

# EE324 Control Systems Lab

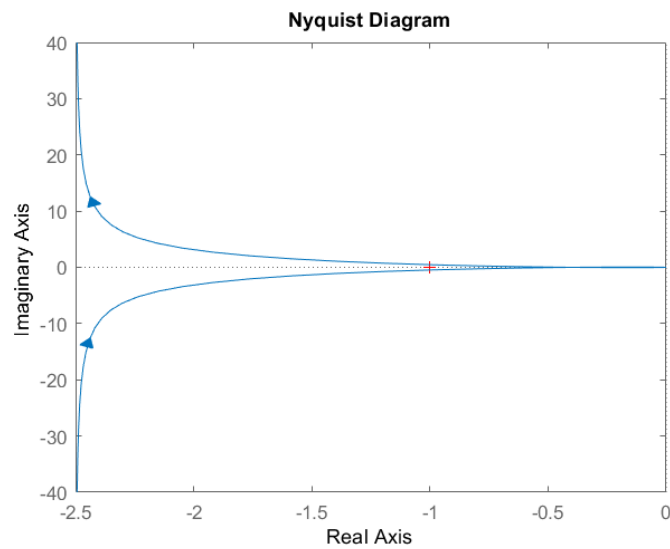
## Problem Sheet 9

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### 1. Problem 1

Given the open-loop system transfer function  $G(s)$ :

$$G(s) = \frac{10}{s\left(\frac{s}{5} + 1\right)\left(\frac{s}{20} + 1\right)}$$

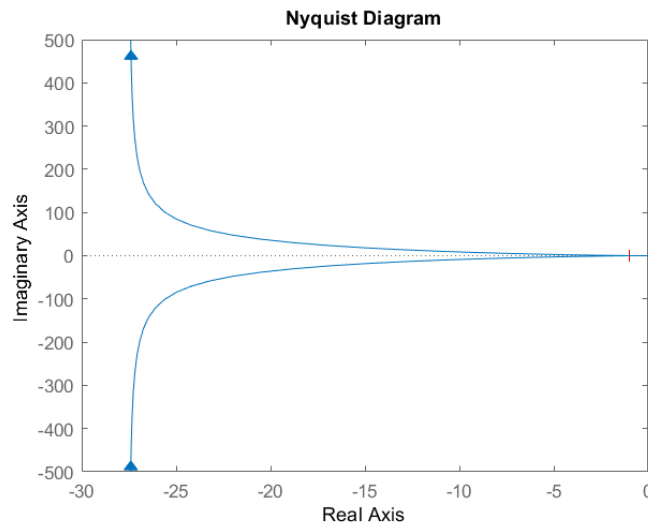


**Figure 1:** Nyquist Plot for  $G(s)$

We obtain gain margin as 7.9588 dB and phase margin as 22.5359°.

#### 1.1. Part (a)

$$C(s) = \frac{s+3}{s+1}$$
$$C(s)G(s) = \frac{10}{s\left(\frac{s}{5} + 1\right)\left(\frac{s}{20} + 1\right)} \left(\frac{s+3}{s+1}\right)$$

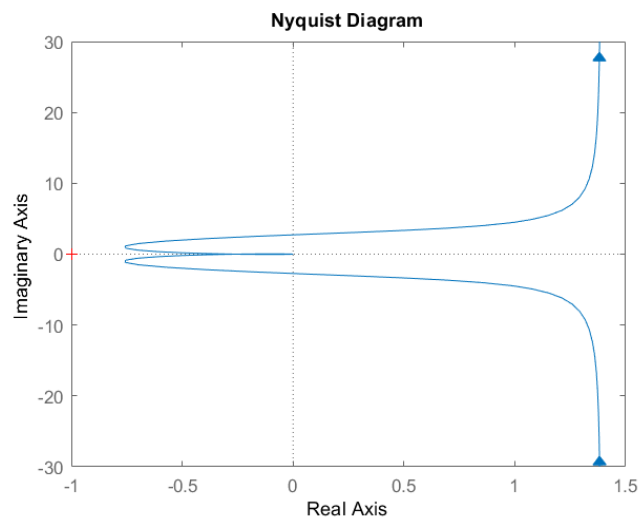


**Figure 2:**  $GM = 2.0762 \text{ dB}$   $PM = 4.0248^\circ$

We obtain gain margin as  $2.0762 \text{ dB}$  and phase margin as  $4.0248^\circ$ .

## 1.2. Part (b)

$$G(s) = \frac{10}{s\left(\frac{s}{5} + 1\right)\left(\frac{s}{20} + 1\right)} \frac{s + 1}{s + 3}$$



**Figure 3:**  $GM = 11.7598 \text{ dB}$   $PM = 43.1732^\circ$

We obtain gain margin as  $11.7598 \text{ dB}$  and phase margin as  $43.1732^\circ$ .

The Lag compensator reduces both the phase and gain margins of  $C(s)G(s)$  as compared to  $G(s)$ , while the lead compensator increases both of them.

## MATLAB Code

```

clear;
close all;
clc;

syms s;
s=tf('s');
G = 10/(s*(s/5 + 1)*(s/20 + 1));

clag = (s+3)/(s+1);
clead = (s+1)/(s+3);

figure;nyquist(G);
[Gm,Pm,~,~] = margin(G);
fprintf("GM = %2.3fdeg \n", 20*log10(Gm));
fprintf("PM = %2.3fdeg \n", Pm);

figure;nyquist(G*clag);
[Gm,Pm,~,~] = margin(G*clag);
fprintf("GM for Lag compensated system = %2.3fdB \n", 20*log10(Gm));
fprintf("PM for Lag compensated system = %2.3fdeg \n", Pm);
figure;nyquist(G*clead);
[Gm,Pm,~,~] = margin(G*clead);
fprintf("GM for Lead compensated system = %2.3fdB \n", 20*log10(Gm));
fprintf("PM for Lead compensated system = %2.3fdeg \n", Pm);

```

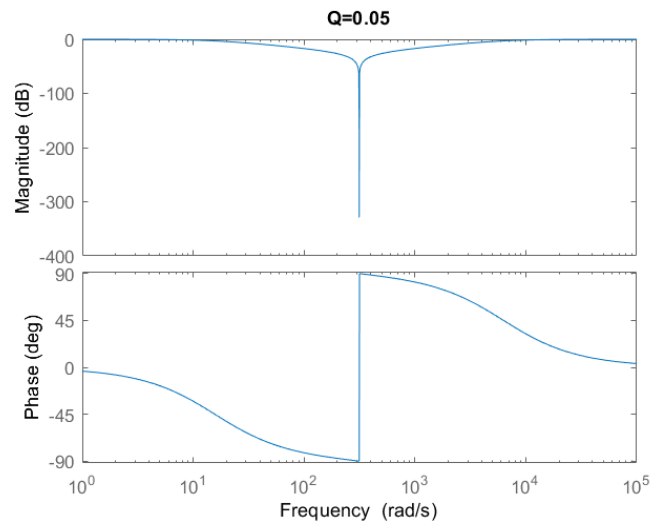
## 2. Problem 2

The transfer function of a standard notch filter is:

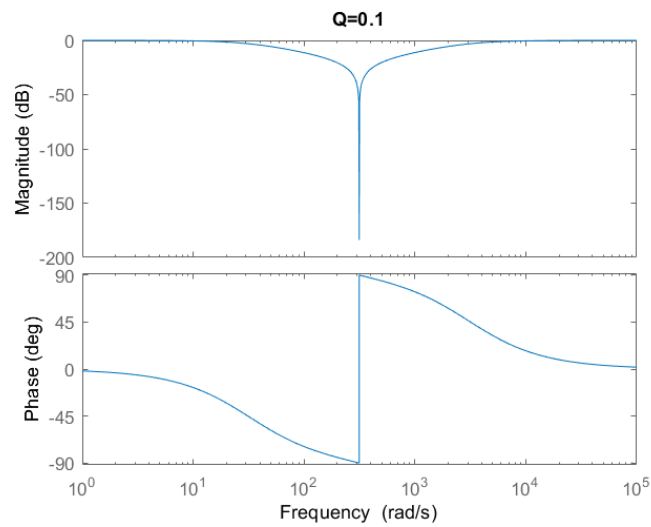
$$H(s) = \frac{s^2 + \omega_z^2}{s^2 + \frac{\omega_z s}{Q} + \omega_z^2}$$
$$H(j\omega) = \frac{\omega_z^2 - \omega^2}{\omega_z^2 - \omega^2 + j\frac{\omega_z \omega}{Q}}$$

We see that we have gain of 1 for very large and very small  $\omega$  and gain around  $\frac{2Q\Delta\omega}{\omega_z}$  for small deviation  $\Delta\omega$  around  $\omega_z$ .

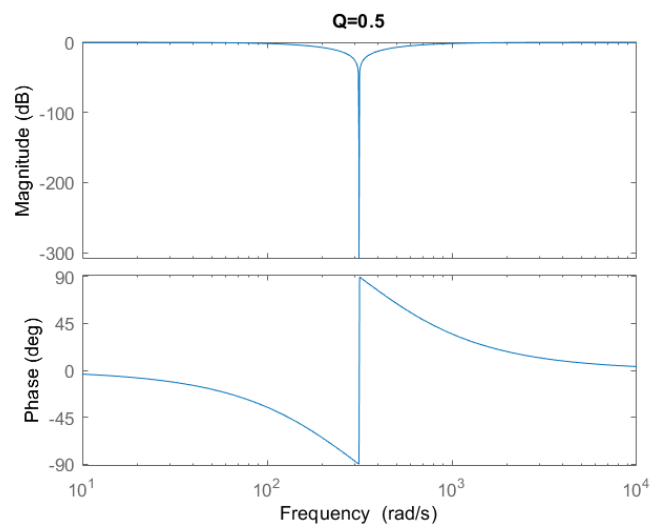
Choosing the following parameter  $\omega_z = 100\pi$  (for 50Hz specification), and varying  $Q$  with values of 0.05, 0.1 and 0.5 we get the following plots:



**Figure 4:**  $Q = 0.05$



**Figure 5:**  $Q = 0.1$



**Figure 6:**  $Q = 0.5$

We see that upon varying  $Q$  we are able to modify the steepness of the magnitude plot for the notch filter and have proven the same by above plots. As  $Q$  increases, the steepness increases.

### MATLAB Code

```
clear;
close all;
clc;

syms s;
s=tf('s');
```

```
omega_z = 2*pi*50;
q = 0.05;
G1 = (s^2 + omega_z^2)/(s^2 + omega_z*s/q + omega_z^2);
figure;bode(G1);title('Q=0.05');

q=0.1;
G2 = (s^2 + omega_z^2)/(s^2 + omega_z*s/q + omega_z^2);

figure;bode(G2);title('Q=0.1');

q=0.5;
G3 = (s^2 + omega_z^2)/(s^2 + omega_z*s/q + omega_z^2);

figure;bode(G3);title('Q=0.5');
```

### 3. Problem 3

Given the system transfer function  $C(s)$ :

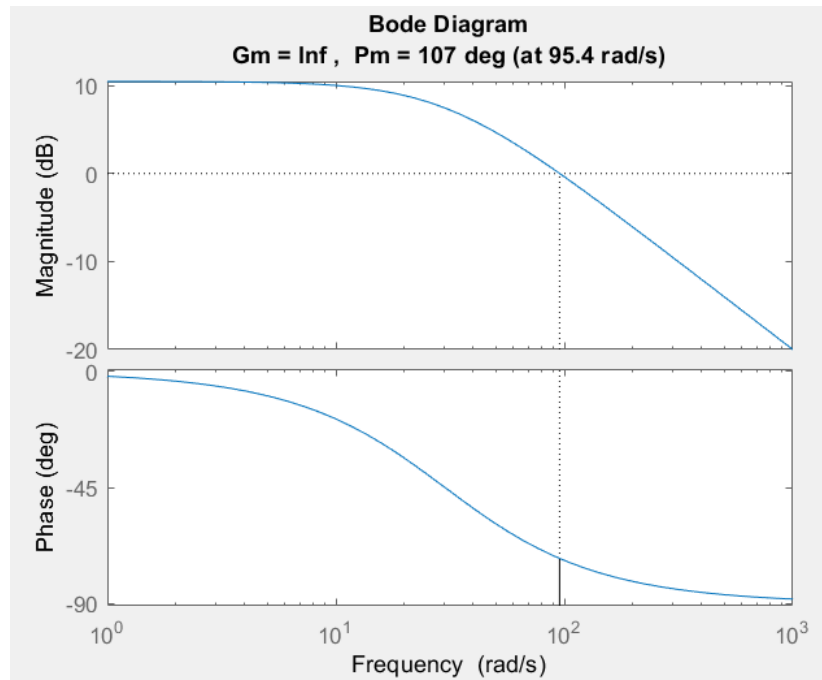
$$C(s) = \frac{100}{s + 30}, \quad G(s) = e^{-sT}$$

$$C(j\omega)G(j\omega) = \frac{100 e^{-j\omega T}}{j\omega + 30}$$

$$\angle C(j\omega)G(j\omega) = \angle C(j\omega) - \omega T$$

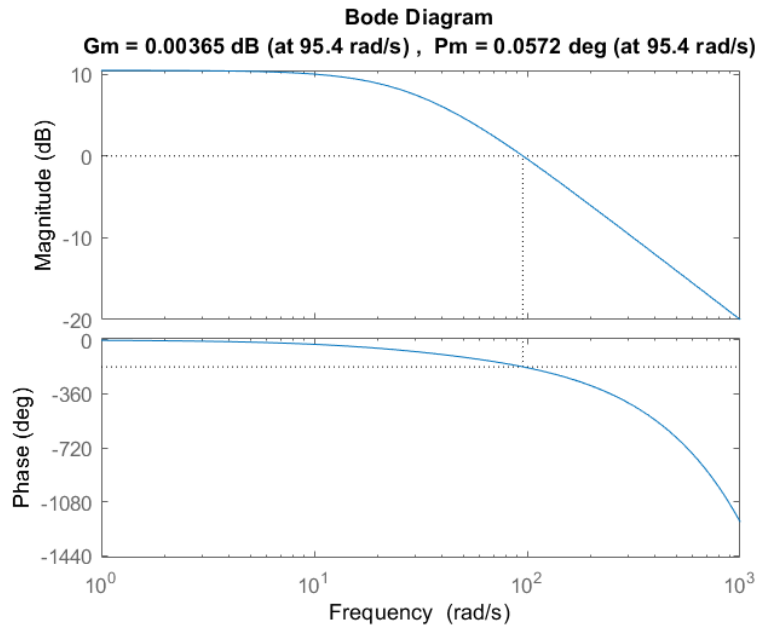
As  $|e^{-sT}| = 1$ , the magnitude plot remains unaffected, and the the phase plot is linearly shifted. For verge of instability (or marginal stability), we require  $\angle \omega_{gcf} = (2k + 1)\pi$ , upon equating we get

$$\begin{aligned} \angle C(j\omega_{gcf}) - \omega_{gcf}T &= (2k + 1)\pi \\ T &= \frac{\angle C(j\omega_{gcf}) - (2k + 1)\pi}{\omega_{gcf}} \end{aligned}$$



**Figure 7: Bode Plot for  $C(s)$**

$$\begin{aligned} \omega_{gcf} &= 95.4 \\ \angle C(j\omega_{gcf}) &= -1.2669 \\ T &= \frac{-1.2669 + \pi}{95.4} \\ &= 0.01965 \\ \therefore G(s) &= e^{-0.01965s} \end{aligned}$$



**Figure 8:** Bode plot for required destabilized system

Without the delay unit, we had infinite gain margin and phase margin of  $\pi - 1.2669 \text{ rads} = 107$  degrees. But with this delay unit we have  $\omega_{pcf} = \omega_{gcf}$  hence 0 gain and phase margin.

#### MATLAB Code

```
clear;
close all;
clc;

syms s;
s=tf('s');
C = 100/(s+30);
%figure;margin(C);
%[Gm,Pm,Wcg,Wcp] = margin(C);

G = exp(-0.01965*s);
figure;margin(G*C);
```

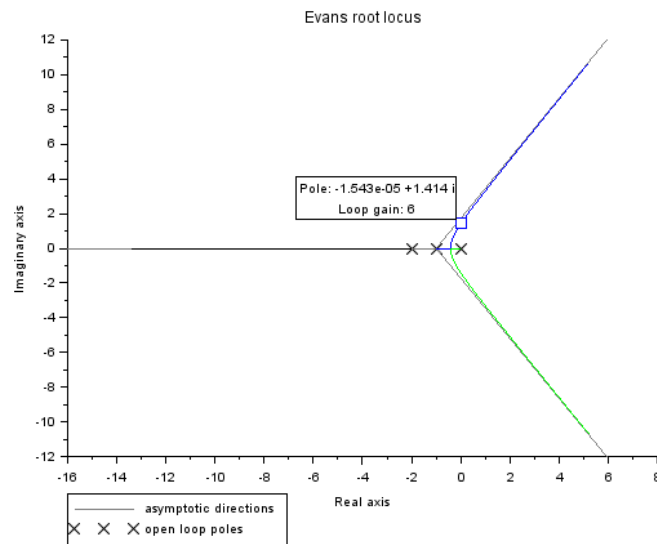


#### 4. Problem 4

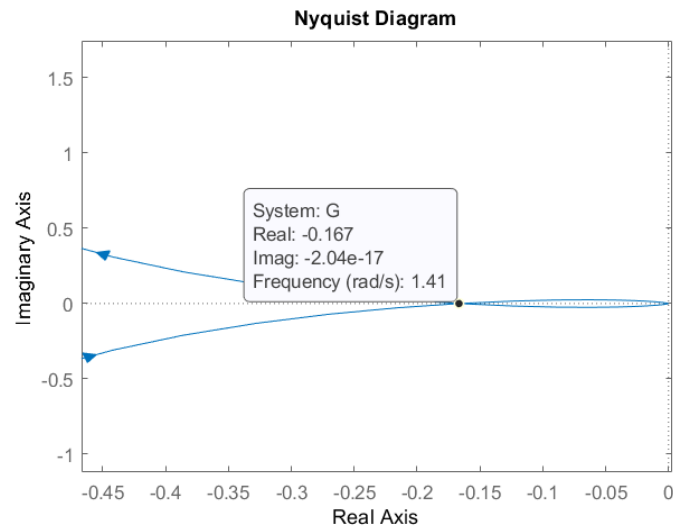
Given the open-loop system transfer function:

$$G(s) = \frac{1}{(s^3 + 3s^2 + 2s)}$$

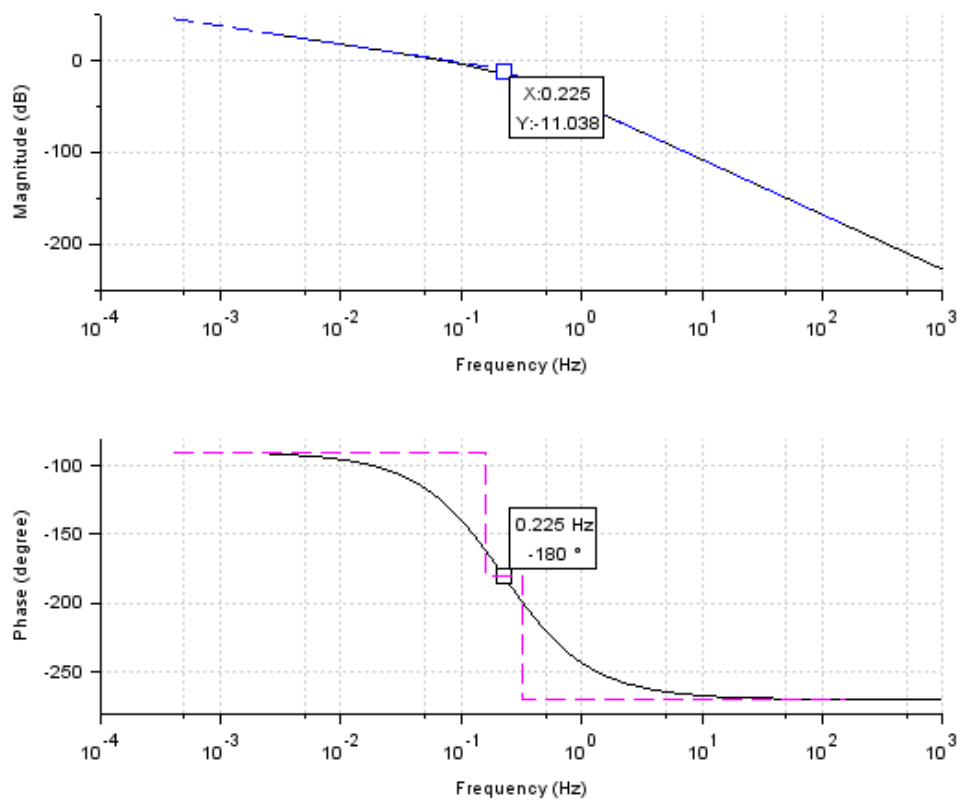
The gain margin is mentioned in linear units when not specified as dB.



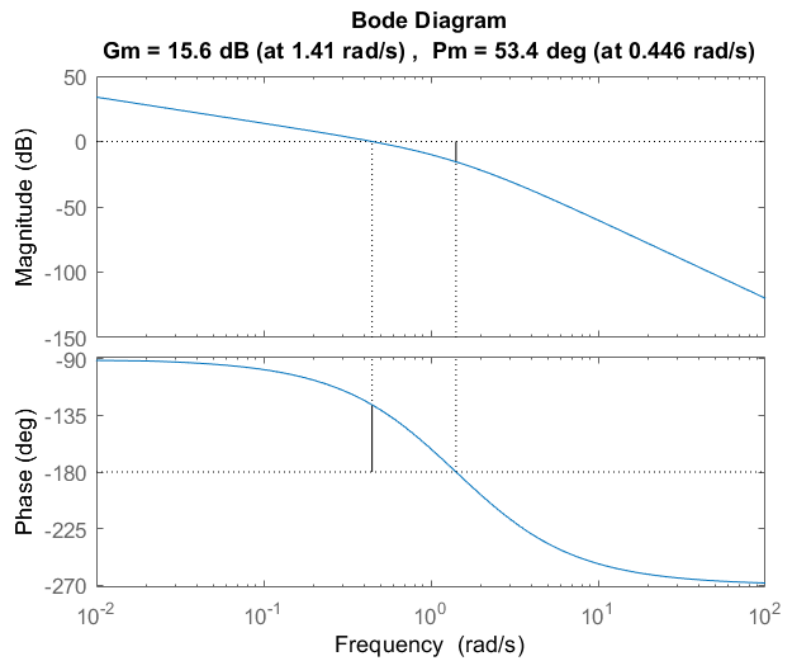
**Figure 9:** Root Locus of  $G(s)$ : critical point marked



**Figure 10:** Nyquist Plot of  $G(s)$ : -p+j0 point marked



**Figure 11: Asymptotic Bode Plot**



**Figure 12: Bode Plot**

| Method Used          | Calculation                                    | K (gain margin magnitude)(in lin units) |
|----------------------|--|---|
| Root locus           | $GM = K_{crit} = 6$                            | 6.000                                   |
| Nyquist plot         | $GM = \frac{1}{ p } = \frac{1}{0.167} = 5.988$ | 5.988                                   |
| Asymptotic Bode plot | $GM = 10^{11.038/20} = 3.564$                  | 3.564                                   |
| Bode plot            | $GM = 10^{15.6/20} = 6.025$                    | 6.025                                   |

### MATLAB Code

```
clear;
close all;
clc;

syms s;
s=tf('s');
G=1/(s^3+3*s^2+2*s);

figure(1);nyquist(G);
figure(2);margin(G);
```

### Scilab Code for assymptotic bode plot and Root locus calculations

```
clear;
clc;

s=poly(0,'s');
G = 1/(s^3+3*s^2+2*s);
sysG = syslin('c',G);

gcf();
evans(sysG);

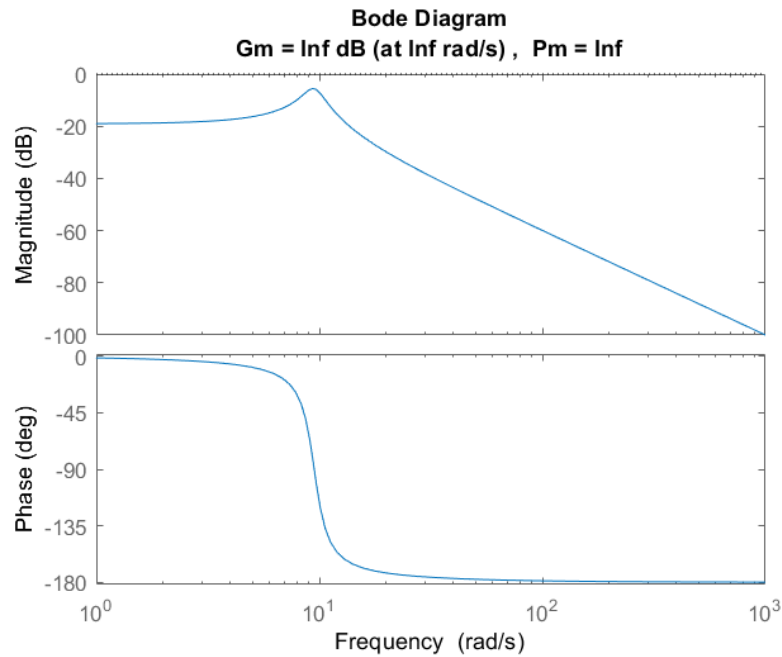
gcf();
bode(sysG);
bode_asymp(sysG);
```

## 5. Problem 5

Given transfer function:

$$G(s) = \frac{10s + 2000}{s^3 + 202s^2 + 490s + 18001}$$

i) We get the following Bode plots



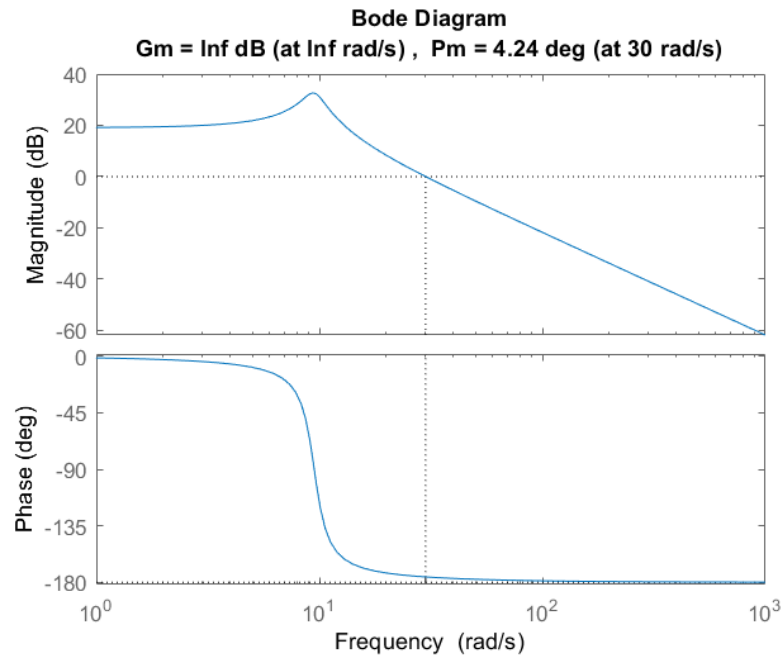
**Figure 13:** Bode Plot of  $G(s)$

Here, we observe that gain margin and phase margin are both infinite in this case.

ii) As it is a 0-order system, we increase proportional gain ' $K$ ' to decrease steady state error to 0.1 for a step response as follows:

$$\begin{aligned} SSE &= \frac{1}{1 + KG(0)} = 0.1 \\ \implies KG(0) &= 9 \\ \implies K &= 9 / G(0) = 81.0045 \end{aligned}$$

iii) The bode plot for the modified open loop system is shown below:

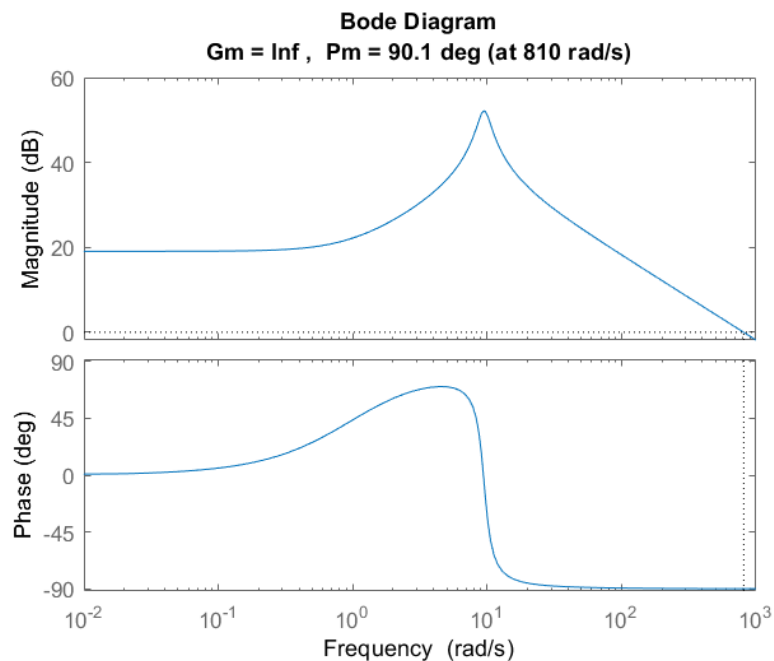


**Figure 14:** Bode plot for  $K \cdot G(s)$

Here we see that system has a phase margin of  $4.24^\circ$ , and gain margin still stays infinite.

iv) Now to improve the phase margin of the system, we add a zero such that the phase stops decreasing around the gain crossover frequency. We add the zero at  $s = -1$ .

$$G_{iv}(s) = \frac{K(10s + 2000)(s + 1)}{s^3 + 202s^2 + 490s + 18001}$$



**Figure 15:** Bode Plot for  $K \cdot G(s) \cdot (s+1)$

v) The closed loop system for  $G_{iv}(s)$  is stable since we have positive gain and phase margins.

#### MATLAB Code

```
clear;
close all;
clc;

syms s;
s=tf('s');

G = (10*s+2000)/(s^3+202*s^2+490*s+18001);
figure;margin(G);

k=81.0045;
figure;margin(k*G);
figure;margin(k*G*(s+1));
```