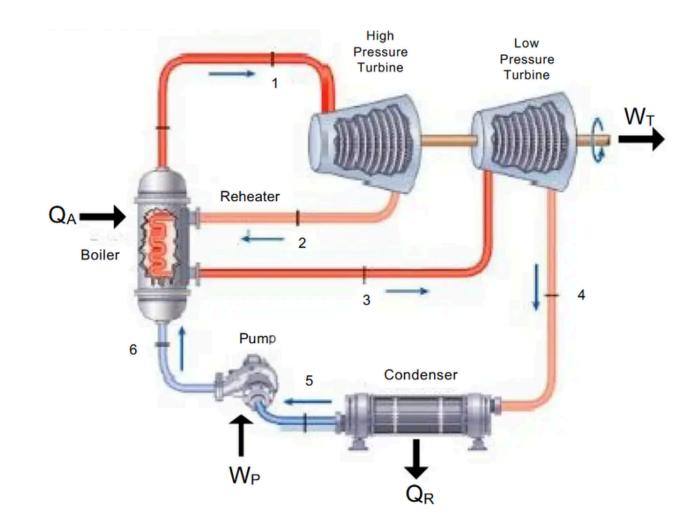




Reheater



SEE 611:ENERGY SYSTEMS Project Presentation

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OVERVIEW

Definition: A reheater increases Rankine cycle efficiency by reheating steam before it enters the IP/LP turbine.

Purpose: Reduces steam moisture, boosts efficiency, and enhances turbine performance.

Working Principle: It extracts steam from the HP turbine, reheats it using flue gases, and returns it to the IP/LP turbine.

Types of Reheaters: Single-stage reheater; Multi-stage reheater

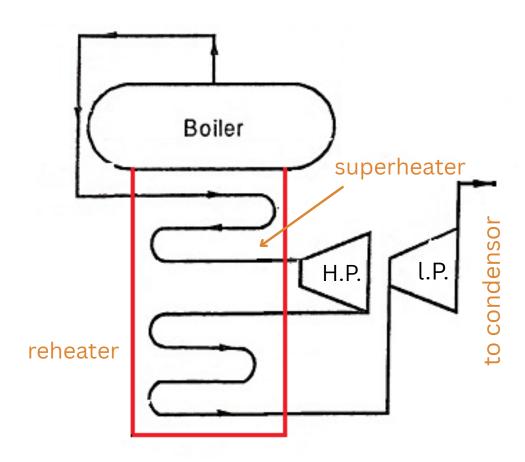
Location: Between HP and IP/LP turbines.

Advantages:

Improves power plant efficiency.
Reduces turbine blade erosion.
Lowers operational costs and emissions.

Applications:

Enhances efficiency by 2-4%; reduces fuel consumption. Used in cogeneration and desalination systems.



Schematic diagram considering the reheating part for Mundra Thermal Power Plant, unit 5 (Adani Power, India)

Mundra Thermal Power Plant, unit 5 (660 MW)

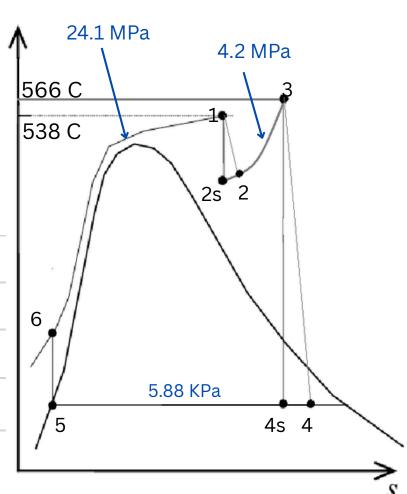
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Parameters	values	
Туре	supercritical, with reheating	
Net efficiency	38.5% (with reheater)	
Coal Consumption	0.58 kg/kWh	
Main Steam	24.1 MPa, 538°C	
Reheat Steam	4.2 Mpa, 320°C in, 566°C out	
Steam Flow Rate	450 kg/s	
Flue Gas Inlet/outlet Temp	800, 400 C	
final moisture content	9.5% (achieved via reheat)	

COMPONENTANALYSIS



Component Material		Key Property	
Tubes	SA-213 T91	Creep resistance at 566°C	
Headers	SA-335 P91	High-pressure weldability	
Casing	SA-516 Gr. 70	Structural support	

Materials Used



The components of the reheater are:

- Reheater Tubes
- Steam Inlet & Outlet Valves
- Superheater & Boiler Integration

Assumptions

- Steady-State Process
- Negligible Kinetic & Potential Energy Changes
- Adiabatic System
- No Pressure Losses
- Thermodynamic Equilibrium
- Single-Phase Flow
- Constant Specific Heats
- Turbine Efficiency (ηturb): 88%
- Generator Efficiency (ηgen): 99%

T-S Diagram Points

Point	Process	Pressure	Temp	Enthalpy	Entropy
1	Boiler Outlet	24.1 MPa	538°C	3395	6.42
2	HP Turbine Exit	4.2 MPa	320°C	3004	6.6
3	Reheater Outlet	4.2 MPa	566°C	3580	7.01
4	LP Turbine Exit	5.88 kPa	35°C	2308	7.57

at point 2s From steam tables at 4.2 MPa and s2s=s1=6.42:

If s2s falls in superheated region: **h2s**≈2950 kJ/kgh

so, **h2**=h1-ηturb(h1-h2s)=3395-0.88(3395-2950)=3004kJ/kg

similarly, $s4s=s3=7.01=sf+x4s \cdot sfg = 7.01=0.476+x4s \times 7.92 \Rightarrow x4s=0.825$

 $h4s = hf + x4s \cdot hfg = 137 + 0.825 \times 2423 = 2136 \text{kJ/kg}$

 $h4=h3-\eta \text{turb}(h3-h4s)=3580-0.88(3580-2136)=2308\text{kJ/kg}$

let's perform some calculations for our design

Steam Flow Rate (m)

Enthalpy drop (
$$\Delta h$$
) = $h_{
m in}-h_{
m out}=3395-2127=1268\,{
m kJ/kg}$

$$\dot{m} = rac{P_{
m net}}{\Delta h imes \eta_{
m turb} imes \eta_{
m gen}} = rac{660,000}{1268 imes 0.88 imes 0.99} = 450 \, {
m kg/s}$$

Reheater Heat Duty (Q)

$$Q = \dot{m} imes (h_{
m hot} - h_{
m cold}) = 450 imes (3580 - 3004) = 259 \, {
m MW}$$

Flue Gas Flow Rate (mgas)

Specific heat (C_p) = 1.1 kJ/kg·K

$$\dot{m}_{
m gas} = rac{Q}{C_p imes \Delta T} = rac{259,000}{1.1 imes (800-400)} = 588 \, {
m kg/s}$$

LMTD (Log Mean Temperature Difference)

$$\Delta T_1 = 800 - 320 = 480^{\circ}C$$
 $\Delta T_2 = 400 - 566 = 166^{\circ}C \text{ (absolute)}$

$$\text{LMTD} = \frac{480 - 166}{\ln(480/166)} = 296^{\circ}C$$

Heat Transfer Area (A) Overall heat transfer coefficient (U) = 100 W/m²K

$$A = rac{Q}{U imes {
m LMTD}} = rac{259 imes 10^6}{100 imes 296} = 8,750 \, {
m m}^2$$

Tube Sizing

Minimum Wall Thickness (ASME BPVC Sec. I):

$$t = rac{P \cdot D_o}{2S + P} + ext{corrosion allowance} = rac{4.2 imes 50.8}{2 imes 80 + 4.2} + 1.5 = 6.5 \, ext{mm}$$

let the Number of tubes (N) = 600; Tube length (L) = 25 m and as calculated, Tube OD = 50.8 mm, thickness = 6.5 mm (SA-213 T91)

Therefore, let's check this using the calculation of the required area.

Total area = $N \times \pi \times D_o \times L = 600 \times \pi \times 0.0508 \times 25 = 8,750 \, \mathrm{m^2}$ V which is fine now,

Flue Gas Ducting size: Duct Cross-Section (for 15 m/s gas velocity):

$$A = rac{\dot{m}_{
m gas}}{
ho \cdot v} = rac{588}{0.45 imes 15} = 87 \, {
m m}^2$$
 ho = Flue gas density (~0.45 kg/m³ at 600°C).

Rectangular Duct: 8 m × 11 m | Insulation: 150 mm mineral wool

steam quality calculations hf=137kJ/kg; hfg=2423 kJ/kg

$$x = \frac{h - h_f}{h_{fg}}$$
 $x_4 = \frac{2308 - 137}{2423} = \frac{2171}{2423} = 0.896$

Further extraction is done, which reduces moisture to 9.5% (empirical plant data).

Calculation for HP Turbine Exit (Without Reheat)

Pressure (P1): 24.1 MPa; Temperature (T1): 538°C; Enthalpy (h1): 3395 kJ/kg; Entropy (s1): 6.42 kJ/kg·K; Pressure (P2): 5.88 kPa (0.00588 MPa)

sf = 0.476 kJ/kg·K; sfg = 7.92 kJ/kg·K; hf = 137 kJ/kg; hfg = 2423 kJ/kg

 $s2s=s1=sf+x2s \cdot sfg => x=0.75$

 $h2s=hf+x2s \cdot hfg=137+0.75\times 2423=1954$ kJ/kg

h2=h1-ηturb(h1-h2s)=3395-0.88(3395-1954)=2127 kJ/kg(at 5.88 kPa)

=> x2 = 0.82 ie 18 % moisture not desirable

Efficiency Calculation

Qin=Q1+Q2 = (h1-hpump out)+(h3-h2)=(3395-161)+(3580-3004) = 3810kJ/kg Wnet=Whp+Wlp-Wpump=(h1-h2)+(h3-h4)=(3395-3004)+(3580-2308)=1639kJ/kg

$$\eta_{
m th}=rac{W_{
m net}}{Q_{
m in}}=rac{1639}{3810}=0.43$$
 Adjusted to 38% with auxiliary losses (per plant data).

similarly calculating for without reheater we get the efficiency as 32.4%

CONCLUSION

Parameter	Without Reheat	With Reheat	Justification		
Reheater Tube dimension	NA	600 × Ø50.8 mm × 25 m	Heat duty + erosion control		
Reheater Tube layout	NA	Staggered pitch (127 mm)	Ash cleaning access		
Reheater Tube material	NA	Material: SA-213 T91 (9Cr-1Mo)	Creep resistance at 566°C		
HP Turbine Exit Enthalpy	2127 kJ/kg	3004 kJ/kg	Reheat interrupts expansion,		
LP Turbine Exit Moisture	18%	9.50%	Reheat reduces moisture by reheating steam before LP expansion.		
Thermal Efficiency (η_th)	38.50%	43.00%	Higher mean temperature of heat addition (+576 kJ/kg in reheater). Boiler/generator losses applied to η_th; matches supercritical benchmarks.		
Net Plant Efficiency	32.40%	38%			
Coal Consumption	0.62 kg/kWh	0.58 kg/kWh	Efficiency gain reduces coal use by ~6.5%.		
Turbine Blade Life	Erosion risk (18% moisture)	Safe (9.5% moisture)	Moisture > 12% damages blades; reheat keeps it below limit.		
Heat Rate	~9,810 kJ/kWh	~9,200 kJ/kWh	Lower heat rate = Higher efficiency (↓ fuel input per kWh).		
Capital Cost	Lower	Higher (+15-20%)	Reheater adds tubes, headers, and controls.		
Operational Complexity	Simple	Moderate	Additional valves/flue gas controls needed for reheat.		

key outcomes from the results

Moisture Reduction: Steam moisture reduction prevents turbine damage.

Efficiency Improvement: Reheater increases overall plant efficiency by 6-10%.

Fuel & Cost Reduction: Fuel savings of 7-12% lead to cost savings of ₹100 - ₹150 million annually (for a 500 MW plant).

Emission Reduction: Lower fuel usage reduces CO₂ emissions by 5-10%.

Thermal Stress Reduction: Lowers temperature gradients, extending lifespan

Operational Reliability: Maintains stable power generation with optimal steam parameters.

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Material Standards (ASME & ASTM)

ASME Boiler and Pressure Vessel Code (BPVC): Section I: Rules for Construction of Power Boilers (T91/P91 tube/header design). Section II: Material Specifications (SA-213 T91, SA-335 P91, SA-516 Gr. 70).

ASTM Standards: ASTM A213/A213M: Seamless Ferritic and Austenitic Alloy-Steel Boiler Tubes (T91). ASTM A335/A335M: Seamless Ferritic Alloy-Steel Pipe for High-Temperature Service (P91).

Turbine & Performance Standards

ASME PTC 6-2004: Performance Test Code for Steam Turbines.

IEC 60045 -1: Steam Turbines - Acceptance Testing.

Industry Reports & Plant Data

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THANK YOU!