

# ECE320: Fields and Waves

## Lab 1 Report: Waves on Transmission Lines

**PRA106**

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## 1 Introduction

This laboratory focused on investigating the characteristics of transmission lines, studying voltage and current propagation along them, as well as its dependence on the nature of load impedance.

## 2 Determining the Characteristic Impedance, $Z_0$

We varied the load on the switch box until we saw little or no traces of reflected waves. This was at  $Z_L = 50\Omega$  which is also equal to the characteristic impedance since we know that the reflections nullify when  $Z_L = Z_0$ . The corresponding waveforms captured at the generator input (channel 1, top) and the transmission line input (channel 2, bottom) are shown in Figure 1.

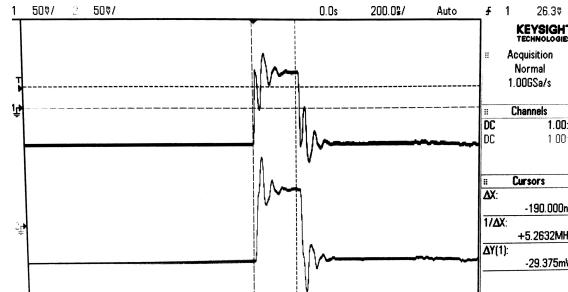


Figure 1: Transmission line terminated with load  $Z_L = Z_0$

## 3 Determining $Z_0$ using $\frac{\tilde{V}^+(z=-L)}{\tilde{I}^+(z=-L)}$

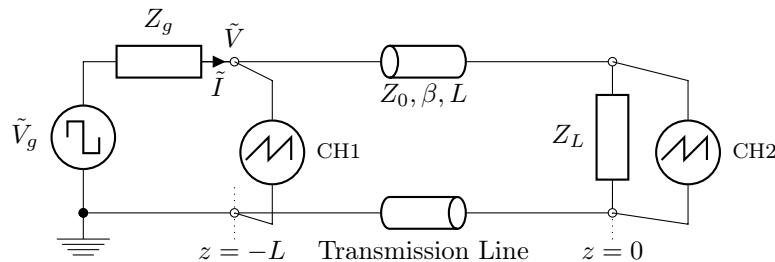


Figure 2: Laboratory setup for studying characteristics of transmission lines

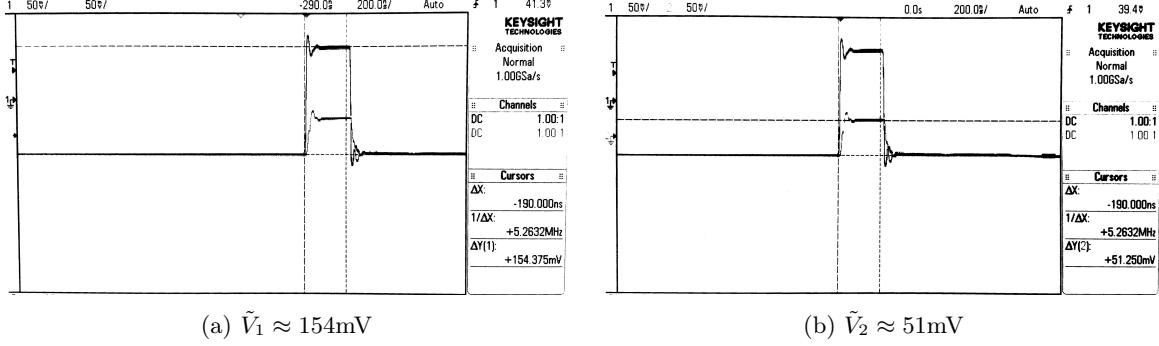


Figure 3:  $\tilde{V}$  measured across  $R_{\text{shunt}} = 100\Omega$

As seen in Figure 3, the voltage at  $\tilde{V}_1 = 154\text{mV}$  and  $v_1 = 51\text{mV}$ . Given the value of  $R_{\text{shunt}} = 100\Omega$ , we can calculate  $\tilde{I}^+ = \frac{0.154 - 0.051}{100} = 1.03\text{mA}$ . From Figure 4, we can see that  $\tilde{V}_2 = \tilde{V}^+$ , and therefore we can confirm the value of  $Z_0$  through the relation,  $Z_0 := \frac{\tilde{V}^+(z=-L)}{\tilde{I}^+(z=-L)} = \frac{51\text{mV}}{1.03\text{mA}} = 49.51\Omega \approx 50\Omega$ .

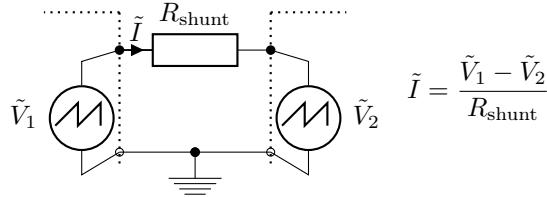


Figure 4: Estimating input current through a shunt resistance

## 4 Observation of Travelling Waves

Observed waveforms at different points on the transmission line can be found in Figure 5.

The recorded time delays,  $\Delta t$ , relative to the input signal are listed in Table 1.

Port	$\Delta t$ (ns)
D	130
E	244
F	368

Table 1: Recorded time delay at different locations along the transmission line

## 5 Determining Velocity of Propagation

The velocity of propagation of the signal can be calculated by the relation  $v_p = \frac{\Delta L}{\Delta t}$ , given that we are able to track the same point on the waveform. Using the data from Table 1, we get that the average velocity of propagation is  $v_{p,\text{avg}} = 2.44 \cdot 10^8 \text{m/s}$ .

Now, to find the relative permittivity, we also know that the phase velocity of an electromagnetic wave in an electrical transmission line with magnetic permeability,  $\mu \approx \mu_0$ , and electric permittivity,  $\epsilon = \epsilon_r \epsilon_0$ , is given by:

$$v_p = \frac{1}{\sqrt{\mu\epsilon}} \implies \frac{v_p}{c} \approx \sqrt{\frac{\mu_0 \epsilon_0}{\mu_0 \epsilon_0 \epsilon_r}} \implies \epsilon_r \approx \frac{c^2}{v_p^2} \approx 1.51$$

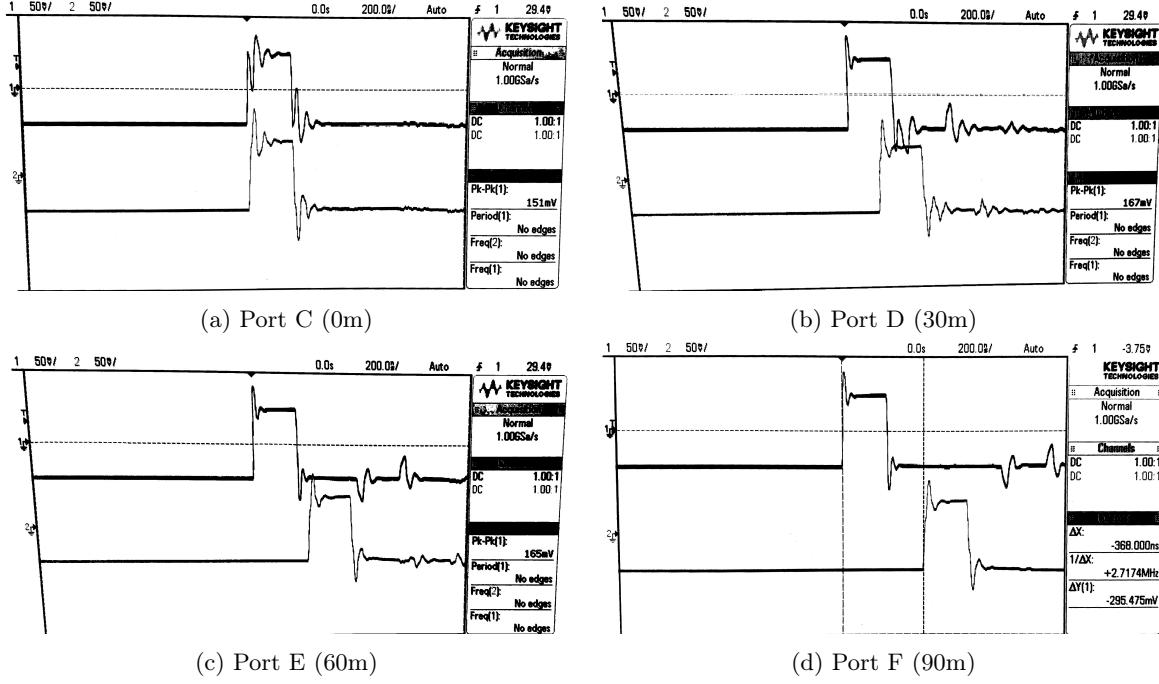


Figure 5: Measured  $V(t)$  at different locations along the transmission line with  $Z_L = Z_0$

The theoretical  $V(t)$  plots in Figure 6 closely match the observations in Figure 5.

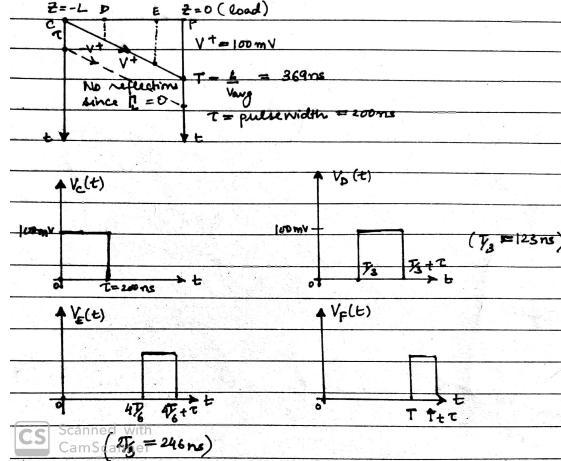


Figure 6: Theoretical bounce diagram and  $V(t)$  plots along the transmission line

## 6 Simple Reflection

There is a load mismatch if  $Z_L \neq Z_0$  and we know that, in this case, reflection of current and voltage occurs at the load, i.e.  $\tilde{v}^- \neq 0$  and  $\tilde{I}^- \neq 0$ . The load reflection coefficient,  $\Gamma_L$ , if defined as:

$$\Gamma_L := \frac{\tilde{V}^-}{\tilde{V}^+} = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Thus, in cases where there is a load mismatch,  $\Gamma_L \neq 0$ , there will be a relection of intensity  $\tilde{V}^- = \Gamma_L V^+$  along the transmission line towards the generator and the steady state for a step input will be achieved after

the voltage and current wave has travelled back and forth once, and this can also be verified using a bounce diagram. The Theoretically for  $Z_L = 100\Omega$ ,  $\Gamma_L = \frac{50\Omega}{150\Omega} = \frac{1}{3}$  and through the measurements, we observe the reflection coefficient  $\Gamma_L = \frac{30mV}{100mV} = \frac{3}{10} \approx \frac{1}{3}$ .

The measurements for reflected voltage waves can be found in Figure 7. Channel 1 (top) waveform has been recorded at port C (0m) and channel 2 (bottom) waveform has been recorded at port F (90m). The pulselength  $\tau$  of the signal was set such that it was equal to the time delay  $T$  for a pulse to reach port F from port C, which made the signal recordings at port C and F exactly out of phase. In terms of magnitude, the signal at port F was a superposition of the incident and reflected wave  $\tilde{V}_F = \tilde{V}^+ + \Gamma_L \tilde{V}^+$ . Similarly at port C, the signal at  $t \in (2T, 3T)$ ,  $\tilde{V}_C = \Gamma_L \tilde{V}^+ = \tilde{V}^-$ , which can all again be verified using a bounce diagram. The theoretical  $V(d)$  graphs for different time points can be found in Figure 8.

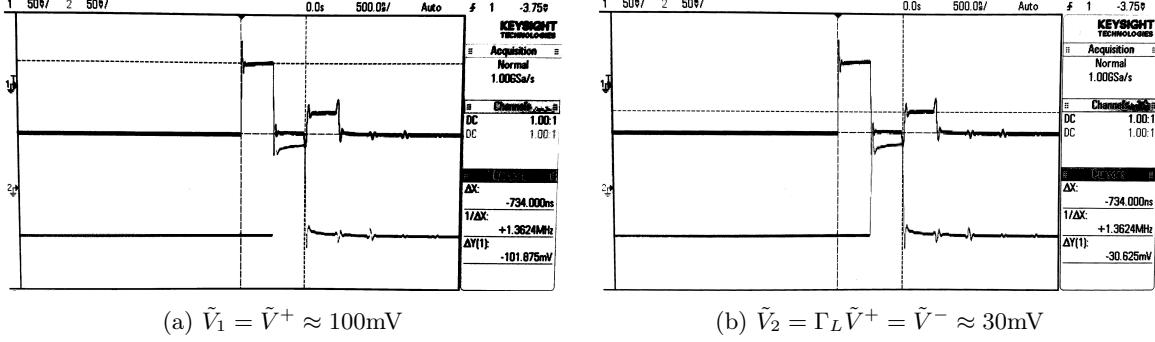


Figure 7:  $\tilde{V}$  measured at port C and port F for input signal with pulselength  $\tau = T$

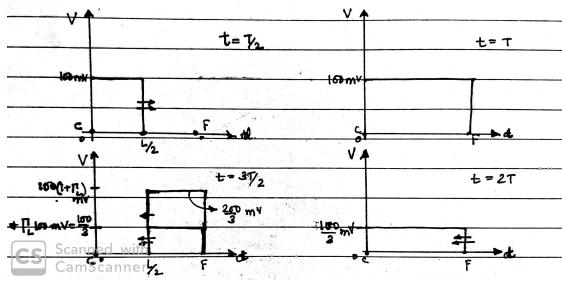


Figure 8:  $V(d)$  plots at different time points

## 7 Multiple Reflections

For mismatched generator side,  $Z_g = 150\Omega$ , as well as the load side,  $Z_L = 20\Omega$ , there will be reflections on both ends of the transmission line.

## 8 Input Impedance and Transmission Line Length

We know that the impedance changes.

$$Z_{in} = Z(z)|_{z=-L} = Z_0 \frac{1 + \Gamma e^{j2\beta z}}{1 - \Gamma e^{j2\beta z}}|_{z=-L} = Z_0 \frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L}$$

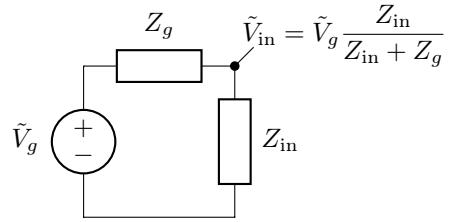


Figure 9: Voltage division over net input impedance,  $Z_{in}$

## 9 Conclusion

Through this lab,

## 10 Notes

All images taken during the lab were post-processed in a batch using a custom script that bit-wise inverts the pixels and binarizes the resulting image based on a custom threshold. No adjustments or modifications were made to the readings, for which the oscilloscope's measurements are also shown alongside the waveforms. All scripts and related work can be found at [github.com/pranshumalik14/ece320-labs](https://github.com/pranshumalik14/ece320-labs).