



CFD in Cyber-Learning Platform at NCHC

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5/5/16

Cyber-Learning Platform at NCHC (<http://www.emedu.org.tw>)

NARLabs

Commitment · Passion · Innovation



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[中心團隊]業務費報銷規定更新

<更多行政公告>

電磁學數位學習網

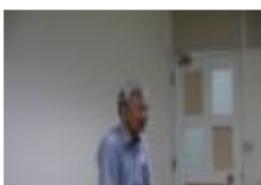
學生專區

電磁學數位學習網

老師管理系統

活動花絮

中心活動



Characteristics of Cyber-Learning Platform at NCHC

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- Management System for Lectures and Students
- Modularization of Teaching Contents
- Multi-Media and Interactive Simulations as Supplemental Teaching Contents
- Learning Path Management System
- Evaluation System

Goal

Enhance Learning Efficiency
of Students in Thermal-Fluid
Engineering Field through
Multi-Media and Simulation
Based Teaching Contents

First-Phase Approaches

- Collection of Thermal-Fluid related Course Information from Universities in Taiwan
- Discussions/Meetings with Professors in Thermal-Fluid Engineering Education Platform to Define Current Educational Challenges, Needs & Wants
- Development of Supplemental Teaching and Software Contents

Multi-Media and Interactive Simulations as Teaching Contents

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- Simulation Animation with JavaScript Presentation
- Experimental Observation vs. Simulation Animation
- Interactive Simulations by Open Source Software
- Software Tools Development with JavaApplet/ JavaScript Presentation (Calculator)

Simulation Animation with JavaScript

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Presentation

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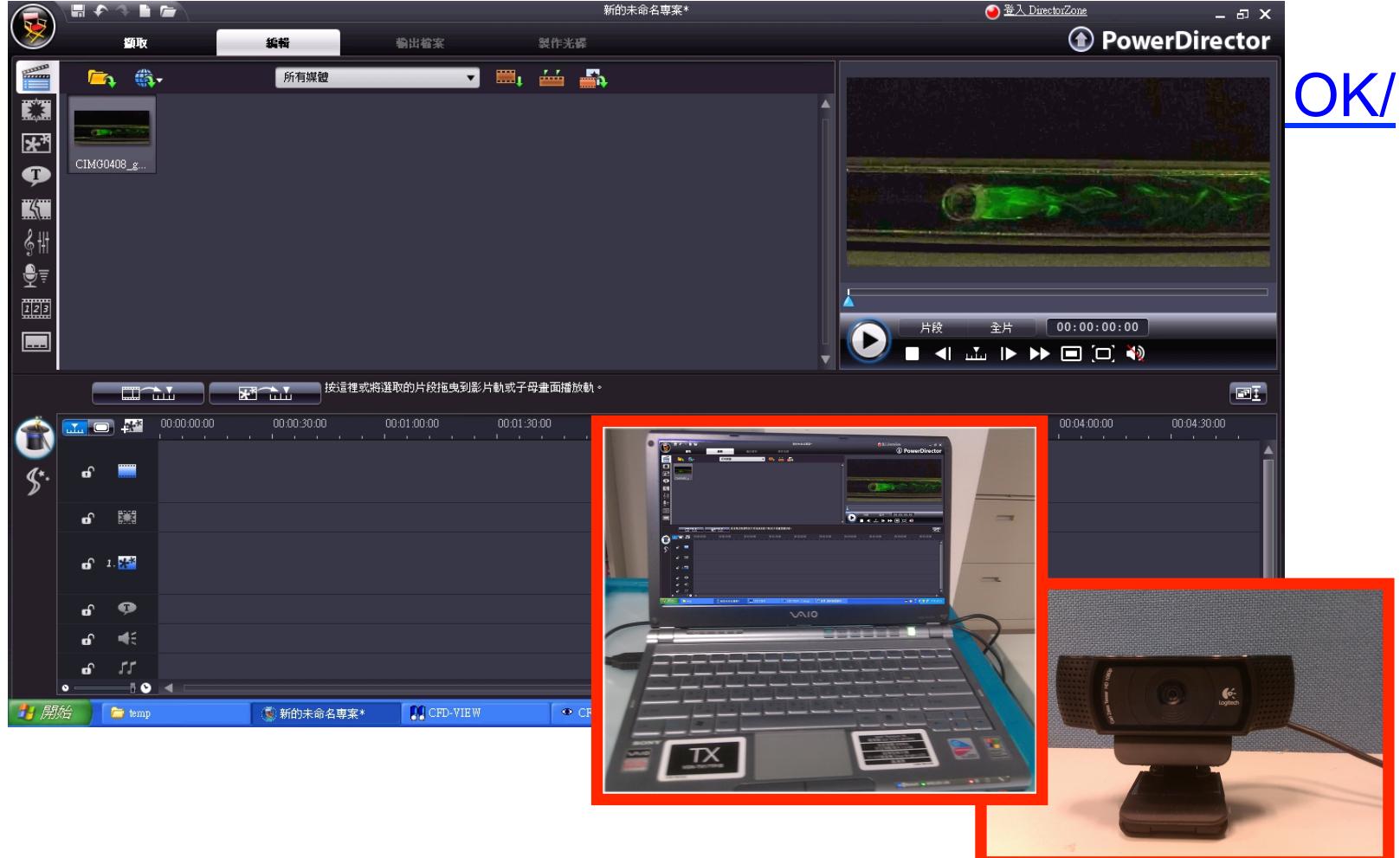
- Timelines, Pathlines, Streaklines, and Streamlines
 - [http://paintingwordnotebook.nchc.org.tw/FM_OK/
En-FM00002 Timeline Pathline Streakline Streamline.html](http://paintingwordnotebook.nchc.org.tw/FM_OK/En-FM00002_Timeline_Pathline_Streakline_Streamline.html)
- No-Slip Boundary Condition
 - [http://paintingwordnotebook.nchc.org.tw/FM_OK/
En-FM00003 No slip BC.html](http://paintingwordnotebook.nchc.org.tw/FM_OK/En-FM00003_No_slip_BC.html)

Experimental Observation vs. Simulation Animation

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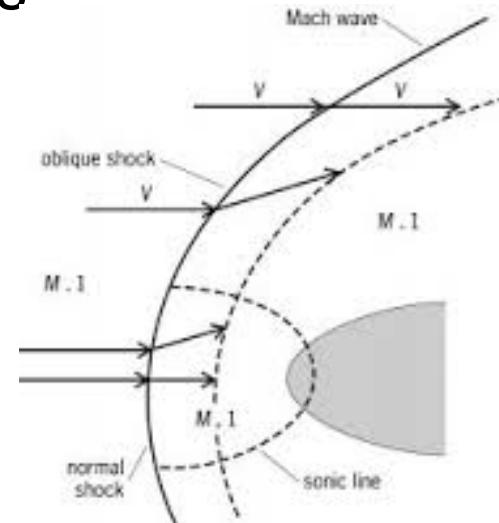
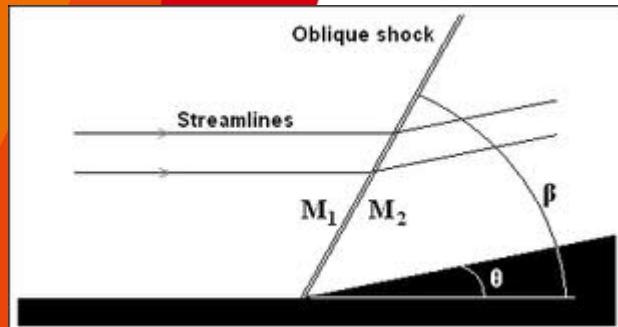
- Flow Over a Cylinder



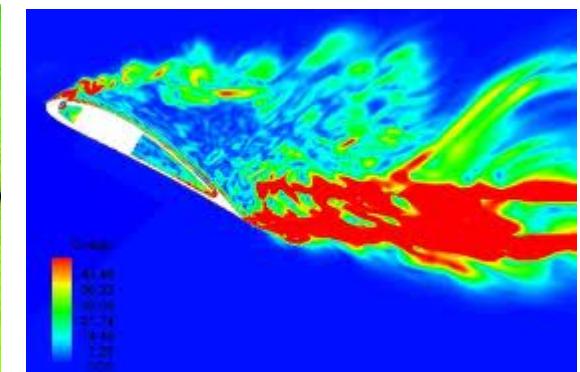
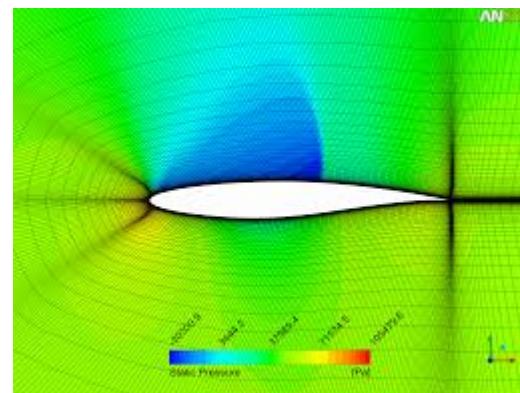
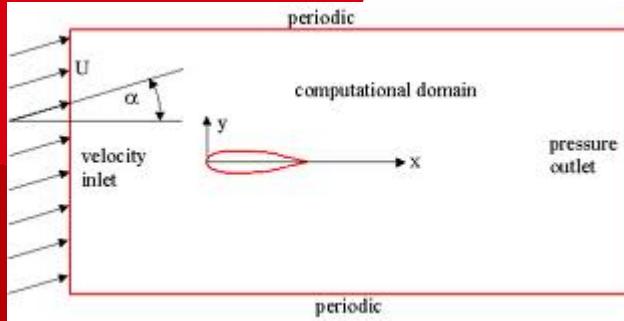
Simulation Based Teaching

Contents (1/4)

- Compressible Flows/Inviscid Flows
 - Oblique shock wave

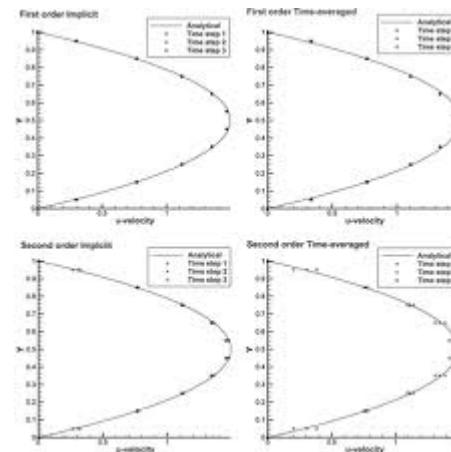
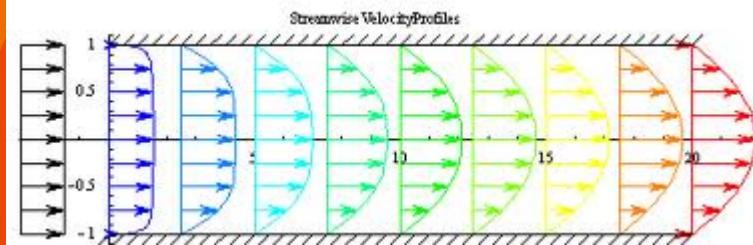


- Flow over an airfoil (NACA0012)



Simulation Based Teaching Contents (2/4)

- Incompressible Flows/Viscous Flows
 - Open channel flow



- Back facing step flow

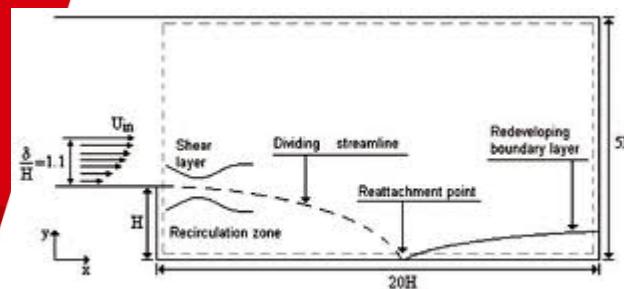
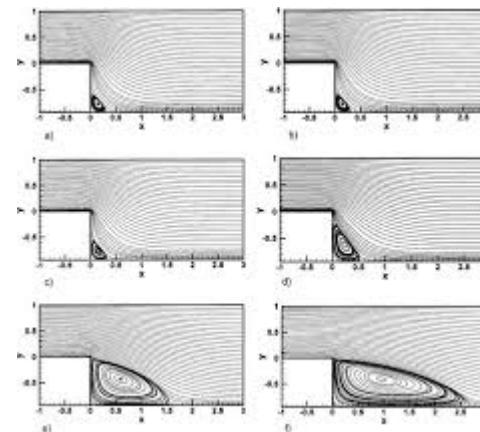


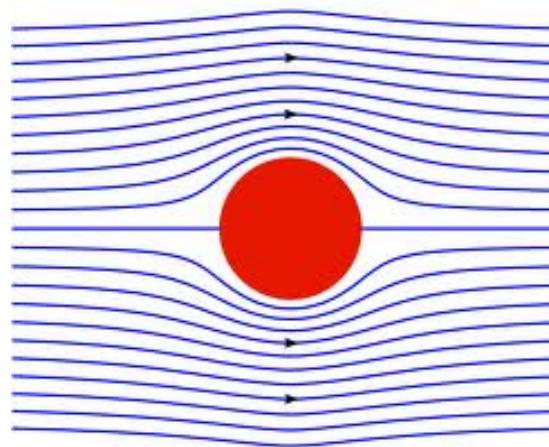
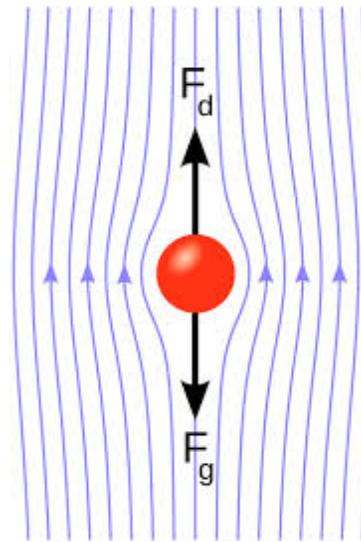
Figure 1. Back step geometry and computational domain.



Simulation Based Teaching

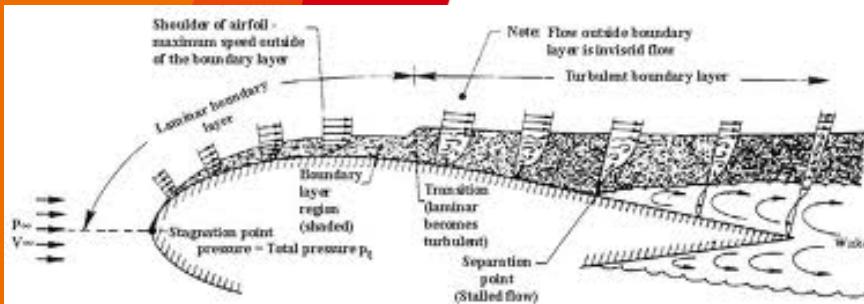
Contents (3/4)

- Incompressible Flows/Viscous Flows
 - Ball dropping
- Potential Flows
 - Flow over a cylinder

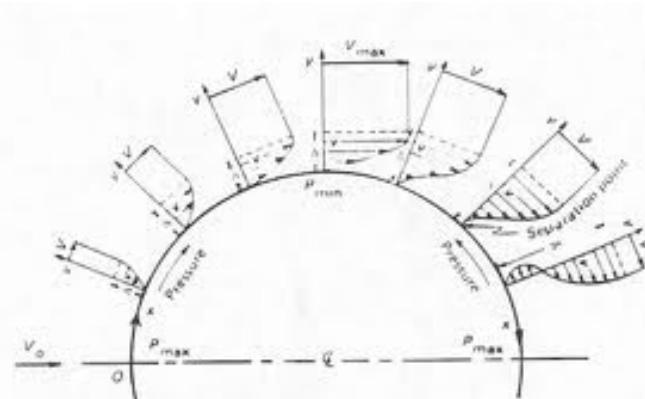
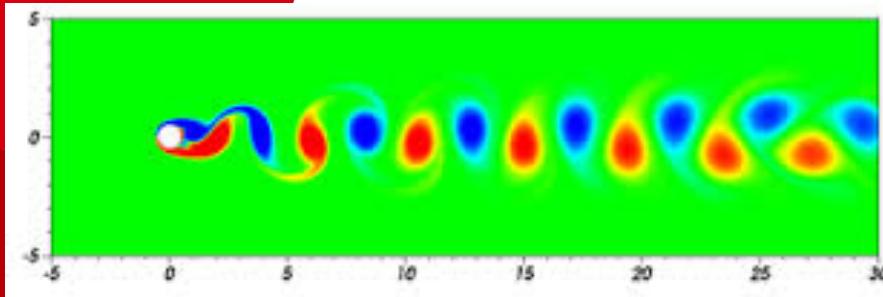


Simulation Based Teaching Contents (4/4)

- Boundary Layer
 - Flow Separation



- Vortex Shedding



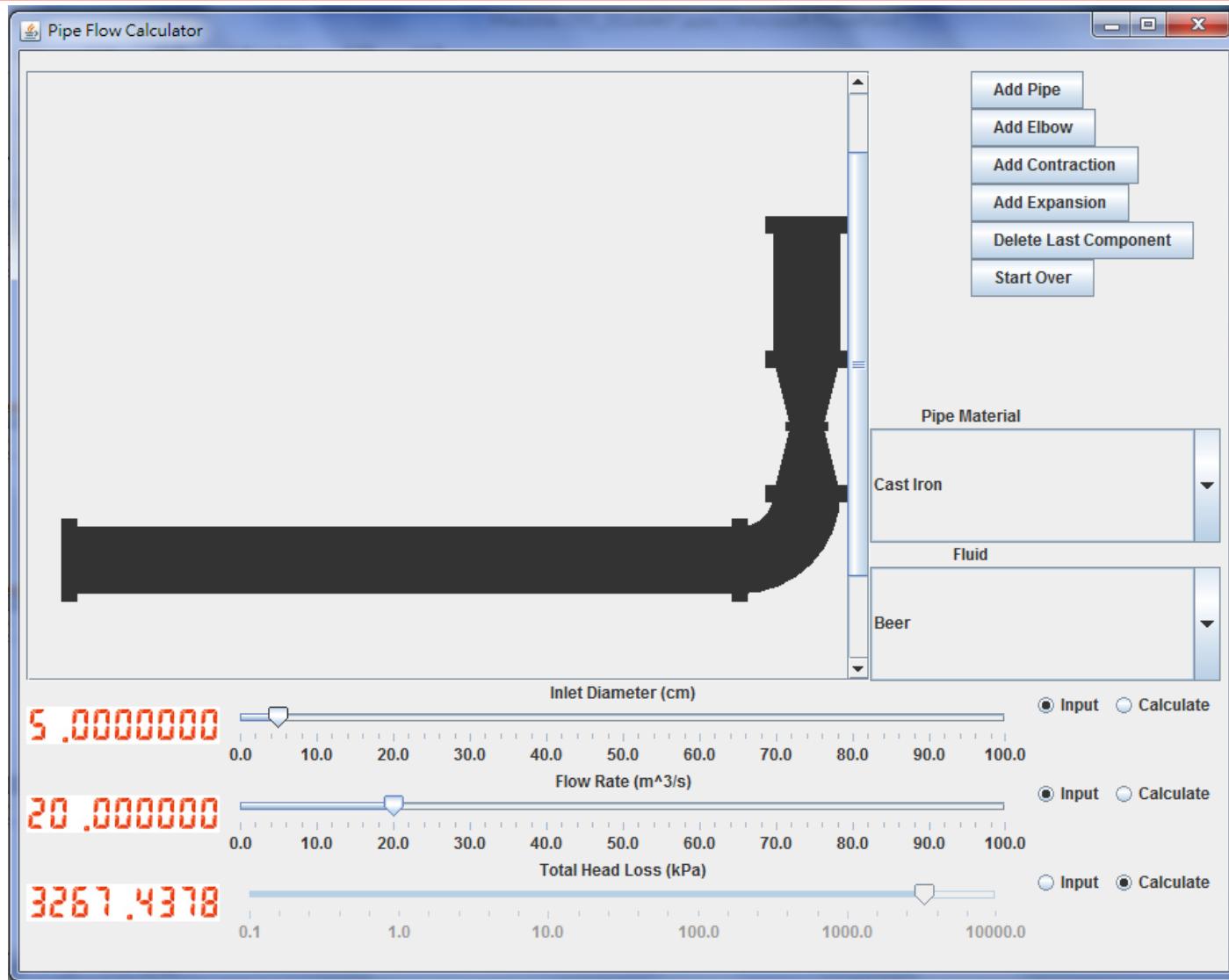
Reynolds Number Effects

$Re < 5$		Creeping flow (no separation)
$5-15 < Re < 40$		A pair of stable vortices in the wake
$40 < Re < 150$		Laminar vortex street
$150 < Re < 3 \times 10^5$		Laminar boundary layer up to the separation point, turbulent wake
$3 \times 10^5 < Re < 3.5 \times 10^5$		Boundary layer transition to turbulent
$Re > 3.5 \times 10^5$		Turbulent vortex street, but the separation is narrower than the laminar case

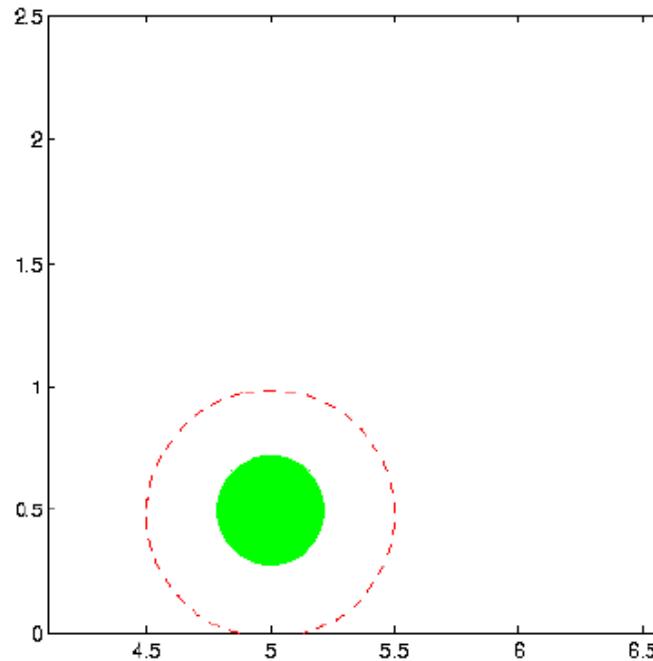
Pipe Flow Calculator

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Interfacial Phenomena: Moving Boundary Problems



Multi-Media and Simulation Based **NARLabs** Teaching Contents (1/2)

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The drag on a circular cylinder placed in a uniform flow can be determined by measuring either the pressure on the surface of the cylinder or a combination of the velocity profile in the wake and the pressure drop in the tunnel. This involves the use of two different control volumes, CV_1 and CV_2 .

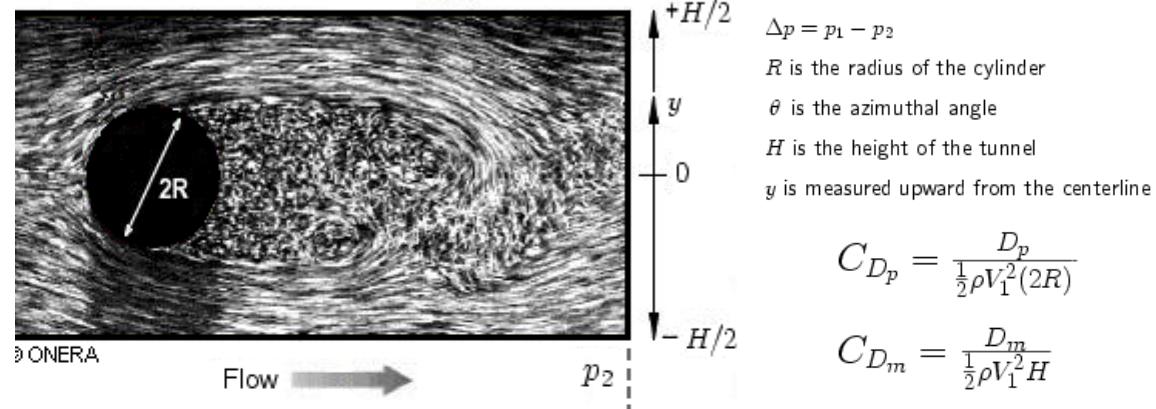
CV_1 encloses the cylinder. If we neglect the surface shear stress, the force on the cylinder is due entirely to the pressure integrated over the surface. The force per unit width is D_p , where

$$D_p = 2 \int_0^\pi p \cos \theta R d\theta$$

CV_2 is inscribed within the tunnel walls. There are momentum fluxes through the upstream and downstream faces, associated with velocities V_1 , which is constant, and V_2 , which varies with y . There is also a pressure difference between the upstream and downstream faces $\Delta p = p_1 - p_2$. If we neglect the shear stresses acting on the wind tunnel walls, the force per unit width is D_m , where

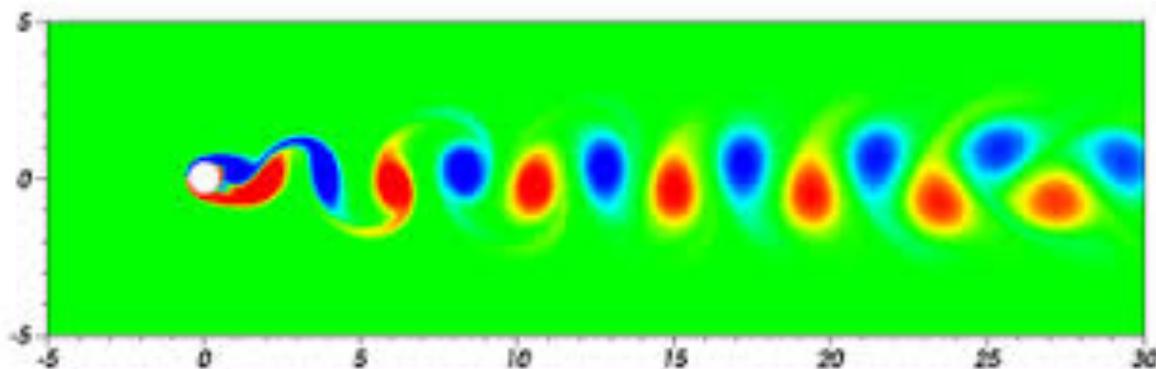
$$D_m = (p_1 - p_2)H + \rho V_1^2 H - 2 \int_0^{H/2} \rho V_2^2(y) dy$$

We usually express aerodynamic forces in terms of non-dimensional coefficients, so we define C_{D_p} and C_{D_m} . We expect $C_{D_p} = C_{D_m}$ for a given speed, i.e. for the same Reynolds number.



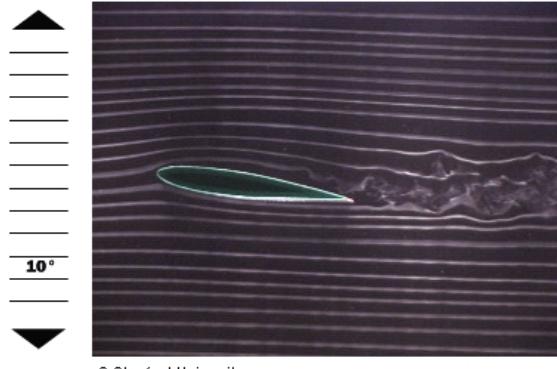
$$C_{D_p} = \frac{D_p}{\frac{1}{2}\rho V_1^2(2R)}$$

$$C_{D_m} = \frac{D_m}{\frac{1}{2}\rho V_1^2 H}$$

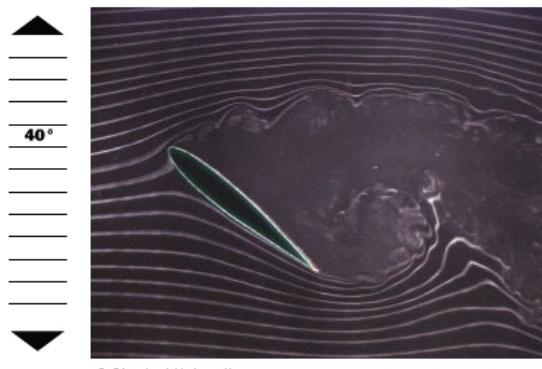


Multi-Media and Simulation Based **NARLabs** Teaching Contents (2/2)

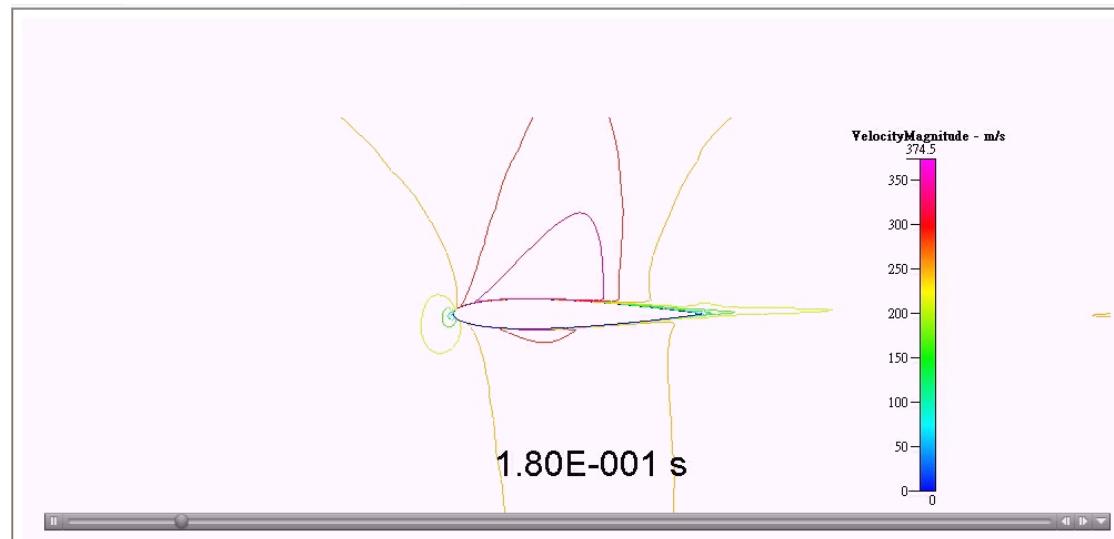
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Future Works

- Continue to Develop Interactive Simulation Cases as Supplemental Teaching Contents
- Integrate Learning Path Management System with Modularization of Teaching Contents
- Development of Applied Software Tools
- Promotion for Thermal-Fluid Engineering Education Platform

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