	[kV]	[deg]	[MW]	[Mvar]	[-]	[kA]	[%]	1						202000000		
Subs	tation	1(1)									1								
Lo	w Side	B.00	1.00	32.89	-38.41						1								
C	ub_1	/Shnt	Bss			0.00	-29.79	0.00	0.52		1								
C	ub 1	/Lne	Line			99.37	22.70	0.97	1.79	44.74	Pv:	960.76 kW	cLod:	0.00	Mvar	L:	1.00)]	
C	ub_1	/Tr2	2-Wi	nding Tr	ansfor	-99.37	7.09	-1.00	1.75	111.13	Tap:	0.00	Min:	-9		Max:	6	5	
Subs	tation	1									Í								
Sv	stem E	Bus.00	1.00	132.00	0.00						Î								
		/Xnet	Exte	rnal Gri	d	99.72	7.59	1.00	0.44		Sk":	10000.00 MVA							
	_	/Tr2					7.59		0.44	111.13	Tap:	0.00	Min:	-9		Max:	6	5	
Term	inal										1								
		33.00	0.98	32.38	-39.97						1								
C	ub 10	(/Pvsys	PV S	ystem(2)		0.00	0.00	1.00	0.00	0.00	1								
	A 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	/Lod		ic Load			9.68	0.98	0.88		P10:	50.00 MW	Q10:	10.00	Mvar				
C	ub 8	/Gensta	t Stat	ic Genera			-10.00		0.91	50.99	I								
C	ub_9	/Lne	Line				-19.68		1.79	44.74	Pv:	960.76 kW	cLod:	0.00	Mvar	L:	1.00) [

References

- 1. <u>Wecc.biz</u>
- 2. Huang, Qiuhua, et al. "A Reference Implementation of WECC Composite Load Model in Matlab and GridPACK." arXiv preprint arXiv:1708.00939 (2017).
- WECC Composite Load Model (CMPLDW) Benchmarking Summary
- 4. WECC Dynamic Composite Load Model (CMPLDW) Specifications
- 5. Reliability Guideline: Developing Load Model Composition Data

Thank you