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**SRM Institute of Science and Technology**  
**College of Engineering and Technology**  
**Department of Electronics and Communication Engineering**

**Academic Year:2025-2026 (ODD)**

**Test: LLT-1 (Case Study & Simulation)**

**Date:27.10.2025**

**Course Code & Title: 21ECC205T-Electromagnetic Theory and Interference**

**Max. Marks: 40**

**Year & Sem & Dept: II/III/ECE**

**Course Articulation Matrix:**

21ECC205T- Electromagnetic Theory and Interference		Program Outcomes (PO)																
		Graduate Attributes												PSO				
CO	Course Outcomes (CO)	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3		
1	Apply the concepts and knowledge to solve problems related to electric field.	-	2	3	-	-	-	-	-	-	-	-	-	-	-	-		
2	Analyse the concepts of Magnetic field and Maxwell's equations in the real-world application.	-	3	2	-	-	-	-	-	-	-	-	-	-	-	-		
3	Translate the phenomenon of guided wave propagation and its mode of propagation.	-	3	2	-	-	-	-	-	-	-	-	-	-	-	-		
4	Describe the importance of transmission line theory applicable to low frequency transmission lines.	-	2	3	-	-	-	-	-	-	-	-	-	-	-	-		
5	Solve transmission line parameter and impedance matching through analytical and graphical methods.	-	2	3	-	-	-	-	-	-	-	-	-	-	-	-		

**(Answer ALL Questions) (4\*10=40 Marks)**

Q. No	Case study Questions	Marks	BL	CO	PO
1	An electric vehicle is facing electronic control system malfunctions caused by EMI from its high-power drive systems. What measures can be taken to enhance electromagnetic compatibility among the vehicle's electronic components?	10	4	4	3
2	A satellite communication system is encountering interference from solar radiation and other electromagnetic disturbances in space. What design strategies can be adopted to ensure reliable communication and reduce EMI?	10	4	4	3
<b>Simulation Questions</b>					
3	A lossless 30 m long transmission line with $Z_0=50\Omega$ is established between two ground stations which operate at 2 MHz. The line is terminated with a load $Z_L = 60+j40\Omega$ . If $u = 0.6c$ on the line. Write a <b>Scilab code</b> to plot the reflection coefficient ( $\Gamma$ ), standing wave ratio (S) and input impedance in smith chart.	10	4	5	3
4	In a satellite base station, a load of $100 + j150 \Omega$ is connected to a $75\Omega$ lossless line. Write a <b>Scilab code</b> to plot the Reflection coefficient ( $\Gamma$ ), SWR value and input impedance ( $Z_{in}$ ) at $0.4\lambda$ from the load.	10	4	5	3

Enhance electromagnetic compatibility (EMC) in electric vehicles (EVs), engineers must implement a multi-layered strategy that addresses both the sources and pathways of electromagnetic interference. This ensures reliable operation of electronic control systems despite the presence of high-power drive systems.

External disturbances can couple into sensitive electronic control units (ECUs), sensors and communication lines, leading to malfunctions or degraded performance. To mitigate these effects and improve EMC, several design and system-level measures are essential:

System Shielding Techniques:

One of the most effective methods is the use of electromagnetic shielding which involves enclosing critical components and cables in conductive materials. This prevents radiated EMI from reaching sensitive electronics.

Filtering Components:

EMI filters, such as common-mode chokes and ferrite beads are placed at power input/output terminals to suppress conducted noise. These filters block high frequency interference while allowing desired signals to pass. Designers often use multistage filters in DC/DC converters and on-board chargers to meet automotive EMC standards.

PCB layout optimization:

Printed circuit board design plays a crucial role in minimizing EMI. Techniques include short trace lengths, proper grounding and segregation of high and low voltage domains. Ground planes should be continuous and connected to chassis ground where appropriate. Differential signal routing and impedance matching also help reduce

susceptibility to noise.

#### ④ Component selection and packaging:

Using components with

low parasitic inductance and capacitance and selecting IC's with build in EMI suppression features, can reduce emissions. Additionally, metal enclosures or EMI gaskets in module packaging help contain ~~emissions~~ radiated noise.

By integrating these measures across the vehicle's architecture - from component level design to system-wide layout - engineers can significantly enhance electromagnetic compatibility. This ensures robust operation of control systems, safety features even in the presence of high power drive systems.

2. Satellite communication systems operate in a uniquely challenging electromagnetic environment. Solar flares, cosmic radiation and charged particles can introduce significant EMI, disrupting signal integrity, degrading onboard electronics and threatening mission success. To combat these threats, designers implement a combination of physical, electrical and architectural safeguards:

##### ① Radiation - Hardened components:

Satellites use radiation-hardened electronics that can withstand ionizing radiation without performance degradation. These components are built with specialized materials and manufacturing processes to resist single-event upsets, latch ups and total ionizing dose effects.

##### ② Shielding and Enclosures:

Electromagnetic shielding is essential to protect sensitive subsystems. Conductive enclosures made of aluminium or composite materials

in embedded multi-layered boards to isolate


③

With embedded metal layers block external EMI. Multi-layered shielding is often used around transponders, RF front ends and digital processors to isolate them from radiated noise.

③ Grounding and Bonding: proper grounding and bonding techniques ensure that all satellite structures and electronic modules share a common electrical reference. This minimizes potential differences that could lead to EMI coupling. Conductive paths are carefully designed to avoid ground loops and ensure low impedance return paths for high frequency currents.

④ Redundancy and Fault Tolerance: critical communication paths are often duplicated with redundant transmitters, antennas and signal processors. This ensures continued operation even if one path is compromised by EMI or radiation damage.

By integrating these strategies, satellite designers can significantly enhance electromagnetic compatibility and ensure robust communication links in space. As satellite constellations grow and missions become more complex, EMI mitigation will remain a cornerstone of reliable aerospace engineering.



# Simulation Questions

1. A lossless 30 m long transmission line with  $Z_0=50\Omega$  is established between two ground stations which operate at 2 MHz. The line is terminated with a load  $Z_L = 60+j40\Omega$ . If  $u = 0.6c$  on the line. Write a **Scilab** code to plot the reflection coefficient ( $\Gamma$ ), standing wave ratio (S) and input impedance in smith chart.

## CODE:

```
// Transmission Line Analysis and Smith Chart Plotting
clear; clc;

// Given parameters
f = 2e6; // Frequency (Hz)
L = 30; // Line length (m)
Z0 = 50; // Characteristic impedance (Ω)
ZL = 60 + %i*40; // Load impedance (Ω)
c = 3e8; // Speed of light (m/s)
u = 0.6*c; // Phase velocity (m/s)

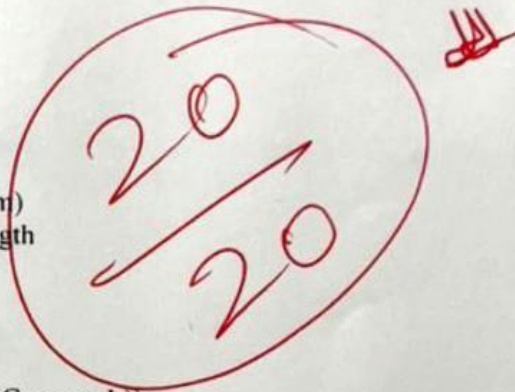
// Calculate derived parameters
lambda = u/f; // Wavelength (m)
beta = 2*%pi/lambda; // Phase constant (rad/m)
electrical_length = L/lambda; // Electrical length

// Calculate reflection coefficient at load
Gamma_L = (ZL - Z0)/(ZL + Z0);
magnitude_Gamma = abs(Gamma_L);
phase_Gamma = atan(imag(Gamma_L), real(Gamma_L));

// Calculate Standing Wave Ratio (SWR)
S = (1 + magnitude_Gamma)/(1 - magnitude_Gamma);

// Calculate input impedance
theta = beta * L; // Electrical length in radians
Z_in = Z0 * (ZL + %i*Z0*tan(theta))/(Z0 + %i*ZL*tan(theta));

// Display results
printf("Transmission Line Analysis Results:\n");
printf("=====\n");
printf("Frequency: %.2f MHz\n", f/1e6);
printf("Line Length: %.1f m\n", L);
printf("Wavelength: %.2f m\n", lambda);
printf("Electrical Length: %.3f wavelengths\n", electrical_length);
printf("Characteristic Impedance: %.1f Ω\n", Z0);
printf("Load Impedance: %.1f + j%.1f Ω\n", real(ZL), imag(ZL));
printf("\n");
printf("Reflection Coefficient (Γ):\n");
printf(" Magnitude: %.4f\n", magnitude_Gamma);
printf(" Phase: %.2f degrees\n", phase_Gamma*180/%pi);
printf(" Complex: %.4f + j%.4f\n", real(Gamma_L), imag(Gamma_L));
printf("\n");
printf("Standing Wave Ratio (S): %.4f\n", S);
printf("\n");
printf("Input Impedance:\n");
printf(" Z_in = %.2f + j%.2f Ω\n", real(Z_in), imag(Z_in));
printf(" Magnitude: %.2f Ω\n", abs(Z_in));
```



```
// Create Smith Chart visualization
// We'll create a custom Smith chart and plot the impedance trajectory
```

```
// Generate points for Smith chart circles
theta_circle = linspace(0, 2*%pi, 200);
```

```
// Resistance circles
r_values = [0.2, 0.5, 1, 2, 5]; // Normalized resistance values
// Reactance circles
x_values = [0.2, 0.5, 1, 2, 5]; // Normalized reactance values
```

```
// Create figure for Smith chart
scf(0);
clf();
xset("colormap", jetcolormap(64));
```

```
// Plot Smith chart background (constant resistance circles)
for i = 1:length(r_values)
    r = r_values(i);
    center_x = r/(1+r);
    radius = 1/(1+r);
```

```
    x_circle = center_x + radius*cos(theta_circle);
    y_circle = radius*sin(theta_circle);
```

```
    plot(x_circle, y_circle, 'k-', 'linewidth', 0.5);
```

```
    // Plot negative y for symmetry
    plot(x_circle, -y_circle, 'k-', 'linewidth', 0.5);
end
```

```
// Plot constant reactance circles
for i = 1:length(x_values)
    x = x_values(i);
    center_x = 1;
    center_y = 1/x;
    radius = abs(1/x);
```

```
    x_circle = center_x + radius*cos(theta_circle);
    y_circle = center_y + radius*sin(theta_circle);
```

```
    plot(x_circle, y_circle, 'b-', 'linewidth', 0.5);
```

```
    // Negative reactance circles
    center_y_neg = -1/x;
    y_circle_neg = center_y_neg + radius*sin(theta_circle);
    plot(x_circle, y_circle_neg, 'r-', 'linewidth', 0.5);
end
```

```
// Plot the real axis
plot([-1, 1], [0, 0], 'k-', 'linewidth', 1);
```

```
// Plot unit circle
plot(cos(theta_circle), sin(theta_circle), 'k-', 'linewidth', 2);
```

```
// Calculate normalized impedances
ZL_normalized = ZL/Zo;
Z_in_normalized = Z_in/Zo;
```

```

// Convert impedances to reflection coefficients
Gamma_ZL = (ZL_normalized - 1)/(ZL_normalized + 1);
Gamma_Zin = (Z_in_normalized - 1)/(Z_in_normalized + 1);

// Plot impedance points on Smith chart
plot(real(Gamma_ZL), imag(Gamma_ZL), 'ro', 'markersize', 8, 'linewidth', 2);
plot(real(Gamma_Zin), imag(Gamma_Zin), 'go', 'markersize', 8, 'linewidth', 2);

// Plot the impedance transformation along the line
positions = linspace(0, L, 100);
Gamma_positions = zeros(1, length(positions));

for i = 1:length(positions)
    l = positions(i);
    Gamma_positions(i) = Gamma_L * exp(-%i*2*beta*l);
end

plot(real(Gamma_positions), imag(Gamma_positions), 'm-', 'linewidth', 2);

// Add labels and legend
xlabel('Real( $\Gamma$ )');
ylabel('Imag( $\Gamma$ )');
title('Smith Chart - Transmission Line Analysis');
legend(['Resistance Circles'; 'Inductive Reactance'; 'Capacitive Reactance'; 'Unit Circle'; ...
        'Load Impedance'; 'Input Impedance'; 'Impedance Locus'], -1);

// Set equal aspect ratio and grid
a = gca();
a.isoview = "on";
a.grid = [1 1]*color('gray')*0.7;
a.data_bounds = [-1.2, -1.2; 1.2, 1.2];

// Create additional plots for detailed analysis
scf(1);
clf();
subplot(2,2,1);

// Plot magnitude of reflection coefficient vs position
positions_plot = linspace(0, L, 200);
Gamma_mag_plot = zeros(1, length(positions_plot));

for i = 1:length(positions_plot)
    l = positions_plot(i);
    Gamma_current = Gamma_L * exp(-%i*2*beta*l);
    Gamma_mag_plot(i) = abs(Gamma_current);
end

plot(positions_plot, Gamma_mag_plot, 'b-', 'linewidth', 2);
xlabel('Position along line (m)');
ylabel('| $\Gamma$ |');
title('Reflection Coefficient Magnitude vs Position');
xgrid(1);

subplot(2,2,2);
// Plot SWR vs position (constant for lossless line)
SWR_plot = S * ones(1, length(positions_plot));
plot(positions_plot, SWR_plot, 'r-', 'linewidth', 2);
xlabel('Position along line (m)');
ylabel('SWR');
title('Standing Wave Ratio vs Position');

```

```

xgrid(1);

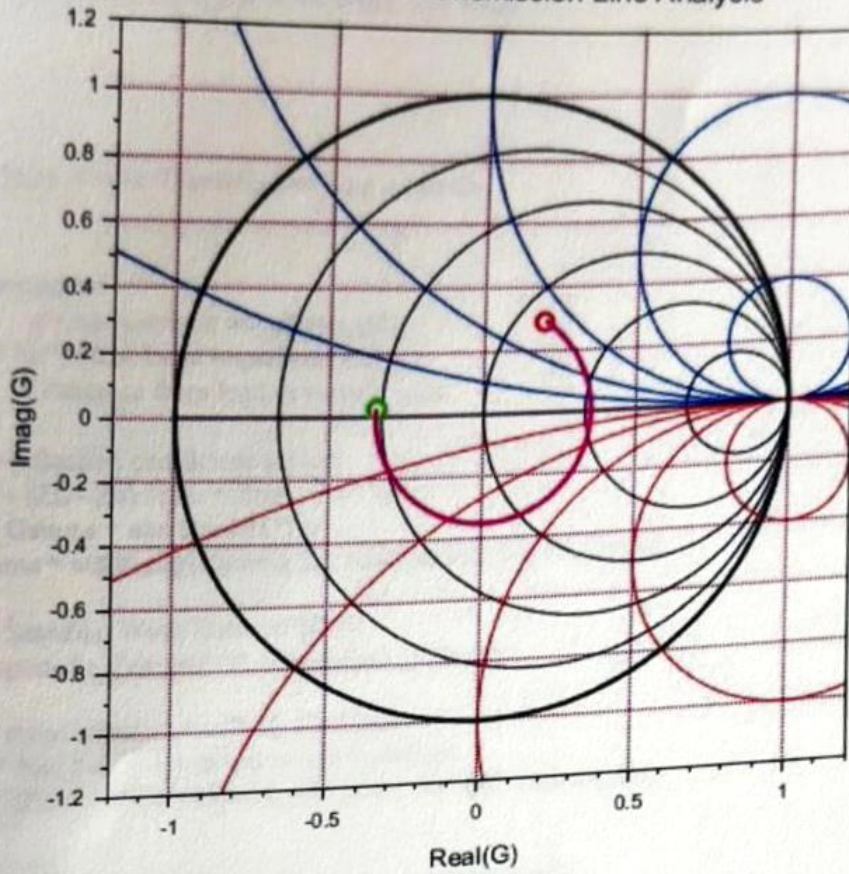
subplot(2,2,3);
// Plot input impedance real part vs position
Z_real_plot = zeros(1, length(positions_plot));
for i = 1:length(positions_plot)
    l = positions_plot(i);
    theta_current = beta * l;
    Z_current = Zo * (ZL + %i*Zo*tan(theta_current))/(Zo + %i*ZL*tan(theta_current));
    Z_real_plot(i) = real(Z_current);
end
plot(positions_plot, Z_real_plot, 'g-', 'linewidth', 2);
xlabel('Position along line (m)');
ylabel('Re(Z) ( $\Omega$ )');
title('Input Resistance vs Position');
xgrid(1);

subplot(2,2,4);
// Plot input impedance imaginary part vs position
Z_imag_plot = zeros(1, length(positions_plot));
for i = 1:length(positions_plot)
    l = positions_plot(i);
    theta_current = beta * l;
    Z_current = Zo * (ZL + %i*Zo*tan(theta_current))/(Zo + %i*ZL*tan(theta_current));
    Z_imag_plot(i) = imag(Z_current);
end
plot(positions_plot, Z_imag_plot, 'm-', 'linewidth', 2);
xlabel('Position along line (m)');
ylabel('Im(Z) ( $\Omega$ )');
title('Input Reactance vs Position');
xgrid(1);

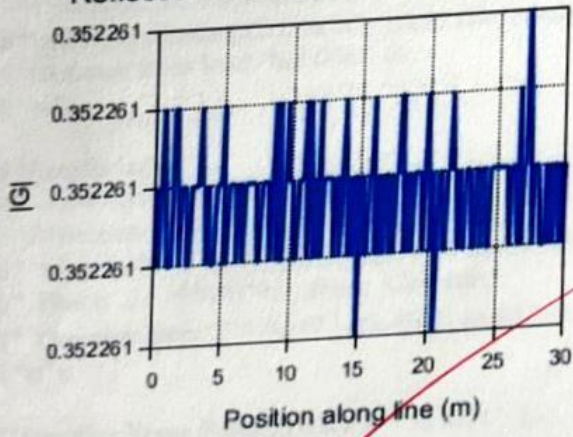
// Display summary in console
printf("\nSummary:\n");
printf("=====\n");
printf("The Smith chart shows:\n");
printf("- Load impedance (red): Z_L = %.1f + j%.1f  $\Omega$ \n", real(ZL), imag(ZL));
printf("- Input impedance (green): Z_in = %.1f + j%.1f  $\Omega$ \n", real(Z_in), imag(Z_in));
printf("- The purple curve shows impedance transformation along the line\n");
printf("- SWR remains constant at %.4f (lossless line)\n", S);

```

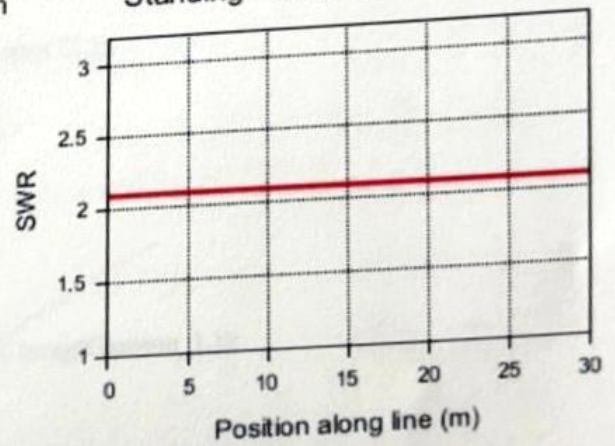
# Smith Chart - Transmission Line Analysis



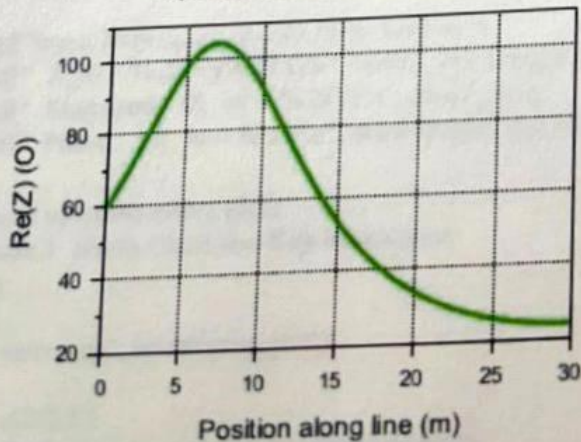
## Reflection Coefficient Magnitude vs Position



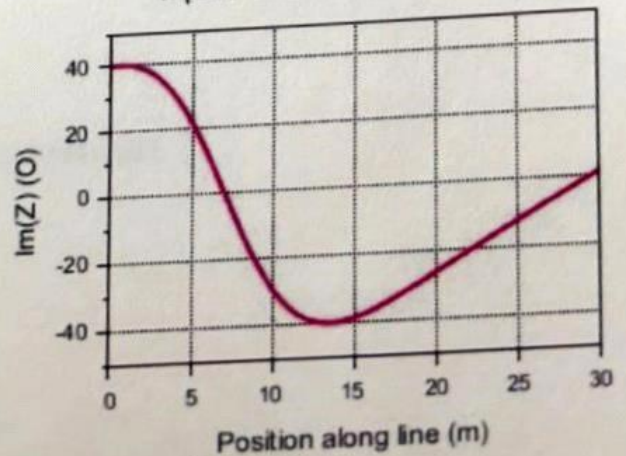
## Standing Wave Ratio vs Position



## Input Resistance vs Position



## Input Reactance vs Position



2. In a satellite base station, a load of  $100 + j150 \Omega$  is connected to a  $75 \Omega$  lossless line. Write a **Scilab code** to plot the Reflection coefficient ( $\Gamma$ ), SWR value and input impedance ( $Z_{in}$ ) at  $0.4\lambda$  from the load.

### CODE:

```
// Satellite Base Station Transmission Line Analysis
clear; clc;

// Given parameters
Zo = 75; // Characteristic impedance ( $\Omega$ )
ZL = 100 + %i*150; // Load impedance ( $\Omega$ )
d = 0.4; // Distance from load in wavelengths

// Calculate reflection coefficient at load
Gamma_L = (ZL - Zo) / (ZL + Zo);
magnitude_Gamma = abs(Gamma_L);
phase_Gamma = atan(imag(Gamma_L), real(Gamma_L)) * 180/%pi;

// Calculate Standing Wave Ratio (SWR)
S = (1 + magnitude_Gamma) / (1 - magnitude_Gamma);

// Calculate input impedance at  $0.4\lambda$  from load
beta_d = 2 * %pi * d; // Electrical length in radians
Z_in = Zo * (ZL + %i*Zo*tan(beta_d)) / (Zo + %i*ZL*tan(beta_d));

// Display results
printf("Satellite Base Station Transmission Line Analysis\n");
printf("=====\n");
printf("Characteristic Impedance (Zo): %.0f  $\Omega$ \n", Zo);
printf("Load Impedance (ZL): %.0f + j%.0f  $\Omega$ \n", real(ZL), imag(ZL));
printf("Distance from load: %.1f  $\lambda$ \n", d);
printf("\n");

printf("Results:\n");
printf("-----\n");
printf("Reflection Coefficient ( $\Gamma$ ):\n");
printf(" Magnitude:  $|\Gamma| = %.4f$ \n", magnitude_Gamma);
printf(" Phase:  $\angle \Gamma = %.2f^\circ$ \n", phase_Gamma);
printf(" Complex form:  $\Gamma = %.4f + j%.4f$ \n", real(Gamma_L), imag(Gamma_L));
printf("\n");

printf("Standing Wave Ratio (SWR): S = %.4f\n", S);
printf("\n");

printf("Input Impedance at  $0.4\lambda$  from load:\n");
printf(" Z_in = %.2f + j%.2f  $\Omega$ \n", real(Z_in), imag(Z_in));
printf(" Magnitude:  $|Z_{in}| = %.2f \Omega$ \n", abs(Z_in));
printf(" Phase:  $\angle Z_{in} = %.2f^\circ$ \n", atan(imag(Z_in), real(Z_in)) * 180/%pi);

// Create comprehensive plots
// Figure 1: Smith Chart and Key Parameters
scf(0);
clf();
xset("colormap", jetcolormap(64));

subplot(2,2,1);
// Plot Reflection Coefficient on complex plane
```

```

theta = linspace(0, 2*pi, 100);
plot(cos(theta), sin(theta), 'k-', 'linewidth', 1); // Unit circle
plot([-1 1], [0 0], 'k:', 'linewidth', 0.5);
plot([0 0], [-1 1], 'k:', 'linewidth', 0.5);

```

```

// Plot Gamma point
plot(real(Gamma_L), imag(Gamma_L), 'ro', 'markersize', 8, 'linewidth', 2);
xlabel('Real( $\Gamma$ )');
ylabel('Imag( $\Gamma$ )');
title('Reflection Coefficient on Complex Plane');
a = gca();
a.isoview = "on";
a.data_bounds = [-1.1, -1.1; 1.1, 1.1];
xgrid(1);

```

```

// Add annotation for Gamma value
xstring(real(Gamma_L)+0.1, imag(Gamma_L)+0.1, sprintf('Γ = %.3f ∠ %.1f°', magnitude_Gamma,
phase_Gamma));

```

```

subplot(2,2,2);
// Display SWR value prominently
bar(1, S, 'r');
a = gca();
a.x_ticks = tlist(["ticks", "locations", "labels"], [1], ["SWR"]);
ylabel('Standing Wave Ratio');
title('Standing Wave Ratio');
ylim([1, 2.5]);
// Add value text
xstring(1, S+0.1, sprintf('S = %.4f, S));

```

```

subplot(2,2,3);
// Display impedance comparison
impedances = [real(ZL), imag(ZL), abs(ZL); real(Z_in), imag(Z_in), abs(Z_in)];
bar([1, 2, 3; 1, 2, 3], impedances, 'grouped');
legend(['Load ZL;', 'Input Z_in', -1);
a = gca();
a.x_ticks = tlist(["ticks", "locations", "labels"], [1,2,3], ["Real", "Imag", "Mag"]);
ylabel('Impedance ( $\Omega$ )');
title('Impedance Comparison');

```

```

subplot(2,2,4);
// Polar plot of Gamma
theta_polar = linspace(0, 2*pi, 100);
polarplot(theta_polar, ones(1,100), 'k-'); // Unit circle
polarplot(phase_Gamma*pi/180, magnitude_Gamma, 'ro', 'markersize', 8, 'linewidth', 2);
title('Reflection Coefficient (Polar)');

```

// Figure 2: Smith Chart Implementation

```

scf(1);
clf();

```

```

// Create custom Smith Chart
theta = linspace(0, 2*pi, 200);

```

```

// Resistance circles
r_values = [0.2, 0.5, 1, 2, 5];
for i = 1:length(r_values)
    r = r_values(i);
    center = r/(r+1);
    radius = 1/(r+1);

```

```

x_circle = center + radius*cos(theta);
y_circle = radius*sin(theta);
plot(x_circle, y_circle, 'b-', 'linewidth', 0.7);
plot(x_circle, -y_circle, 'b-', 'linewidth', 0.7);
end

// Reactance circles
x_values = [0.2, 0.5, 1, 2, 5];
for i = 1:length(x_values)
    x = x_values(i);
    center_x = 1;
    center_y = 1/x;
    radius = abs(1/x);
    x_circle = center_x + radius*cos(theta);
    y_circle = center_y + radius*sin(theta);
    plot(x_circle, y_circle, 'r-', 'linewidth', 0.7);

    // Negative reactance
    center_y_neg = -1/x;
    y_circle_neg = center_y_neg + radius*sin(theta);
    plot(x_circle, y_circle_neg, 'g-', 'linewidth', 0.7);
end

// Unit circle and axes
plot(cos(theta), sin(theta), 'k-', 'linewidth', 2);
plot([-1 1], [0 0], 'k-', 'linewidth', 1);

// Calculate normalized impedances and their Gamma points
ZL_norm = ZL/Zo;
Z_in_norm = Z_in/Zo;

Gamma_ZL = (ZL_norm - 1)/(ZL_norm + 1);
Gamma_Zin = (Z_in_norm - 1)/(Z_in_norm + 1);

// Plot impedance points
plot(real(Gamma_ZL), imag(Gamma_ZL), 'ro', 'markersize', 10, 'linewidth', 3);
plot(real(Gamma_Zin), imag(Gamma_Zin), 'go', 'markersize', 10, 'linewidth', 3);

// Plot impedance transformation along the line
positions = linspace(0, d, 50);
Gamma_trajectory = zeros(1, length(positions));
for i = 1:length(positions)
    dist = positions(i);
    beta_dist = 2 * %pi * dist;
    Gamma_trajectory(i) = Gamma_L * exp(-%i * 2 * beta_dist);
end
plot(real(Gamma_trajectory), imag(Gamma_trajectory), 'm-', 'linewidth', 2);

// Formatting
xlabel('Real( $\Gamma$ )');
ylabel('Imag( $\Gamma$ )');
title('Smith Chart - Satellite Base Station Analysis');
legend(['Resistance Circles'; 'Inductive Reactance'; 'Capacitive Reactance'; ...
    'Unit Circle'; 'Load ZL'; 'Input Z_in @ 0.4 $\lambda$ '; 'Impedance Locus'], -1);
a = gca();
a.isoview = "on";
a.data_bounds = [-1.1, -1.1; 1.1, 1.1];
a.grid = [1 1]*color('gray')*0.5;

// Add impedance values on the chart

```

```

xstring(real(Gamma_ZL)+0.05, imag(Gamma_ZL)+0.05, ...
    sprintf('Z_L = %.0f+j%.0fΩ', real(ZL), imag(ZL)));
xstring(real(Gamma_Zin)+0.05, imag(Gamma_Zin)+0.05, ...
    sprintf('Z_in = %.1f+j%.1fΩ', real(Z_in), imag(Z_in)));

// Figure 3: Parameter variation along transmission line
scf(2);
clf();

// Analyze along entire wavelength
positions_full = linspace(0, 1, 200); // 0 to 1 wavelength
Gamma_full = zeros(1, length(positions_full));
Z_in_full = zeros(1, length(positions_full));
SWR_full = zeros(1, length(positions_full));

for i = 1:length(positions_full)
    dist = positions_full(i);
    beta_dist = 2 * %pi * dist;
    Gamma_current = Gamma_L * exp(-%i * 2 * beta_dist);
    Gamma_full(i) = Gamma_current;

    Z_current = Zo * (ZL + %i*Zo*tan(beta_dist)) / (Zo + %i*ZL*tan(beta_dist));
    Z_in_full(i) = Z_current;

    SWR_full(i) = (1 + abs(Gamma_current)) / (1 - abs(Gamma_current));
end

subplot(3,1,1);
plot(positions_full, abs(Gamma_full), 'b-', 'linewidth', 2);
xlabel('Distance from Load (λ)');
ylabel('|Γ|');
title('Reflection Coefficient Magnitude vs Position');
xgrid(1);
// Mark our point of interest
plot(d, abs(Gamma_L * exp(-%i * 2 * 2*%pi*d)), 'ro', 'markersize', 8, 'linewidth', 2);
xstring(d, abs(Gamma_L * exp(-%i * 2 * 2*%pi*d)) + 0.05, '0.4λ point');

subplot(3,1,2);
plot(positions_full, SWR_full, 'r-', 'linewidth', 2);
xlabel('Distance from Load (λ)');
ylabel('SWR');
title('Standing Wave Ratio vs Position');
xgrid(1);
plot(d, (1 + abs(Gamma_L * exp(-%i * 2 * 2*%pi*d))) / (1 - abs(Gamma_L * exp(-%i * 2 * 2*%pi*d))), ...
    'ro', 'markersize', 8, 'linewidth', 2);

subplot(3,1,3);
plot(positions_full, real(Z_in_full), 'g-', 'linewidth', 2, 'label', 'Real(Z_in)');
plot(positions_full, imag(Z_in_full), 'm-', 'linewidth', 2, 'label', 'Imag(Z_in)');
xlabel('Distance from Load (λ)');
ylabel('Impedance (Ω)');
title('Input Impedance vs Position');
legend(['Real Part', 'Imaginary Part'], -1);
xgrid(1);
plot(d, real(Z_in), 'go', 'markersize', 8, 'linewidth', 2);
plot(d, imag(Z_in), 'mo', 'markersize', 8, 'linewidth', 2);

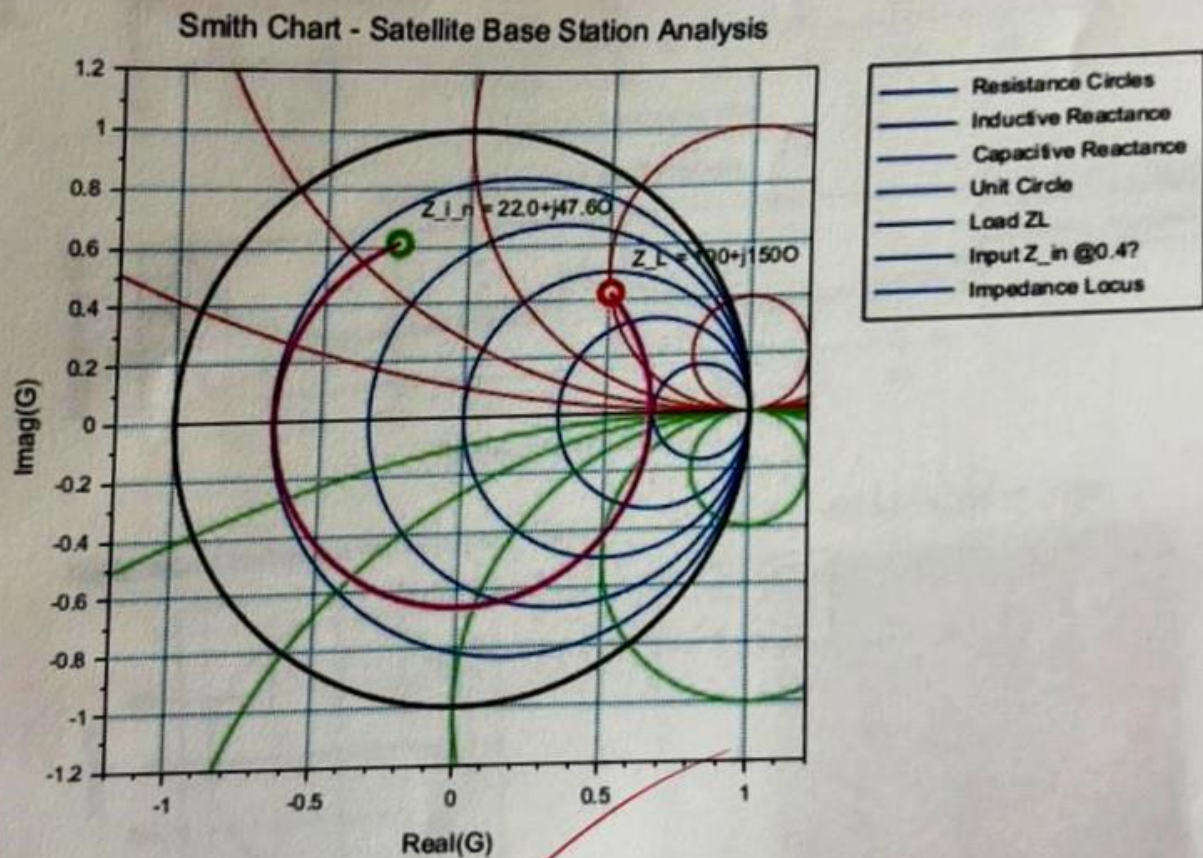
// Print detailed analysis
printf("\nDetailed Analysis:\n");
printf("=====\n");

```

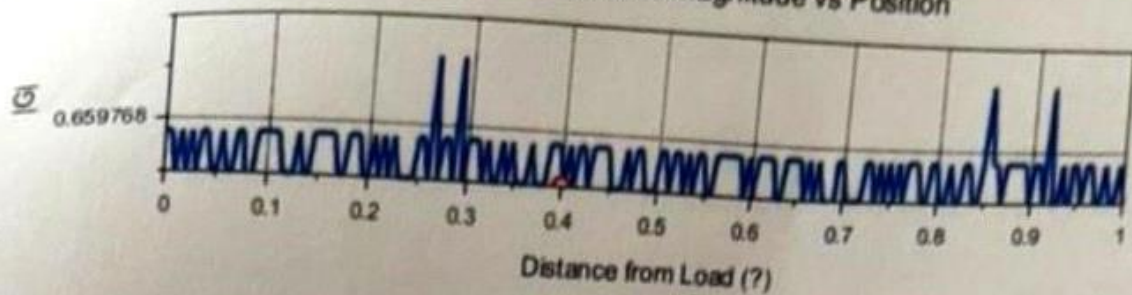
```

printf("Normalized Load Impedance: Z_L/Zo = %.3f + j%.3f\n", real(ZL_norm), imag(ZL_norm));
printf("Normalized Input Impedance: Z_in/Zo = %.3f + j%.3f\n", real(Z_in_norm), imag(Z_in_norm));
printf("\n");
printf("At 0.4λ from load:\n");
printf(" Reflection Coefficient rotates by: %.1f° clockwise\n", d * 720);
printf(" New Gamma phase: %.1f°\n", atan(imag(Gamma_L * exp(-%i * 2 * beta_d)), ...
    real(Gamma_L * exp(-%i * 2 * beta_d)))*180/%pi);
printf("\n");
printf("The Smith chart shows the impedance transformation from load to input.\n");
printf("The purple curve represents how the impedance appears to change along the line.\n");

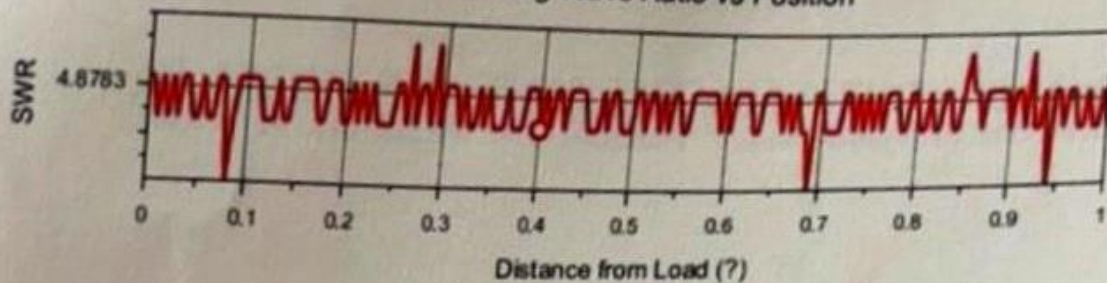
```



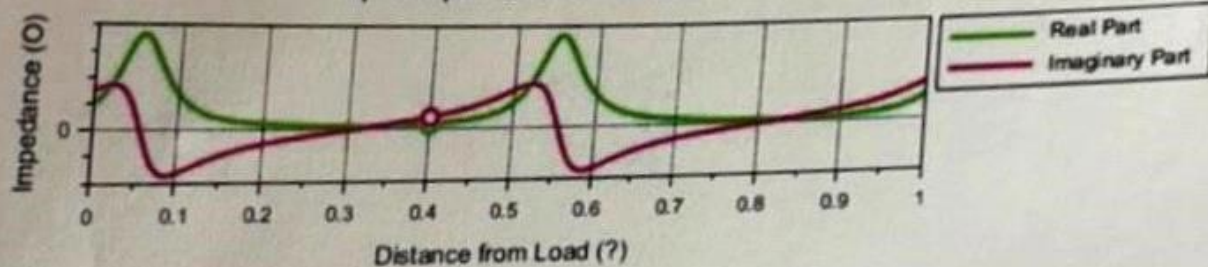
Reflection Coefficient Magnitude vs Position



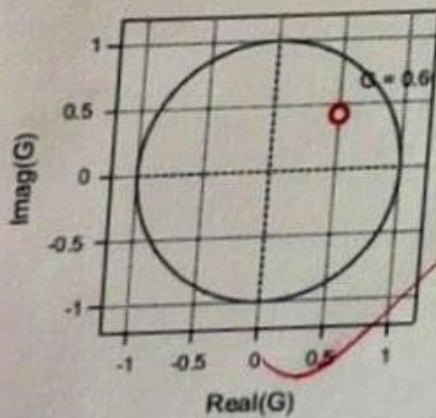
Standing Wave Ratio vs Position



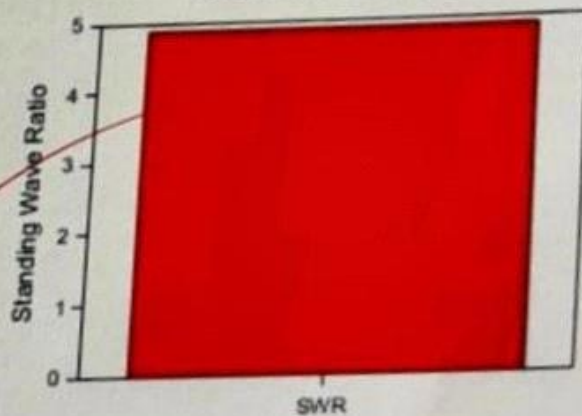
Input Impedance vs Position



Reflection Coefficient on Complex Plane



Standing Wave Ratio



Impedance Comparison

Impedance (Ω)