

## MAE 579 Wind Energy Fall 2021

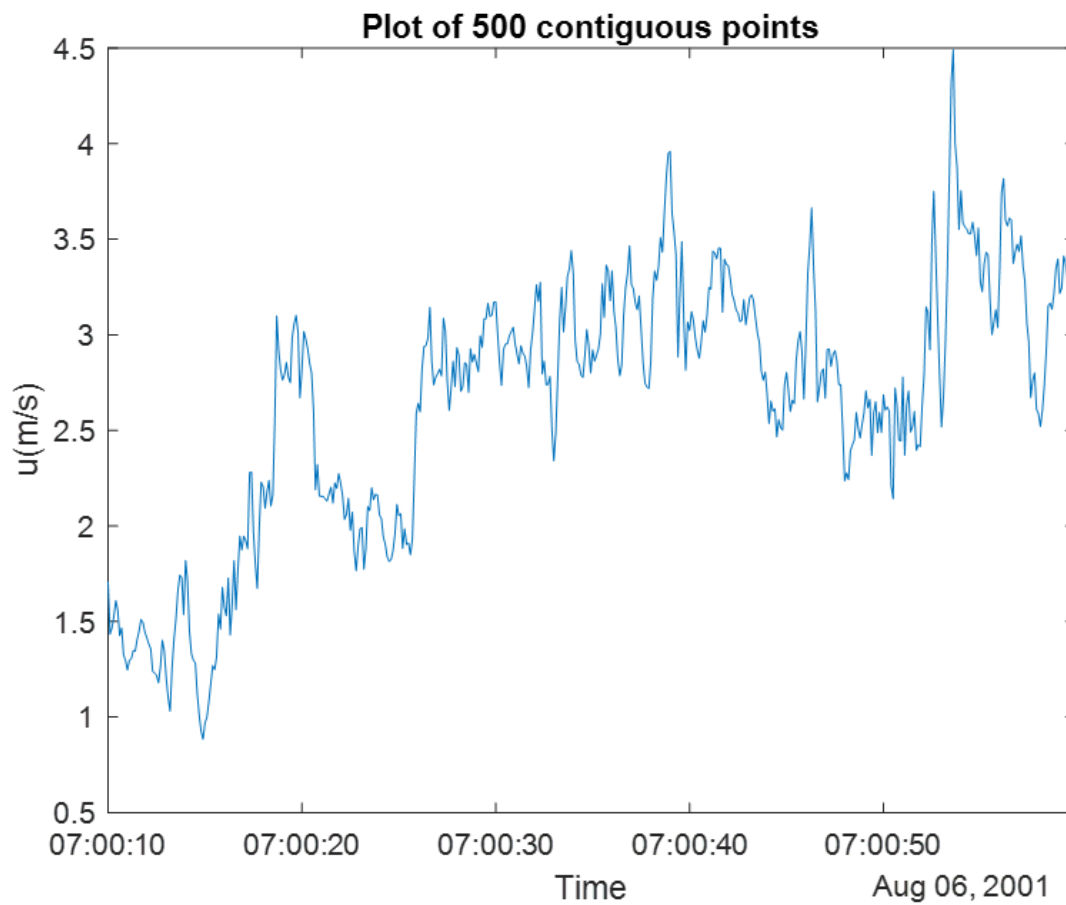
### HW4

Wind Analysts: Rajesh Ramesh, Pranav Pawar

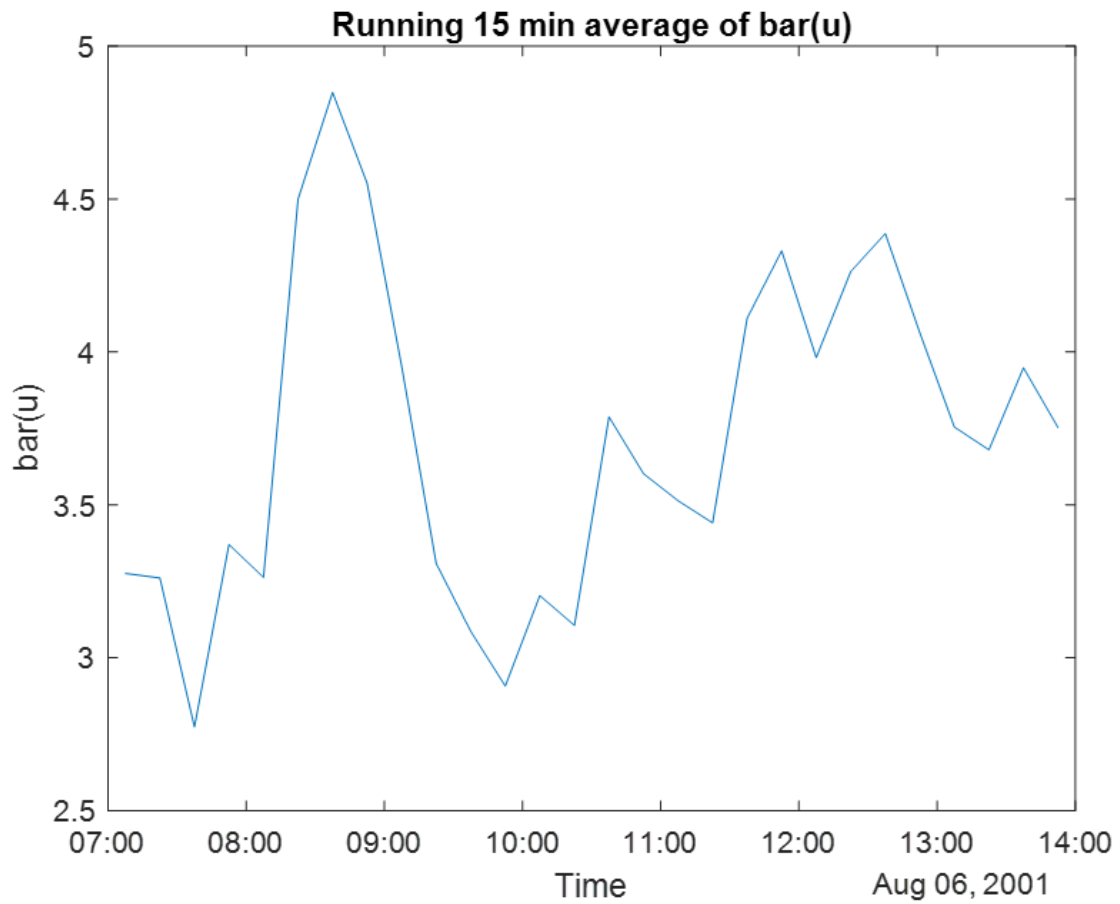
Arizona State University

2.a) Time is in units of day (Last time – first time = 0.291=7/24). Index of time array increments by 0.1s (since 7 hrs = 25200s and there are 252000 elements)

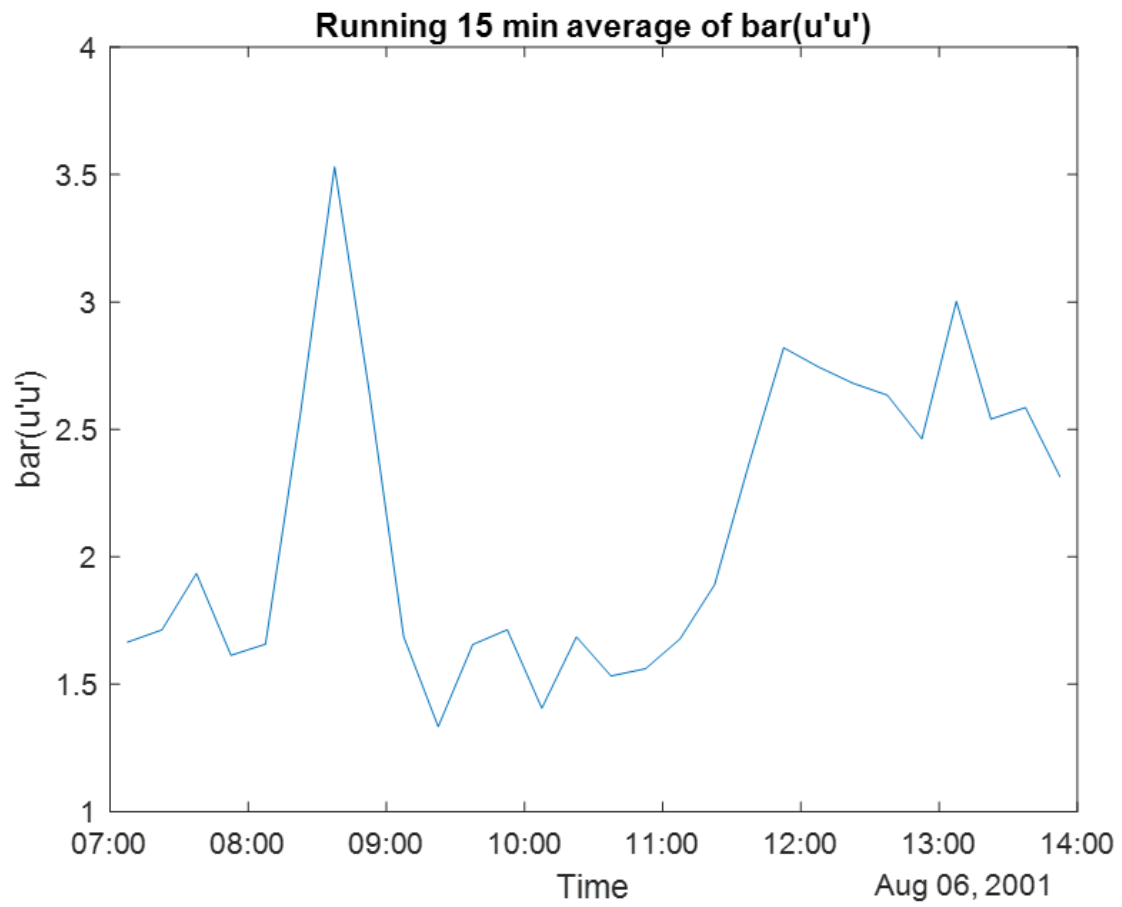
2.b)



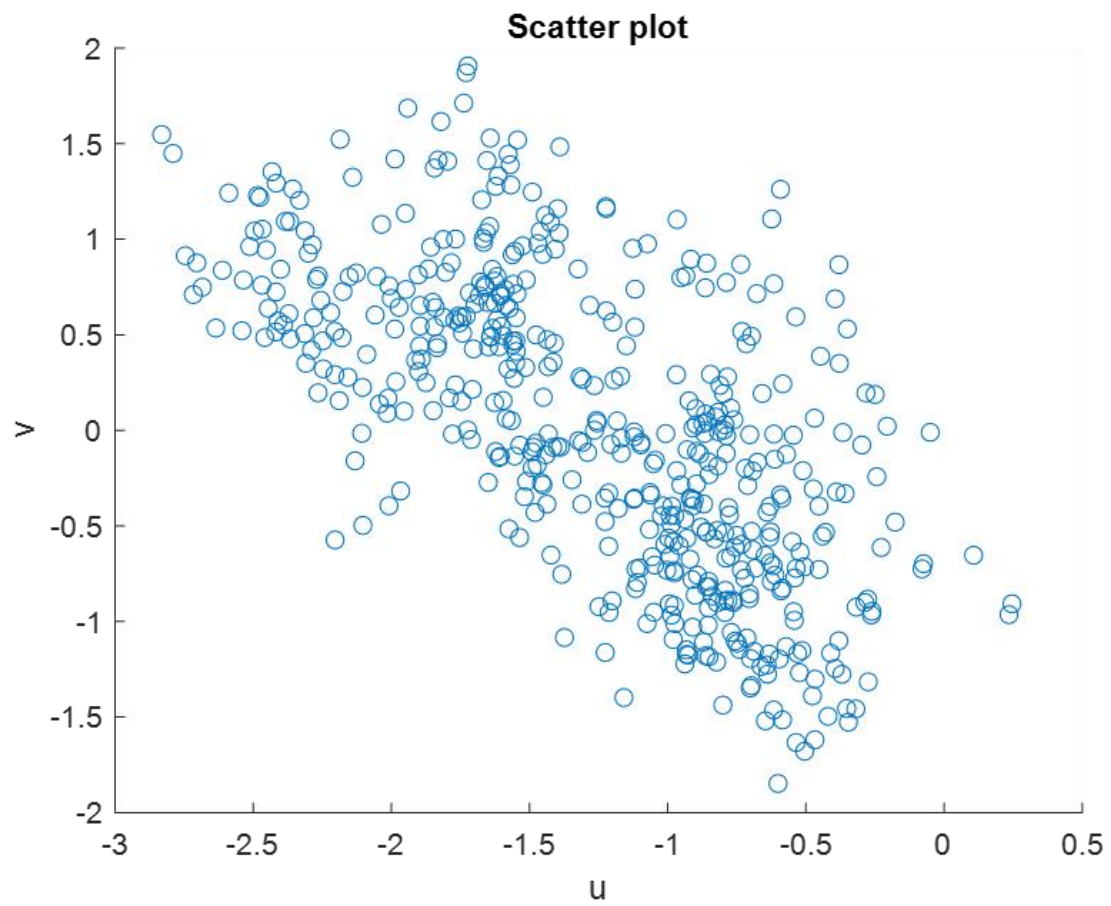
2.c) The average wind speed over 15 min varies with time. Therefore, this is a case of a non-stationary process.



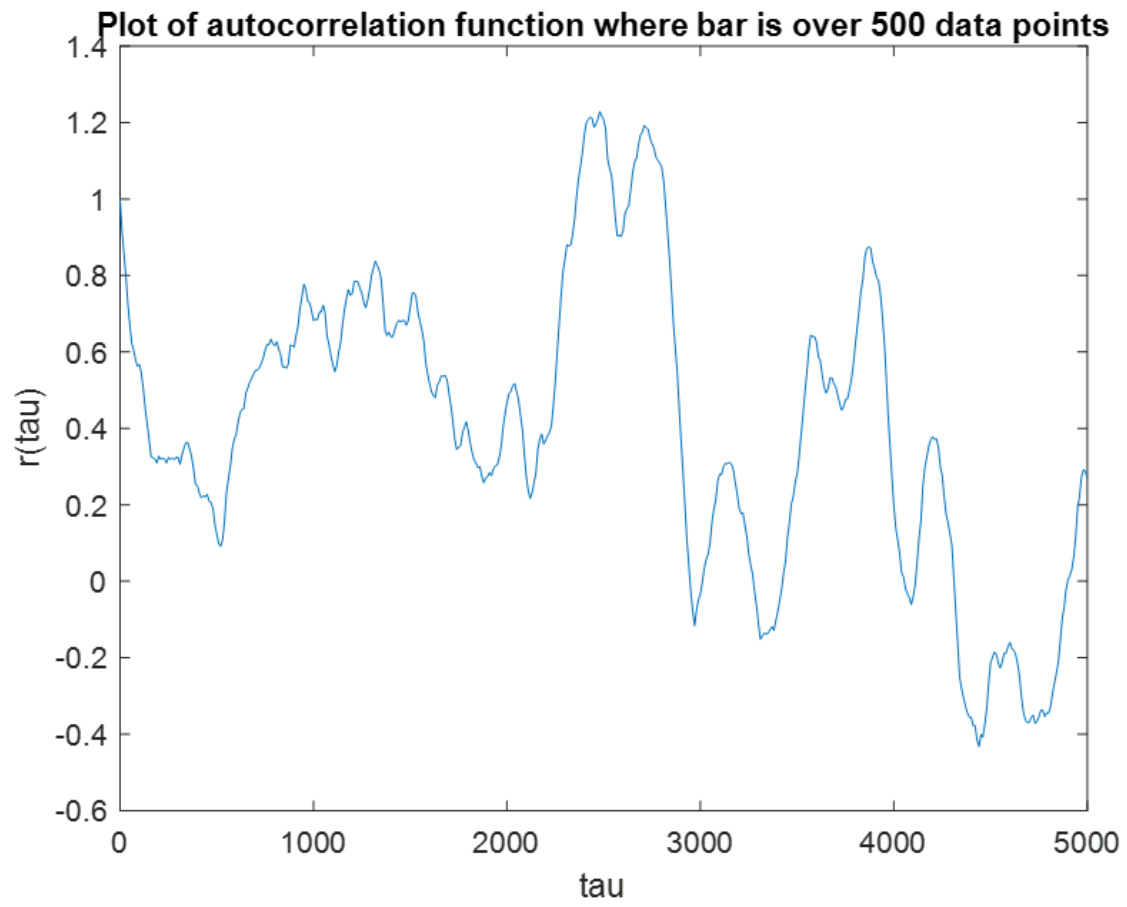
2.d)  $\overline{u'u'} = 2.1290$  where bar is over all time

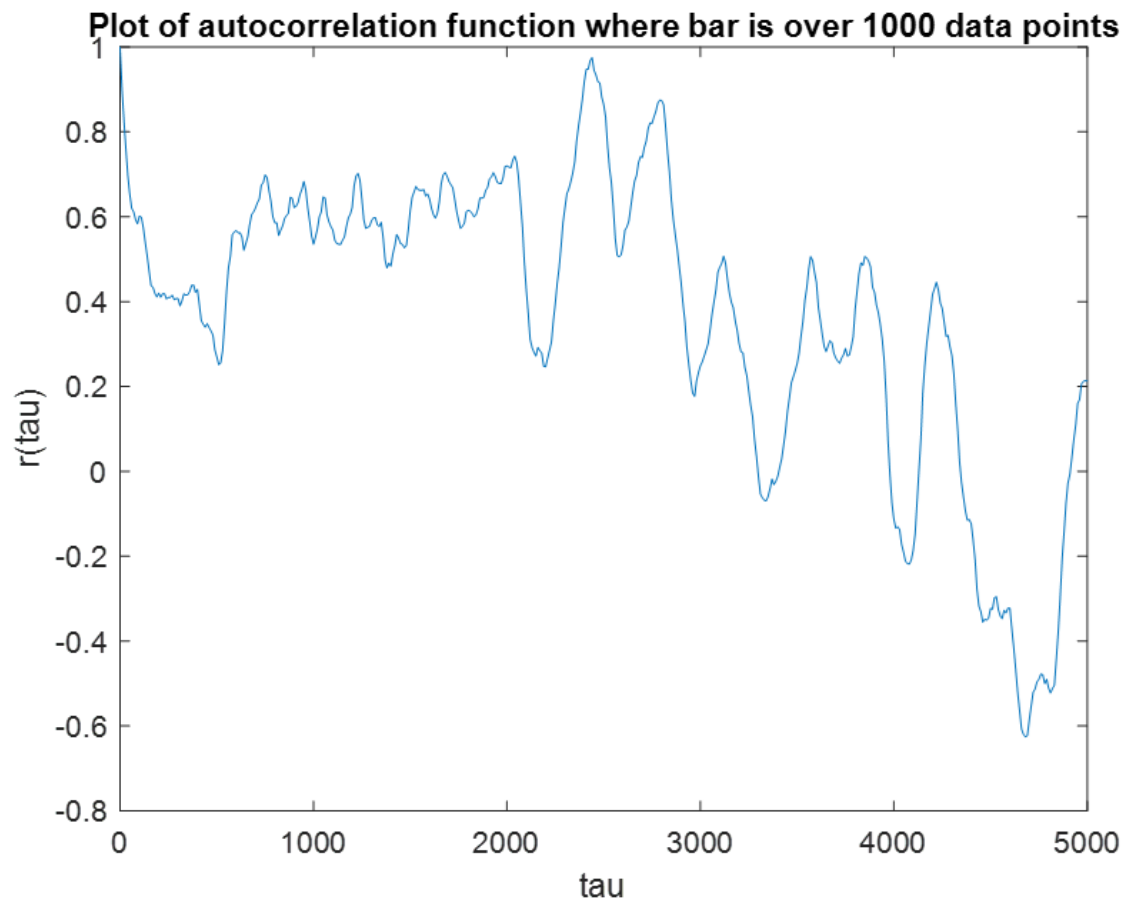


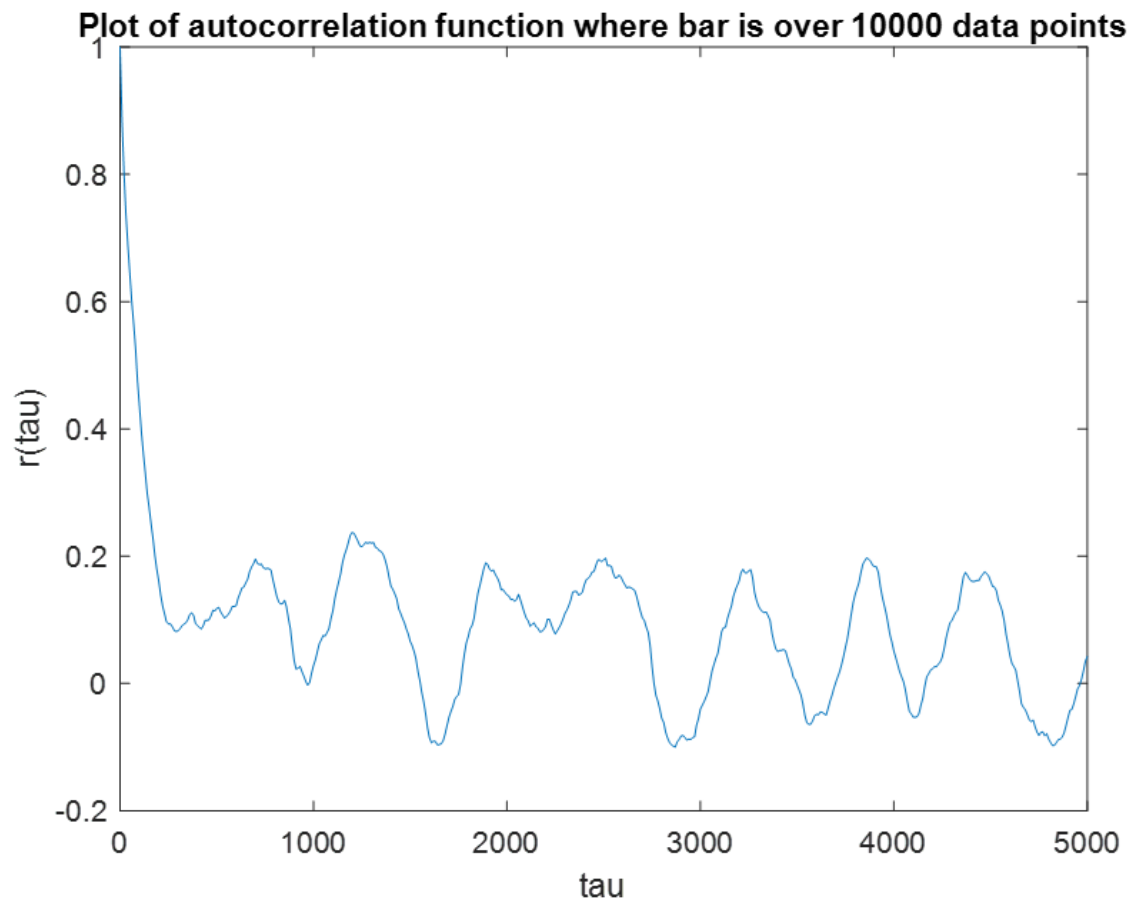
2.e)



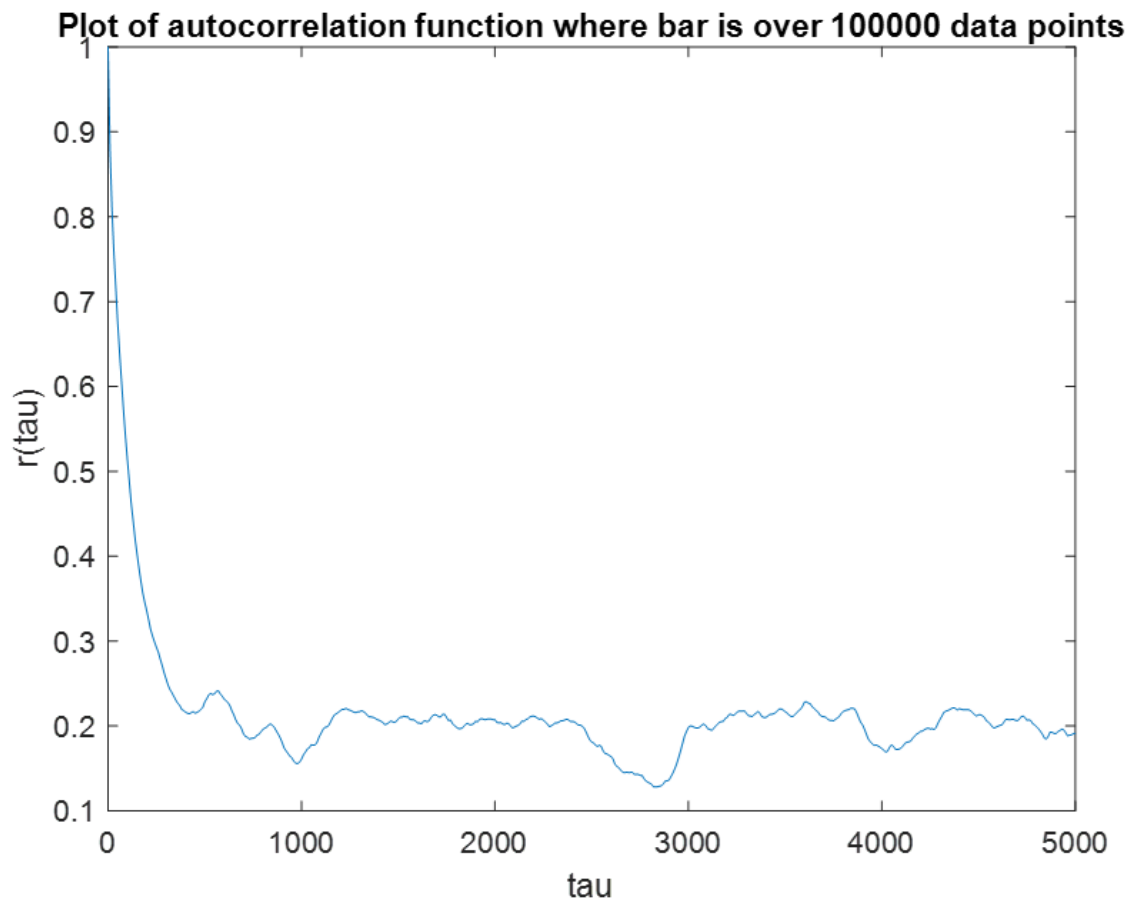
2.f)

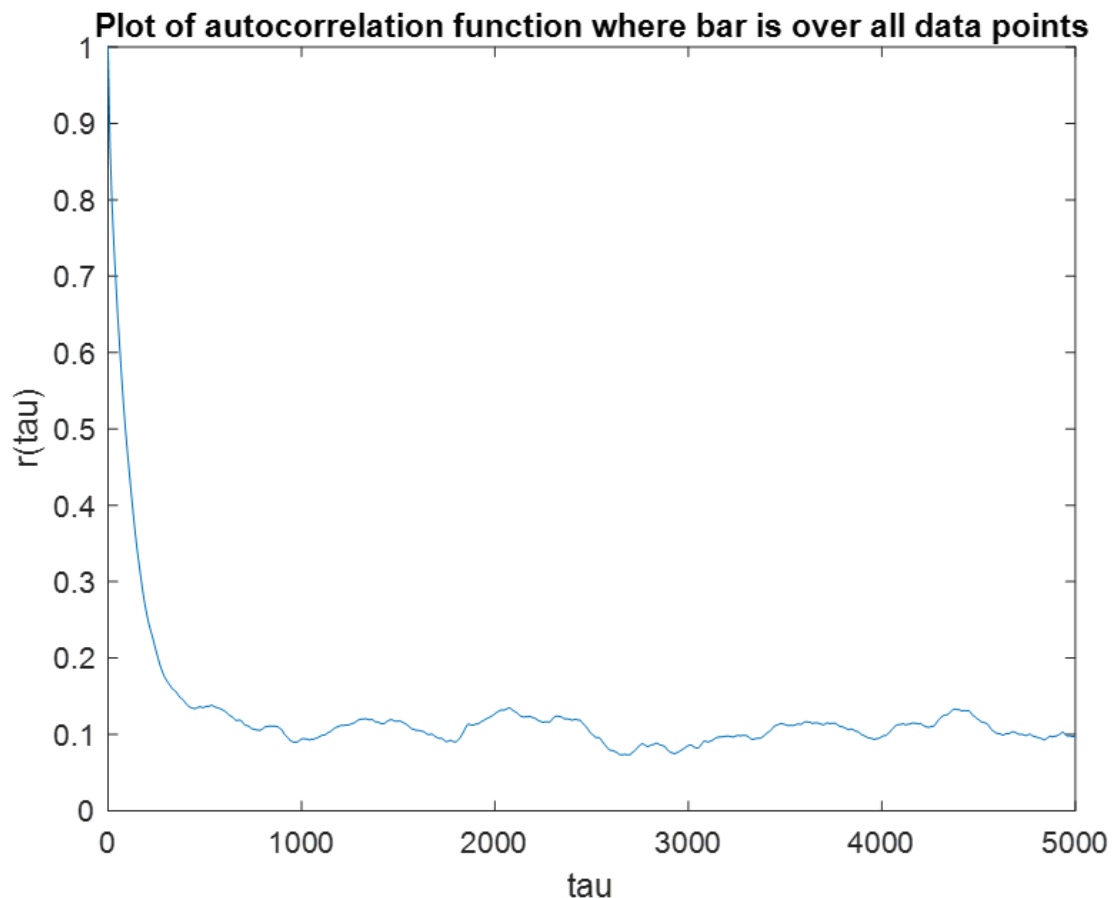












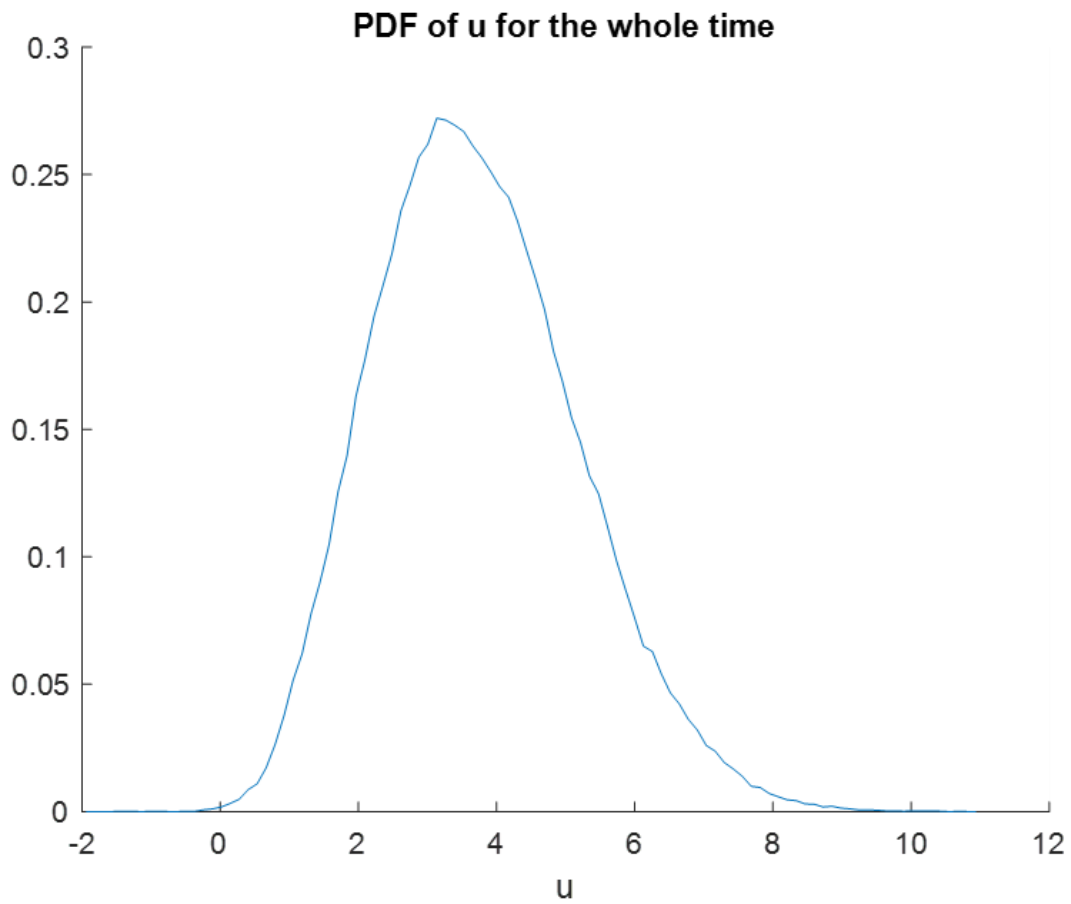
For all graphs, initially the  $u'$  and  $u'$  at  $\Delta t$  are autocorrelated as the value of  $R$  is large and positive. However, with time progression, the value of  $R$  diminishes as the fluctuation points become uncorrelated to each other. This is because for larger values of  $\tau$  the velocities at  $t$  and  $t+\tau$  are not in the same coherent eddy structure. For shorter values of  $\tau$ , the velocities at  $t$  and  $t+\tau$  are in the same coherent eddy structure, so they have more correlation.

Interestingly, for graph plots for 500, 1000 bar mean averages, large negative values are encountered as  $u_1(t)$  is auto-correlated to opposite signs of  $u_2(t)$ .

For higher bar averaging, there is no auto-correlation among the two  $u'$  time intervals. Yet, you see larger  $R$  auto correlation for lower bar averaging values.

In conclusion, autocorrelation is observed over smaller intervals among  $u'$  and  $u'\Delta t$  and diminishes over higher time averaging.

2.g)



```
>> pdf_integral=trapz(v,f1)
```

```
pdf_integral =
```

```
1
```

```
>> pdf_u_integral=trapz(v,f1.*v)
```

```
pdf_u_integral =
```

```
3.7149
```

### 3. Betz Derivation (included in the last section)

### 4. QBLADE: Testing Implementation of BEM Theory using QBLADE (BEM Code)

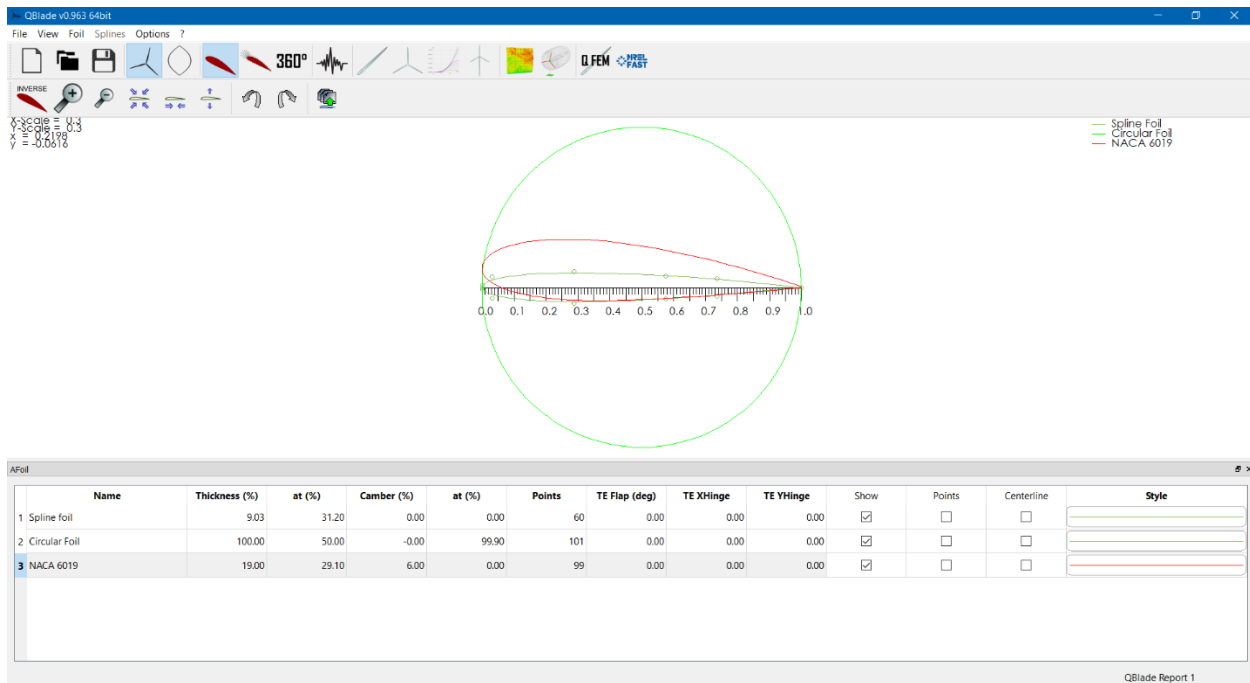


Figure 1: Importing “canned” NACA foils in QBlade

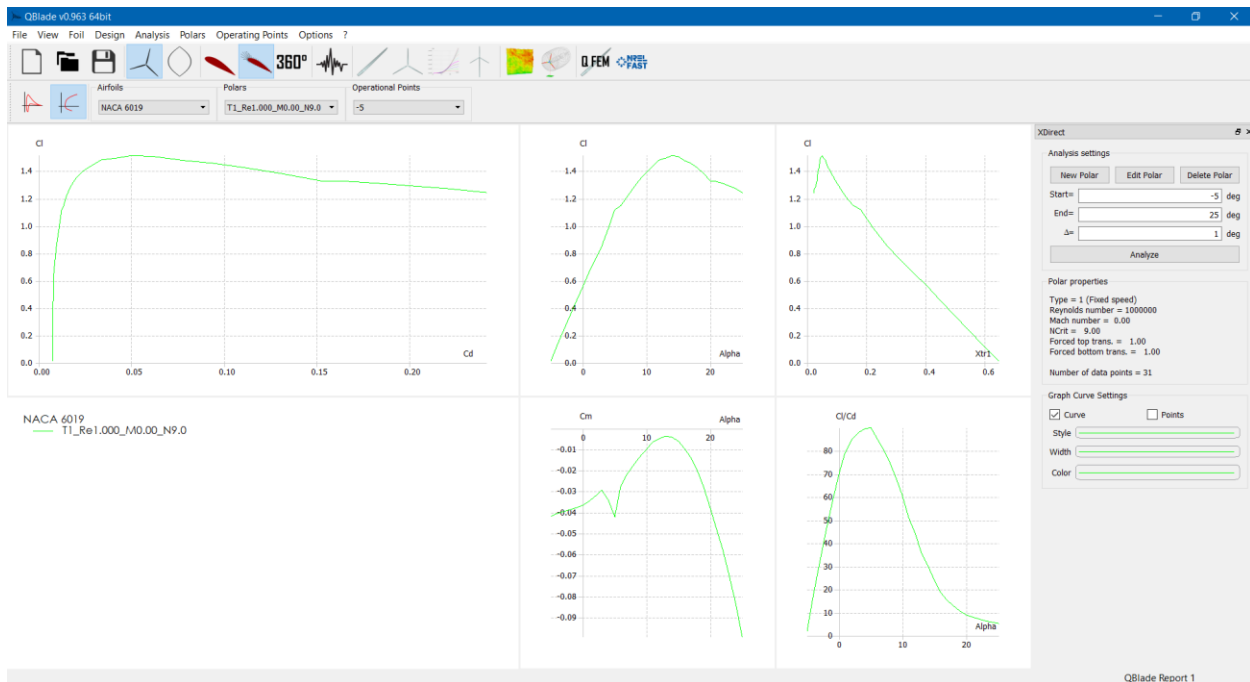


Figure 2: XFOIL Direct Analysis module to create polar to simulate flow around the airfoil

## HW4 MAE 579 Wind Energy



Figure 3: 360° Polar extrapolation module

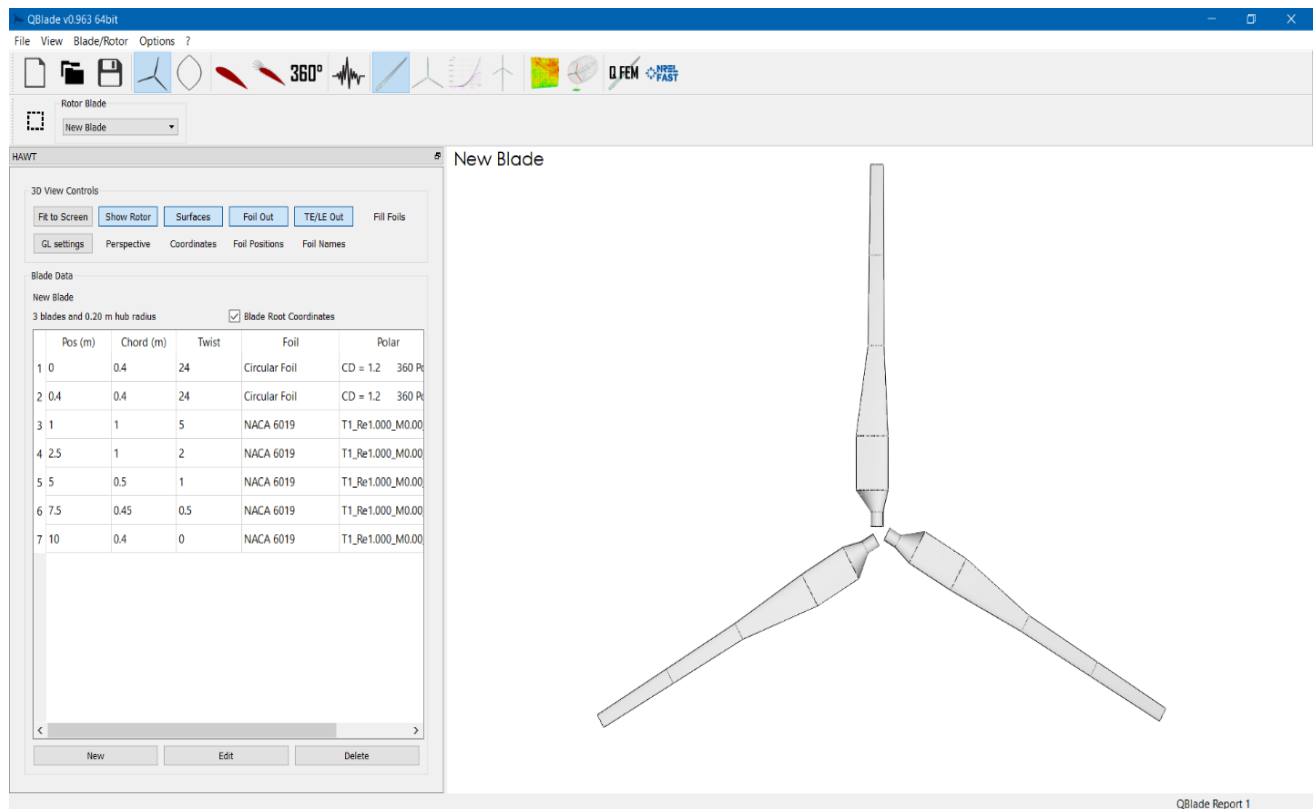


Figure 4: HAWT blade design and optimization submodule

## HW4 MAE 579 Wind Energy

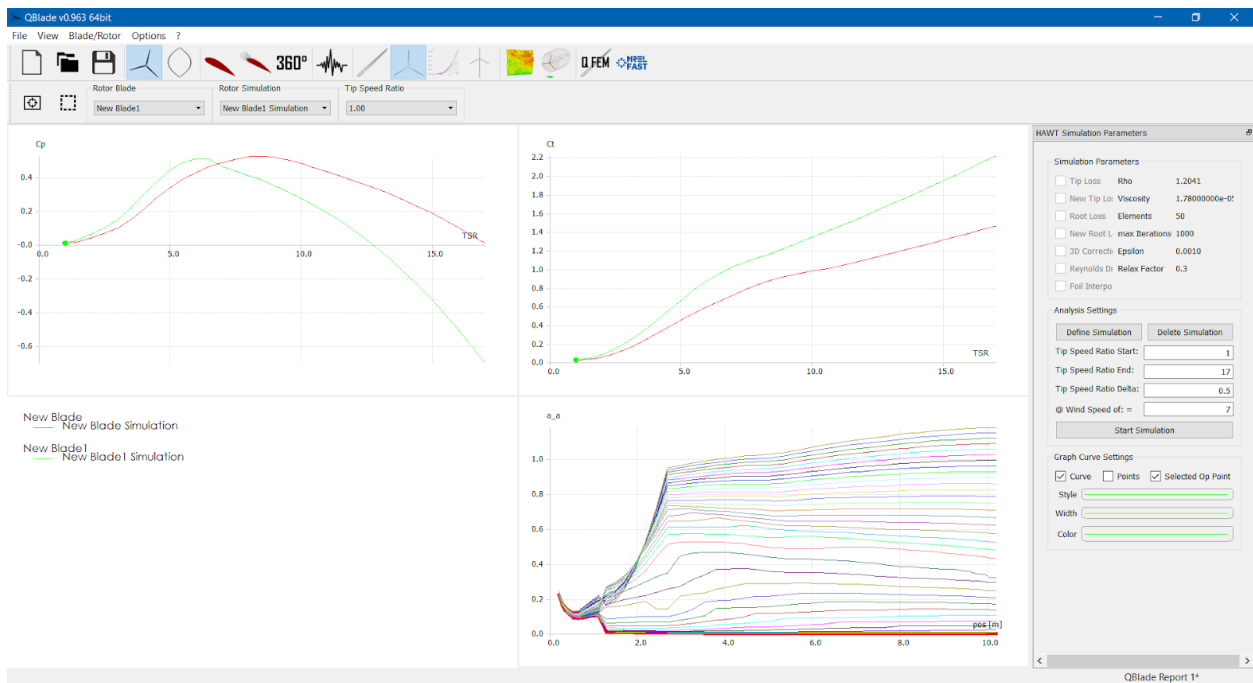


Figure 5: HAWT rotor simulation submodule

## 5. Reynold's Decomposition in diffusion term of Navier Stokes Equation

steps to build wind farm: gather data

$$u_i = \bar{U}_i + u_i'$$

2) 
$$\nu \frac{\partial^2 u_i}{\partial x_j^2} = \nu \frac{\partial^2 (\bar{U}_i + u_i')}{\partial x_j^2} = \nu \left( \frac{\partial^2 \bar{U}_i}{\partial x_j^2} + \frac{\partial^2 u_i'}{\partial x_j^2} \right)$$

time 
$$= \nu \left[ \frac{\partial^2 \bar{U}_i}{\partial x_j^2} + \frac{\partial^2 u_i'}{\partial x_j^2} \right]$$

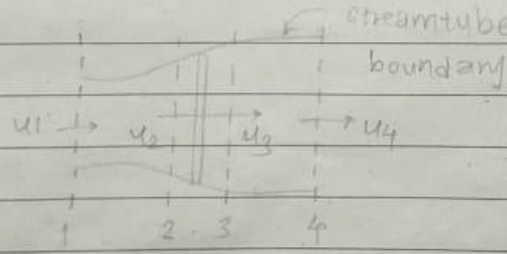
mean + fluctuation

Apply Reynold's decomposition

$$= \nu \left[ \frac{\partial^2 \bar{U}_i}{\partial x_j^2} + \frac{\partial^2 \bar{u}_i'}{\partial x_j^2} \right]$$

$$= \nu \frac{\partial^2 \bar{U}_i}{\partial x_j^2}$$

commutation rule

3)  streamtube boundary

Assumption:

- 1) homogenous, incompressible, steady state fluid flow
- 2) No frictional drag
- 3) non-rotating wake

conservation of linear momentum, thrust equal & opposite to rate of change of momentum of air stream.

$$T = \dot{m} (u_1 - u_4)$$

... steady state flow — (A)

Bernoulli's at 1, 2 & 3, 4,

$$p_1 + \frac{1}{2} \rho u_1^2 = p_2 + \frac{1}{2} \rho u_2^2 \quad (1)$$

$$p_3 + \frac{1}{2} \rho u_3^2 = p_4 + \frac{1}{2} \rho u_4^2 \quad (2)$$

Assume,  $p_1 = p_4$ ,  $u_2 = u_3$

Thrust,  $T = A_2 (p_3 - p_4)$  — (3)

eqn (1) - (2) & substitute in (3)

$$P_1 + \frac{1}{2} \rho U_1^2 = P_2 + \frac{1}{2} \rho U_4^2$$

$$P_2 - P_1 = \frac{1}{2} \rho (U_1^2 - U_4^2) \quad - (14)$$

Put (14) in (13)

$$T = A_2 \cdot \frac{1}{2} \rho (U_1^2 - U_4^2) \quad - (15)$$

equating thrust eqn from (15) & (14) (Bernoulli's & linear momentum)

$$\dot{m} (U_1 - U_4) = A_2 \cdot \frac{1}{2} \rho (U_1^2 - U_4^2) \quad \dot{m} = (\rho A U)_2 = (\rho A U)_4$$

$$U_2 = \frac{U_1 + U_4}{2} \quad - (16)$$

a: fractional decrease in wind velocity freestream of rotor plane

$$a = \frac{U_1 - U_2}{U_1}$$

$$U_2 = U_1 (1 - a) \quad - (17)$$

$$U_4 = U_1 (1 - 2a) \quad \text{from (6)} \quad - (18)$$

from eqn (17) (18) (15)

$$T = \frac{1}{2} A_2 \rho (U_1^2 - U_4^2)$$

$$T = \frac{1}{2} A_2 \rho (U_1 + U_4) (U_1 - U_4)$$

$$T = \frac{1}{2} A_2 \rho (U_1 + U_1 - 2aU_1) (U_1 - U_1 + 2aU_1)$$

$$T = \frac{1}{2} A_2 \rho (2U_1 - 2aU_1) (+2aU_1)$$

$$T = \frac{1}{2} \rho A_2 (4aU_1^2 - 4a^2U_1^2)$$

$$T = \frac{1}{2} \rho A U^2 (4a(1-a)) \quad \begin{matrix} U_1 = U \\ A_2 = A \end{matrix}$$



$$C_T = \frac{\text{Thrust force} = T}{\text{Dynamic force} = \frac{1}{2} \rho U^2 A}$$

$$C_T = 4a(1-a)$$

thrust coefficient

$$C_T \text{ max, } \frac{dC_T}{da} = 0$$

$$C_T = 4a - 4a^2$$

$$\frac{dC_T}{da} = 4 - 8a = 0$$

$$a = \frac{1}{2}$$

$$T_{\text{max}} = \frac{1}{2} \rho U^2 A$$

thrust at  
Betz power  
limit

$$C_{T \text{ max}} = 4\left(\frac{1}{2}\right) - 4\left(\frac{1}{4}\right)$$

$$= 2 - 1$$

$$C_{T \text{ max}} = 1$$

max thrust  
coefficient limit

(1) thrust at Betz power limit ( $a = 1/3$ )

$$C_T = 4\left(\frac{1}{3}\right) \left[1 - \frac{1}{3}\right]$$

$$C_T = \frac{8}{9}$$

Betz  
limit

thrust at  
Betz limit

## HW4 MAE 579 Wind Energy

### Matlab Code:

#### Main file

```
close all
clear
%load sonic_segment.mat
load MAE_577_sonic_segment.mat

%b
figure(1)
formatted_time=datetime(2001,8,6,7,0,0)+seconds((time-time(1))*24*60*60);
plot(formatted_time(12001:12501),u(12001:12501))
xlim([formatted_time(12001) formatted_time(12501)])
xlabel('Time')
ylabel('u(m/s)')
title('Plot of 500 contiguous points')
%c running 15 min average of bar(u)
i=1;
j=1;
while i<252000
    u_mean(j)=mean(u(i:i+8999));
    t_mean(j)=(2*i+9000)/2;
    t_mean(j)=t_mean(j)/(10*60);
    i=i+9000;
    j=j+1;
end

formatted_time_mean=datetime(2001,8,6,7,0,0)+minutes(t_mean);
figure(2)
plot(formatted_time_mean,u_mean);
title('Running 15 min average of bar(u)')
xlabel('Time')
ylabel('bar(u)')

%d running 15 minute average of bar(u'u')
u_mean=mean(u);
for i=1:252000
    u_prime(i)=u(i)-u_mean;
    u_prime_squared(i)=u_prime(i)*u_prime(i);
end

j=1;
i=1;
while i<252000
    u_prime_squared_mean(j)=mean(u_prime_squared(i:i+8999));
    t_mean(j)=time(i+4500);
    i=i+9000;
    j=j+1;
end

u_prime_squared_mean_all_time=mean(u_prime_squared);

figure(3)
plot(formatted_time_mean,u_prime_squared_mean)
title("Running 15 min average of bar(u'u')")
xlabel('Time')
ylabel("bar(u'u')")

%e scatter plot of u and v
figure(4)
scatter(u_prime(1:500),u_prime(3401:3900))
```

## HW4 MAE 579 Wind Energy

```
xlabel('u')
ylabel('v')
title('Scatter plot')

%f autocorrelation
tau=[0:10:5000];
T0=100;
auto_correlation=zeros(5,length(tau));
auto_correlation_normalized=zeros(5,length(tau));
self_correlation=zeros(5,length(tau));
self_correlation_normalized=zeros(5,length(tau));

T=[500 1000 10000 100000 252000];
for j=1:length(tau)
    for i=1:5
        for t=T0:T0+T(i)-1

auto_correlation(i,j)=auto_correlation(i,j)+(u_prime(wrap(t))*u_prime(wrap(t+tau(j))))
;
            self_correlation(i,j)=self_correlation(i,j)+u_prime(wrap(t))*u_prime(wrap(t));
        end
        auto_correlation(i,j)=auto_correlation(i,j)/T(i);
        self_correlation(i,j)=self_correlation(i,j)/T(i);
        auto_correlation_normalized(i,j)=auto_correlation(i,j)/self_correlation(i,j);
    end
end

figure(5)
plot(tau,auto_correlation_normalized(5,:));
title('Plot of autocorrelation function where bar is over all data points')
xlabel('tau')
ylabel('r(tau)')

%g pdf of u over all time
a=-2;
b=11;
N=100;
dv=(b-a)/N;
v=zeros(N,1);
f=zeros(N,1);

for i=1:N
    for j=1:size(u)
        if(u(j)>=a+(i-1)*dv && u(j)<a+i*dv)
            f(i)=f(i)+1;
        end
    end
    v(i)=a+(i-0.5)*dv; % mid point of wind speed bin
end

f1=f/(252000*dv);
figure(6)
plot(v,f1)
%integral
pdf_integral=trapz(v,f1);
pdf_u_integral=trapz(v,f1.*v);

title("PDF of u for the whole time")
xlabel('u')
```

Function file - wrap.m

```
function [index] = wrap(input_index)
if input_index>252000
    index = input_index-252000;
else
    index=input_index;
end
```