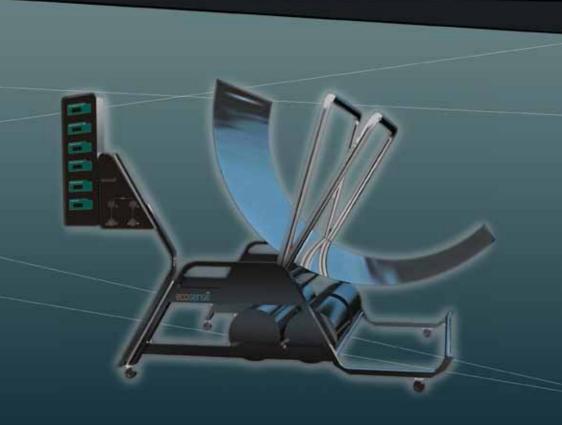
ecosense INSIGHT SOLAR



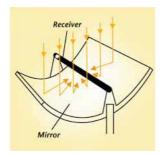
Solar Concentrator

Training System Experiment **Manual**

includes 8 experiments with step by step guidance

Insight Solar Introduction:

A parabolic trough is a type of solar thermal collector that is straight in one dimension and curved as a parabola in the other two, lined with a polished metal mirror. The energy of sunlight which enters the mirror parallel to its plane of symmetry is focused along the focal line, where an absorber tube is placed for collecting the solar radiation. The mirror is oriented so that sunlight which it reflects is concentrated on the tube, which contains a fluid which is heated to a high temperature by the energy of the sunlight. The hot fluid can be used for many purposes. Often, it is piped to a heat engine, which uses the heat energy to drive machinery or to generate electricity.



Theory:

Parabolic trough system consists of following components:

Parabolic reflector.

It is the mirror in the form of parabolic shape which reflects all the radiation at the focus of a parabola. This reflector is mounted over a structure which can move from east to west with the help of sun tracker.

Absorber tube or receiver.

It is a metal pipe or tube coated with black nickel or chromium and sealed with glass tube. Black coating increases the absorption of tube while glass glazing decreases the convection losses from tube.

©DOs

☼DON'Ts

- Always set the reflector
 Don't look at the direction normal to sun radiation beam before starting the experiment with the help of switches in tracking system.
- Both storage tanks should be completely filled before starting the experiment.
- Receiver tube should be completely filled with oil and water.
- Always set the required receiver tube at the focus before starting of experiment
- All three way valves and close valve should be at right position through out the experiment.
- FRP switches for sensor selection should be at right position through out the experiment.
- Insulation jackets should cover storage tank completely and should be tight enough to prevent the convective losses.

- reflector without
- Don't start anv of the pumps before selecting the three way valve position
- Don't pump the oil through receiver tube after filling the indicator vent
- Don't pump the water through receiver tube after filling the indicator vent of tank
- Don't start the experiment without setting the reflector sheet normal to sun rays
- Don't shade the reflector sheet at any point of time during the experiment
- Don't touch the receiver tube during the experiment

• Sun tracker:

It is the device which rotates the complete structure from east to west direction. It works on timer algorithm and sensor based algorithm.

Table-1: Overall Specifications of the system

S.No.	Components	Specifications
1	Heat generating unit with tracking system	
<u> </u>	Parabolic reflector	
	• Length	4 ft
	Arc length (perimeter)	6 ft
	Depth	0.68 ft
	• Focal length	1.99 ft
	Material	SS with mirror film
	Sun tracker	Single axis
	Absorber tube	
	Length	4 ft
	Diameter	1 inch
	Absorber material	Copper, SS
	Insulation material (for pipe)	PUF
	Piping material	GI and copper
2	Storage unit	
	Supply tanks	2 (one for water and another for oil)
		46 to (for support of 10 to (for oil)
	• Capacity	46 ltr (for water) and 10 ltr (for oil)
	Material	SS
	Storage tank	2 (one with Heat exchanger and other without heat exchanger)
	• capacity	28 ltr
	material	SS
	Insulation used	Glass wool with rexene
	Tank insulation thickness	2cm
	Pipe insulation thickness	1cm
	Working fluid	Water and oil
3	Control unit	
	Pump (for water)	
	Power rating	0.1 HP
	• Head	6 m
	Pump (for oil)	
	Power rating	0.5 HP
	• Head	10m
	Different meters	
	Thermometers	
	Flow meter	
	Radiation meter	
	Anemometer	
4	Accessories	
	Experimental manual	
	Tools for piping and connections	
	• Oil	
	<u> </u>	

Important parameters of a parabolic trough heating system:

The performance of a parabolic trough system depends upon different design and atmospheric parameters.

The meaning and importance of some of the most dominating parameters are described below.

Overall Heat Loss Coefficient (U₁):

All the heat that is received by the receiver tube does not result into useful energy. Some of the heat gets lost to the surrounding. The amount of heat loss depends upon the convective, conductive and radiative heat loss coefficients.

Estimation of heat loss coefficient of the system is important for its performance evaluation. A higher value of heat loss coefficient indicates the lower heat resistance and hence the lower efficiency.

Among all heat loss parameters the top loss contributes the most. The top heat loss coefficient is a function of various parameters which includes the temperature of the receiver tube, ambient temperature, wind speed, emissivity of the receiver tube

Heat Removal Factor (F_R) :

Heat removal factor represents the ratio of the actual useful energy gain to the useful energy gain if the entire receiver were at the fluid inlet temperature. It depends upon the factors like inlet and outlet fluid temperature, the ambient temperature, area of the tube etc. The importance of heat removal factors remains with the efficiency of the system. For a highly efficient system a higher value of heat removal factor is must.

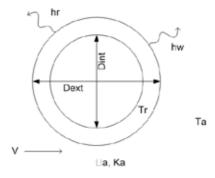
Efficiency (η):

Efficiency is the most important factor for a system. This factor determines the system's output. For a parabolic trough system the efficiency is defined as the ratio of the useful energy delivered to the energy incident on the aperture of trough.

Basic Equations to calculate different parameters:

A. Heat Loss coefficient (U₁)

U_L is the overall heat transfer coefficient from the receiver tube to the ambient air. This is very important and complex factor which tells us the heat loss per unit area per unit temp difference from receiver tube to ambient. In our case there is no glass glazing therefore, U_L will be expressed in two terms only (as shown below). By multiplying this factor with tube area and temp diff. between tube and ambient, we will get the total heat loss from the tube to ambient.



Cross sectional view of receiver tube

 U_L = h_0 + h_c (eq. 1)

Where,

h_w: Convective heat transfer coefficient between tube and atmosphere

h_r: Radiative Heat transfer coefficient of radiation

h_w and h_r can be expressed by using following formulae

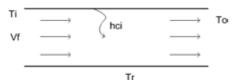
$$h_w = Nu_n * K_a/D_{ext}$$
Where, Nu. can be calculated by following formulae
For 0.13<1000, $Nu_a = 0.4 + 0.54 \times Re_a^{0.6}$
For 10004<50000, $Nu_a = 0.3 \times Re_a^{0.6}$
Where $Re_a = V * D_{ext}/v_a$

$$h_T = \varepsilon * \sigma * (T_T + T_a) * (T_T^2 + T_a^2)$$

By putting fix values of some parameters, U_L can be expressed by following equations

$$U_L = 1.7^{\circ}10^{-6} \cdot (T_c + T_a) \cdot (T_c^2 + T_a^2) + 25.746^{\circ}(V)^{0.6} \dots$$
 for $V = 0.67$ (IA)
 $U_L = 1.7^{\circ}10^{-6} \cdot (T_c + T_a) \cdot (T_c^2 + T_a^2) + 0.427 + 277.76^{\circ}(V)^{0.62} \text{ .for } V > 0.67$ (1B)

B. F factors of a receiver tube (F/, FR,)



Flow in receiver tube

1. Collector efficiency factor (F'):

Collector efficiency factor is constant for any collector design and fluid flow rate. This represents the ratio of actual useful energy gain to the useful energy gain that would result if the receiver tube surface temperature had been at the fluid temperature.

F' = (Actual useful heat collection rate)/ (Usefull heat collection rate when the absorbing plate is at the local fluid temperature)

Mathematically,

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{cl}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$
 Equ. 2

h_{ci} calculation:

For water:
$$\begin{split} h_{COS} &= \frac{\mathcal{K}_{w}}{D_{00}} + [3.6 + \frac{0.0068 + [D_{00}/L] + 5 \sigma_{w} P_{00}}{1 + 0.04 + [(D_{00}/L] + 8 \kappa_{w} P_{N}]^{2/3}}] \\ Ra_{w} &= V_{w} + D_{00} P_{00} \\ \mathbb{E}_{w} &= m/(\rho_{w} + 3.14 + \frac{856}{4}) \\ PT_{0} &= m_{w} + C_{POS}/K_{w} \\ \mu_{w} &= 0.0160 + \rho_{w} + (f_{c} - 273)^{-000} \\ \rho_{w} &= 1000 + [1 - \frac{(f_{c} + 273)^{-000}}{(34002 + f_{c} + 2540)[-(f_{c} + 277)^{2}]} + (f_{c} - 273)^{-0.00} \\ PT_{w} &= 112.55 \cdot \left[1 - \frac{(f_{c} + 15.04)}{5002 + (f_{c} - 204.07) + (f_{c} - 277)^{2}}\right] + (f_{c} - 273)^{-0.00} \end{split}$$

For oil:
$$\begin{split} &h_{ci(oil)} = \frac{\kappa_{cit}}{v_{oot}} * Nu_{oilt} \\ Ν_{oilt} = 3.66 + \frac{0.065 * \left(\frac{D_{int}}{L}\right) * Re * Pr}{1 + 0.04 * \left[\left(\frac{D_{oot}}{L}\right) * Re * Pr\right]^{2/3}} \\ ℜ = V_{oii} * D_{t}/v_{oil} \\ &V_{oii} = \frac{m_{oil}}{\rho_{oil} * A_{Cii}} \\ ⪻_{oil} = \mu_{oil} * C_{p(oil)}/K_{oii} \end{split}$$

Heat Removal Factor (FR): Heat removal factor is constant for any collector design and fluid flow rate. This represents the ratio of actual useful energy gain to the useful energy gain that would result if the receiver tube surface temperature had been at the fluid inlet temperature.

$$F_{R}{=}\frac{\text{Actual wrefull energy gain}}{\text{useful energy gain if the entire collector were at the fluid inlet temperature}}$$

Mathematically,

Another formula for F_R

$$F_{R} = \frac{mc_{p}}{A_{int}U_{L}} \left[1 - \exp\left(-\frac{U_{L}F/A_{int}}{mc_{p}}\right)\right] \qquad (eq.3)$$

For unite:

$$F_R=2.04 \times 10^6 \times \frac{m_e}{\nu_e} \{1 - \exp\left(-4.91 \times 10^{-3} \times \frac{\sigma_e F}{m_e}\right)\}$$
 (eq.3A)
For oil
 $F_R=4.2 \times 10^6 \times \frac{m_e}{\nu_e} \{1 - \exp\left(-2.38 \times 10^{-7} \times \frac{9.4^6}{\mu_e}\right)\}$ (eq.3B)

C. Thermal Efficiency of the collector (η)

It is the ratio of the Useful heat gain to the Total input solar energy

Mathematically,

$$\eta = m * Cp * \frac{T_o - T_i}{A_a * I_b}$$
 (eq.4)

For water:

$$\eta = 2024 * \dot{m} * \frac{T_0 - T_1}{I_0}$$
 (eq.4A)

For oil:

$$\eta = 996.62 * \hat{m} * \frac{T_0 - T_i}{I_b}$$
 (eq.4B)

D. Comparison of theoretically achieved and experimentally achieved temperature values

Experimental values will be obtained by using different thermometers while theoretical values can be achieved by using following formulae

$$T_r = T_m + \frac{m * C_p * (T_o - T_l)}{h_{cl} * \pi * D_{ext} * L}$$
 (eq.5A)

$$T_m = \frac{T_i + T_0}{2}$$
 (eq.5B)

$$T_o = T_t + \frac{Q_u}{m * C_p}$$
 (eq.5C)

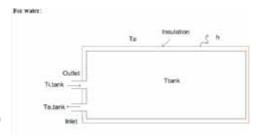
Values of m, C_p and h_{ci} can be obtained from above formulae.

E. Heat loss in piping

For water:
Loss in piping =
$$4187 * ih * (T_a - T_{feasil})$$
 (eq.6.4)
For oil:
Loss in piping = $= 2061 * ih * (T_a - T_{feasil})$ (eq.68)

Rate of heat loss in piping = $m^* C_p^* (T_o - T_{tank})$ (eq.6)

F. Heat loss in storage tank

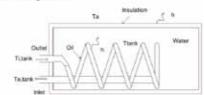


Heat transfer eq. for tank water

$$T_{tank,x}^* = \frac{28 * T_{tank,x} - \dot{m} * T_{tank}}{28 - \dot{m}}$$

Heat loss in tank (in t sec) = $28 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$ (eq.7A)

For nill Heat exchanger calculation



$$\begin{split} T_{e,tank} &= T_{tank} - \left(T_{tank} - T_{i,tank}\right) * \exp\left(-h_{el(oli)} * \frac{A_{Cu}}{m_{oll}}\right) \\ h_{el(oli)} &= \frac{\kappa_{ell}}{p_{out}} * Nu_{oll} \\ Nu_{oli} &= 3.66 + \frac{0.065 * \left(\frac{D_{inl}}{L}\right) * Re * Pr}{1 + 0.04 * \left[\left(\frac{D_{inl}}{L}\right) * Re * Pr\right]^{2/3}} \end{split}$$

$$Re = V_{oil} * D_i/v_{oil}$$

$$V_{oil} = \frac{\dot{m}_{oil}}{\rho_{oil} * A_{Cu}}$$

$$Pr_{o(t} = \mu_{oit} * C_{p(o(t))}/K_{o(t)}$$

Sensible heat delivered to water by oil

$$Q_{oil} = \hat{m}_{oil} * C_{p(oii)} * (T_{itank} - T_{e,tank})$$

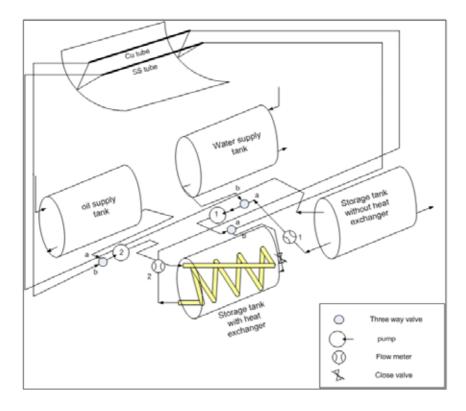
This sensible heat will raise the temperature of water from previous one

$$Q_{oll} = \hat{m}_w * C_{p(w)} * (T_{tank,x} - T^*_{tank,x})$$

Heat loss in tank (in t sec) =
$$27 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$$
 (eq.7B)

Experimental set-up: Different components of parabolic trough system are connected to each other in following manner.

There are two types of parameters viz. weather parameters (radiation and wind speed) and user defined parameters (flow rate, insulation thickness and inlet water temperature).



Weather parameters cannot be changed by user so user has to perform the experiment in parts (different time of day). During a part of experiment, weather parameters will be same (or will remain unchanged) but will be changed in other part of the experiment. Fixed parameter will remain the same during the complete experiment.

Insight Solar

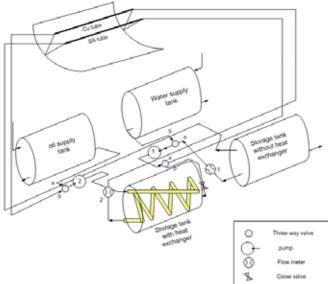
Experiment No. 1

Objective: Determine the Performance (U_L, F_R, η) of the Parabolic Trough collector with fixed parameters with (i) Water and (ii) Oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' condition

- and valve-2 will be positioned at 'a' condition. Insulation thickness (of tank and pipe) will not be changed during this experiment.
- (ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve-2 can be positioned at any position as a close valve is present there in the middle of valve-2 and heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' condition. Insulation thickness (of tank and pipe) will not be changed during this experiment.



Observations:

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T,	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Following equations will be used for evaluation of different parameters.

Experiment No. 1

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A. 4A, 5A, B, C, 6A and 7A.

UL =
$$1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} \dots$$
 for $V < 0.67$

$$\begin{array}{l} UL = 1.7*10^{-9*} \left(T_r + T_a \right) \left(T_r^2 + T_a^2 \right) + 0.427 \\ + 277.76*(V)^{0.53}...... \text{ for V} > 0.67 \end{array}$$

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_F}\right]} \qquad F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_F}\right]}$$

$$F_R = 2.04 * 10^6 * \frac{m_w}{U_L} \left[1 - \exp\left(-4.91 * 10^{-7} * \frac{U_L F^{-1}}{m_w}\right)\right] \qquad F_R = 4.2 * 10^6 * \frac{m_w}{U_L} \left[1 - \exp\left(-2.38 * 10^{-7} * \frac{U_L F^{-1}}{m_w}\right)\right]$$

$$\eta = 2024 * m_t * \frac{T_0 - T_1}{m_w}$$

$$\eta = 996.62 * m_t * \frac{T_0 - T_1}{m_w}$$

Theoretical values of different temperature values

$$\begin{split} T_r &= T_m + \frac{\dot{m}*C_p*(T_o - T_{i)}}{h_{ci}*\pi*D_{ext}*L} \\ T_m &= \frac{T_i + T_o}{2} \\ T_o &= T_i + \frac{Q_u}{\dot{m}*C_p} \end{split}$$

Loss in piping =4187 *m* $(T_0-T_{i,tank})$

Heat loss in tank (in t sec) = $28*C_0*$ $\left(T_{tank,x} - 1 - T^*_{tank,x}\right)$

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{f} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

FR=4.2 *
$$10^6 * \frac{m_W}{v_L} [1 - \exp(-2.38 * 10^{-7} * \frac{v_L F'}{m_W})]$$

$$\eta = 996.62 * \dot{m} * \frac{T_o - T_i}{t_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m}*C_p*(T_o - T_i)}{h_{ci}*\pi*D_{ext}*L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping = $2061 * \dot{m} * (T_o - T_{i,ta*k})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$

Results: Calculate all performance parameters of this system.

Notes

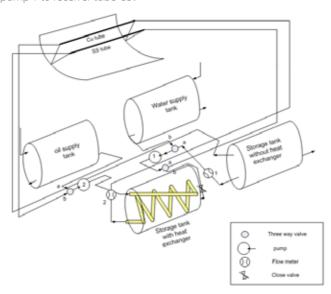
Insight Solar **Experiment No. 2**

Objective: Determine the Performance (UL, FR, η) of the Parabolic Trough collector with varying solar insolation with (i) Water and (ii) Oil as working fluid.

Experimental set-up: Set-up for this experiment will remain same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'.

- Insulation thickness (of tank and pipe) will not be change during this experiment.
- (ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be changed during this experiment.



Observations:

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S.	Time	Solar	Wind	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow
no.	(sec)	insolation								rate (Kg/
		(W/m ²)	(m/sec)							sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Evaluate the performance parameters for each set keeping solar insolation constant for this set. Following equations will be used for evaluation of different parameters.

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

UL =
$$1.7*10^{-9}* (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6}..... for V < 0.67$$

$$\begin{array}{l} UL = 1.7*10^{-9*} \ (T_r + T_a) \ (T_r^2 + T_a^2) + 0.427 \\ + \ 277.76*(V)^{0.53} \ \dots \ \text{for } V > 0.67 \end{array}$$

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{cl}D_{lnc}} + \frac{D \cdot \ln(D_{ext}/D_{lnc})}{2 \cdot K_T}\right]}$$

$$F_2 = 2.04 \times 10^6 \times \frac{m_W}{1 - \exp\left(-4.91 \times 10^{-7} \times \frac{U_L F^{(1)}}{1 - \exp\left(-4.91 \times 10^{-7} \times \frac{U_L F^{(1)$$

$$\eta = 2024 * \dot{m} * \frac{T_o - T_i}{I_h}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_{i)}}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_1 + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{\dot{m} * C_p}$$

Loss in piping =4187 *m*(T_o - $T_{i tank}$)

Heat loss in tank (in t sec) = $28 \, ^{\circ}C_{p}^{}$ ($T_{tank,x}^{}$ -1- $T_{tank,x}^{*}$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$\mathsf{F_{R}=2.04 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}}\right)\right]$$

$$\eta = 996.62 * \hat{m} * \frac{T_e - T_i}{I_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping =2061 * \dot{m} * $(T_o - T_{i tank})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T^*_{tank,x})$

Results: Calculate values of different parameters.

Notes

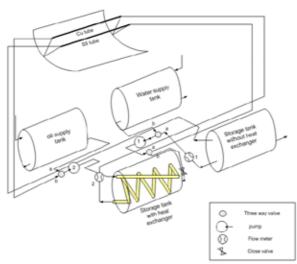
Insight Solar **Experiment No. 3**

Objective: Determine the Performance (U_L, F_R, η) of the Parabolic Trough collector with varying flow rate of fluid with (i) Water and (ii) Oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and

- pipe) will not be change during this experiment. Flow rate of water can be changed by changing voltage of pump A.
- (ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be change during this experiment. Flow rate of oil can be changed by changing voltage of pump B.



Observations:

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation		T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/
		(W/m²)	(m/sec)							sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S.	Time	Solar	Wind	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow
no.	(sec)	insolation								rate (Kg/
		(W/m ²)	(m/sec)							sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Calculate all the parameters for each set by keeping mass flow rate constant in a set. Following equations will be used for evaluation of different parameters.

Experiment No. 3

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} \dots$$
 for $V < 0.67$

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} \dots for V > 0.67$$

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{cl}D_{int}} + \frac{D^{-}\ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$F_2 = 2.04 \times 10^6 \times \frac{ih_{tr}}{I_{tr}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{U_L F_{tr}^{(1)}}{I_{tr}}\right)\right]$$

$$\eta = 2024 * \dot{m} * \frac{T_0 - T_1}{I_0}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_o}{2}$$

$$T_m = \frac{Q_u}{2}$$

$$T_o = T_i + \frac{Q_u}{m*C_n}$$

Loss in piping =4187 *m*(
$$T_a$$
- T_{iran})

Heat loss in tank (in t sec) = $28 C_p^*$ ($T_{tank,x}^- - 1 - T_{tank,x}^*$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{et}D_{int}} + \frac{D-\ln[D_{ext}/D_{int}]}{2 * K_T}\right]}$$

$$\mathsf{F_{R}=2.04 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{-7} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}}\right)\right] \\ \mathsf{F_{R}=4.2 \times 10^{-7} \times \frac{m_{w}}{v_{L}}} \left[1 - \exp\left(-2.38 \times 10^{$$

$$\eta = 996.62 * \dot{m} * \frac{T_e - T_i}{I_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping =2061 * \dot{m} * $(T_o - T_{i tank})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$

Results: Calculate different parameters values.

Notes

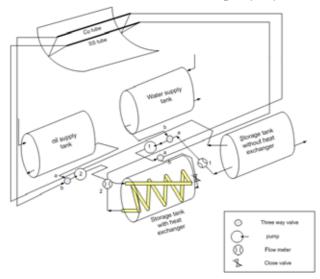
Insight Solar **Experiment No. 4**

Objective: Determine the Performance (U_L, F_R, η) of the Parabolic Trough collector with changing insulation thickness with (i) water and (ii) oil as working fluid

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and

- pipe) will not be change during this experiment. Flow rate of water can be changed by changing voltage of pump A.
- (ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be change during this experiment. Flow rate of oil can be changed by changing voltage of pump B.



Experiment No. 4

Observations:

(i). For insulation of some fix thickness

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T,	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

(ii). For insulation of other thickness

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T,	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
		,			Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Calculate all parameters for each set by keeping same insulation thickness in a set. Following equations will be used for evaluation of different parameters.

Experiment No. 4

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} \dots$$
 for $V < 0.67$

$$\begin{split} UL &= 1.7*10^{.9*} \left(T_r + T_a \right) \left(T_r^2 + T_a^{\ 2} \right) + 0.427 \\ &+ 277.76*(V)^{0.53} \ \dots \quad \text{for } V > 0.67 \end{split}$$

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ct}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$F = 2.04 \cdot 106 \cdot \frac{10_U}{L} + \frac{1$$

$$\eta = 2024 * \dot{m} * \frac{T_o - T_i}{I_h}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_{ij})}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_o}{2}$$

$$T_o = T_i + \frac{Q_u}{\dot{m} * C_p}$$

Loss in piping =4187 *m* $(T_o-T_{i tank})$

Heat loss in tank (in t sec) = $28*C_p*$ ($T_{tank,x}$ -1- $T*_{tank,x}$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

UL =
$$1.7*10^{-9}* (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6}..... for V < 0.67$$

UL =
$$1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} \dots$$
 for V > 0.67

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ct}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$\mathsf{F_{R}} = 2.04 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}} \right) \right]$$

$$\mathsf{F_{R}} = 4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}} \right) \right]$$

$$\eta = 996.62 * \dot{m} * \frac{T_o - T_i}{t_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping = 2061 * \dot{m} * $(T_o - T_{i tank})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T^*_{tank,x})$

Results: Calculate values of different parameters.

Notes

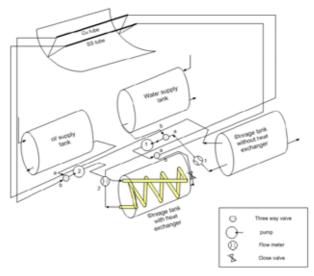
Insight Solar **Experiment No. 5**

Objective: Determine the Performance (U_L, F_R, η) of the Parabolic Trough collector with different inlet water temperature with (i) water and (ii) oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and

- pipe) will not be change during this experiment. Flow rate of water can be changed by changing voltage of pump A.
- (ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be change during this experiment. Flow rate of oil can be changed by changing voltage of pump B.



Observations:

(i). For inlet water temperature =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
		l			Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

(ii). For inlet water temperature

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
		,			Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Calculate all parameters for each set by keeping particular inlet water temperature in a set. Following equations will be used for evaluation of different parameters.

Experiment No. 5

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

UL =
$$1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} \dots$$
 for $V < 0.67$

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} \dots for V > 0.67$$

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{cl}D_{int}} + \frac{D \cdot \ln(D_{ext}/D_{int})}{2 \cdot K_T}\right]}$$

$$F_2 = 2.04 \times 10^6 \times \frac{rh_w}{L} \left[1 - \exp\left(-4.91 \times 10^{-7} \times U_L F^{-1}\right) + \frac{1}{2} + \frac$$

$$\eta = 2024 * \dot{m} * \frac{T_o - T_i}{I_h}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_{i)}}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_1 + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{\dot{m} * C_p}$$

Loss in piping =4187 *m* $(T_o-T_{i tank})$

Heat loss in tank (in t sec) = $28*C_p*$ ($T_{tank,x}$ -1- $T*_{tank,x}$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

UL =
$$1.7*10^{-9}* (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6}..... for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ct}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$\mathsf{F_{R}} = 2.04 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}} \right) \right]$$

$$\mathsf{F_{R}} = 4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}} \right) \right]$$

$$\eta = 996.62 * \dot{m} * \frac{T_o - T_i}{t_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping =2061 * \dot{m} * $(T_o - T_{i \text{ tank}})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$

Results: Calculate values of different parameters.

Notes

Insight Solar **Experiment No. 6**

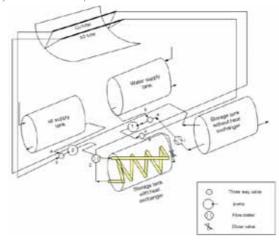
Objective: Determine the Performance (UL, FR, η) of the Parabolic Trough collector with different wind speed with (i) water and (ii) oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and pipe) will not be change during this experiment. Wind speed can't be changed by user but this experiment

can be performed at different time of a day or different day to see the effect of performance in different wind speed.

For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be change during this experiment. Wind speed can't be changed by user but this experiment can be performed at different time of a day or different day to see the change in wind speed.



Observations:

(i). For wind speed =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S.	Time (sec)	Solar insolation	Wind	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/
110.	(300)	(W/m²)	(m/sec)							sec)
		J.			Set 1					·
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

(ii). For wind speed =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T,	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Calculate all parameters for each set by keeping constant wind speed for a set. Following equations will be used for evaluation of different parameters.

Experiment No. 6

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

UL =
$$1.7*10^{-9}* (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6}..... for V < 0.67$$

$$\begin{split} UL &= 1.7*10^{.9*} \left(T_r + T_a \right) \left(T_r^2 + T_a^{\ 2} \right) + 0.427 \\ &+ 277.76*(V)^{0.53} \ \dots \quad \text{for } V > 0.67 \end{split}$$

$$F' = \frac{\frac{1}{U_L} \frac{1}{D_{ext}} \frac{1}{D_{ext}}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ct}D_{int}} + \frac{D-\ln(D_{ext}/D_{int})}{2+K_T}\right]}$$

$$\eta = 2024 * \dot{m} * \frac{T_0 - T_1}{I_0}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_{ij})}{h_{ci} * \pi * D_{ext} * L}$$

$$T_r = \frac{T_i + T_o}{T_o}$$

$$T_m = \frac{T_1 + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{\dot{m} * C_p}$$

Loss in piping =4187 *m* $(T_o-T_{i tank})$

Heat loss in tank (in t sec) = $28*C_p*$ ($T_{tank,x}$ -1- $T*_{tank,x}$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$\mathsf{F_{R}} = 2.04 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-4.91 \times 10^{-7} \times \frac{v_{L}F^{\square}}{m_{w}} \right) \right]$$

$$\mathsf{F_{R}} = 4.2 \times 10^{6} \times \frac{m_{w}}{v_{L}} \left[1 - \exp\left(-2.38 \times 10^{-7} \times \frac{v_{L}F^{/}}{m_{w}} \right) \right]$$

$$\eta = 996.62 * \dot{m} * \frac{T_o - T_i}{I_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ei} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping = 2061 * \dot{m} * $(T_o - T_{i \text{ rank}})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T^*_{tank,x})$

Results: Calculate values of different parameters.

Notes

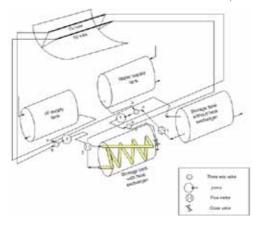
Insight Solar **Experiment No. 7**

Objective: Determine the Performance (UL, FR, η) of the Parabolic Trough collector with different ambient temperature with (i) water and (ii) oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and pipe) will not be change during this experiment. Ambient temperature can't be changed by

- user but this experiment can be performed at different time of a day or different day to see the impact on performance at different ambient temperature.
- For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Insulation thickness (of tank and pipe) will not be change during this experiment. Ambient temperature can't be changed by user but this experiment can be performed at different time of a day or different day to see the change in ambient temperature.



Observations:

(i). For ambient temperature =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
		l			Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

(ii). For ambient temperature =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
					Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
		,			Set 1					
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Calculate all parameters for each set for constant ambient temperature. Following equations will be used for evaluation of different parameters.

Experiment No. 7

(i) Water as working fluid:

Performance parameters will be evaluated with the help of eq. 1A, 2, 3A, 4A, 5A, B, C, 6A and 7A.

UL =
$$1.7*10^{-9}* (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6}..... for V < 0.67$$

UL =
$$1.7*10^{-9*}$$
 ($T_r + T_a$) ($T_r^2 + T_a^2$) + 0.427 + $277.76*$ (V)^{0.53} for V > 0.67

$$F' = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ct}D_{int}} + \frac{D \cdot \ln(D_{ext}/D_{int})}{2 \cdot K_T}\right]}$$

$$E_{T} = 2.04 \times 10^6 \times \frac{\ln_W}{L} \left[1 - \exp\left(-4.91 \times 10^{-7} \times U_E^{-1}\right)\right]$$

$$\eta = 2024 * \dot{m} * \frac{T_o - T_i}{I_h}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_{i)}}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_1 + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{\dot{m} * C_p}$$

Loss in piping =4187 *m* $(T_o-T_{i tank})$

Heat loss in tank (in t sec) = $28*C_p*$ ($T_{tank,x}$ -1- $T*_{tank,x}$)

(ii) Oil as working fluid: Performance parameters will be evaluated with the help of eq. 1B, 2, 3B, 4B, 5A, B, C, 6B and 7B.

$$UL = 1.7*10^{-9*} (T_r + T_a) (T_r^2 + T_a^2) + 25.746*(V)^{0.6} for V < 0.67$$

$$UL = 1.7*10^{.9*} (T_r + T_a) (T_r^2 + T_a^2) + 0.427 + 277.76*(V)^{0.53} for V > 0.67$$

$$F^{/} = \frac{\frac{1}{U_L}}{\left[\frac{1}{U_L} + \frac{D_{ext}}{h_{ci}D_{int}} + \frac{D \cdot \ln[D_{ext}/D_{int}]}{2 \cdot K_T}\right]}$$

$$F_R = 2.04 * 10^6 * \frac{m_w}{v_L} \left[1 - \exp\left(-4.91 * 10^{-7} * \frac{v_L F^{\square}}{m_w} \right) \right]$$

$$F_R = 4.2 * 10^6 * \frac{m_w}{v_L} \left[1 - \exp\left(-2.38 * 10^{-7} * \frac{v_L F^{\square}}{m_w} \right) \right]$$

$$\eta = 996.62 * \dot{m} * \frac{T_o - T_i}{I_b}$$

Theoretical values of different temperature values

$$T_r = T_m + \frac{\dot{m} * C_p * (T_o - T_i)}{h_{ci} * \pi * D_{ext} * L}$$

$$T_m = \frac{T_i + T_0}{2}$$

$$T_o = T_i + \frac{Q_u}{m \cdot C_p}$$

Loss in piping =2061 * \dot{m} * $(T_o - T_{i \text{ tank}})$

Heat loss in tank (in t sec) = $27 * C_p * (T_{tank,x-1} - T_{tank,x}^*)$

Results: Calculate values of different parameters.

Notes

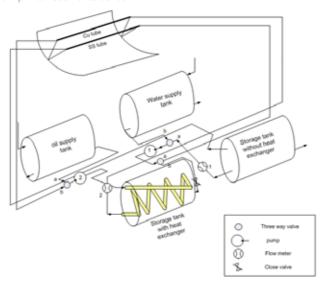
Insight Solar **Experiment No. 8**

Objective: Find an optimum flow rate of fluid for getting minimum heat losses (or maximum heat gain) for different insulation thickness with (i) water and (ii) oil as working fluid.

Experimental set-up: Set-up for this experiment will remain the same as discussed earlier in the starting of this manual. But for this experiment, we have to make tank and receiver tube selection.

(i) For this, we have to fix the V-clamp such that SS receiver tube will remain at focus of parabolic reflector. Valve-1 will be positioned at 'b' direction and valve-2 will be positioned at 'a' direction. So that water will flow from pump 1 to receiver tube 'SS'. Insulation thickness (of tank and pipe) will not be change during this experiment. Tank insulation thickness will not be changed for one set of observation.

(ii) For this, we have to fix the V-clamp such that Copper receiver tube will remain at focus of parabolic reflector. Valve 1 will be position at 'a' direction. Valve 2 will be position at 'b' direction so that water will flow form pump 1 to heat exchanger tank. Close valve will cut the connection of this tank from water tank (tank no.1). Valve-3 will be positioned at 'b' direction. Tank insulation thickness will not be changed for one set of observation



Observations:

(i). For insulation thickness=

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T,	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
	Set 1									
1										
2										
3										
	Set 2									
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
	Set 1									
1										
2										
3										
					Set 2					
1										
2										
3										

(ii). For insulation thickness =

Tank insulation thickness =

Pipe insulation thickness =

Set A: Water as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T,	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
	Set 1									
1										
2										
3										
					Set 2					
1										
2										
3										

Set B: Oil as working fluid

S. no.	Time (sec)	Solar insolation (W/m²)	Wind velocity (m/sec)	T _a	T _r	T _i	T _o	T _{i tank}	T _{tank}	Mass flow rate (Kg/ sec)
	Set 1									
1										
2										
3										
					Set 2					
1										
2										
3										

Calculations: Mass flow rate, wind velocity, solar insolation and insulation thickness will remain the same during the calculation of different parameters. If any of weather parameter changes, do the calculation in parts in which all parameters remain constant all the time. Following equations will be used for evaluation of different parameters.

(i) Water as working fluid:

Heat gain by fluid in receiver tube = $\dot{m} * C_{\mathbb{R}^{(w)}} * (T_0 - T_i)$

Loss in piping =4187 * \hat{m} * $(T_o - T_{i \ tank})$

$$\text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 4187 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_{i \ tank}) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) - 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) + 2061 * \hat{m} * (T_o - T_i) \\ \text{Net heat gain} = \hat{m} * C_{g(n)} * (T_o - T_i) + 2061 * \hat{m} * ($$

(ii) Oil as working fluid:

Heat gain by fluid in receiver tube = $\dot{m} * C_{p(oi)}*(T_o - T_i)$ Loss in piping =2061 * \hat{m} * $(T_o - T_{i \ tank})$

Notes			

Insight Solar

Nomenclatures:

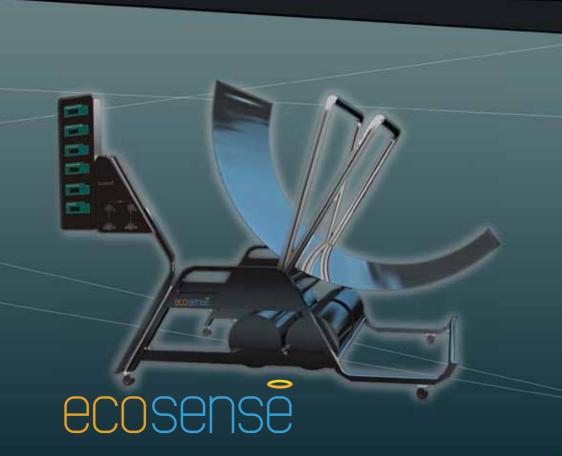
h _w	Convective heat transfer coefficient between tube and atmosphere	μ_{w}	Dynamic viscosity of water
h _r	Radiative Heat transfer coefficient of radiation	$Cp_{\scriptscriptstyle{(w)}}\\K_{\scriptscriptstyle{w}}$	Specific heat of water (4.187KJ/Kg/0K) Thermal conductivity of water (0.6 W/m/0K)
T,	Receiver tube temp.	Re _{oil}	Reynolds no. of oil
T	Ambient temp.	Pr _{oil}	Prandtl no. of oil
K _a	Thermal conductivity of air (0.026W/m/K)	V _{oil}	Oil velocity
V	wind velocity	U _{oil}	Kinematic viscosity of oil (3.0*10-5m2/s)
Nu _a	Nusselt no. of air	0	Density of oil (900 Kg/m3)
Re	Reynolds no. of air	ρ _{oil}	Dynamic viscosity of oil (0.027Ns/m2)
U _a	Kinematic viscosity of air (1.6*10-	$\mu_{\text{oil}} \\ \text{Cp}_{\text{(oil)}}$	Specific heat of oil (2061J/Kg/0K))
	5m2/s)		Thermal conductivity of oil (0.165
3	Emissivity of receiver tube material (black nickel = 0.66)	K _{oil}	W/m/0K)
σ	Stefan-Boltzman constant (5.67×10−8 W m−2 K−4)	A_{int}	Internal cross sectional area of receiver tube (3.14*(0.0125) ² = 0.00049m ²)
U _L	overall heat transfer coefficient (can be calculated by eq.1)	m	Flow rate of fluid (in Kg/sec)
D _{ext}	External diameter of receiver tube	C_p	Specific heat of fluid (water or oil)
	(0.025m)	A_{a}	Aperture area of parabolic reflector (1.695*1.22 = 2.068 m2)
D_{int}	Internal diameter of receiver tube (0.023m)	T ₀	Receiver tube outlet temp.
h _{ci}	Convective heat transfer coefficient	T,	Receiver tube outlet temp.
'ci	between receiver tube and water	T,	Receiver tube temp
K _r	Thermal conductivity of receiver tube		Tube inlet temp.
	material (copper and stainless steel in our system)	T _i	Tube outlet temp.
I	Length of receiver tube (1.2m)	T _o	Instantaneous reading of tank water
Re _w	Reynolds no. of water	$T_{\text{tank,x}}$	temperature
Pr _w	Prandtl no. of water	T _{tank,x} *	Supposed to be previous tank water
V _w	Water velocity	tui ityx	temperature before mixing of hot incoming water
U _w	Kinematic viscosity of water (16.68*10-6m2/s)	$T_{\text{tank,x}}$	Previous reading of tank water temperature
V _w	Water flow velocity	t	Time (in sec) between current
$\rho_{\rm w}$	Density of water		reading an previous reading

Notes		

Notes	

About Ecosense

Ecosense provides world class training solutions in renewable energy and clean environment. As a group of engineers, researchers and designers, Ecosense has developed cutting edge products to create skilled human resource for renewable energy sector. Founded by group of IIT graduates, Ecosense is dedicated towards building mechanisms that will develop highly skilled workforce that enables the development of clean environment for human race.



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