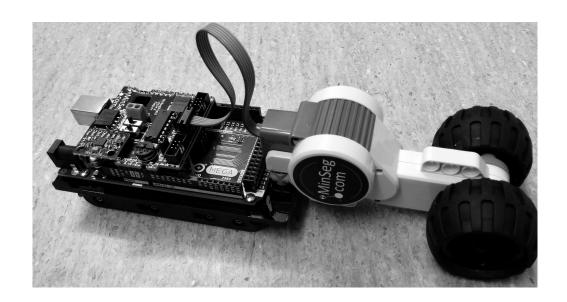
Angle estimation using gyros and accelerometers

This version: January 23, 2018



REGLER	RTEKNIK	
AUTOMATIC CONTROL		
LINK	ÖPING	

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Chapter 1

Introduction

The purpose of this lab is to illustrate sensors, measurements, filtering and simple sensor fusion. Our goal is to estimate the tilt-angle of the MinSeg. By extracting information from both the accelerometers and the gyro and combining these using low-pass and high-pass filters, we will create a better estimate of the angle of the MinSeg, compared to a naive approach of using only the gyro, or only the accelerometer.



Figure 1.1: Intuitive Aerial AB in Linköping develops a camera-carrying Hexacopter. For high-precision autonomous flight (and filming), it is important to know the orientation (pitch-, roll- and yaw-angles) of the system. Gyros and accelerometers are used to extract as much information as possible, with as little error and noise as possible.

1.1 Hardware set-up

The lab is based on three main hardware components.

To begin with, we have a standard desktop computer. This computer is used to automatically develop and deploy code using MATLAB and SIMULINK models.

We use a board which is equipped with an accelerometer and a gyro. The board is built around an Arduino micro-controller which runs the autogenerated code. The Arduino computer also communicates with the desktop computer and thus allows us to look at the measurements.

The Arduino board together with the motor and wheels is called the Min-Seg.

1.2 Trouble shooting

Complaints about COM port or connection when downloading to board Disconnect USB-cable and connect it again.

Complaints about OUT OF MEMORY when compiling code Save your model and restart MATLAB.

Chapter 2

Preparation

The questions below, and all questions throughout the document marked as **Preparation** must be done before attending the lab. Note that there are additional preparation exercises in Chapter 3.

Solutions to all questions should be available upon request from the lab assistant, and the preparation exercises in Chapter 3 are preferably written in this printed documented.

The scheduled time spent with the laboratory equipment is only a small part of the complete lab, as a major part is spent on the theoretical material during preparations.

Preparation 1 *Read Chapter 1 and 2 in the auxiliary course compendium.*

Preparation 2 Gyros allows us to measure the angular velocity, which we can integrate (numerically in practice) to obtain the rotation angle. The problem is that the angular velocity measurements have errors.

We typically divide errors into a fixed constant error (called bias or calibration error) and a faster varying error term (noise) which is 0 on average. Consider the measurement of a true angular velocity $\omega(t)$ which we want to integrate to obtain the true rotation angle $\theta(t) = \int_0^t \omega(\tau) d\tau$. Let the measurement be $\omega_m(t)$. A simple description uses a bias b, noise amplitude ε and noise frequency N,

$$\omega_m(t) = \omega(t) + b + \epsilon \sin(Nt)$$
 (2.1)

Integrate this expression analytically and derive an expression for the estimated angle $\theta_m(t) = \int_0^t \omega_m(\tau) d\tau$ (you assume initial conditions to be 0). The solution will consist of the true angle, a linear term, and a periodic term. Verify that the term in the error $\theta(t) - \theta_m(t)$ that depends on b will grow as time increases (called linear dift), but the term coming from the high-frequency noise will be limited and decrease the larger N is.

Preparation 3 To obtain the rotation angle $\theta(t)$, we have to compute the integral $\theta(t) = \int_0^t \omega(\tau) d\tau$. However, we cannot integrate perfectly on a computer with a finite number of samples, and must use an approximation. One such integral approximation is a rectangle approximation based on Euler backwards. With measurements $\omega(kT_s)$ for $k=0,1,\ldots$ and sample-time T_s , the approximation is given by

$$\theta(kT_s) = \theta((k-1)T_s) + T_s\omega(kT_s) \tag{2.2}$$

Consider the case in Figure 2.1 where a signal $\omega(t)$ has been sampled with $T_s = 1$ second. Illustrate graphically in the figure how the integral from t = 0 to t = 4 is computed by rectangle approximation, and confirm that the approximation leads to the estimate $\theta(4) = 9.5$. Note that the value $\omega(0)$ never is used in the backwards approximation. You initialize the angle estimate to $\theta(0) = 0$.

Preparation 4 When working with sampled signals, we often use the z-transform for notational convenience. Instead of working with $\theta(kT_s)$ we introduce its transform $\theta(z)^1$, and the unit delay-operator $\frac{1}{z}$ to express $\theta((k-1)T_s)$, i.e., the transform of "previous value" $\theta((k-1)T_s)$ is $\frac{1}{z}\theta(z)$. Introduce this notation for (2.2) and show that the integral approximation algorithm (2.2) can be represented as

$$\mathbf{\theta}(z) = \frac{T_s z}{z - 1} \mathbf{\omega}(z) \tag{2.3}$$

In other words, the Euler backwards algorithm is described by the discrete-time transfer function $\frac{T_s z}{z-1}$.

Preparation 5 Read the complete lab-pm. There are more theoretical questions in the pm which you are supposed to complete as preparation.

 $^{^{1}\}mathrm{To}$ avoid using capital greek letters, we indicate signal transforms by bold letters in this text

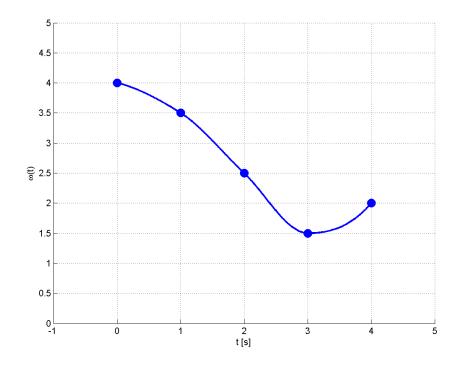


Figure 2.1: A continuous signal sampled (dots) with $T_s = 1$ second.

Preparation 6 Print this document. You must bring a physical copy to the lab.

Chapter 3

The lab

The lab will primarily consist of experimentation and data collection, using theoretical results and strategies derived during your preparation.

Items labeled **Preparation** are questions you are supposed to solve and fill out before attending the lab.

Items labeled **Task** are questions you answer and solve when attending the lab and have access to the hardware.

3.1 Gyro and accelerometer

The board is equipped with a gyro measuring angular velocity around 3 axes, and an accelerometer measuring linear acceleration in the same axes. The accelerometer and gyro hardware are placed on the blue board as indicated in Figure 3.1. The measurements are done in a body-fixed coordinate system as indicated in Figure 3.2.

The gyro

Although the gyro is the natural sensor to use for estimating an angle (as it measures the derivative of an angle), it has some problems. To begin with, the gyro measurements can only give us angles relative to initial orientation, as we simply integrate the angular velocity. In many applications, we



Figure 3.1: The accelerometer and gyro are placed on the blue board on the bottom left of the figure (here MPU-6050, on some devices it says ITG/MPU). The sensors are capable of measuring up to 4*g* accleration and an angular velocity of 250°/*s*. The blue board combining an accelerometer and a gyro is called an IMU (inertial measurement unit). Retail price in the order of 50SEK. An IMU with similar performance was at least 100x as expensive 20 years ago, and 10 times as large.

are interested in the absolute angle of the device, such as knowing if the MinSeg is standing straight up or not. In addition to this, the sensor has bias errors, meaning that the angle estimate will drift. Even if we leave the device completely still, the preparations showed that any bias in the angular velocity measurement will lead to a growing error in the angle estimate.

In the lab, we are only studying the tilt-angle of the MinSeg, i.e., the balancing angle of the MinSeg relative to the surface (0° degree when lying flat on a table, and -90° when standing straight up). Consequently, we are only interested in rotations around the x-axis (rotations in the y-z plane) and thus only use one of the gyro measurements.

The accelerometer

The accelerometer might seem unrelated to the orientation of the device, as it measures the three linear accelerations of the object. However, the acceleration is measured relative to free-fall, meaning that when the device

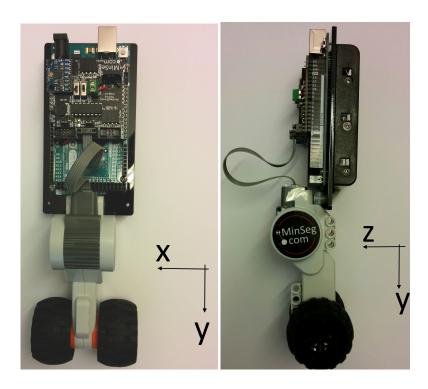


Figure 3.2: Body-fixed coordinate system used for accelerometer and gyro.

is kept still, there should be an acceleration of magnitude $\sqrt{a_x^2 + a_y^2 + a_z^2} = 9.8 m/s^2$. The way this magnitude is distributed on the three body-fixed accelerations $a_x(t)$, $a_y(t)$ and $a_z(t)$ will give us information about the absolute orientation.

Consider the coordinate system of the setup in Figure 3.2. When the device is lying flat on a table with the battery holder facing down, we should see the measurements $a_x = 0$, $a_y = 0$ and $a_z = 9.8$ (The device is accelerating up from the table, relative to free-fall. An alternative view is that there is a force in the positive z-direction). When in perfect balancing mode, i.e., tilted up and standing on its wheels, the measurements should be $a_x = 0$, $a_y = -9.8$ and $a_z = 0$. The device is still accelerating up from the table relative to free-fall (normal force up from table), but y is pointing downwards, hence the negative sign.

From this, it is clear that when we are balancing the device on its wheels and it is sufficiently still, the tilt-angle is related to the relative size of the acceleration components a_y and a_z . No movement should occur in the x-directions, and thus a_x will be 0.

In practice the MinSeg is never completely still when balancing, so a_y and

 a_z will contain parts that come from actual movements, which will influence the computed angle, i.e., we will see noise on the angle estimate. Another problem is that the accelerometer might have been installed slightly tilted, which will give us a bias on the acceleration signals. However, since we never integrate the acceleration signals in this application, this bias will not lead to any kind of drift, but just a constant error on the angle estimate.

3.1.1 Gyro experiments

The first part of the lab will concentrate on the gyro, and in particular the gyro signal for rotation around the x-axis in the y-z plane. Start MATLAB and the SIMULINK file minseg/sensor/template1 on the desktop (shown in Figure 3.3).

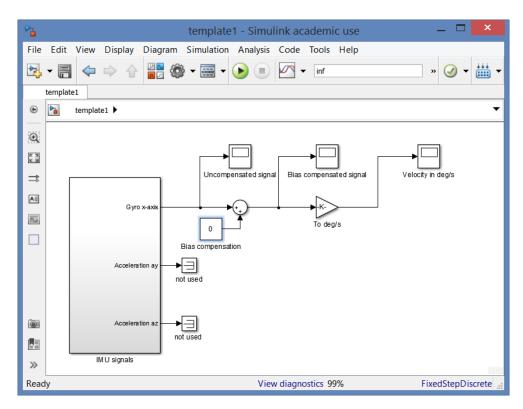


Figure 3.3: Template for gyro angle estimator.

Preparation 7 The largest possible angular velocity the gyro can measure is $250^{\circ}/s$. When the gyro senses this rate, it outputs the value 32768 (2^{15} , the largest possible number that can be encoded using 16 bits, 1 bit is used for

the sign). How should the measurement be scaled to go from tinteger value, to the unit deg/s .	he measurea
Task 1 Check the value in the gain block to confirm your prepa measurement scaling.	ration on the
Task 2 Assemble the MinSeg as shown on the front-page, and p Seg flat on the table with the battery holder facing down, and USB cable. Compile, download and run the code by pressing to button. Study the plot with the uncompensated measurement. Seg is stationary, the true angular velocity is 0, so everything you surement errors (and perhaps extremely small rotations due to the table). Make a rough estimate of the bias level, i.e., the constant (2.1). Stop the code by pressing the square black box next to the	d connect the the green run . As the Min- ou see is mea- vibrations in ant error b in
Preparation 8 A simple way to reduce the bias error is to estimand then modify the measurement so that the signal varies arou Of course, this only works if the bias really is constant (it never a timight change with temperature etc), but it is a good start. A	ind 0 instead. is in practice,

Task 3 Update the constant in the Bias compensation block such that the bias level on your device is compensated for. Download and confirm the

change by looking at the plot of the compensated signal to see that it fluctuates around 0. Also study the plot showing the angular velocity in degrees per second. Approximately how large is the amplitude of the fast varying measurement errors?
We are now ready to start integrating the adjusted angular velocity measurements. To obtain the angle, all we have to do is to integrate the signal using the approximation in preparation exercise 3.
Task 4 Extend your model according to Figure 3.4. The Discrete-time Integerator block can be found under Discrete in the library browser. Double-click the discrete-time integrator block in your model and change the Integrator method to Integration: Backward Euler, and change the sample-time to −1 (which means it uses the sample-time 0.04 seconds specified in the model configuration). The Gain should be left at 1.0. Apply and close. You have now defined the integral approximation to be computed exactly as in preparation exercise 3
Task 5 Start the code, and study the angle estimate plot. Note that it does not stay constant, despite the MinSeg being completely still. This is due to a remaining bias error and what you are seeing is mainly the linear drift. Find out how long it takes for the angle to drift 1°. This is a typical performance measure on a gyro implementation. The longer it takes, the better. Your solution will probably be in the order of 5 – 30 seconds, which means that after some minutes, the angle estimate is completely wrong. Rotate the MinSeg so that it stands on its wheels. The angle estimate should change –90°.

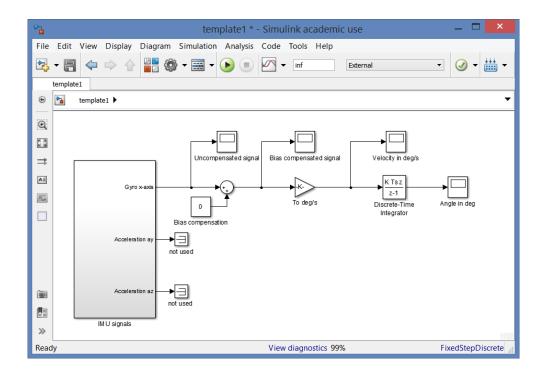


Figure 3.4: Integrated bias-compensated gyro measurements.

3.1.2 Accelerometer experiments

Let us now turn to angle estimation from the accelerometer signals. Study Figure 3.5. If the device is stationary at an angle, the total acceleration is $g = 9.8 m/s^2$ and it is pointing downwards, and thus the accelerometer measures g upwards (as it measures relative to free-fall). This acceleration signal will be picked up in the body-fixed coordinate system through the acceleration measurements $a_y(t)$ and $a_z(t)$. By geometry, we have $\theta(t) = \arctan(a_y(t)/a_z(t))$. Note that a_y will be negative from the definition of the coordinate system in Figure 3.2, hence the angle will be negative in the current definition.

Of course, if the MinSeg ever was in the angle illustrated in Figure 3.5, it would not be stationary but had to be moving. This means there might be additional forces and resulting accelerations acting, but the idea here is to see those effects as noise.

Task 6 Open the model **template2**. Double-click the gyro angle estimator and update the bias compensation to the value you found earlier. Download the code and study the angle estimate from the accelerometer signals, and

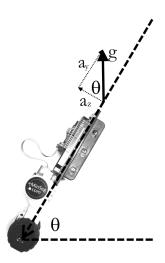


Figure 3.5: The acceleration relative to free-fall will be picked up in a stationary situation on the two coordinates $a_y(t)$ and $a_z(t)$ allowing us to compute the tilt-angle θ

compare it to the angle estimates from the gyro, both displayed in the same
plot, when you tilt the MinSeg back and forth slowly. How do they compare and differ?
Task 7 See what happens with the angle estimates if you rotate the MinSeg quickly and go beyond the measurement limit 250°/s in the gyro (hold the
MinSeg firmly in both the motor and the board so you don't break it in the connection between the board and the motor)

Task 8 Move the MinSeg around while keeping the tilt angle constant (such as standing straight up and moving it left to right quickly). How do the two angle estimates perform now?

3.1.3 Sensor fusion with complementary filter

What you should have seen now is that the angle estimated using the gyro behaves well on a short time-frame, but drifts on a long time-frame (suffers from low-frequency errors which are integrated). The angle estimate from accelerometer signal on the other hand has no drift (good in a long time-frame), but has more noise (bad on a short time-frame, high-frequency errors). We would like to combine the merits from the two sensors, while avoiding the drawbacks of them. In other words, we trust the long-term average of the accelerometer angle estimate but not any of its fast changes, while we have no confidence in the long-term value of the gyro estimate.

Recall the estimate generated by the gyro signal. Call this estimate θ_g and consider the discrete-time computation with approximated integral.

$$\theta_g(kT_s) = \theta_g((k-1)T_s) + T_s\omega(kT_s)$$
(3.1)

If the estimate ever goes bad (due to drift for instance), it will never get better. If all movements end, the angle estimate will stay at its last value. What we could do is to bring it back to a somewhat correct value periodically. For instance, we could reset it to the value obtained from the accelerometer estimator every 10 seconds, or similar heuristics. A more clever idea is to continuously use the angle estimate from the accelerometers. Let the accelerometer angle estimate be called $\theta_a(kT_s)$, and introduce a new estimate $\theta_c(kT_s)$ which is a slight variation of the gyro integration

$$\theta_c(kT_s) = (1 - \alpha)\theta_a(kT_s) + \alpha(\theta_c((k - 1)T_s) + T_s\omega(kT_s))$$
(3.2)

The constant α is typically close to 1. When it is 1, we obtain the gyro solution, and when it is 0 we obtain the accelerometer solution. What we are doing is that we are slowly pushing the estimate $\theta_c(kT_s)$ towards $\theta_a(kT_s)$, while still using the high-precision gyro measurements to detect rotations. Effectively, we will eliminate the drift, while retaining the good short time-frame qualities of the gyro. Using multiple sensors with different characteristics like this is called sensor fusion.

Preparation 9 With z^{-1} denoting unit time-delay, show that (3.2) can be written as

$$\mathbf{\theta}_{c}(z) = \frac{(1-\alpha)z}{z-\alpha}\mathbf{\theta}_{a}(z) + \frac{T_{s}\alpha z}{z-\alpha}\mathbf{\omega}(z)$$
 (3.3)

Preparation 10 With $\theta_g(z) = \frac{T_s z}{z-1} \omega(z)$ denoting our original gyro estimate, show that the solution (3.3) alternatively can be written as

$$\mathbf{\theta}_c(z) = \frac{(1-\alpha)z}{z-\alpha}\mathbf{\theta}_a(z) + \frac{\alpha(z-1)}{z-\alpha}\mathbf{\theta}_g(z)$$
 (3.4)

Hence, the new solution θ_c we propose is a sum of our two old solutions θ_a and θ_g , each of them filtered. Let us look at the frequency response of those filters (here with $\alpha = 0.9$ and $T_s = 0.025s$)

```
z = tf('z',0.025);
Ha = (1-0.9)*z/(z-.9);
Hg = 0.9*(z-1)/((z-.9));
bodemag(Ha,Hg);legend('Ha','Hg');
```

The result is seen in Figure 3.6. We see that the filter $H_a(z)$ used on the accelerometer angle estimate is a low-pass filter (removes fast variations and only keeps slow variations) and the filter $H_g(z)$ for the gyro angle estimate is a high-pass filter (removes the slow drift and only keeps fast variations). The name complementary filter comes from the fact that the two filters sum to 1 (check in (3.4)!).

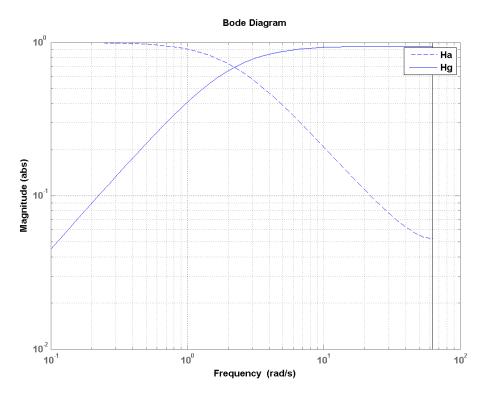


Figure 3.6: Amplitude gain for the two filters used in the complementary filter approach. The accelerometer solution is low-pass filtered, while the gyro solution is high-pass filtered

Preparation 11 In the block diagram in Figure 3.7, values and connections are missing. Insert the values α , $1 - \alpha$ and T_s in suitable blocks, and draw the connection, to implement the computation in (3.2). As a hint, standard Euler backwards as in (3.1) is implemented in Figure 3.8.

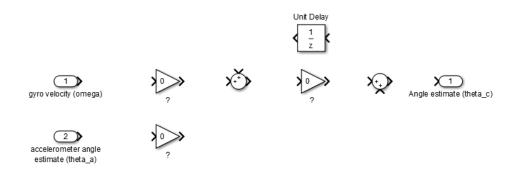


Figure 3.7: Insert missing values and connection to implement the complementary filter (3.3)

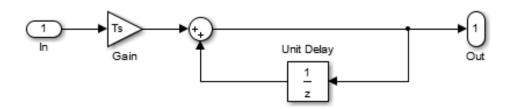


Figure 3.8: Example showing how discrete-time integral approximation (Euler backwards) would be implemented manually, $Out(kT_s) = Out((k-1)T_s) + T_sIn(k)$

Task 9 Open *template3* and set the two gains on the accelerometer signals as specified in the text next to them. This operation is done to account for the fact that we currently have two different types on IMUs, and is not related to any theory described here.

Task 10 Double-click the **Complementary filter** block, and complete it according to the preparation exercise. Use $\alpha = 0.9$ and Ts = 0.04. Update the bias compensation in the gyro angle estimator. Start the code and study the three angle estimate solutions. How do they compare? Try other values on α such as 0.5 and 0.99. Try the robustness of the angle estimate by using a completely wrong value on the bias compensation (add an extra 50 or so) which will cause the gyro angle estimate to drift away.

The angle estimate from the accelerometer signals are based on the raw accelerometer signals. An acceleration of 1 g leads to a measurement of 8192 while no acceleration should lead to the measurement 0. In our computation of the angle based on these signals, we have not scaled the data to m/s^2 , as the scaling cancels out when we perform the division before taking arctan. However, we should compensate for calibration error / bias in the accelerometer signals.

Task 11 In Accelerometer angle estimator, add bias compensation to the two measurement signals $a_y(t)$ and $a_z(t)$ to improve the accelerometer angle estimator. When lying flat on the table, $a_y(t)$ should be 0, and $a_z(t)$ should be 8192 (the accelerometer is built such that it outputs an integer between -2^{15} to 2^{15} when going from -4 g to 4 g, thus 1 g will be $2^{13} = 8192$). You thus have to rebuild the model in the Accelerometer angle estimator block to incorporate bias compensation on both a_y and a_z as in the Gyro angle estimator block. Tuning the bias compensation is done exactly as when you tuned the gyro bias compensation, there are plot scopes available for both signals. Can you improve the precision of the accelerometer angle estimator, and thus the complementary filter estimate?

3.2 Summary and reflections

Summarize and reflect on what you have seen and learned in this lab.

Questions	Answers
1. A gyro measures	☐ An angle
	☐ An angular velocity
	☐ An angular acceleration
2. A low-pass filter	□ removes high-frequency content
	□ removes low-frequency content
3. A high-pass filter	□ removes high-frequency content
	□ removes low-frequency content
4. Accelerometers are	□ when moving very slowly
suitable for computing the angle	□ when moving around a lot
5. Gyros are good for	☐ finding changes in angle
	☐ finding the absolute angle
35 . 1	

Most unclear to me is still: