TESTING OF TOOL

8.1 SOLVING SIMPLY SUPPORTED BEAM

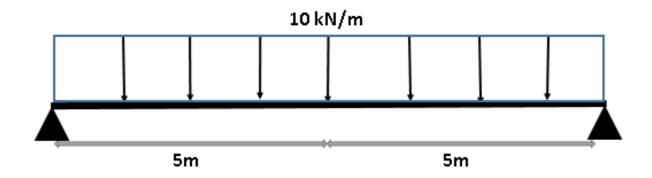


Fig 8.1 Simply supported beam

Length of the beam = 10m, and a square cross section of 0.25m*0.5m. Young's modulus is 200GPa.

```
I = 2.6 x 10<sup>-3</sup> m<sup>4</sup> and A= 0.125 m<sup>2</sup>

%% Data Input Section

E_M=[2*10^8;2*10^8];

I_M=[2.6*10^(-3); 2.6*10^(-3)];

A_M=[0.125;0.125];

node=[0 0;5 0;10 0];

conn=[1 2;2 3];

fdof=[3 5 6 9];

f(2)=-25;f(5)=-50;f(8)=-25; % Y-forces

f(3)=-20.83;f(6)=-20.83+20.83;f(9)=20.83; % Z-moments
```

Above input snippet is based on the 3 DOF per node analogy. The output of the program is given in Fig 8.2. The Distorted geometry, BMD and the SFD are given is subsequent figures. Since, this question involves UDL, hence the shape of SFD and BMD is not correct, but the nodal values of SFD and BMD are exact.

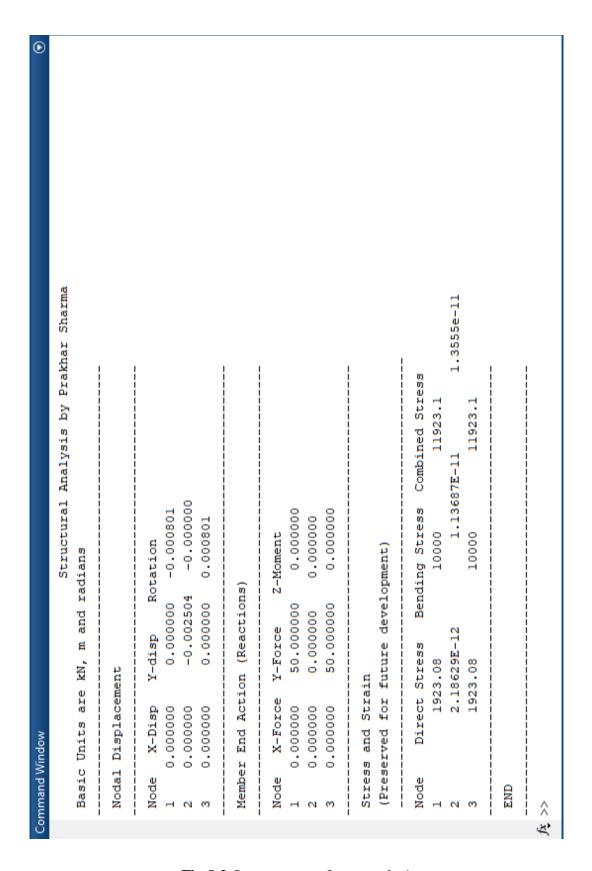


Fig 8.2 Output screen for example-1

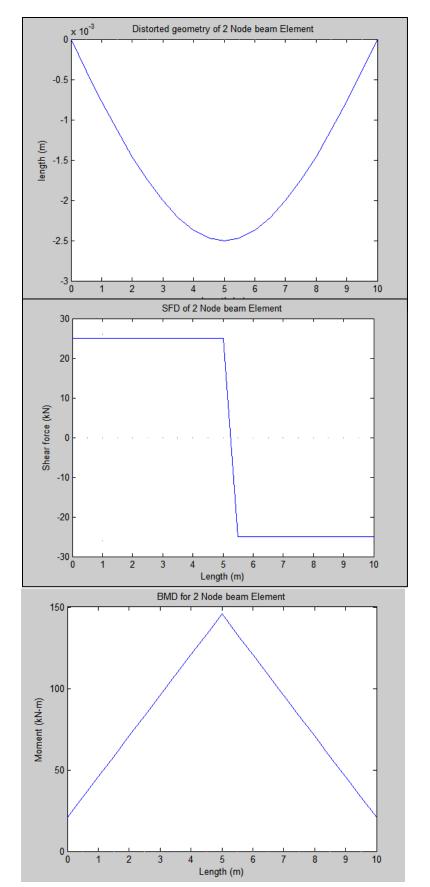


Fig 8.3 Distorted geometry of example-1

Fig 8.4 SFD of example-1

Fig 8.5 BMD of example-1

8.2 SOLVING FIXED BEAM

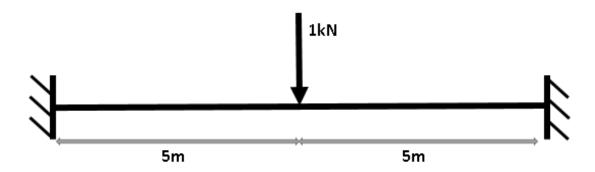


Fig 8.6 Fixed Beam

```
E= 2 \times 10^{8} \, \text{kN/m}^{2}
I= 4 \times 10^{-6} \, \text{m}^{4}
%% Data Input Section
E\_M=[2*10^{8};2*10^{8}];
I\_M=[4*10^{(-6)}; \ 4*10^{(-6)}];
A\_M=[0;0]; \ \ \% \ \text{Not applicable for beams}
node=[0 \ 0;5 \ 0;10 \ 0];
conn=[1 \ 2;2 \ 3];
fdof=[4 \ 5 \ 6];
f(5)=-1;
```

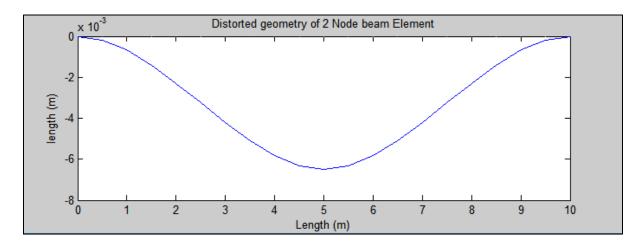


Fig 8.7 Distorted geometry of example-2

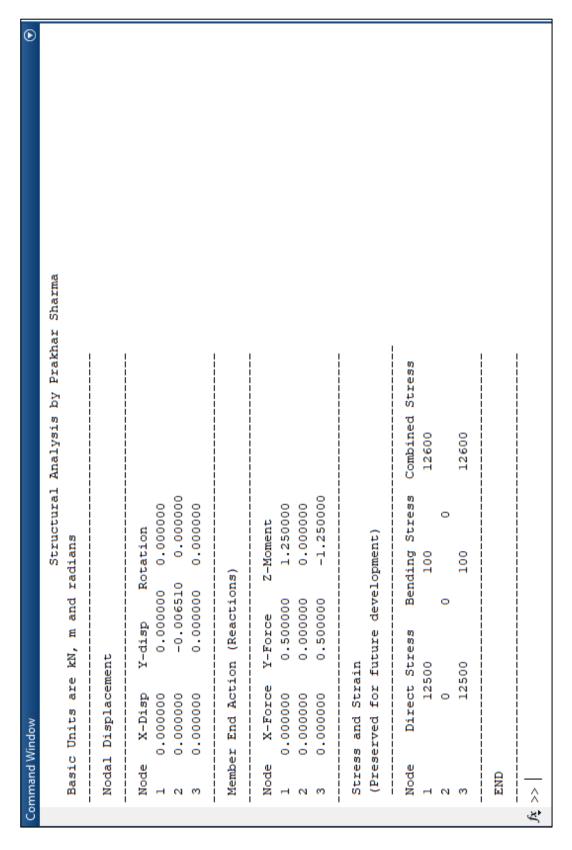


Fig 8.8 Output screen for example-2

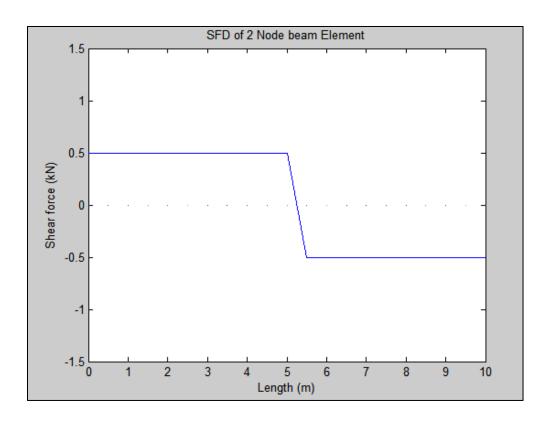


Fig 8.9 SFD for example-2

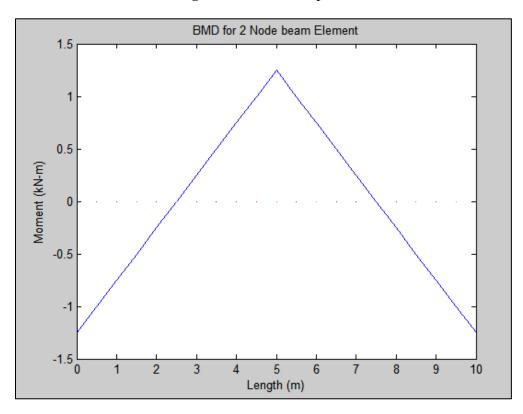


Fig 8.10 BMD for example-2

8.3 SOLVING CANTILEVER BEAM

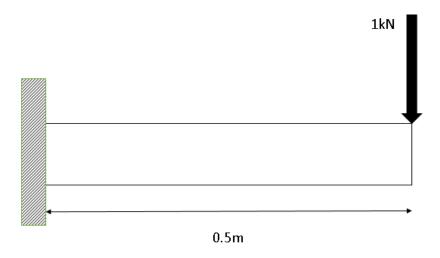


Fig 8.11 Cantilever Beam

```
E= 2 x 10<sup>8</sup> kN/m<sup>2</sup>

I= 4 x 10<sup>-6</sup> m<sup>4</sup>

%% Data Input Section

E_M=[2*10^8];

I_M=[4*10^(-6)];

A_M=[0;0]; % Not applicable for beams node=[0 0;0.5 0];

conn=[1 2];

fdof=[4 5 6];

f(5)=-1;
```

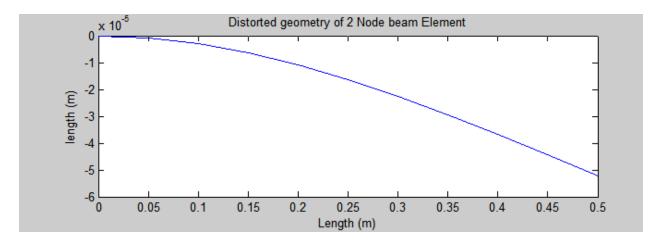


Fig 8.12 Distorted geometry of example-3

ပိ	Command Window	
	Structural Analysis b Basic Units are kN, m and radians	Structural Analysis by Prakhar Sharma ians
	Nodal Displacement	
	Node X-Disp Y-disp Rotation 1 0.000000 0.000000 0.000000 2 0.000000 -0.000052 -0.000156	
	Member End Action (Reactions)	
	Node X-Force Y-Force Z-Moment 1 0.000000 1.000000 0.500000 2 0.000000 0.000000 0.000000	
	Stress and Strain (Preserved for future development)	
	Node Direct Stress Bending Stress Combined S 1 25000 200 25200 2 2.22045E-11 1.77636E-13	Combined Stress 25200 6E-13 2.23821e-11
	END	
X,	<< \$j	

Fig 8.13 Output for example-3

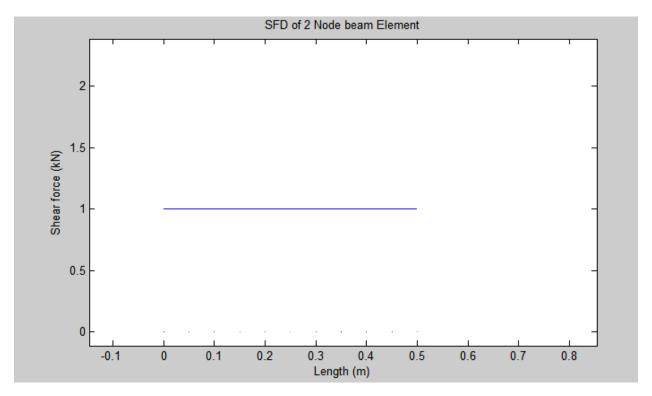


Fig 8.14 SFD for example-3

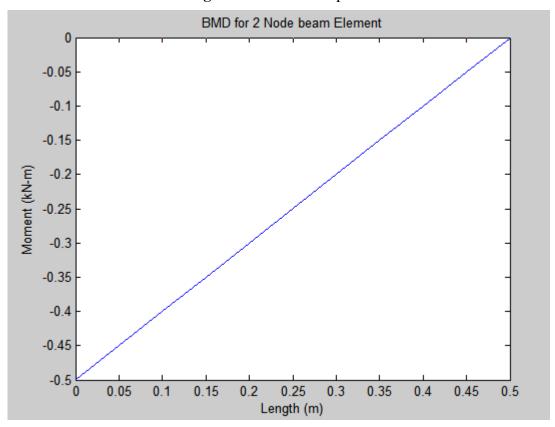


Fig 8.15 BMD for example-3

8.4 SOLVING 2D PORTAL FRAME

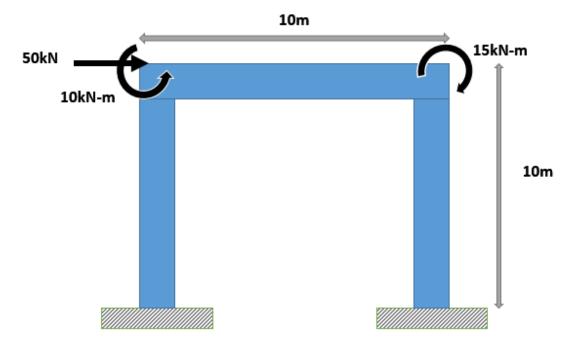


Fig 8.16 2D Frame

```
E= 2 \times 10^8 \, \text{kN/m}^2, \, 4 \times 10^8 \, \text{kN/m}^2, \, 3 \times 10^8 \, \text{kN/m}^2
I= 4 \times 10^{-6} \, \text{m}^4, \, 3.56 \times 10^{-6} \, \text{m}^4, \, 4.14 \times 10^{-6} \, \text{m}^4
A=0.01 \, \text{m}^2, \, 0.02 \, \text{m}^2, \, 0.0129 \, \text{m}^2
%% Data Input Section
E\_M=[2*10^{\circ}8, 4*10^{\circ}8, 3*10^{\circ}8];
I\_M=[4*10^{\circ}(-6), 3.56*10^{\circ}(-6), 4.14*10^{\circ}(-6)];
A\_M=[0.01; 0.02, 0.0129];
node=[0 \, 0; 0 \, 10, 10 \, 10, 10 \, 0];
conn=[1 \, 2, 2 \, 3, 3 \, 4];
fdof=[4 \, 5 \, 6 \, 7 \, 8 \, 9];
f(4)=50;
f(6)=10;
f(9)=-15;
```

Since, I have used trial function of insufficient order and hence the visual output will never be correct. Nevertheless, our textual output will be always true.

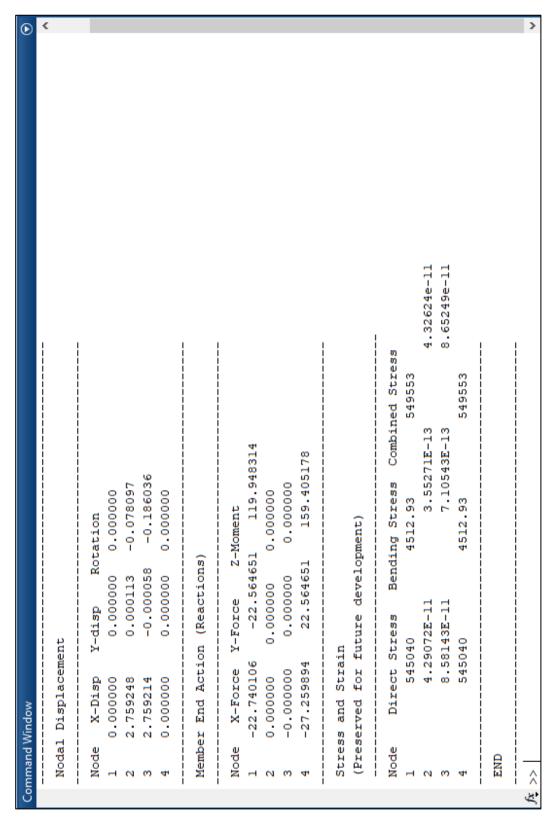


Fig 8.17 Output for example-4